



31 October 2019

Eric Cornwell  
Georgia Department of Natural Resources  
Environmental Protection Division  
Air Protection Branch  
4244 International Parkway, Suite 120  
Atlanta, Georgia 30354-3908


Dear Mr. Cornwell:

RE: SIP Permit Application  
BD Covington  
Air Quality Permit 3841-211-0021-S-0-04-0

Enclosed is a SIP application for our 8195 Industrial Blvd. Covington GA 30014 location. The application describes the additional voluntary emission controls we plan to install to reduce fugitive emissions of Ethylene Oxide. These emissions are not regulated by Subpart O (40 CFR 63.360).

If you have any questions or comments regarding this information, please contact me at (770) 652-2049.

Sincerely,



John LaMontagne  
Process Technology Engineer  
Urology and Critical Care Division  
Becton, Dickinson and Company

cc: K. Hays, GA EPD  
R. Pasdon

With Air Dispersion Modeling files. (USB Flash Drive)

Certified: 70092250000127474828



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Sincerely,

A handwritten signature in blue ink, appearing to read "John LaMontagne", is written over a faint, light blue circular stamp.

John LaMontagne  
Process Technology Engineer  
Urology and Critical Care Division  
Becton, Dickinson and Company

cc: **K. Hays, GA EPD**  
R. Pasdon

Without Air Dispersion Modeling files

Certified: 70092250000127474811



## SIP AIR PERMIT APPLICATION

### EPD Use Only

Date Received: \_\_\_\_\_ Application No. \_\_\_\_\_

### FORM 1.00: GENERAL INFORMATION

#### 1. Facility Information

Facility Name: BD Covington  
AIRS No. (if known): 04-13-217 - 00021  
Facility Location: Street: 8195 Industrial Blvd  
City: Covington Georgia Zip: 30014 County: Newton  
Is this facility a "small business" as defined in the instructions? Yes:  No:

#### 2. Facility Coordinates

Latitude: 85° 36' 42" NORTH Longitude: 83° 50' 17" WEST  
UTM Coordinates: \_\_\_\_\_ EAST \_\_\_\_\_ NORTH ZONE \_\_\_\_\_

#### 3. Facility Owner

Name of Owner: Becton, Dickinson and Company  
Owner Address Street: 1 Becton Drive  
City: Franklin Lakes State: NJ Zip: 07417

#### 4. Permitting Contact and Mailing Address

Contact Person: John LaMontagne Title: Process Technology Engineer  
Telephone No.: 770 784 6186 Ext. \_\_\_\_\_ Fax No.: 770 788 5519  
Email Address: john.lamontagne@BD.com  
Mailing Address: Same as:  Facility Location:  Owner Address:  Other:   
If Other: Street Address: \_\_\_\_\_  
City: \_\_\_\_\_ State: \_\_\_\_\_ Zip: \_\_\_\_\_

#### 5. Authorized Official

Name: Ron Pasdon Title: Sr. Operations Mgr. Covington  
Address of Official Street: 8195 Industrial Blvd.  
City: Covington State: GA Zip: 30014

This application is submitted in accordance with the provisions of the Georgia Rules for Air Quality Control and, to the best of my knowledge, is complete and correct.

Signature:  Date: 31 Oct. 2019

**6. Reason for Application: (Check all that apply)**

- New Facility (to be constructed)
  Revision of Data Submitted in an Earlier Application  
 Existing Facility (initial or modification application)
 Application No.: \_\_\_\_\_  
 Permit to Construct
 Date of Original Submittal: \_\_\_\_\_  
 Permit to Operate  
 Change of Location  
 Permit to Modify Existing Equipment:
 Affected Permit No.: \_\_\_\_\_

**7. Permitting Exemption Activities (for permitted facilities only):**

Have any exempt modifications based on emission level per Georgia Rule 391-3-1-.03(6)(i)(3) been performed at the facility that have not been previously incorporated in a permit?

- No
  Yes, please fill out the SIP Exemption Attachment (See Instructions for the attachment download)

**8. Has assistance been provided to you for any part of this application?**

- No
  Yes, SBAP
  Yes, a consultant has been employed or will be employed.

If yes, please provide the following information:

Name of Consulting Company: Trinity Consultants

Name of Contact: Justin Fickas

Telephone No.: 678 441-9977 Fax No.: \_\_\_\_\_

Email Address: \_\_\_\_\_

Mailing Address: Street: 3495 Piedmont Rd

City: Atlanta State: GA Zip: 30305

Describe the Consultant's Involvement:

Air Dispersion Modeling

**9. Submitted Application Forms: Select only the necessary forms for the facility application that will be submitted.**

No. of Forms	Form
1	2.00 Emission Unit List
	2.01 Boilers and Fuel Burning Equipment
	2.02 Storage Tank Physical Data
	2.03 Printing Operations
	2.04 Surface Coating Operations
	2.05 Waste Incinerators (solid/liquid waste destruction)
	2.06 Manufacturing and Operational Data
1	3.00 Air Pollution Control Devices (APCD)
	3.01 Scrubbers
	3.02 Baghouses & Other Filter Collectors
	3.03 Electrostatic Precipitators
1	4.00 Emissions Data
1	5.00 Monitoring Information
	6.00 Fugitive Emission Sources
1	7.00 Air Modeling Information

**10. Construction or Modification Date**

Estimated Start Date: Construction estimated to start in December 2019

11. If confidential information is being submitted in this application, were the guidelines followed in the "Procedures for Requesting that Submitted Information be treated as Confidential"?

No       Yes

**12. New Facility Emissions Summary**

Criteria Pollutant	New Facility	
	Potential (tpy)	Actual (tpy)
Carbon monoxide (CO)		
Nitrogen oxides (NOx)		
Particulate Matter (PM) (filterable only)		
PM <10 microns (PM10)		
PM <2.5 microns (PM2.5)		
Sulfur dioxide (SO <sub>2</sub> )		
Volatile Organic Compounds (VOC)		
Greenhouse Gases (GHGs) (in CO <sub>2</sub> e)		
Total Hazardous Air Pollutants (HAPs)		
Individual HAPs Listed Below:		

**13. Existing Facility Emissions Summary**

Criteria Pollutant	Current Facility		After Modification	
	Potential (tpy)	Actual (tpy)	Potential (tpy)	Actual (tpy)
Carbon monoxide (CO)	27.77	2.98	27.77	2.98
Nitrogen oxides (NOx)	54.1	5.69	54.1	5.69
Particulate Matter (PM) (filterable only)	2.76	0.30	2.76	0.30
PM <10 microns (PM10)	2.76	0.30	2.76	0.30
PM <2.5 microns (PM2.5)	2.76	0.30	2.76	0.30
Sulfur dioxide (SO <sub>2</sub> )	5.02	0.50	5.02	0.50
Volatile Organic Compounds (VOC)	6.29	0.70	5.81	0.41
Greenhouse Gases (GHGs) (in CO <sub>2</sub> e)	30956	19734	30956	19734
Total Hazardous Air Pollutants (HAPs)	0.98	0.35	0.50	0.07
Individual HAPs Listed Below:				
Ethylene Oxide	0.5	0.3	0.019	0.014


**14. 4-Digit Facility Identification Code:**

SIC Code: 3841 SIC Description: Surgical & Medical Instruments & Apparatus  
 NAICS Code: 339112 NAICS Description: Surgical and Medical Instrument Manufacturing

**15. Description of general production process and operation for which a permit is being requested. If necessary, attach additional sheets to give an adequate description. Include layout drawings, as necessary, to describe each process. References should be made to source codes used in the application.**

This application is for the addition of Emission Controls for currently non-captured emissions of Ethylene Oxide (EO) at an existing medical device sterilization facility. The existing regulated process which includes the Sterilization Chamber Exhaust Vent, Chamber Vent, and Aeration Exhaust are not being modified. Information for these systems has been included in previous permit applications and will not be repeated here. This application is specific to additional emission controls being installed to capture and treat emissions not captured by current control equipment. No increase in the usage of EO will result from this proposed fugitive emission control project. The new controls will be comprised of two Local Exhaust Ventilation Systems:

System One (SYS1) will capture potential emissions from the five Sterilization Vessel Rooms (VRM1, VRM2, VRM3, VRM4, VRM5), the Vessel to Aeration Transfer Corridor (NCO1), and the EO Dispensing Room (DRM1). Reference Attachment C.

System Two (SYS2) will capture potential emissions from the Work in Progress Area (WIP1) where product is stored after Sterilization and prior to shipment. Reference Attachment D.

The captured emissions will be treated using Advanced Air Technologies Model DR490 "Dry Bed Scrubbers" designed to achieve an estimated 99% destruction efficiency.

**16. Additional information provided in attachments as listed below:**

- Attachment A - Floor Plan
- Attachment B - Plot Plan with proposed new stack locations
- Attachment C - System 1 Flow Diagram
- Attachment D - System 2 Flow Diagram
- Attachment E - Mass Balance Calculations.
- Attachment F - Monitoring Recommendations
- Attachment G - Advanced Air Technologies DR-490 Equipment Information
- Attachment H - Air Dispersion Modeling

**17. Additional Information: Unless previously submitted, include the following two items:**

- Plot plan/map of facility location or date of previous submittal: Attachment B
- Flow Diagram or date of previous submittal: Attachment C & D

**18. Other Environmental Permitting Needs:**

Will this facility/modification trigger the need for environmental permits/approvals (other than air) such as Hazardous Waste Generation, Solid Waste Handling, Water withdrawal, water discharge, SWPPP, mining, landfill, etc.?

- No     Yes, please list below:

**19. List requested permit limits including synthetic minor (SM) limits.**

Proposed Permit Conditions

Permittee shall initially test performance of System1 (SYS1) and System2 (SYS2) to confirm ethylene oxide removal efficiency of at least 99% on a concentration basis within 60 days of commissioning of each system and within 60 days following any replacement of dry bed media.

Removal efficiency across each system (SYS1 and SYS2) shall be demonstrated on a concentration reduction basis using simultaneous samples of inlet and outlet gases by Summa Canisters using EPA Method TO-15 with analysis by GC/MS in the Selective Ion Monitoring (SIM) acquisition mode. During sampling of the inlet and outlet concentrations across each system, the outlet stack airflows will be measured using EPA Methods 1, 2, and 4 for determination of volumetric flow rate and moisture content, and calculation of mass emission rate of ethylene oxide.

Permittee shall sample the outlet from System1 (SYS1) and System2 (SYS2) once each month by Summa Canisters using EPA Method TO-15 with analysis by GC/MS in the Selective Ion Monitoring (SIM) acquisition mode to determine concentration of ethylene oxide in the exhaust airflow stream.

Permittee shall track monthly concentration data versus baseline conditions and, in consultation with the dry bed manufacturer, determine when media replacement is warranted to maintain at least 99% removal efficiency.

**20. Effective March 1, 2019, permit application fees will be assessed. The fee amount varies based on type of permit application. Application acknowledgement emails will be sent to the current registered fee contact in the GECO system. If fee contacts have changed, please list that below:**

**Fee Contact name:**

**Fee Contact email address:**

**Fee Contact phone number:**

**Fee invoices will be created through the GECO system shortly after the application is received. It is the applicant's responsibility to access the facility GECO account, generate the fee invoice, and submit payment within 10 days after notification.**

Facility Name: BD Covington

Date of Application: 31 October 2019

**FORM 2.00 – EMISSION UNIT LIST**

Emission Unit ID	Name	Manufacturer and Model Number	Description
VRM1	Vessel Room 1	N/A	Dedicated Room for Sterilization Chamber 1
VRM2	Vessel Room 2	N/A	Dedicated Room for Sterilization Chamber 2
VRM3	Vessel Room 3	N/A	Dedicated Room for Sterilization Chamber 3
VRM4	Vessel Room 4	N/A	Dedicated Room for Sterilization Chamber 4
VRM5	Vessel Room 5	N/A	Dedicated Room for Sterilization Chamber 5
NCO1	Vessel to Aeration Transfer	N/A	Common corridor between Vessel Rooms and Aeration Cells
DRM1	EO Dispensing	N/A	Dedicated Room for Dispensing EO from supply drums to each Vessel Room
WIP1	Work in Progress	N/A	Common area where sterilized product is stored prior to shipment











Facility Name: BD Covington

Date of Application: 31 October 2019

**FORM 5.00 MONITORING INFORMATION**

Emission Unit ID/ APCD ID	Emission Unit/APCD Name	Monitored Parameter		Monitoring Frequency
		Parameter	Units	
VRM1/SYS 1	Vessel Room1/System1	EO Concentration at outlet of SYS1	ppm	Reference Attachment F
VRM2/SYS 1	Vessel Room2/System1	EO Concentration at outlet of SYS1	ppm	Reference Attachment F
VRM3/SYS 1	Vessel Room3/System1	EO Concentration at outlet of SYS1	ppm	Reference Attachment F
VRM4/SYS 1	Vessel Room4/System1	EO Concentration at outlet of SYS1	ppm	Reference Attachment F
VRM5/SYS 1	Vessel Room5/System1	EO Concentration at outlet of SYS1	ppm	Reference Attachment F
NCO1/SYS 1	Vessel to Aeration Transfer/System1	EO Concentration at outlet of SYS1	ppm	Reference Attachment F
DMR1/SYS 1	EO Dispensing/System1	EO Concentration at outlet of SYS1	ppm	Reference Attachment F
WIP1/SYS2	Work in Progress/System2	EO Concentration at outlet of SYS2	ppm	Reference Attachment F

**Comments:**  
Monitoring detail described in attachment F

**FORM 7.00 – AIR MODELING INFORMATION: Stack Data**

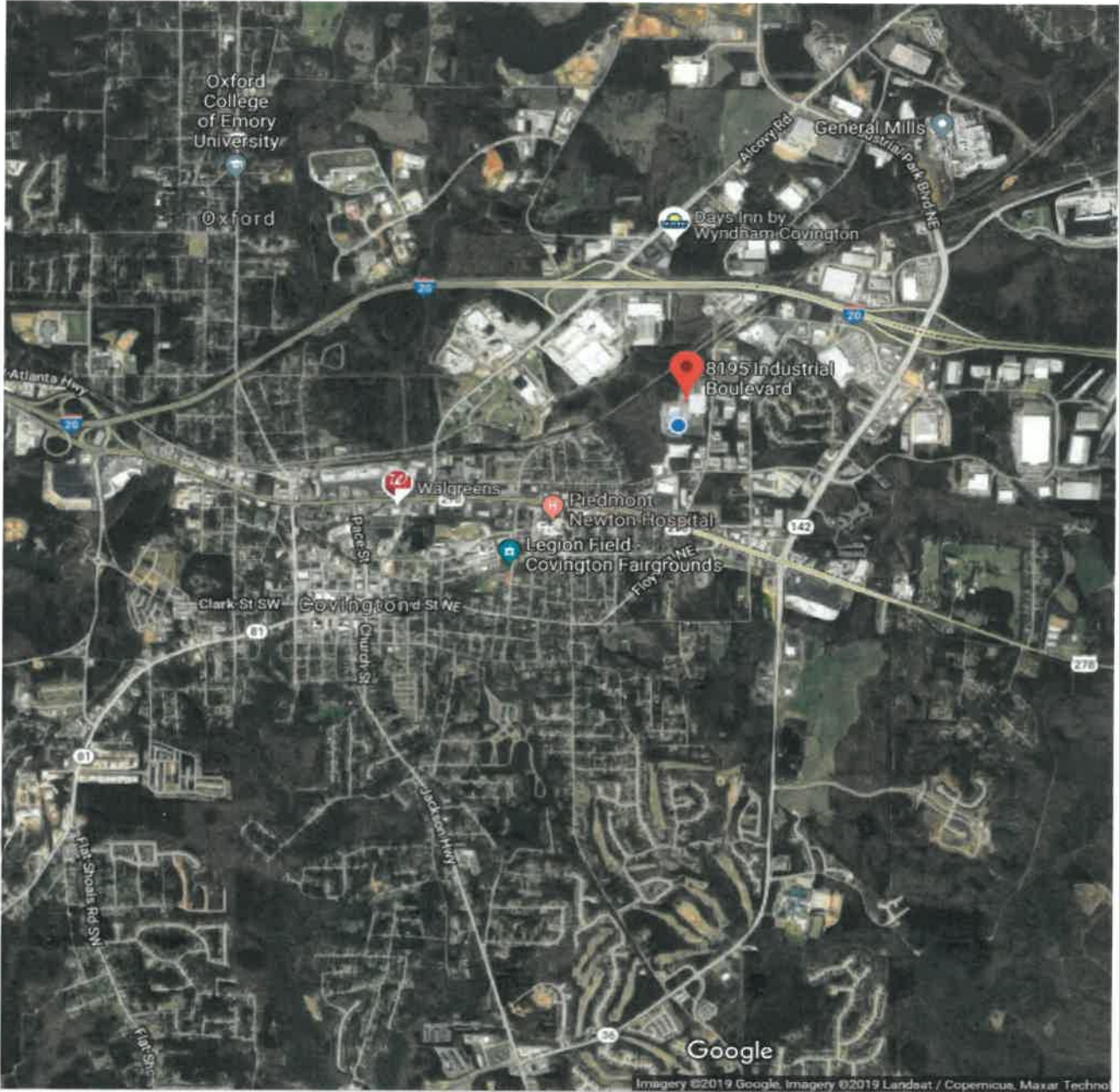
Stack ID	Emission Unit ID(s)	Stack Information			Dimensions of largest Structure Near Stack		Exit Gas Conditions at Maximum Emission Rate			
		Height Above Grade (ft)	Inside Diameter (ft)	Exhaust Direction	Height (ft)	Longest Side (ft)	Velocity (ft/sec)	Temperature (°F)	Flow Rate (acfm)	
									Average	Maximum
STK1	VRM1, VRM2, VRM3, VRM4, VRM5, NCO1, DMR1,	100	3.83	To the Sky	30	50	52	70	21,000	36,000
STK2	WIP1	100	5.17	To the Sky	30	50	50.8	70	64,000	64,000

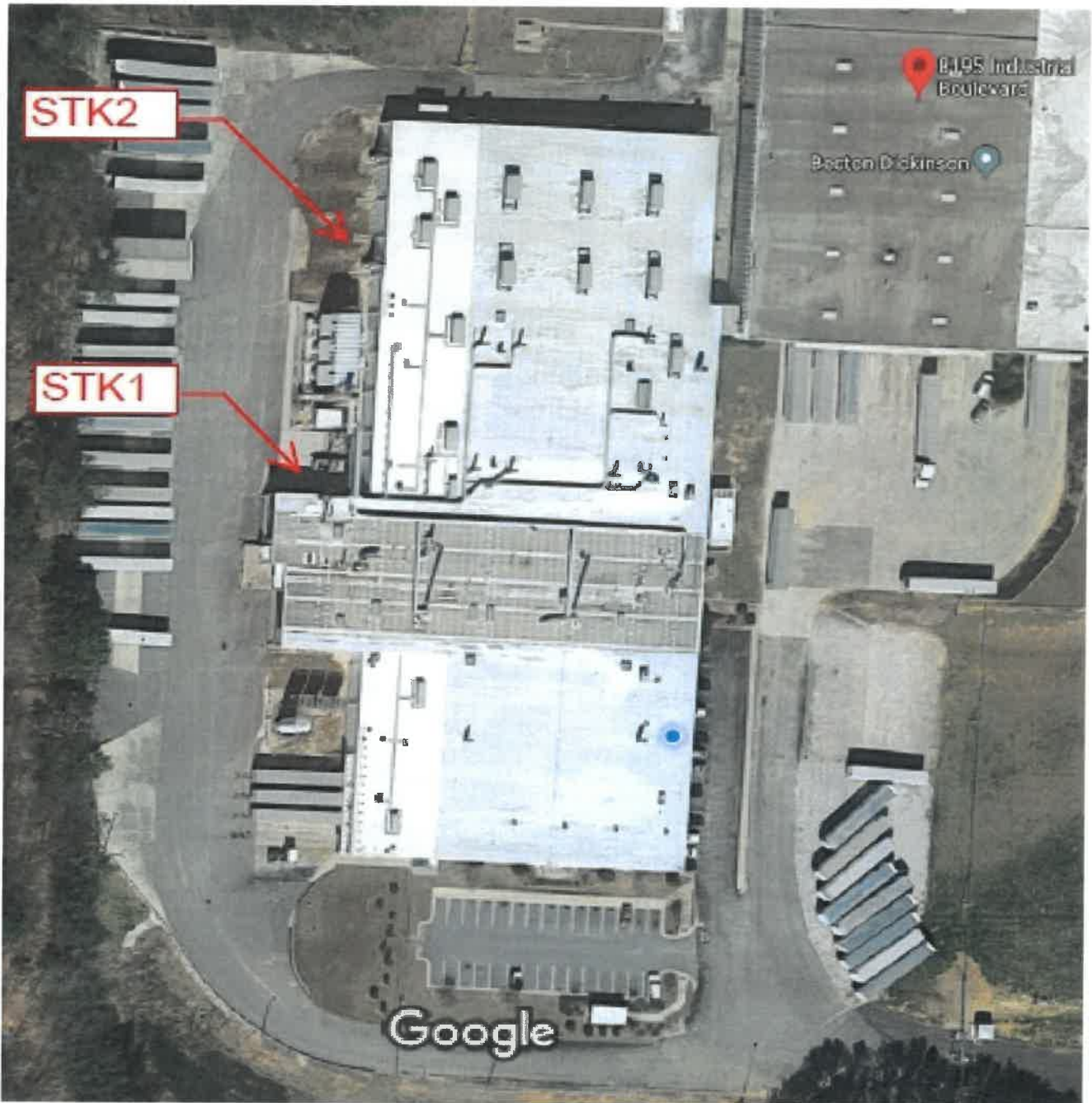
**NOTE:** If emissions are not vented through a stack, describe point of discharge below and, if necessary, include an attachment. List the attachment in Form 1.00 *General Information*, Item 16.

n/a









## Attachment C

### BD Covington SIP Application

#### General Description

The intent of the mechanical systems design upgrade is to capture unregulated, fugitive Ethylene Oxide (EO) emissions inside the facility and reduce the potential for releases of these emissions to atmosphere. An effective means of containing emissions is to capture EO at the source. The capture and treatment systems will utilize pressure differential strategies. Using negatively pressurized spaces, extraction will direct air from the lowest EO concentrations to the highest concentrations in the building and then send this exhaust air through an EO destruction process. Existing exhaust fans (WIP1) will be replaced with a dedicated EO capture and destruction systems. Further, the shipping area will be enclosed. The new systems are designed to reduce captured emissions by 99% at the outlet.

#### System 1 Description/Flow Diagram

System One (SYS1) will capture potential emissions from the five Sterilization Vessel Rooms (VRM1, VRM2, VRM3, VRM4, VRM5), the Vessel to Aeration Transfer Corridor (NCO1), and the EO Dispensing Room (DRM1). All SYS1 exhaust will be manifolded into a Dry Bed System with variable speed exhaust fan with a maximum capacity of 36,000 cfm. The system will maintain negative pressure, with respect to outside, in the Vessel Rooms, Vessel to Aeration Transfer Corridor, Drum Dispensing and use local ventilation exhaust to capture and destruct EO.

##### Normal Mode:

Vessel Rooms (VRM1-VRM5) will exhaust 4,000 cfm each, DMR1 will exhaust 1,000 cfm, NCO1 hoods will be off. Total cfm = 21,000. The other Vessel rooms, DMR1, and NCO1 can increase cfm, to a total of 36,000 cfm, if monitoring equipment detects elevated EO levels.

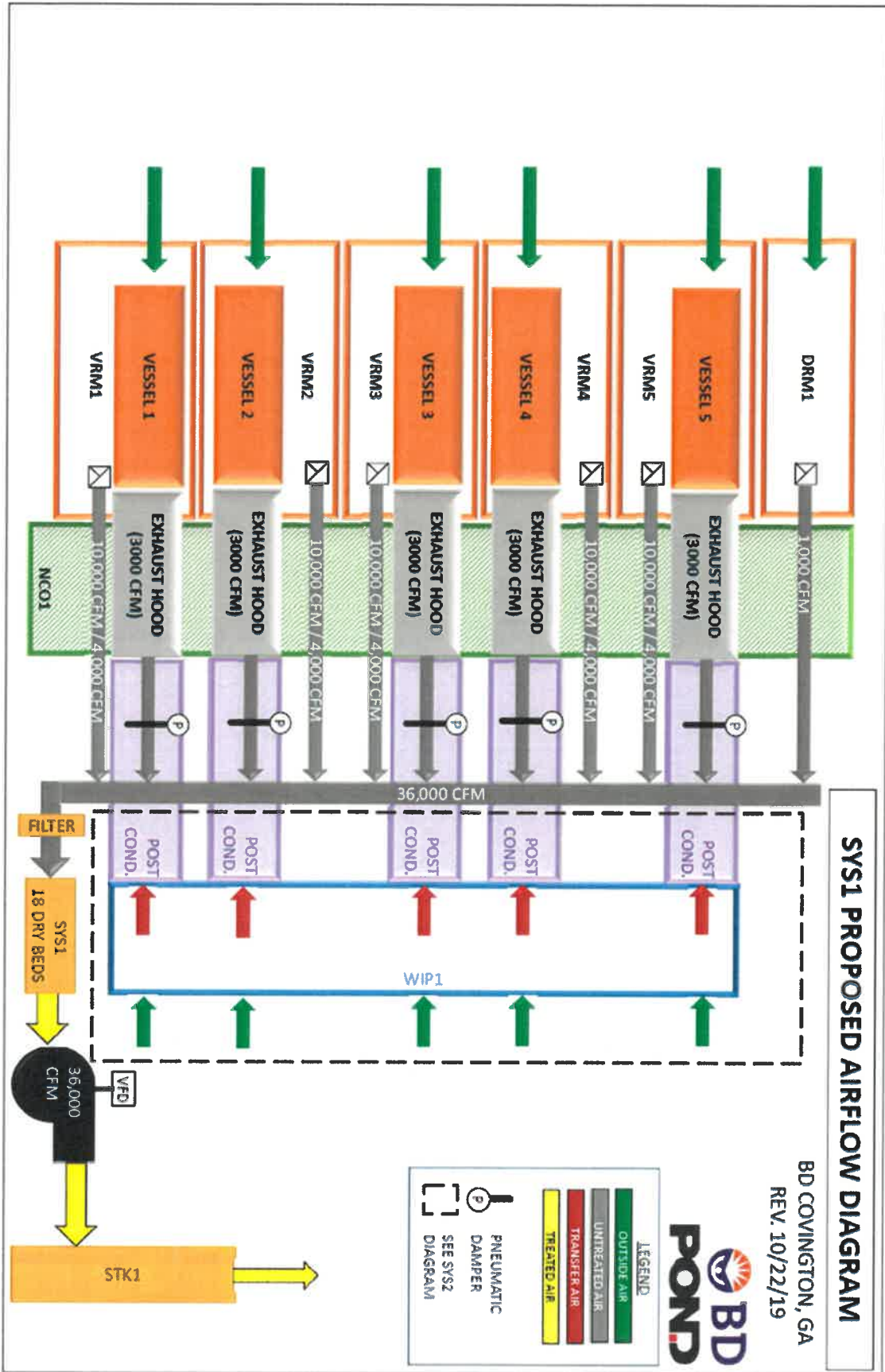
##### Chamber Unloading Mode:

When a chamber is being unloaded the room exhaust will ramp to 10,000 cfm (all other vessel rooms will be at 4,000 cfm) the corresponding NCO1 hood will go to 3,000 cfm exhaust (all other hoods will be off). DMR1 will remain at 1,000 cfm. Total cfm = 30,000. The other Vessel rooms can increase cfm, to a total of 36,000 cfm, if monitoring equipment detects elevated EO levels.

##### Emergency Mode:

SYS1 will also incorporate a safety feature that will serve to shut down the system in the case of a major EO leak ( $\geq 25\%$  of LEL or 7,500ppm). The AAT Dry Beds are designed for a maximum limit of 10,000 ppm and can ignite if overfed leading to potential fire or explosion. An EO sensor will be located in the SYS1 inlet duct and will activate a shutdown sequence based on an internal setpoint. EO emissions will not be captured in this emergency situation. This event will also trigger a sterilization process shutdown. It should be noted that BD has not experienced levels of this magnitude in its twenty-year history and this safety system is being included only to prevent a personnel injury in the event of a catastrophic failure.

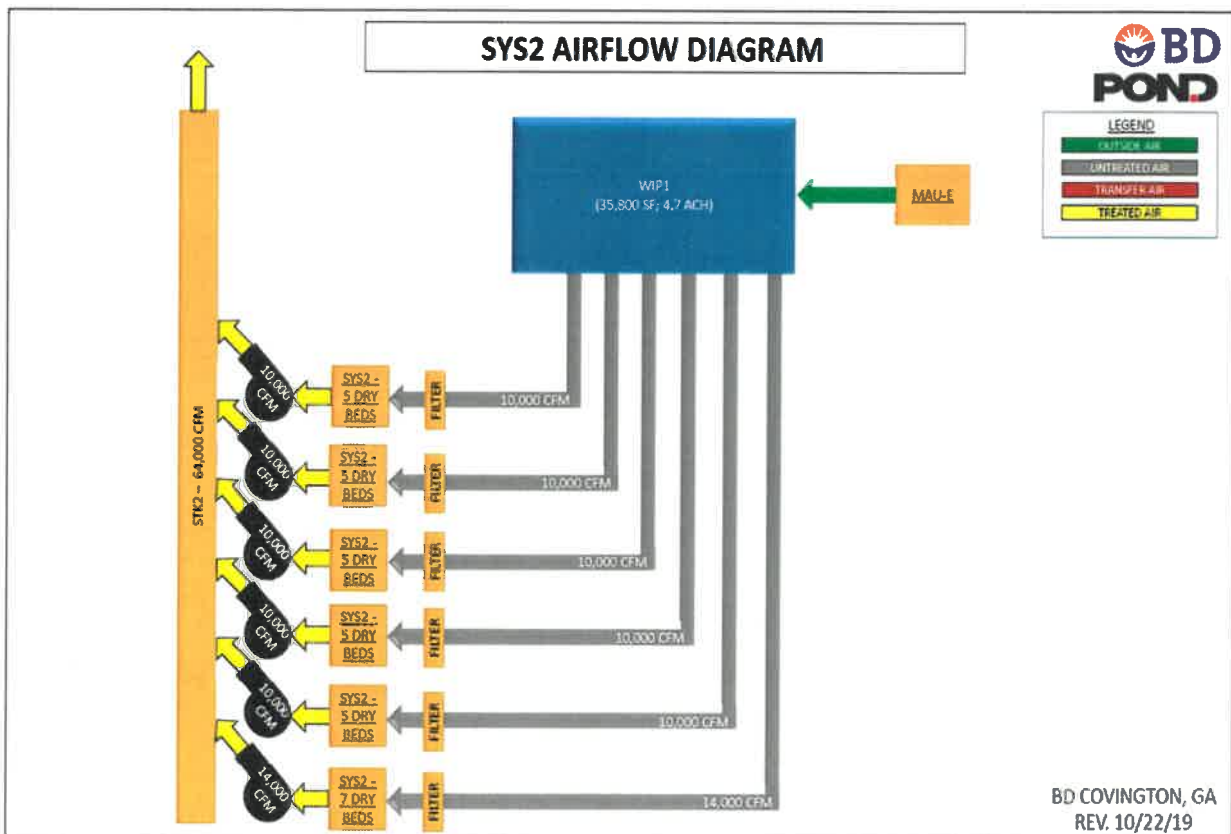
BD Covington SIP Application



BD Covington SIP Application

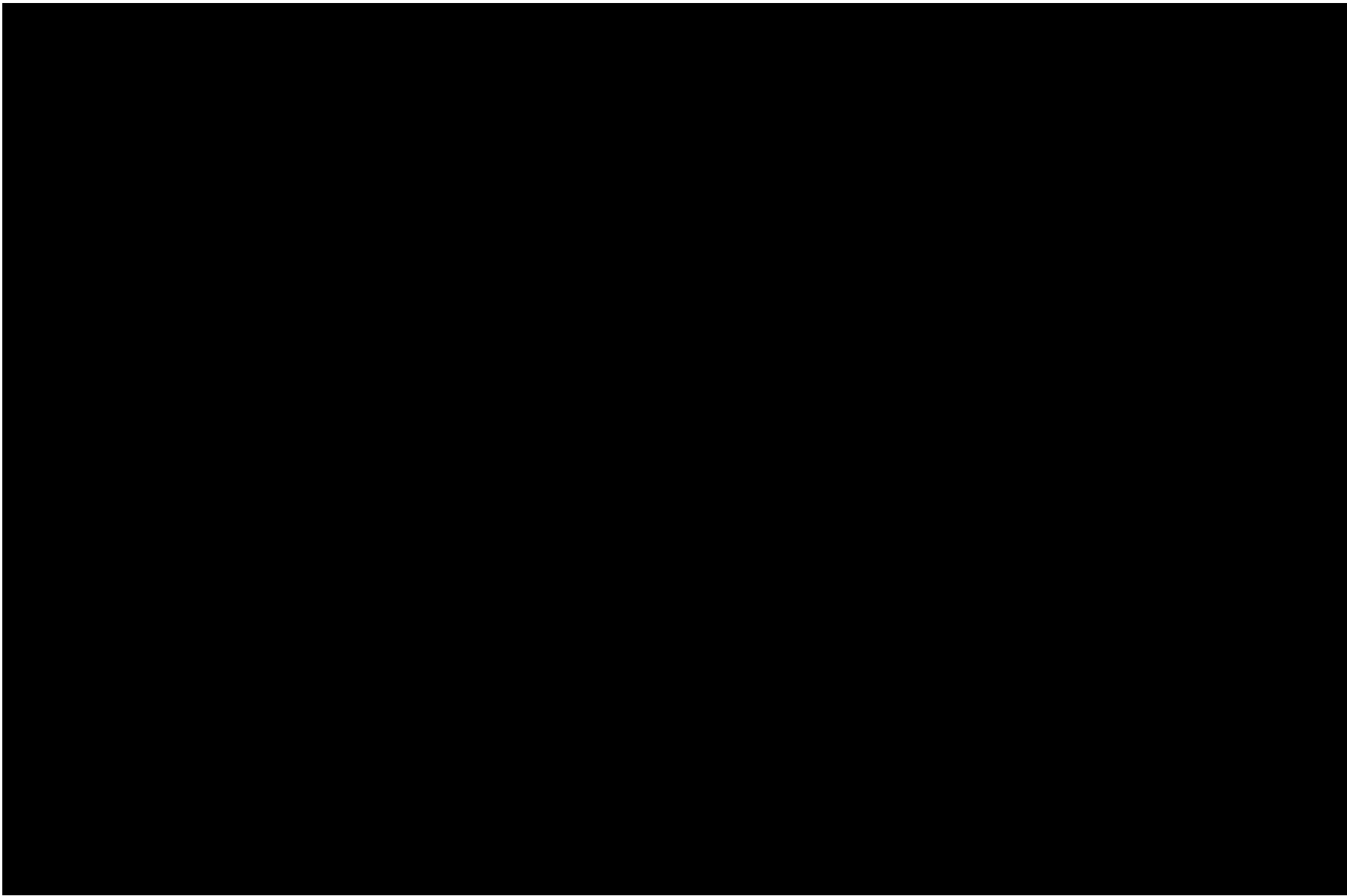
System 2 Description/Flow Diagram

System Two (SYS2) will capture potential emissions from the Work in Progress Area (WIP1) where product is stored after Sterilization and prior to shipment. All SYS2 exhaust will be manifolded into a Dry Bed System with multiple variable speed exhaust fans for a maximum capacity of 64,000 cfm. The exhaust fans will be routed to a common Stack (STK2). The system will maintain negative pressure, with respect to outside, in the WIP1 area. The area pressure will be monitored with pressure sensors and fans will modulated to maintain a negative pressure in the space. Administrative controls will be implemented to ensure building integrity is preserved, doorways are managed, and air flows/pressures are maintained per design. The shipping area will be enclosed to aid in containment of emissions.



ATTACHMENT E		Page 1 of 2	
<b>Becton, Dickinson and Company</b>			
Mass Balance Calculations for SIP Application (PTE)			
Facility: Covington, GA			
<b>Input data:</b>			
Ethylene oxide usage		█ b/yr	Total usage based on Mass Balance
Sterilizer removal efficiency <sup>1</sup>		99.9%	Based on partial pressure calculation estimate
RTO efficiency, aeration		99.970%	Based on 2019 Performance Testing
RTO efficiency, vessels		99.999%	Based on 2019 Performance Testing
Product transfer time, sterilizer to aeration		5 min	
Aeration time		16 hr	
Aeration Unload time		10 min	
System 1 removal efficiency		99%	Assume 99% Based on vendor literature
System 2 removal efficiency		99%	Assume 99% Based on vendor literature
System 2 Safety Factor		4.00	Safety factor included to account for variation in future products and product density which may impact EO residuals.
<b>Assumptions:</b>			
Product absorption <sup>2</sup>		█	
EO degassing rate constant, k <sup>3</sup>		█ lb/hr	
Miscellaneous fugitive loss <sup>4</sup>		100 lb	captured in system 1
<b>Calculations:</b>			
<b>Sterilizer:</b>			
EO into sterilizers		█ lb	Total usage based on Mass Balance minus miscellaneous fugitive loss
EO absorbed by product		2,135.6 lb	
EO in sterilizer not absorbed by product		█ lb	
EO exhausted to RTO from vac/air wash		█ lb	
EO exhausted to RTO from vent		531.8 lb	
Sterilizer exhaust to RTO		█ lb	
Sterilizer exhaust removed by RTO		█ lb	
Sterilizer exhaust to atmosphere after RTO		5.3 lb	
<b>Transfer:</b>			
EO offgas during product transfer to aeration		0.51%	EO will off-gas from products during aeration per equation: $C = C_0 e^{-kt}$ , where C = Final EO concentration, C <sub>0</sub> = EO concentration at time 0, k = EO degassing rate constant, and t = degassing time in hrs.
EO offgas during product transfer to aeration		10.9 lb	This will be captured by system one
<b>Aeration:</b>			
EO remaining in product entering aeration		2,124.7 lb	
Offgas during aeration		62.6%	
Offgas during unloading		0.0	
EO offgas during aeration		1,330.6 lb	
To RTO during aeration		1,330.6 lb	
To RTO during aeration unload		8.1 lb	
Total aeration to RTO		1,338.7 lb	
Aeration removed by RTO		1,338.3 lb	
Aeration exhaust to atmosphere after RTO		0.4 lb	
<b>System 1:</b>			
Into System 1		110.9 lb	
Removed by System 1		109.8 lb	
System 1 exhaust to atmosphere		1.1 lb	
<b>System 2:</b>			
Into System 2		3,144.0 lb	Includes System 2 Safety Factor
Removed by System 2		3,112.6 lb	
System 2 exhaust to atmosphere		31.4 lb	
<b>Exhausted before Modification:</b>			
EO exhausted to atmosphere from RTO		5.7 lb	
EO Exhausted to atmosphere by system 1		110.9 lb	
EO Exhausted by to atmosphere System 2		786.0 lb	Does not include Safety Factor <sup>5</sup>
<b>Total EO exhausted to atmosphere</b>		<b>902.6 lb</b>	<b>Before Modifications</b>
		<b>0.5 Tons</b>	
<b>Exhausted after Modification:</b>			
EO exhausted to atmosphere from RTO		5.7 lb	
EO Exhausted to atmosphere by system 1		1.1 lb	
EO Exhausted by to atmosphere System 2		31.4 lb	Does include Safety Factor
<b>Total EO exhausted to atmosphere</b>		<b>38.3 lb</b>	<b>After Modifications</b>
		<b>0.019 Tons</b>	
Note 1	This estimates how much EO is removed during post exposure vacuum washes but does not include what is in the product at the time it transfers to Aeration		
Note 2	Estimates the amount of EO in the product when it starts the transfer to aeration		
Note 3	An estimate based on Product EO Residue Testing performed by BD laboratory personnel.		
Note 4	An estimate of potential EO emissions from pump/valve packaging, flange losses, EO supply drum changes, and non-routine losses.		
Note 5	The Safety Factor is only included in the After Modification calculations as this insures the new System is designed to account for variation in future products and product density which may impact EO residuals.		

ATTACHMENT E		Page 2 of 2
<b>Becton, Dickinson and Company</b>		
Mass Balance Calculations for SIP Application (Actual)		
Facility:	Covington, GA	
<b>Input data:</b>		
Ethylene oxide usage	█ lb/yr	Total usage based on Mass Balance (CY 2018)
Sterilizer removal efficiency <sup>1</sup>	99.9%	Based on partial pressure calculation estimate
RTO efficiency, aeration	99.970%	Based on 2019 Performance Testing
RTO efficiency, vessels	99.999%	Based on 2019 Performance Testing
Product transfer time, sterilizer to aeration	5 min	
Aeration time	16 hr	
Aeration Unload time	10 min	
System 1 removal efficiency	99%	Assume 99% Based on vendor literature
System 2 removal efficiency	99%	Assume 99% Based on vendor literature
System 2 Safety Factor	4.00	Safety factor included to account for variation in future products and product density which may impact EO residuals.
<b>Assumptions:</b>		
Product absorption <sup>2</sup>	█	
EO degassing rate constant, k <sup>3</sup>	█ lb/hr	
Miscellaneous fugitive loss <sup>4</sup>	100 lb	captured in system 1
<b>Calculations:</b>		
<b>Sterilizer:</b>		
EO into sterilizers	█ lb	Total usage based on Mass Balance minus miscellaneous fugitive loss
EO absorbed by product	1,561.2 lb	
EO in sterilizer not absorbed by product	█ lb	
EO exhausted to RTO from vac/air wash	█ lb	
EO exhausted to RTO from vent	388.7 lb	
Sterilizer exhaust to RTO	█ lb	
Sterilizer exhaust removed by RTO	█ lb	
Sterilizer exhaust to atmosphere after RTO	3.9 lb	
<b>Transfer:</b>		
EO offgas during product transfer to aeration	0.51%	EO will off-gas from products during aeration per equation: $C = C_0 e^{(-kt)}$ , where C = Final EO concentration, C <sub>0</sub> = EO concentration at time 0, k = EO degassing rate constant, and t = degassing time in hrs.
EO offgas during product transfer to aeration	8.0 lb	This will be captured by system one
<b>Aeration:</b>		
EO remaining in product entering aeration	1,553.2 lb	
Offgas during aeration	62.6%	
Offgas during unloading	1.0%	
EO offgas during aeration	972.7 lb	
To RTO during aeration	972.7 lb	
To RTO during aeration unload	5.9 lb	
Total aeration to RTO	978.6 lb	
Aeration removed by RTO	978.3 lb	
Aeration exhaust to atmosphere after RTO	0.3 lb	
<b>System 1:</b>		
Into System 1	108.0 lb	
Removed by System 1	106.9 lb	
System 1 exhaust to atmosphere	1.1 lb	
<b>System 2:</b>		
Into System 2	2,298.4 lb	Includes System 2 Safety Factor
Removed by System 2	2,275.4 lb	
System 2 exhaust to atmosphere	23.0 lb	
<b>Exhausted before Modification:</b>		
EO exhausted to atmosphere from RTO	4.2 lb	
EO Exhausted to atmosphere by system 1	108.0 lb	
EO Exhausted by to atmosphere System 2	574.6 lb	Does not Includes System 2 Safety Factor <sup>5</sup>
<b>Total EO exhausted to atmosphere</b>	<b>686.8 lb</b>	<b>Before Modifications</b>
	<b>0.3 Tons</b>	
<b>Exhausted after Modification:</b>		
EO exhausted to atmosphere from RTO	4.2 lb	
EO Exhausted to atmosphere by system 1	1.1 lb	
EO Exhausted by to atmosphere System 2	23.0 lb	Includes System 2 Safety Factor
<b>Total EO exhausted to atmosphere</b>	<b>28.2 lb</b>	<b>After Modifications</b>
	<b>0.014 Tons</b>	
Note 1	This estimates how much EO is removed during post exposure vacuum washes but does not include what is in the product at the time it transfers to Aeration	
Note 2	Estimates the amount of EO in the product when it starts the transfer to aeration	
Note 3	An estimate based on Product EO Residue Testing performed by BD laboratory personnel.	
Note 4	An estimate of potential EO emissions from pump/valve packaging, flange losses, EO supply drum changes, and non-routine losses.	
Note 5	The Safety Factor is only included in the After Modification calculations as this insures the new System is designed to account for variation in future products and product density which may impact EO residuals.	



*Note: Redacted information was inadvertently disclosed and was not part of BD's Application.*



## Attachment F

### BD Covington SIP Application

BD has not identified an US EPA- or GA EPD-approved stack test method that will measure the concentrations of unregulated, fugitive emissions of ethylene oxide (EO), which are expected to be less than 0.2 ppm, that will enter the dry systems' inlets or the resulting, reduced concentrations of EO at the dry bed systems' outlets or the combined stacks.<sup>1</sup> For these reasons, BD proposes to demonstrate the control efficiency of the dry bed systems using the following sample collection and analysis methods, which are based EPA Method TO-15.

Based upon available information, BD anticipates that the ethylene oxide (EO) concentrations at the inlet and outlet of the proposed systems will be relatively low (i.e., typically less than 0.2 ppmv) and essentially not reliably detected by standard EPA stack testing methods (e.g., EPA Method No. 18). To overcome this limitation, the approach described below employs a gas sampling technique capable of achieving lower detection limits.

When the inlet and outlet concentrations are close to the limits of detection of the analytical equipment it becomes mathematically impossible to prove the specified destruction efficiency. We are currently investigating monitoring technologies and methods that would allow practical measurement of the relatively low levels of EO expected at the outlet of the proposed emission systems with the intent to be able to confirm a 99% reduction or an equivalent emission standard. BD welcomes any alternate sample/analysis methods may be that GA EPD may recommend.

BD proposes that the initial compliance tests and subsequent monthly monitoring of System1 and System2 as follows:

#### Initial Compliance Testing:

- Demonstrate 99% ethylene oxide removal efficiency of the dry bed systems across each control System using simultaneous samples of inlet and outlet gases by Summa Canisters using EPA Method TO-15 with analysis by GC/MS in the Selective Ion Monitoring (SIM) acquisition mode.
- During this sampling of the inlet and outlet concentrations across each system, the outlet stack airflows will be measured using EPA Methods 1, 2, and 4 for determination of volumetric flow rate and moisture content.

---

<sup>1</sup> Advanced Air Technologies, Inc. (AAT), the manufacturer of the dry bed systems, has claimed that that emissions "of EtO will be 99% or = 1 ppmv, whichever is less stringent, when operated per AAT operations manual and other parameters of project design." BD has based its calculations of the removal of unregulated, fugitive EO emissions on AAT's manufacturer's claims. To its knowledge, BD's installation of the AAT dry bed systems to control EO in the concentrations found in the unregulated, fugitive emissions of the substance at the Covington plant is the first such installation anywhere. BD, nonetheless, believes that the dry bed systems will reduce the unregulated, fugitive emissions of EO by 99%.

- Using the above-measured airflow and concentration data, the mass emission rate from each System will be calculated and reported.
- These data will be used to establish baseline conditions against which subsequent monitoring data (collected as described below) will be considered in determining when media replacement should be initiated.

This compliance testing regime will be repeated after completion of any future media replacement.

Routine Monitoring:

- Sample the outlet from each dry bed system on a monthly basis by Summa Canisters using EPA Method TO-15 with analysis by GC/MS in the Selective Ion Monitoring (SIM) acquisition mode and determine concentration of ethylene oxide in the exhaust airflow stream.
- Monthly concentration data will be tracked and compared with baseline data.
- Trending of the monthly concentration data versus baseline will be used in consultation with the dry bed manufacturer to determine when media replacement is warranted to maintain at least 99% removal efficiency.

ATTACHMENT G

BD Covington SIP Application

The abatement method is chemisorption (adsorption accompanied by chemical reaction) by means of Advanced Air Technology dry beds containing sulfonated polymer of styrene. Once the chemisorption process has occurred, the amount of EO is reduced by at least 99%. See table below:

ISO 9001 : 2008 Certified



**ADVANCED AIR TECHNOLOGIES, INC.**  
 300 Earl Sleseman Drive  
 Corunna, MI 48817  
 ( Michigan - USA )

Phone: 989-743-5544  
 Fax: 989-743-5624  
 Toll Free: 800-295-6583

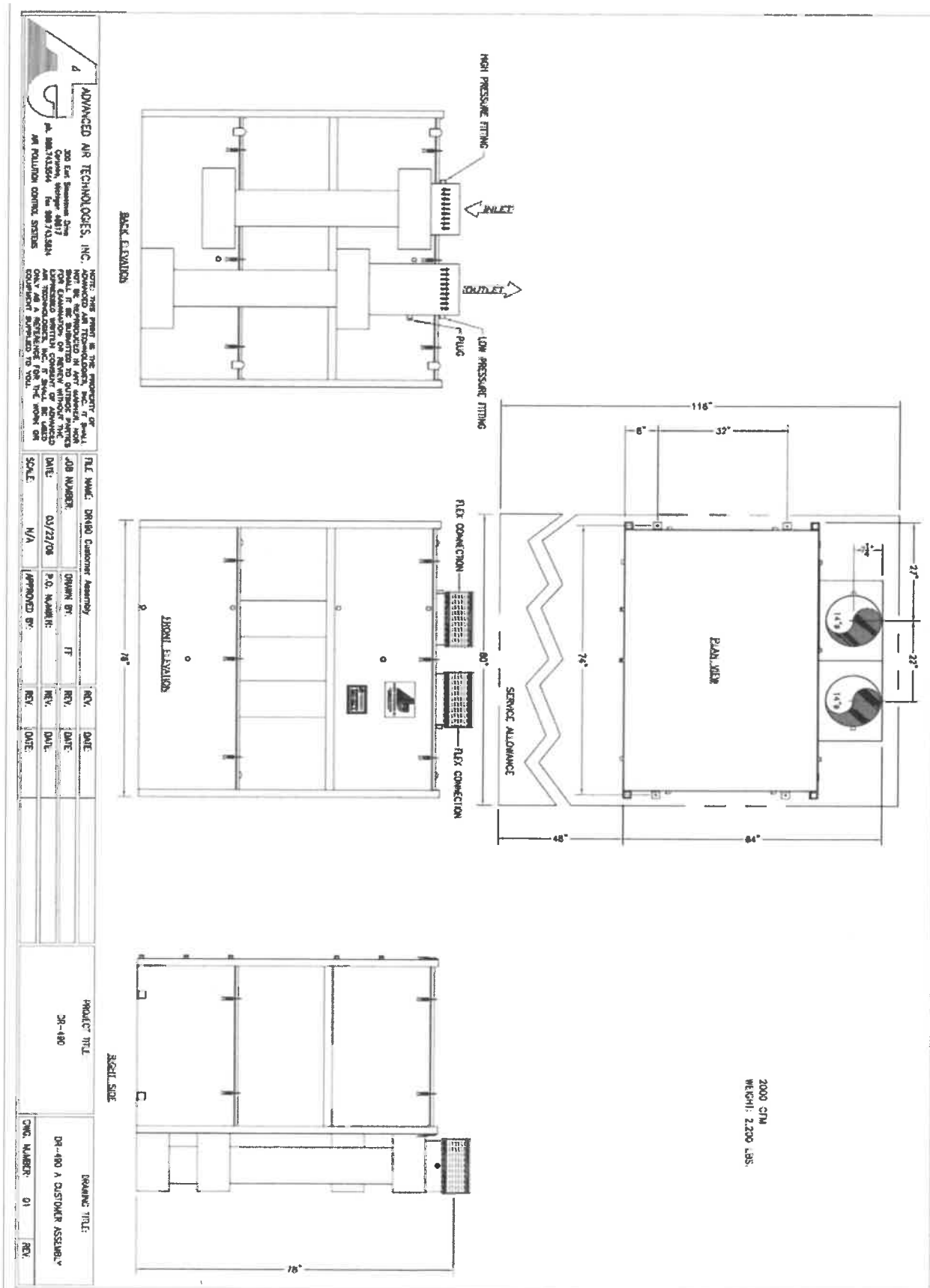
[www.advairtech.com](http://www.advairtech.com)

**AAT, INC. DR-490 ETHYLENE OXIDE ABATOR**  
**REMOVAL EFFICIENCY DECAY**  
**(BASED ON 2000 SCFM AIR FLOW RATE)**

<b>lb. EtO Treated/lb. Reactant</b>	<b>lb. EtO Previously Treated</b>	<b>EtO % Removal Efficiency</b>
0	0	99.995
0.05	45	99.97
0.10	90	99.95
0.15	135	99.92
0.20	180	99.9
0.25	225	99.5
<b>0.30</b>	<b>270</b>	<b>99</b>
0.35	315	98
0.40	360	97
0.45	405	95
0.50	450	85
0.52	468	0

# ATTACHMENT G

## BD Covington SIP Application



ADVANCED AIR TECHNOLOGIES, INC.  
300 East Shannon Drive  
Covina, California 91724  
P.O. BOX 703284  
SAN ANTONIO, TEXAS 78270-3284

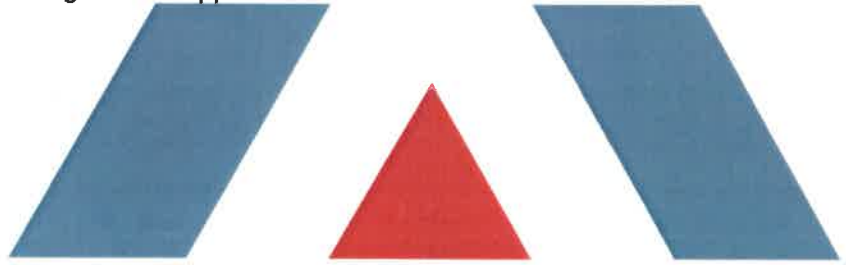
NOTE: THIS PRINT IS THE PROPERTY OF  
ADVANCED AIR TECHNOLOGIES, INC. IT SHALL  
BE RETURNED TO THE COMPANY WITHOUT  
REQUIREMENT OF REVIEW WITHOUT THE  
SIGNATURE OF THE COMPANY. IT SHALL BE  
VALID ONLY AS A REFERENCE FOR THE WORK ON  
CONTRACT SPECIFIED THEREON.

FILE NAME:	DR-480 Customer Assembly
JOB NUMBER:	TF
DATE:	03/22/08
SCALE:	N/A
APPROVED BY:	
REV.	DATE
REV.	DATE
REV.	DATE

PRODUCT TITLE:	DR-480
DRAWING TITLE:	DR-480 A CUSTOMER ASSEMBLY
CHK. NUMBER:	01
REV.	

Attachment H

BD Covington SIP Application



# ETHYLENE OXIDE EMISSIONS IMPACT ASSESSMENT

**BD > Covington Facility**

Prepared By:

**TRINITY CONSULTANTS**

October 2019

Project 191101.0218

**Trinity**  
**Consultants**

*Environmental solutions delivered uncommonly well*

## 1. ETHYLENE OXIDE EMISSIONS IMPACT ASSESSMENT

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EPD regulates the emissions of toxic air pollutants (TAPs) through a program approved under the provisions of GRAQC Rule 391-3-1-.02(2)(a)3(ii). A TAP is defined as any substance that may have an adverse effect on public health, excluding any specific substance that is covered by a State or Federal ambient air quality standard. Procedures governing the EPD's review of toxic air pollutant emissions as part of air permit reviews are contained in EPD's *Guideline for Ambient Impact Assessment of Toxic Air Pollutant Emissions (the Guideline)*.<sup>1</sup>

This assessment included dispersion modeling for ethylene oxide from the facility.

### 1.1. MODELING ASSESSMENT

Modeling conducted was done with the AERMOD (v19191) dispersion model. Meteorological data utilized for the modeling assessment was obtained from the Georgia EPD website.<sup>2</sup> Meteorological data utilized was processed using AERMET (v18081), AERSURFACE (v13016), and AERMINUTE (v15272) with the adjusted surface friction velocity option (ADJ\_U\*). Five consecutive years of meteorological data (2014-2018) were utilized in the modeling assessment, with surface meteorological data from the Atlanta Hartsfield Jackson airport and upper air data from Falcon Field in Peachtree City, Georgia. This assessment was performed in accordance with the *Guideline*.

#### 1.1.1. Source Parameters

Ethylene oxide emissions were modeled as point sources from three specific facility stack locations. For point sources, AERMOD requires the stack height (m), inside stack exit diameter (m), temperature (K), and exit gas velocity (m/s) to be specified. Table 1-1 provides a summary of the location and stack parameters used in the dispersion model for the point sources. The modeled emission rates reflect the current DRE for the RTO (incinerator) at the Covington plant, and assume a 99% reduction of all fugitive emissions of EtO from the plant, which reflects the performance of the dry bed filters proposed in the permit application for which this modeling was performed.

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<sup>1</sup> *Guideline for Ambient Impact Assessment of Toxic Air Pollutant Emissions*. Georgia Department of Natural Resources, Environmental Protection Division, Air Protection Branch, Revised, May 2017.

<sup>2</sup> <https://epd.georgia.gov/air-protection-branch-technical-guidance-0/air-quality-modeling/georgia-aermet-meteorological-data>

Table 1-1. Point Source Parameters

Source	Easting (meter)	Northing (meter)	Modeled Emissions (lb/yr)	Modeled Emissions (lb/hr)	Modeled Emissions (g/s)	Stack Height (ft)	Stack Height (m)	Stack Temperature (F)	Stack Temperature (K)	Exit Velocity (ft/s)	Exit Velocity (m/s)	Flow (cfm)	Stack Diameter (in)	Stack Diameter (m)
RTU	236,424.2	3,722,295.0	5.7	6.51E-04	8.21E-05	50	15.24	250	394.26	30.5	9.29	23,000	48	1.219
System 1	236,404.2	3,722,273.3	1.1	1.26E-04	1.59E-05	100	30.48	70	294.26	30.3	9.23	21,000	46	1.167
System 2	236,423.6	3,722,313.7	31.4	3.58E-03	4.52E-04	100	30.48	70	294.26	50.8	15.48	64,000	62	1.575

BD Covington SIP Application

**1.1.2. Land Use Classification**

Classification of land use in the immediate area surrounding a facility is important in determining the appropriate dispersion coefficients to select for a particular modeling application. The selection of either rural or urban dispersion coefficients for a specific application should follow one of two procedures. These include a land use classification procedure or a population-based procedure to determine whether the area is primarily urban or rural.<sup>3</sup>

Of the two methods, the land use procedure is considered more definitive. The land use within the total area circumscribed by a 3-kilometer (km) radius circle around the facility was classified using the land use typing scheme proposed by Auer. If land use types I1 (Heavy Industrial), I2 (Light Industrial), C1 (Commercial), R2 (Residential; Small Lot Single Family & Duplex), and R3 (Residential; Multi-Family) account for 50% or more of the circumscribed area, urban dispersion coefficients should be used; otherwise, rural dispersion coefficients are appropriate.

AERSURFACE (v13016) was used for the extraction of the land-use values in the domain. The results of the land use analysis evaluation were as follows.

Each USGS NLCD92 land use class was compared to the most appropriate Auer land use category to quantify the total urban and rural area. Table 1-2 summarizes the results of this land use analysis. As approximately 93.7% of the area can be classified as rural, rural dispersion coefficients were used. The AERSURFACE files are enclosed in Appendix A.

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<sup>3</sup> 40 CFR Part 51, Appendix W, the Guideline on Air Quality Models (January 2017) – Section 7.2.1.1(b)(i)  
BD | Ethylene Oxide Emissions Impact Assessment



## BD Covington SIP Application

Table 1-2. Summary of Land Use Analysis

USGS NLCD92		Auer Scheme		Rural/ Urban	Land Area
Land Class	Land Class Description	Land Use Type	Land Use Description		
11	Open Water	A5	Water Surfaces/Rivers/Lakes	Rural	0.8%
12	Perennial Ice/Snow	A5	Water Surfaces/Rivers/Lakes	Rural	0.0%
21	Low Intensity Residential	R1	Common Residential	Rural	7.8%
22	High Intensity Residential	R2 and R3	Compact Residential (Single Family, Multi-Family & Duplex)	Urban	0.9%
23	Commercial/Industrial/ Transportation	I1, I2, and C1	Heavy and Light-Moderate Industrial & Commercial	Urban	5.4%
31	Bare Rock/Sand/Clay	A3	Undeveloped	Rural	0.0%
32	Quarries/Strip Mines/Gravel	A4	Undeveloped Rural	Rural	0.2%
33	Transitional	A3	Undeveloped/Uncultivated	Rural	1.8%
41	Deciduous Forest	A4	Undeveloped Rural	Rural	29.1%
42	Evergreen Forest	A4	Undeveloped Rural	Rural	19.9%
43	Mixed Forest	A4	Undeveloped Rural	Rural	13.2%
51	Shrubland	A3	Undeveloped/Uncultivated	Rural	0.0%
61	Orchards/Vineyard/Other	A2	Agricultural Rural	Rural	0.0%
71	Grasslands/Herbaceous	A3	Undeveloped/Uncultivated	Rural	0.0%
81	Pasture/Hay	A2	Agricultural Rural	Rural	7.0%
82	Row Crops	A2	Agricultural Rural	Rural	3.8%
83	Small Grains	A2	Agricultural Rural	Rural	0.0%
84	Fallow	A2	Agricultural Rural	Rural	0.0%
85	Urban/Recreational Grasses	A1	Metropolitan Natural	Rural	2.5%
91	Woody Wetlands	A4	Undeveloped Rural	Rural	7.6%
92	Emergent Herbaceous Wetlands	A4	Undeveloped Rural	Rural	0.2%

### 1.1.3. Building Downwash

The effects of building downwash for each of the stack emission points were evaluated in terms of the proximity of the stack to nearby structures. The purpose of this evaluation is to determine if stack discharges might become caught in the turbulent wakes of these structures leading to downwash of the plumes. Wind blowing around a building creates zones of turbulence that are greater than if the building were absent.

## Attachment H

### BD Covington SIP Application

For these modeling analyses, the direction-specific building dimensions used as input to the AERMOD model were calculated using the U.S. EPA's BPIP PRIME, version 04274. BPIP PRIME is designed to incorporate the concepts and procedures expressed in the GEP Technical Support document, the Building Downwash Guidance document, and other related documents.<sup>4</sup>

For the BPIP analysis, the structure elevations (buildings and stacks) were estimating using the AERMAP processor (v18081). Terrain elevations from the USGS 1-arc second NED were used for AERMAP processing. In all modeling analysis data files, the location of emission points and structures were represented in the UTM coordinate system, zone 17, NAD 83.

EPA has promulgated stack height regulations that restrict the use of stack heights in excess of "Good Engineering Practice" (GEP) in air dispersion modeling analyses. Under these regulations, that portion of a stack in excess of the GEP height is generally not creditable when modeling to determine source impacts. This essentially prevents the use of excessively tall stacks to reduce ground-level pollutant concentrations.

This equation is limited to stacks located within five times the lesser dimension (5L) of a building structure. Stacks located at a distance greater than 5L from a building structure are not subject to the wake effects of the structure. The wind direction-specific downwash dimensions and the dominant downwash structures used in this analysis are determined using BPIP. In general, the lowest GEP stack height for any source is 65 meters by default.<sup>5</sup> The BPIP evaluation indicates that none of the facility emission unit stacks exceed GEP stack height.

Input and output files from the BPIP downwash analysis are provided in the electronic files included in Appendix A.

#### 1.1.4. Receptor Grid Coordinate System

Modeled concentrations were calculated at ground-level receptors placed along the facility fenceline and on a variable Cartesian receptor grid. Fenceline receptors were spaced no more than 25 meters apart. Beyond the fenceline, receptors were placed with 100 meters spacing on a Cartesian grid extending outward from the facility. An approximately 25 km by 25 km modeling domain with a receptor spacing of 100 meters was created.

Also, five residential receptors, as identified in a modeling memo prepared by the Georgia Environmental Protection Division (EPD) in June 2019, were also placed within the receptor grid system to provide predicted modeled impacts consistent with the results presented by the EPD in their June 2019 memo.<sup>6</sup>

Receptor elevations and hill heights required by AERMOD were determined using the AERMAP terrain preprocessor (v18081). Terrain elevations from the USGS 1-arc second NED were used for AERMAP processing. In all modeling analysis data files, the location of receptors were represented in the UTM coordinate system, zone 17, NAD 83.

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<sup>4</sup> U.S. EPA, Office of Air Quality Planning and Standards, Guidelines for Determination of Good Engineering Practice Stack Height (Technical Support Document for the Stack Height Regulations) (Revised), Research Triangle Park, North Carolina, EPA 450/4-80-023R, June 1985.

<sup>5</sup> 40 CFR 51.100(ii)

<sup>6</sup> <https://epd.georgia.gov/bd-becton-dickinson-and-company-covington>  
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## BD Covington SIP Application

**1.1.5. Modeling Results**

Using the source parameters specified in Table 1-1, and additional model setup as described above, AERMOD was executed for each of the five years of meteorological data to determine the maximum predicted modeled 1-hr and annual concentrations of ethylene oxide at each receptor location. Table 1-3 below summarizes the MGLC for each averaging period. Hourly concentrations were adjusted to a 15-min averaging period based on the *Guideline* (15-min MGLC = 1-hr MGLC \* 1.32).

Table 1-3. Maximum Predicted Modeled Impacts

Year	Max Annual Concentration ( $\mu\text{g}/\text{m}^3$ )	Annual AAC ( $\mu\text{g}/\text{m}^3$ )	Max Hourly Concentration ( $\mu\text{g}/\text{m}^3$ )	Max 15-min Concentration ( $\mu\text{g}/\text{m}^3$ )	15-minute AAC ( $\mu\text{g}/\text{m}^3$ )
2014	6.0E-04	3.3E-04	0.29	0.38	900
2015	5.3E-04		0.03	0.04	
2016	5.4E-04		0.03	0.04	
2017	4.6E-04		0.04	0.05	
2018	5.5E-04		0.05	0.06	

While maximum predicted modeled impacts exceed the annual AAC, the locations where the annual AAC are exceeded are limited to locations in much closer proximity to the facility when compared to modeling conducted by the Georgia EPD for their June 7<sup>th</sup>, 2019 modeling memo. The distance from the facility at which the model predicts exceedances of the annual AAC has been reduced by approximately 95% due to the proposed changes. The magnitude of the predicted modeled annual impacts have been reduced more than 99.5% when compared to modeling conducted by the Georgia EPD for their June 7<sup>th</sup>, 2019 modeling memo.

Analyses were also conducted to evaluate predicted modeled impacts at each of five identified residential receptors by the Georgia EPD. Table 1-3 below summarizes the annual average maximum predicted modeled impacts at the five residential receptor locations previously identified by the Georgia EPD.

Table 1-4. Maximum Predicted Modeled Impacts at EPD Identified Residential Receptors

Residential Area	Easting (meter)	Northing (meter)	Max Annual Concentration ( $\mu\text{g}/\text{m}^3$ )	Averaging Period	Annual AAC ( $\mu\text{g}/\text{m}^3$ )	Ratio of Result to AAC
R1	236,932.5	3,722,361.2	2.7E-04	Annual	3.3E-04	0.82
R2	236,137.9	3,721,995.0	1.3E-04	Annual	3.3E-04	0.39
R3	236,163.0	3,721,885.6	8.0E-05	Annual	3.3E-04	0.24
R4	237,343.8	3,721,603.8	2.2E-04	Annual	3.3E-04	0.67
R5	235,611.0	3,722,319.2	2.5E-04	Annual	3.3E-04	0.76

All air dispersion modeling files are included in Appendix A.

**APPENDIX A. ELECTRONIC TOXICS MODELING FILES**

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