Prepared for



ENVIRONMENTAL PROTECTION DIVISION

Approved Solid Waste Management Program

Approved By:

Crisp County Power Commission 202 S. 7th Street Cordele, Georgia 31015

GROUNDWATER MONITORING AND STATISTICAL ANALYSIS PLAN

FOR PLANT CRISP ASH POND AND SECONDARY ASH AREAS

CRISP COUNTY POWER COMMISSION Crisp County, Georgia



Geosyntec^D consultants

engineers | scientists | innovators

Georgia Certificate of Authorization No. PEF000260, Exp. 06/30/2026

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LIST OF ACRONYMS

ANOVA	Analysis of Variance
CCPC	Crisp County Power Commission
CCR	Coal Combustion Residuals
C.F.R.	Code of Federal Regulations
DO	Dissolved Oxygen
GA EPD	Georgia Environmental Protection Division
LSASD	Laboratory Services and Applied Science Division
MCL	Maximum Contaminant Level
MW	Megawatt
NELAC	National Environmental Laboratory Accreditation Conference
NTU	Nephelometric Turbidity Unit
ORP	Oxidation Reduction Potential
PL	Upper Prediction Limit
PQL	Practical Quantitation Limit
RCRA	Resource Conservation and Recovery Act
SESD	Science and Ecosystem Support Division
SOP	Standard Operating Procedure
SSI	Statistically Significant Increase
SSL	Statistically Significant Level
SWFPR	Site-wide False Positive Rate
USEPA	United States Environmental Protection Agency
UTL	Upper Tolerance Limit

CERTIFICATION BY QUALIFIED PROFESSIONAL

I hereby certify that this Groundwater Monitoring Plan was prepared by, or under the direct supervision of, a "Qualified Groundwater Scientist," in accordance with the Georgia Rules of Solid Waste Management. In accordance with Georgia Rules for Solid Waste Management, a "Qualified Groundwater Scientist" is a professional engineer or geologist registered to practice in Georgia who has received a baccalaureate or postgraduate degree in the natural sciences or engineering and has sufficient training and experience in groundwater hydrology and related fields that enable that individual to make sound professional judgments regarding groundwater monitoring, contaminant fate and transport, and corrective action. The design of the groundwater monitoring system was developed in compliance with the Georgia Environmental Protection Division (GA EPD) Rules of Solid Waste Management, Chapter 391-3-4-.10.

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1. INTRODUCTION

This Groundwater Monitoring and Statistical Analysis Plan has been prepared for Crisp County Power Commission (CCPC's) Plant Crisp ash pond and two former coal ash disposal areas (referred in this document as secondary ash areas). The ash pond had a Groundwater Monitoring and Statistical Analysis Plan dated April 2020 and approved by Georgia Environmental Protection Division (GA EPD). This *Groundwater Monitoring and Statistical Analysis Plan dated Secondary Ash Areas* has been prepared to serve for both the ash pond and the secondary ash areas as requested by GA EPD in their letter dated 24 April 2023.

In April 2015, the United States Environmental Protection Agency (USEPA) issued new regulations regarding the disposal of coal combustion residuals (CCR) under 40 C.F.R. §257, Subpart D, referred to as the "USEPA CCR Rule" (USEPA, 2015a). Facilities regulated under the CCR Rule are required to develop and sample a groundwater monitoring well network to evaluate if the CCR disposal units are impacting downgradient groundwater quality. As part of the evaluation, the analytical data collected during the sampling events must undergo statistical analysis to evaluate if any statistically significant increases (SSIs) in analyte concentrations above background levels or any statistically significant levels (SSLs) exceeding the groundwater protection standard (GWPS) exist. A description of acceptable statistical programs is provided in USEPA's document *Statistical Analysis of Groundwater Data at RCRA Facilities, Unified Guidance* (USEPA, 2009), which is commonly referred to as the "Unified Guidance."

The USEPA CCR Rule is not prescriptive regarding what statistical analysis should be selected to ensure groundwater data are interpreted in a consistent matter and the results meet certification requirements. Geosyntec Consultants, Inc. (Geosyntec) prepared this Groundwater Monitoring and Statistical Analysis Plan on behalf of CCPC to develop a procedure for groundwater monitoring and a process regarding the selection of the appropriate statistical analysis of groundwater data collected from monitoring wells. The Groundwater Monitoring and Statistical Analysis Plan provides: (i) discussions on groundwater monitoring well network for both the ash pond and secondary ash areas; (ii) groundwater sampling methods; (iii) laboratory analytical methods; and (iv) a narrative description of the statistical approach and methods to be used in accordance with the USEPA CCR Rule reporting requirements [40 C.F.R. §257.93(f)(6)]. The document describes procedures for collecting, preserving, shipping, and laboratory analysis of groundwater samples as well as statistical procedures to be used to establish background conditions, implement detection monitoring, and implement assessment monitoring (as



needed) for the CCPC ash pond and secondary ash areas. This document does not include statistical procedures for corrective action monitoring which should be developed when a corrective action groundwater monitoring program is established, if groundwater remedial action is necessary.

2. SITE LOCATION AND BACKGROUND

CCPC Plant Crisp is a dual-fuel (coal and natural gas) electrical generation facility located in Warwick, Georgia. The byproducts of power generation through the combustion of coal (commonly referred to as CCR) at Plant Crisp included mainly fly ash and bottom ash. The CCR was disposed into a 6.5-acre ash pond located within the plant property. The coal burning and resulting sluicing operation was completed in March 2017. To comply with both the United States Environmental Protection Agency's (USEPA's) 40 C.F.R. 257 and Georgia Environmental Protection Division's (GA EPD's) Solid Waste Management, Chapter 391-3-4-.10, CCPC is currently closing the ash pond by removal and disposal of the CCR at the Crisp County Sanitary Landfill. During the decommissioning of the ash pond, two former coal ash disposal areas (also referred to herein as the secondary ash areas) were discovered. Secondary Ash Area 1 and Secondary Ash Area 2 cover approximately 0.9 and 3.4 acres, respectively. The secondary ash areas are located on undeveloped land that are either naturally forested or landscaped grass fields (**Figure 2-1**).

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3. GROUNDWATER MONITORING WELL NETWORK

3.1 Overview

The groundwater monitoring system for the ash pond includes one upgradient monitoring well (MW-U1) and three downgradient monitoring wells (MW-D1, MW-D2, and MW-D3). The groundwater monitoring system for the secondary ash areas includes two upgradient monitoring wells (MW-U1 and MW-U2) and six downgradient monitoring wells (MW-D4 through MW-D9) located immediately downgradient of the secondary ash areas. Monitoring wells MW-D4, MW-D5, MW-D6 were installed downgradient of Secondary Ash Area 2. Monitoring wells MW-D7, MW-D8, and MW-D9 were installed downgradient of Secondary Ash Area 1. Details of the monitoring well installation are provided below. The locations of the monitoring wells are shown on **Figure 3-1**.

3.2 Selection of Well Locations

Existing hydrogeologic information was evaluated prior to placement of the groundwater monitoring well network. This included review of soil boring/piezometer information from historical geotechnical and hydrogeologic investigations performed between 1965 and 2014. Detailed description of the historical information has been provided in the *Hydrogeologic Assessment Report for Plant Crisp Ash Pond and Secondary Ash Areas* dated July 2023. The upgradient monitoring wells were installed beyond the upgradient limit of the ash pond and the secondary ash areas and are screened in the uppermost aquifer and in the same lithologic units as the downgradient wells (in the alluvium and upper portion of the residuum). The downgradient monitoring wells were installed at the edge of the waste boundary and also screened in the uppermost aquifer. Distance between the monitoring wells was selected so that potential release of CCR constituents will be immediately detected. The spacing between the downgradient monitoring wells considered site-specific hydrogeologic factors listed in Table II-1 of GA EPD's Manual for Groundwater Monitoring dated September 1991 (GA EPD, 1991).

3.3 Borehole Drilling, Well Installation, Abandonment, and Reporting

3.3.1 Ash Pond

The groundwater monitoring system includes one upgradient monitoring well (MW-U1) and three monitoring wells (MW-D1, MW-D2, and MW-D3) located immediately downgradient of the ash pond to the southwest, northwest, and north, respectively.

Drilling

Drilling and monitoring well installation were performed in February 2017 by Environmental Monitoring Services of Woodstock, GA under the supervision of a Geosyntec engineer. Borings were advanced to depths up to 40 feet below ground surface (ft bgs). The boreholes were advanced using a combination of direct push technology (DPT) and hollow stem auger drilling methods. Continuous soil cores collected via acetate DPT core sleeves were logged by a Geosyntec engineer. After reaching the desired drilling depth, each borehole was reamed to a six-inch diameter borehole using a hollow-stem auger drilling method.

Well Design and Construction

Monitoring wells were constructed of Schedule 40 polyvinyl chloride (PVC) casing and 10-ft slotted (0.010-inch) PVC screen. The monitoring wells were installed at depths ranging between 20 ft and 34 ft (Table 3-1). A filter pack consisting of quartz sand, fineto medium-grained (approximately 20-40 Sieve size) was installed around the well screens and extended to approximately two ft above the top of the screen. The filter pack was added by pouring from the surface (gravity feed process) into the well annulus area between the drill casing and the PVC riser pipe assembly. Approximately two feet bentonite pellets were placed above the filter pack. After the bentonite pellets were allowed to hydrate, the remaining annular space was grouted using a cement-bentonite grout at 90/10 ratio. Well risers for the monitoring wells were installed extending a minimum of 3.2 ft above ground surface. Concrete surface pads and protective surface casings were installed at each monitoring well location. A lockable steel outer surface casing was installed over the PVC well casing within the 2 ft \times 2 ft \times 6 in concrete pad. The steel outer protective casing was pushed into the concrete slurry. The annular space between the extended PVC riser pipe and the steel outer protective cover was filled with washed pea gravel to approximately six inches below the top of the PVC. Two weep holes were drilled on opposite sides at the base of the steel outer protective casing. Four concrete-filled protective bollards were installed around each monitoring well and set in concrete. The bollards extend approximately 3 ft above ground surface and were painted vellow for high visibility. A schematic showing surface completion of the groundwater monitoring wells is provided in Figure 3-2. The wells were developed 24 hours after well installation. In June 2017, Geosyntec prepared the Groundwater Monitoring System Certification in compliance with the requirements of 40 C.F.R. §257.91(f).

If additional wells are installed in the future, the well screen design will be in accordance with USEPA Guidance on Design and Installation of Monitoring Wells dated 16 January 2018 (SESDGUID-101-R2). For formations consisting primarily of fines (silts and clays), a 0.010" screen slots with a 20-40 sand filter pack will be used. Screen length shall not exceed 10 feet without EPD's approval.

Drilling equipment will be decontaminated prior to drilling and between boreholes or well installations in accordance with U.S. Environmental Protection Agency's Laboratory Science and Applied Science Operating Procedure LSASDPROC-205-R4 dated 22 June 2020 (USEPA, 2020), which includes washing with Liquinox[®] detergent and tap water, rinsing with tap water, and rinsing again with deionized or distilled water.

Surveying

Surveying of the northing, easting, top of casing elevation, and ground surface elevation of the monitoring wells was conducted by J.B. Faircloth & Associates, P.C. under the supervision of a land surveyor licensed in Georgia. Horizontal coordinates were surveyed to an accuracy of 0.5 ft and are provided in the State Plane NAD83 Georgia West Zone coordinate system. Ground surface elevations and top of casing elevations were surveyed to an accuracy of 0.01 ft and are referenced to the NAVD88 datum. A copy of the land surveyor's certification drawing is provided in **Appendix A**. The boring logs and well construction diagrams for these monitoring wells are presented in **Appendix B**.

If additional wells are installed in the future, the horizontal coordinates of the well will be surveyed to an accuracy of 0.5 ft and are provided in the State Plane NAD83 Georgia West Zone coordinate system. Ground surface elevations and top of casing elevations will be surveyed to an accuracy of 0.01 ft and are referenced to the NAVD88 datum.

Well Abandonment

Monitoring wells will be abandoned using industry-accepted practices and using the Manual for Groundwater Monitoring (GA EPD, 1991) and Georgia Water Well Standards Act of 1985 [Official Code of Georgia Annotated (O.C.G.A.) 12-5-120, 1985] as guides. Neat Portland cement or bentonite will be used as appropriate to complete abandonment and seal the well borehole.

Per Georgia Rule 391-3-4-.10(6)(g), monitoring wells require abandonment and replacement after two consecutive dry sampling events, unless an alternate schedule is approved by the GA EPD. Well replacement and/or abandonment will be performed

under the direction of a professional geologist (P.G) or engineer (P.E.) registered in the state of Georgia. A minor modification shall be submitted in accordance with Rule 391-3-4-.02 prior to the installation or decommissioning of monitoring wells.

Reporting

If a change is made to the groundwater monitoring well network (installation of additional wells or abandonment of an existing well), the well installation will be performed in accordance with the USEPA Guidance on Design and Installation of Monitoring Wells dated 16 January 2018 (SESDGUID-101-R2). Following well installation or abandonment, a well installation report or abandonment report will be submitted to the GA EPD within 60 days of installation or abandonment. The report will be certified by a qualified groundwater scientist. For installed wells, the following information will be included:

- well identification;
- name of drilling contractors and type of drill rig;
- date/time of construction;
- drilling method and drilling fluid if used;
- documentation that the driller, at the time the monitoring wells were installed, had a bond on file with the Water Well Advisory Board;
- borehole diameter and well casing diameter;
- well location given to within an accuracy of 0.5 feet based upon survey from acceptable survey point;
- well depth (± 0.1 ft);
- documentation of ground surface elevation (±0.01 ft); documentation of top of casing elevation (±0.01 ft) and screen top and bottom elevation;
- type of protective well cap and sump dimensions for each well;
- drilling and lithologic logs;



- schematic of the well with dimensions;
- casing and screen materials;
- screen slot size;
- screened interval in feet below ground surface and elevation;
- details of filter pack construction including material;
- filter pack emplacement method (narrative);
- seal emplacement method and type/volume of sealant;
- surface seal and volumes/mix of annular seal material;
- well development date;
- well turbidity following development; and
- narrative of well development method and specific well development procedure.

In accordance with the Georgia Water Well Standards act (O.C.G.A. § 12-5-134(5)(d)(vii)), at least once every five years, the owner of the property on which a monitoring well is constructed shall have the monitoring well(s) inspected by a professional engineer or professional geologist, who shall direct appropriate remedial corrective work to be performed if the well does not conform to standards.

3.3.2 Secondary Ash Areas

The groundwater monitoring system for the secondary ash areas include two upgradient monitoring wells (MW-U1 and MW-U2) and six downgradient monitoring wells (MW-D4 through MW-D9). Monitoring wells MW-D4, MW-D5, and MW-D6 were installed immediately downgradient of the Secondary ash area 2. Monitoring wells MW-D7, MW-D8, and MW-D9 were installed immediately downgradient of Secondary ash areas 1.

Drilling

Drilling and monitoring well installation were performed in May 2022 by GSE, Inc. of Trinity, Alabama under the supervision of a Geosyntec geologist. The Drilling and

monitoring well installation were performed in accordance with the USEPA Guidance on Design and Installation of Monitoring Wells dated 16 January 2018 (SESDGUID-101-R2). Borings were advanced to depths up to 35 feet below ground surface (ft bgs). Six-inch diameter boreholes were advanced using sonic drilling method. Continuous soil cuttings collected during borehole drilling were logged by a Geosyntec geologist.

Well Design and Construction

After reaching the desired drilling depth, two-inch diameter monitoring wells were constructed of Schedule 40 polyvinyl chloride (PVC) casing and 10-ft slotted (0.010-inch) PVC screen. The monitoring wells were installed at depths ranging between 24 ft and 34 ft bgs (**Table 3-1**). A filter pack consisting of quartz sand, fine- to medium-grained (approximately 20-40 Sieve size) was installed around the well screens and extended to approximately two feet above the top of the screen. The filter pack was added by pouring from the surface (gravity feed process) into the well annulus area between the drill casing and the PVC riser pipe assembly. Approximately two feet of bentonite chips were placed above the filter pack. After the bentonite chips were allowed to hydrate for approximately 24 hours, the remaining annular space was grouted using a cement-bentonite grout at 90/10 ratio. Well risers for the monitoring wells were installed extending between 2.5 feet and 4 feet above ground surface. The boring logs and well construction diagrams for these monitoring wells are presented in **Appendix B**.

Concrete surface pads and protective surface casings were installed at each monitoring well location. A lockable steel outer surface casing was installed over the PVC well casing within the 3 ft \times 3 ft \times 6-inch concrete pad. The steel outer protective casing was pushed into the concrete slurry. The annular space between the extended PVC riser pipe and the steel outer protective cover was filled with washed pea gravel to approximately six inches below the top of the PVC. Two weep holes were drilled on opposite sides at the base of the steel outer protective casing. Four concrete-filled protective bollards were installed around each monitoring well and set in concrete. The bollards extend approximately 3 feet above ground surface and were painted yellow for high visibility. A schematic showing surface completion of the groundwater monitoring wells is provided in Figure 3-2. The wells were developed 24 hours after well installation using surging and pumping until the turbidity of the groundwater was less than 10 nephelometric turbidity units (NTU). Geosyntec prepared the Groundwater Monitoring System Certification for the secondary ash areas in compliance with the requirements of 40 C.F.R. §257.91(f) in August 2022.

If additional wells are installed in the future, the well screen design will be in accordance with USEPA Guidance on Design and Installation of Monitoring Wells dated 16 January 2018 (SESDGUID-101-R2). For formations consisting primarily of fines (silts and clays), a 0.010" screen slots with a 20-40 sand filter pack will be used. Screen length shall not exceed 10 feet without EPD's approval.

Drilling equipment will be decontaminated prior to drilling and between boreholes or well installations in accordance with U.S. Environmental Protection Agency's Laboratory Science and Applied Science Operating Procedure LSASDPROC-205-R4 dated 22 June 2020 (USEPA, 2020), which includes washing with Liquinox[®] detergent and tap water, rinsing with tap water, and rinsing again with deionized or distilled water.

Surveying

Surveying of the northing, easting, top of casing elevation, and ground surface elevation of the monitoring wells was conducted by J.B. Faircloth & Associates, P.C. under the supervision of a land surveyor licensed in Georgia. Horizontal coordinates were surveyed to an accuracy of 0.5 feet and are provided in the State Plane NAD83 Georgia West Zone coordinate system. Ground surface elevations and top of casing elevations were surveyed to an accuracy of 0.01 feet and are referenced to the NAVD88 datum. A copy of the land surveyor's certification drawing is provided in **Appendix A**.

If additional wells are installed in the future, the horizontal coordinates of the well will be surveyed to an accuracy of 0.5 ft and are provided in the State Plane NAD83 Georgia West Zone coordinate system. Ground surface elevations and top of casing elevations will be surveyed to an accuracy of 0.01 ft and are referenced to the NAVD88 datum.

Potentiometric Surface Map

The potentiometric surface map depicts the groundwater flow direction from the southeast to the northwest (**Figure 3-3**). The groundwater flow direction has been consistent with historical conditions indicating no seasonal fluctuation in groundwater flow direction. **Table 3-2** presents a summary of groundwater elevation data between May 2022 and April 2023 from the monitoring wells and surface water elevation data from Lake Blackshear. Hydraulic gradients calculated between MW-U1 and MW-D9, between MW-D4 and MW-D9, and between Lake Blackshear and MW-D3 are also included in **Table 3-2**. The mean hydraulic gradient of approximately 0.012 ± 0.001 ft/ft is fairly consistent and not significantly different from historical measurements.

Consistent temporal and spatial hydraulic gradients are indicative of little to no seasonal and spatial fluctuations in groundwater flow velocity.

Well Abandonment

The well abandonment procedure discussed above for the ash pond wells will be followed for the monitoring wells at the secondary ash areas.

Reporting

The reporting procedure discussed above for the ash pond wells will be followed for the monitoring wells at the secondary ash areas.

4. GROUNDWATER SAMPLING AND ANALYSIS PROGRAM

According to 40 C.F.R. §257.93(a) the groundwater monitoring program must include consistent sampling and analysis procedures to provide accurate representation of groundwater quality at the background and downgradient wells as required. CCPC's groundwater monitoring program has been designed to collect groundwater from the uppermost aquifer that accurately represents the quality of background groundwater that has not been affected by leakage from a CCR unit, and accurately represents the quality of groundwater passing the waste boundary of the CCR unit.

The groundwater monitoring system for the ash pond includes one upgradient monitoring well (MW-U1) and three monitoring wells (MW-D1, MW-D2, and MW-D3) located immediately downgradient of the ash pond. The monitoring well network for the secondary ash areas include two wells (MW-U1 and MW-U2) for background monitoring. Existing background well (MW-U1) will have historical monitoring data for that will be used for the secondary ash areas. In addition, six newly installed monitoring wells (MW-D4 through MW-D9) will be used for compliance/downgradient monitoring. Sampling frequency will be consistent with requirements of CCR rule [40 C.F.R. §257.94(b) and 40 C.F.R. §257.95(d)(1)].

The sampling and analysis program as outlined below includes procedures and techniques for: (i) sample collection; (ii) sample preservation and shipment; (iii) quality assurance and quality control; (iv) chain of custody control; and (v) laboratory analytical methods.

4.1 <u>Groundwater Sampling Procedures</u>

In compliance with 40 C.F.R. §257.93(c) groundwater levels will be measured in each monitoring well immediately prior to purging, each time groundwater is sampled. Groundwater levels will be measured to the nearest 0.01 feet using an electrical water level indicator and used to calculate rate and direction of groundwater flow each time groundwater is sampled. A potentiometric surface map for the uppermost aquifer will be generated using the measured water levels, except during establishing the background conditions. The potentiometric surface maps will allow for a quantitative assessment of groundwater flow rate and direction.

Groundwater sampling from monitoring wells will be performed in accordance with the USEPA Laboratory Services & Applied Science Division (LSASD, Athens, Georgia) Operating Procedure (LSASDPROC-301-R6) (USEPA, 2023). Groundwater samples will be collected using a low-flow sampling method. Peristaltic pump tubing or



submersible pump will be placed in the approximate mid-portion of the screened interval of the well. To ensure that the samples collected are representative of the groundwater in the aquifer, field parameters will be measured during purging. Temperature, pH, conductivity, oxidation-reduction potential (ORP), dissolved oxygen (DO), and turbidity will be measured using a Horiba U-53 water quality meter or equivalent and a HACH 2100P or equivalent turbidity meter. Measurements will be taken within an enclosed flow-through cell to minimize effects of contact with air. The well is considered stabilized and ready for sample collection when the indicator parameters have stabilized for three consecutive readings at a minimum:

- ± 0.1 for pH
- $\pm 5\%$ for specific conductance
- $\pm 10\%$ or ± 0.2 mg/L (whichever is greater) for DO where DO>0.5mg/L
- <10 NTU for turbidity
- Temperature Record only, not used for stabilization criteria
- ORP ± 20 mV.

The groundwater samples will be collected in laboratory provided containers. Following sampling, the bottles will be sealed, labeled, packed in ice, and shipped under chain-of-custody (COC) protocol to a certified laboratory. The chain-of-custody procedures will be conducted in accordance with the USEPA's Laboratory Services and Applied Science Division Operating Procedure for Sample and Evidence Management LSASDPROC-005-R4 dated 3 November 2021 (USEPA, 2021).

The COC record will contain the following information:

- Sample identification numbers;
- Signature of sample collector;
- Date and time of collection;
- Sample type;
- Sample point identification;

- Number of sample containers;
- Signature of person(s) involved in the chain of possession;
- Dates and times of possession by each individual; and
- Notated date(s) and time(s) of sample transfer between individuals.

The samples will remain in the custody of assigned personnel, an assigned agent, or the laboratory. If the samples are transferred to other employees for delivery or transport, the sampler or possessor will relinquish possession and the samples must be received by the new owner. If the samples are being shipped, a hard copy COC will be signed and enclosed within the shipping container. Samplers will use COC forms provided by the analytical laboratory or use a COC form similarly formatted and containing the information listed above.

4.2 Field and Laboratory Quality Assurance/ Quality Control

During the past monitoring events from the ash pond and secondary ash areas, one field duplicate sample has been collected during each monitoring event. This practice was consistent with the Sampling and Analysis Plan approved for the ash pond. The field duplicate samples were shipped to the laboratory for analysis for quality assurance and quality control. The field duplicate samples were collected by filling additional containers at the same location, and the field duplicates were assigned a unique sample identification number.

For future groundwater monitoring events, field duplicates, field blanks, and equipment blanks will be collected and shipped to the laboratory for analysis.

Daily calibration of field instruments will be conducted and documented as follows:

- calibration of field instruments will occur daily and follow the recommended (specific) instrument calibration procedures provided by the manufacturer and/or equipment manual specific to each instrument.
- daily calibration will be documented on field forms and these field forms will be included in groundwater monitoring reports.

- instruments will be recalibrated as necessary (e.g. when calibration checks indicate significant variability), and any recalibration steps will be documented on field calibration forms.
- calibration of the instruments will also be checked if any readings during sampling activities are suspected.
- replacement probes and meters will be obtained as a corrective action if recalibration does not improve instrument function. Calibration field forms will be provided as part of each groundwater report's quality control documentation.

All non-disposable and non-dedicated tools which contact sample media will be decontaminated prior to the collection of each sample. Decontamination solutions will be kept in labeled plastic containers. Disposable nitrile gloves will be worn during all decontamination procedures. Because new tubing and external pump (Geopump or similar) will be used at the landfill, the water level indicator and the field water quality meter are the only pieces of equipment that will require decontamination.

The water level indicator will be decontaminated in accordance with LSASDPROC-205-R4 dated 22 June 2020 (USEPA, 2020), which includes the following procedure:

- 1. Wash with Liquinox[®] detergent and tap water.
- 2. Rinse with tap water.
- 3. Rinse with deionized or distilled water.

The probe portions of the field water quality meter for pH, conductivity, dissolved oxygen, turbidity, and temperature will be decontaminated by rinsing with deionized or distilled water.

During each groundwater monitoring event, field sampling conditions including well signage, well access, sampling and purging equipment condition, and any site conditions that may affect sampling will be noted and maintained in field logbooks.

4.3 <u>Laboratory Analysis</u>

In compliance with 40 C.F.R. §257.93(b), the groundwater samples will be analyzed for constituents listed in Appendices III and IV of Part §257 of the CCR rule (referred herein as Appendix III and Appendix IV constituents). For detection monitoring, these

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constituents include boron, calcium, chloride, fluoride, pH, sulfate, and total dissolved solids from Appendix III Part §257 (Table III-2); and for assessment monitoring these constituents include antimony, arsenic, barium, beryllium, cadmium, chromium, cobalt, fluoride, lead, lithium, mercury, molybdenum, selenium, thallium, and radium 226 & 228 combined from Appendix IV Part §257 (Table III-3). All constituents will be analyzed as total recoverable, where samples are not field filtered. Table 4-1 presents the list of Appendix III and Appendix IV constituents and the laboratory analytical methods. The groundwater samples will be analyzed using methods specified in EPA Manual SW-846, EPA 600/4-79-020, Standard Methods for the Examination of Water and Wastewater (SM18-20), EPA Methods for the Chemical Analysis of Water and Wastes (MCAWW), ASTM, or other suitable analytical methods approved by GA EPD. The method used will be able to reach a suitable practical quantification limit to detect natural background conditions at the facility. The groundwater samples will be analyzed by licensed and accredited laboratories through the National Environmental Laboratory Accreditation Conference (NELAC). Field instruments used to measure pH must be accurate and reproducible to within 0.1 Standard Units (S.U.).

5. STATISTICAL ANALYSIS DURING DETECTION MONITORING

Groundwater quality data from each sampling event will be statistically evaluated to determine if there has been a statistically significant change in groundwater chemistry. Historical background data will be used to determine statistical limits.

Groundwater sampling frequency during the detection monitoring shall be at least semiannual [40 C.F.R. §257.95(b)] except when there is no adequate groundwater flow to sample wells semi-annually. The alternative frequency shall be no less than annual [40 C.F.R. 257.94(d)].

According to 40 C.F.R. \$257.93(f), the owner or operator of the CCR unit must select one of the statistical methods specified in paragraphs (f)(1) through (5) of this section to be used in evaluating groundwater monitoring data for each specified constituent. The statistical test chosen shall be conducted separately for each constituent in each monitoring well. CCPC will use the following statistical methods to analyze groundwater data collected during the detection monitoring.

5.1 <u>Physical Independence</u>

Most statistical analyses require separate sampling events to be statistically independent. Statistical independence of groundwater samples is most likely to be realized when the samples are collected at time intervals that are sufficiently far apart that the samples are not from the same volume of groundwater. In such cases, the samples of groundwater are considered physically independent. To ensure physical independence, the minimum time between sampling events must be longer than the residence time of groundwater that would be collected in the monitoring well. The minimum time interval between sampling events (t_{min}) can be determined by calculating the groundwater velocity, as follows:

$$v = \frac{\text{Ki}}{n_e}$$

 $t_{min} = \frac{\text{D}}{\text{v}}$

where:

v = groundwater velocity;



K = hydraulic conductivity;

i = hydraulic gradient

 $n_{\rm e}$ = effective porosity;

 t_{\min} = minimum time interval between sampling events;

D = well bore volume (i.e., diameter of well and surrounding filter pack)

5.2 <u>Testing for Outliers</u>

Outliers are extreme data points that may represent an anomaly or error. Data sets will be visually inspected for outliers using a time-series plot or statistical methods such as USEPA 1989 Outlier Screening method or Tukey's Outlier Screening method. Potential outliers will be evaluated for potential sources of error or evidence that the data point is not representative. Errors will be corrected prior to further statistical analysis. Nonrepresentative data points may be excluded from the statistical analysis based on professional judgment. A discussion will be added in the groundwater report as to how the outlier was identified and why it was excluded.

5.3 <u>Testing for Normality</u>

Data will be tested for normal distribution using the Shapiro-Wilk test (for sample size up to 50) or the Shapiro-Francia test (for sample sizes greater than 50). If the data appear not to be normally distributed, then data may be transformed mathematically (e.g., log, natural log, square root, cube root) such that the transformed data follow a normal distribution (the data will be transformed because many statistical analyses assumes that the sample data are normally distributed). Alternatively, a non-parametric test (i.e., a test that does not assume a particular data distribution) may be used.

5.4 Establishing Background

Between eight and ten independent background samples will be collected in accordance with the recommendations of the Unified Guidance. The samples will be analyzed for Appendix III and IV constituents from background wells MW-U1 and MW-U2, and each downgradient monitoring well for the ash pond and secondary ash areas as part of the initial monitoring period [40 C.F.R. §257.94(b)]. Background samples from the ash pond monitoring wells were collected in 2017. For the monitoring wells at the secondary ash

areas, CCPC already collected six background sampling events between July 2022 and April 2023 and will complete the eight background sampling events in 2023. Initially, background data will be evaluated for statistically significant temporal trends using the Theil-Sen slope estimator with Mann-Kendall trend test ($\alpha = 0.05$). The trend test will be used to estimate the rate of change (increasing, no change, or decreasing) over time for each constituent. Statistically significant increases in background data (or decreasing trend in pH) could be attributed to a release from the CCR unit or another source, and further investigation may be needed.

When a trend test shows no statistically significant trend in background data, the data will be tested for normality using the methods outlined in Section 5.3. In compliance with 40 C.F.R. §257.93 (g)(1), when the data follows a normal or transformed normal distribution, parametric methods will be used. When the data do not follow a normal or transformed normal distribution, or when more than 50% of the data are non-detect, non-parametric methods may be used.

5.5 Evaluating Statistically Significant Increases (SSIs)

Statistical analysis of groundwater data during the detection monitoring will be performed in compliance with the USEPA Unified Guidance (USEPA, 2009). The USEPA CCR Rule specifically lists four methods acceptable for statistical analysis: analysis of variance (ANOVA), tolerance intervals, prediction intervals, and control charts [40 C.F.R.§257.93(f)]. Of these methods, the Unified Guidance recommends prediction limits combined with retesting for maintaining a low site wide false positive rate (SWFPR) while providing high statistical power. ANOVA is not recommended as the USEPA CCR Rule mandates a minimum type I error (α) of 0.05, at which it would be difficult to maintain an annual SWFPR less than 10% (Unified Guidance). Control charts are acceptable as long as parametric methods can be used since there is no nonparametric counterpart to the control chart.

Prediction interval and control charts can be used for interwell comparison (data from pooled background monitoring wells used for background data set). Interwell comparison will be used when there are no statistically significant trends in the background data. An interwell statistical method will be used to compare Appendix III groundwater monitoring data to background conditions. For prediction interval, background data are used to construct a concentration prediction limit (PL), which is then compared to one or more observations from the downgradient well. The acceptable range of concentrations includes all values that are lower than the prediction limit. The

prediction interval will have the form [0, PL], with the upper limit PL as the comparison of importance.

If a sample does not exceed the calculated PL (or control limit), then it can be concluded that an SSI has not occurred. If the initial sample exceeds the PL (or control limit), then a resample will be collected and analyzed prior to the next regularly scheduled sampling event. If both the initial result and the subsequent resample exceed the PL (or control limit), then an SSI can be concluded.

If the statistical evaluation indicates an SSI for one or more Appendix III constituents, the data will be evaluated to assess whether the SSI is caused by a release from the CCR unit. If the evaluation demonstrates that the SSI is caused by natural variability, sampling, analysis or statistical error, or a release from another source, the demonstration will be made in writing and certified by a qualified professional engineer within 90 days of detecting an SSI [40 C.F.R. §257.94(3)(2)]. If a successful demonstration is not completed within the 90-day period, CCPC will initiate an assessment monitoring program as required under 40 C.F.R. §257.95.

5.5.1. Handling Non-Detects in Background Data

If non-detect data are infrequent (less than 15%), half of the reporting limit (RL) can be used in place of these data without significantly altering the results of a statistical test. When at least half of the data are non-detect, non-parametric prediction intervals with retesting will be used. If all of the background data are non-detect, then the Double Quantification Rule¹ will be used. According to this rule, if a sample and verification resample from the downgradient wells both exceed the practical quantitation limit (PQL) at a particular monitoring point, then a confirmed exceedance is registered (i.e., an SSI can be concluded). Where available, estimated results less than the RL (i.e., "J-flagged" data) will be used, and these data will be considered detections for the purposes of statistical analysis.

¹ Double Quantification Rule is appropriate for detection monitoring because analytical results from the downgradient wells are compared with background concentrations.

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6. STATISTICAL ANALYSIS DURING ASSESSMENT MONITORING

In compliance with 40 C.F.R. §257.95(a), assessment monitoring is required when an SSI is identified over background levels for one or more of the constituents listed in Appendix III. Within 90 days of triggering an assessment monitoring program and annually thereafter, the monitoring wells must be sampled and analyzed for Appendix IV constituents [40 C.F.R. §257.95(b)]. Within 90 days of obtaining the results from this sampling event and on at least on a semi-annual basis thereafter, all monitoring wells must be sampled for all parameters in Appendix III and for those constituents in appendix IV that were detected during the initial assessment monitoring event [40 C.F.R. §257.95(d)(1)].

Statistical analysis of groundwater data during the assessment monitoring will be performed in compliance with the Unified Guidance (USEPA, 2009). Groundwater protection standards (GWPSs) must be established for each constituent in Appendix IV detected in groundwater [40 C.F.R. §257.95(h)], which was adopted into the GA EPD Rules for Solid Waste Management 391-3-4-.10 on February 22, 2022. The GWPS shall be:

- (1) the maximum contaminant level (MCL) established under 40 C.F.R. §141.62 and §141.66.
- (2) where an MCL has not been established:
 - (i) Cobalt 0.006 mg/L;
 - (ii) Lead 0.015 mg/L;
 - (iii) Lithium 0.040 mg/L; and
 - (iv) Molybdenum 0.100 mg/L.
- (3) the upper tolerance limit (UTL) computed from background well data for constituents where the UTL is higher than the MCL or rule-specified GWPS.

If a constituent is not detected in background groundwater, then the Double Quantification Rule can be used, in which case the UTL is the most recent reporting limit or PQL, and two consecutive downgradient concentrations higher than the GWPS will constitute a statistically significant level.

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After the GWPS is established, the data will be evaluated to determine whether they are statistically significantly higher than the GWPS. To compare the new data with the fixed standard of the GWPS, the Unified Guidance recommends using confidence intervals around the mean or median². Confidence intervals around the mean will be used when the data follows a normal or transformed normal distribution. Confidence interval around the median will be used when data distributions are non-normal. When at least 50% of the recent data set is non-detect, a parametric confidence interval will not be used. Instead, non-parametric prediction or tolerance intervals will be used. In these cases, the upper prediction limit or upper tolerance limit is set either the highest or second highest concentration measured in the background dataset.

² Confidence interval is recommended in the Unified Guidance during compliance/assessment and corrective action monitoring. A confidence interval is derived for a constituent from the compliance well data and compared with Groundwater Protection Standard (GWPS). According to the Unified Guidance, if the entire confidence interval (i.e., both the lower and upper confidence limits) lies below the fixed GWPS in either a compliance/assessment or corrective action setting, there is statistically significant evidence that the true concentration from the well (e.g., the mean or the median) is less than the GWPS and the constituent concentrations at the well are considered to be in compliance. Conversely, if the confidence interval lies entirely above the GWPS, the evidence suggests that the true concentration exceeds the standard, and that concentrations at the well are out of compliance. Because confidence intervals explicitly account for variation and uncertainty in the sample data used to construct them, the use of a double quantification rule and verification resampling is not needed to identify statistically significant levels (SSLs).



7. **REPORTING**

CCPC will submit annual groundwater monitoring reports in accordance with 40 C.F.R. §257.90(e) and semi-annual groundwater reports in accordance with 391-3-4-.10(6)(c). The annual and semiannual groundwater monitoring reports will be submitted to EPD within 90 days after sampling and analysis in accordance with the Georgia Comprehensive Rules and Regulations Rule 391-3-4.10. The report will include the following items:

- certification by a qualified groundwater scientist;
- summary of the site's history and monitoring system status;
- brief discussion of the geology/hydrogeology of the site;
- groundwater monitoring compliance status;
- documentation of dry or non-functioning wells;
- identification of any groundwater wells that were installed or decommissioned during the preceding year, along with a narrative description of why these actions were taken.
- overview of purging and sampling protocols;
- comparison to established standards;
- discussion of results;
- water table measurements;
- NELAC certification;
- analytical data;
- chain-of-custody documentation;
- statistical analysis;
- recommendations for future monitoring;

- up to date well inspection by a qualified groundwater scientist (at least once every five years);
- trend charts (if applicable);
- plume map (if applicable); and
- updated potable water well survey (if applicable);
- copies of well-purging logs;
- copies of the original daily field instrument calibration sheets, indicator parameter and parameter stabilization;
- potentiometric surface contour map for the aquifer(s) being monitored, signed, and sealed by a Georgia-registered P.G. or P.E.;
- groundwater flow rate and direction calculations;
- semi-annual assessment monitoring results (if applicable);
- field logs and forms will be kept for each sampling event, and will include the following, but not be limited to, well signage, well access, sampling and purging equipment condition, and any site conditions that may affect sampling;
- a narrative discussion of any transition between monitoring programs (e.g., the date and circumstances for transitioning from detection monitoring to assessment monitoring in addition to identifying the constituent(s) detected at a statistically significant increase over background levels);
- table of current analytical results for each well, highlighting statistically significant increases and concentrations above the background for Appendix III constituents or above groundwater protection standards for Appendix IV constituents, as applicable; and
- if an alternate source demonstration has been completed during the previous monitoring period, it will be included in the semi-annual groundwater report.

8. **REFERENCES**

- GA EPD (1991). Manual for Groundwater Monitoring. Department of Natural Resources, Georgia Environmental Protection Division, September 1991.
- Rules and Regulations of the State of Georgia (2016). Solid Waste Management Rule 391-3-4-.10. Revised March 8, 2018.
- USEPA (2009). Statistical Analysis of Groundwater Data at RCRA Facilities: Unified Guidance. EPA 503/R-09-007.
- USEPA (2021). Laboratory Services and Applied Science Division (LSASD, Athens, Georgia) Sample and Evidence Management (LSASDPROC-005-R4).
- USEPA (2015a). Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule (40 C.F.R. Part §257).
- USEPA (2023). Laboratory Services & Applied Science Division (LSASD, Athens, Georgia) Operating Procedure, Groundwater Sampling (SESDPROC-301-R4).
- USEPA (2020). Laboratory Services and Applied Science Division (LSASD, Athens, Georgia) Operating Procedure, Field Equipment Cleaning and Decontamination (LSASDPROC-301-R6).

TABLES

Table 3-1. Monitoring Well Construction Details Crisp County Power Commission Plant Crisp Ash Pond and Secondary Ash Areas

Well ID	Installation Date	Well Location	Northing ⁽¹⁾	Easting ⁽¹⁾	Ground Surface Elevation ⁽²⁾ (ft)	Top of Casing Elevation ⁽²⁾ (ft)	Total Well Depth Below Ground Surface (ft)	Screen Depth Interval Below Ground Surface (ft)	Screen Interval Elevation ⁽²⁾ (ft)	Screen Interval Lithologic Information
MW-D1	2/22/2017	Downgradient	670708.47	2365315.12	238.10	241.77	19.50	9.25-19.25	228.85-218.85	Alluvium and Residual Soil
MW-D2	2/21/2017	Downgradient	671291.61	2365308.73	229.14	232.66	19.75	9.50-19.50	219.64-209.64	Alluvium and Residual Soil
MW-D3	2/22/2017	Downgradient	671291.07	2365715.53	229.77	233.77	19.50	9.25-19.25	220.52-210.52	Alluvium and Residual Soil
MW-D4	5/12/2022	Downgradient	669875.01	2365444.95	244.22	246.51	27.25	17.00-27.00	227.22-217.22	Residual Soil
MW-D5	5/16/2022	Downgradient	670216.49	2365178.72	238.31	241.16	33.00	22.75-32.75	215.56-205.56	Residual Soil
MW-D6	5/13/2022	Downgradient	670393.04	2365406.13	249.85	252.63	34.25	24.00-34.00	225.85-215.85	Residual Soil
MW-D7	5/13/2022	Downgradient	671054.07	2365037.89	227.21	230.18	24.40	14.15-24.15	213.06-203.06	Residual Soil
MW-D8	5/13/2022	Downgradient	671186.85	2364861.25	223.90	226.76	25.00	14.75-24.75	209.15-199.15	Residual Soil
MW-D9	5/14/2022	Downgradient	671482.27	2364959.09	218.99	221.42	24.80	14.55-24.55	204.44-194.44	Residual Soil
MW-U1	2/23/2017	Upgradient	669996.79	2366420.55	246.28	249.52	33.75	23.50-33.50	222.78-212.78	Alluvium and Residual Soil
MW-U2	5/12/2022	Upgradient	669748.63	2366247.88	245.69	248.79	27.75	17.50-27.50	228.19-218.19	Residual Soil

<u>Notes:</u> ft = feet

NAVD = North American Vertical Datum.

The easting, northing, and TOC elevations were obtained from a revised survey performed by J.B. Faircloth & Associates, P.C. on 19 November 2019 and 2 May 2022.

⁽¹⁾ :The easting and northing coordinates in North American Datum (NAD) 1983, State Plane, Georgia-West, feet.

⁽²⁾: Elevations referenced to the North American Vertical Datum of 1988 (NAVD88).

Table 3-2. Summary of Groundwater Elevations, Hydraulic Gradients, and Flow Velocities Crisp County Power Commission Plant Crisp Ash Pond and Secondary Ash Areas

	T (0)		Groundwater Monitoring Date														
Well ID	Top of Casing Elevation (ft	5/26/2022		6/8/2022		7/8/2022		10/19/2022		12/5/2022		1/18/2023		3/1/2023		4/26/2023	
wen iD	MSL)	Depth to	Groundwater														
	MSL)	Groundwater (ft)	Elevation ⁽¹⁾ (ft)														
MW-U1	249.52	12.53	236.99	13.11	236.41	14.59	234.93	14.62	234.90	15.61	233.91	13.08	236.44	9.25	240.27	12.1	237.42
MW-U2	248.79	12.18	236.61	12.48	236.31	14.03	234.76	14.24	234.55	14.94	233.85	12.48	236.31	8.57	240.22	11.24	237.55
MW-D1	241.77	15.57	226.20	15.98	225.79	16.35	225.42	16.34	225.43	15.9	225.87	15.28	226.49	14.29	227.48	15.75	226.02
MW-D2	232.66	13.60	219.06	14.60	218.06	15.66	217.00	15.77	216.89	14.33	218.33	13.82	218.84	13.04	219.62	12.63	220.03
MW-D3	233.78	7.83	225.95	8.44	225.34	8.99	224.79	9.45	224.33	8.63	225.15	7.85	225.93	7.49	226.29	7.83	225.95
MW-D4	246.51	11.43	235.08	12.05	234.46	13.00	233.51	13.46	233.05	13.70	232.81	12.04	234.47	9.39	237.12	11.00	235.51
MW-D5	241.16	8.27	232.89	8.64	232.52	9.94	231.22	10.41	230.75	10.48	230.68	9.22	231.94	7.51	233.65	8.90	232.26
MW-D6	252.63	22.47	230.16	22.96	229.67	23.85	228.78	24.03	228.60	23.83	228.80	22.19	230.44	20.65	231.98	22.5	230.13
MW-D7	230.18	7.92	222.26	8.57	221.61	9.22	220.96	9.29	220.89	8.66	221.52	7.85	222.33	6.79	223.39	6.64	223.54
MW-D8	226.76	7.94	218.82	8.61	218.15	9.34	217.42	9.14	217.62	8.08	218.68	7.43	219.33	6.87	219.89	6.52	220.24
MW-D9	221.42	6.98	214.44	8.67	212.75	10.63	210.79	10.49	210.93	8.04	213.38	5.99	215.43	6.04	215.38	6.95	214.47
	e Blackshear Julic Gradient		236.91		237.00		236.99		236.99		233.25		237.01		236.95		236.95
	MW-U1 and MW-	- 0.011		0.011		0.012		0.012		0.010		0.010		0.012		0.011	
	0.01 and 0.000																
1	09 (IL/ IL)																
Flow Velo	city Between MW-	Residual Soil	3	4	1	4	4		4	3	3	3	5	4	1	5	3
U1 and M	/W-D9 (ft/vear)	Alluvium and		avium and		9		9		7		0		9		0	
	(,),,	Residual Soil	8		9		9		9	/		5)		9		, ,
	ulic Gradient																
	MW-D4 and MW-	0.0	12	0.013		0.013		0.013		0.011		0.011		0.013		0.012	
I	09 (ft/ft)																
Flow Velo	city Between MW-	Residual Soil	idual Soil 4 4		4		4		4		3		4		4		
	/IW-D9 (ft/year)	Alluvium and	9	10		10		10		9		8		10		9	
		Residual Soil	esidual Soil		0	10			10		, 		,	1	0	9	
	ulic Gradient																
	Lake Blackshear	0.0	12	0.0)13	0.0	013	0.0	014	0.0	09	0.0	12	0.0)12	0.0	12
and M	1W-D3 (ft/ft)																
	city Between Lake	Residual Soil	4	4	1	4	4		4	3	3	4	<u>l</u>	4	1	4	Ł
	ear and MW-D3 ft/year)	Alluvium and	9	1	0	1	0	1	10	7	7	ç)	ç)	ç)
	it, year)	Residual Soil															

<u>Notes:</u> ft = feet

⁽¹⁾: Elevations referenced to the North American Vertical Datum of 1988 (NAVD88).

ft/ft = feet per foot

--: The depth to water measurement was not repretative of the static water level.
 --: The depth to water measurement was not repretative of the static water level.
 Horizontal distance between MW-U1 and MW-D9 is 2075 ft. Distance between MW-D4 and MW-D9 is 1690 ft, distance between Lake Blackshear and MW-D3 is 905 ft.
 Groundwater flow velocity was calculated using average horizontal hydraulic conductivity for residual soil of 0.17 ft/day and the average horizontal hydraulic conductivity for alluvium and residual soil of 0.41 ft/day.

Table 4-1. Monitored Constituents and Laboratory Analytical MethodsCrisp County Power CommissionPlant Crisp Ash Pond and Secondary Ash Areas

Appendix III to 40 CFR §257 - Constituents for Detection Monitoring						
Analyte	Laboratory Analytical Method					
Boron	EPA Method 6020					
Calcium	EPA Method 6020					
Chloride	USEPA method number 300.0/300.1/9250/9251/9253/9056A					
Fluoride	USEPA method number 300.0/300.1/9214/9056A					
pH	USEPA method number 150.1 field					
Sulfate	USEPA method number 9035/9036/9038/300.0/300.1/9056A					
Total Dissolved Solids (TDS)	EPA Method SM 2540C					
Appendix IV to 40 CF	R §257 - Constituents for Assessment Monitoring					
Analyte	Laboratory Analytical Method					
Antimony	EPA Method 6020					
Arsenic	EPA Method 6020					
Barium	EPA Method 6020					
Berylium	EPA Method 6020					
Cadmium	EPA Method 6020					
Chromium	EPA Method 6020					
Cobalt	EPA Method 6020					
Fluoride	USEPA method number 300.0/300.1/9214/9056A					
Lead	EPA Method 6020					
Lithium	EPA Method 6020					
Mercury	EPA Method 7470A					
Molybdenum	EPA Method 6020					
Selenium	EPA Method 6020					
Thallium	EPA Method 6020					
Radium 226 and 228 Combined	EPA Method 9315 & 9320					

FIGURES



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consultants

KENNESAW, GA

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PROJECT NO.

FILE NO.

FIGURE NO.

DOCUMENT NO.

GW8836

GA230223

2-1

SITE LOCA AYOUT.MXD

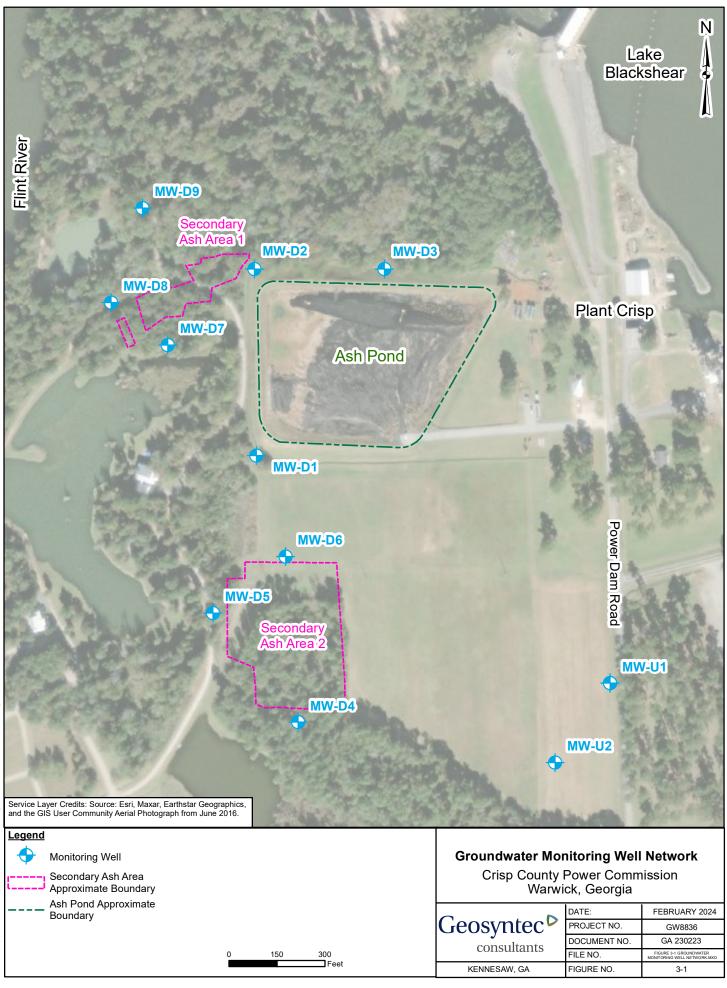
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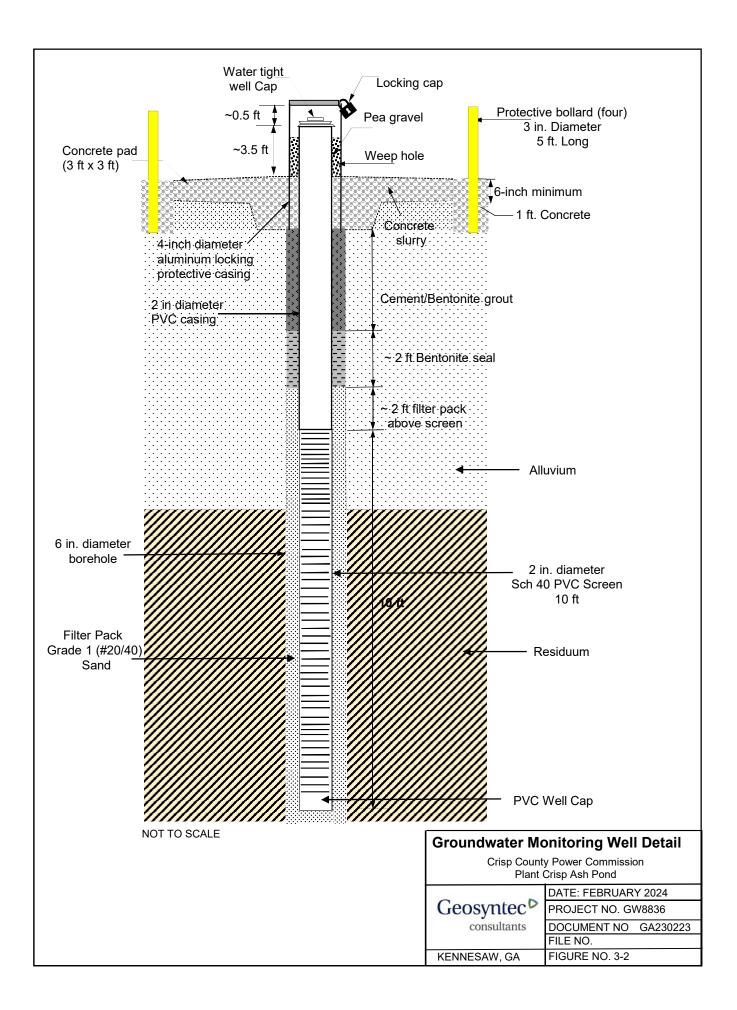
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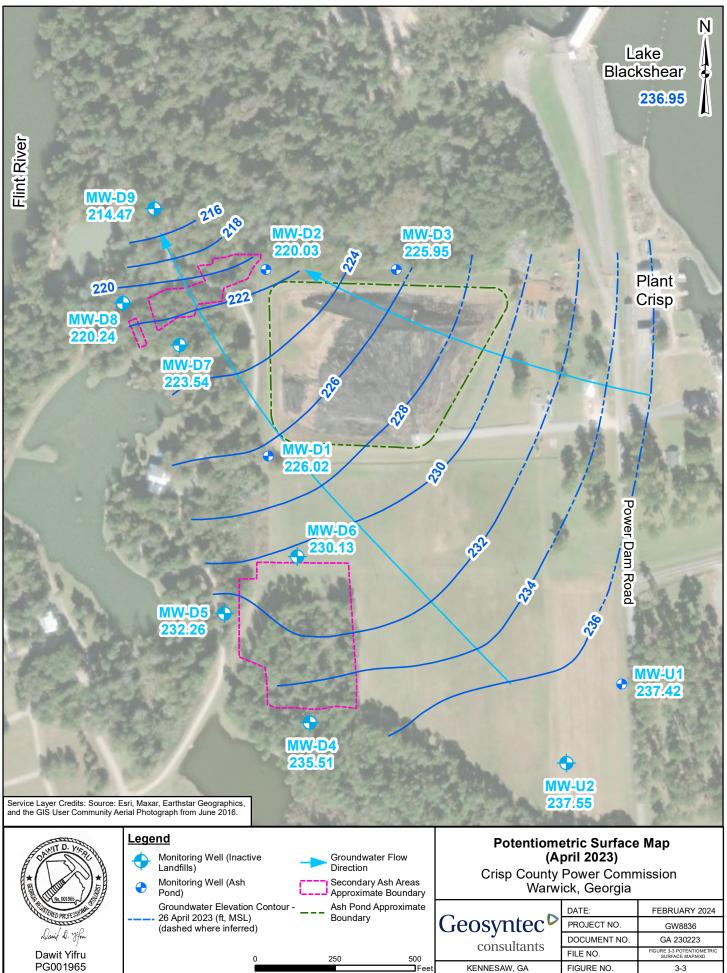
250

Note: Parcel map obtained from Worth County, Georgia Board of Tax Assessors.

500

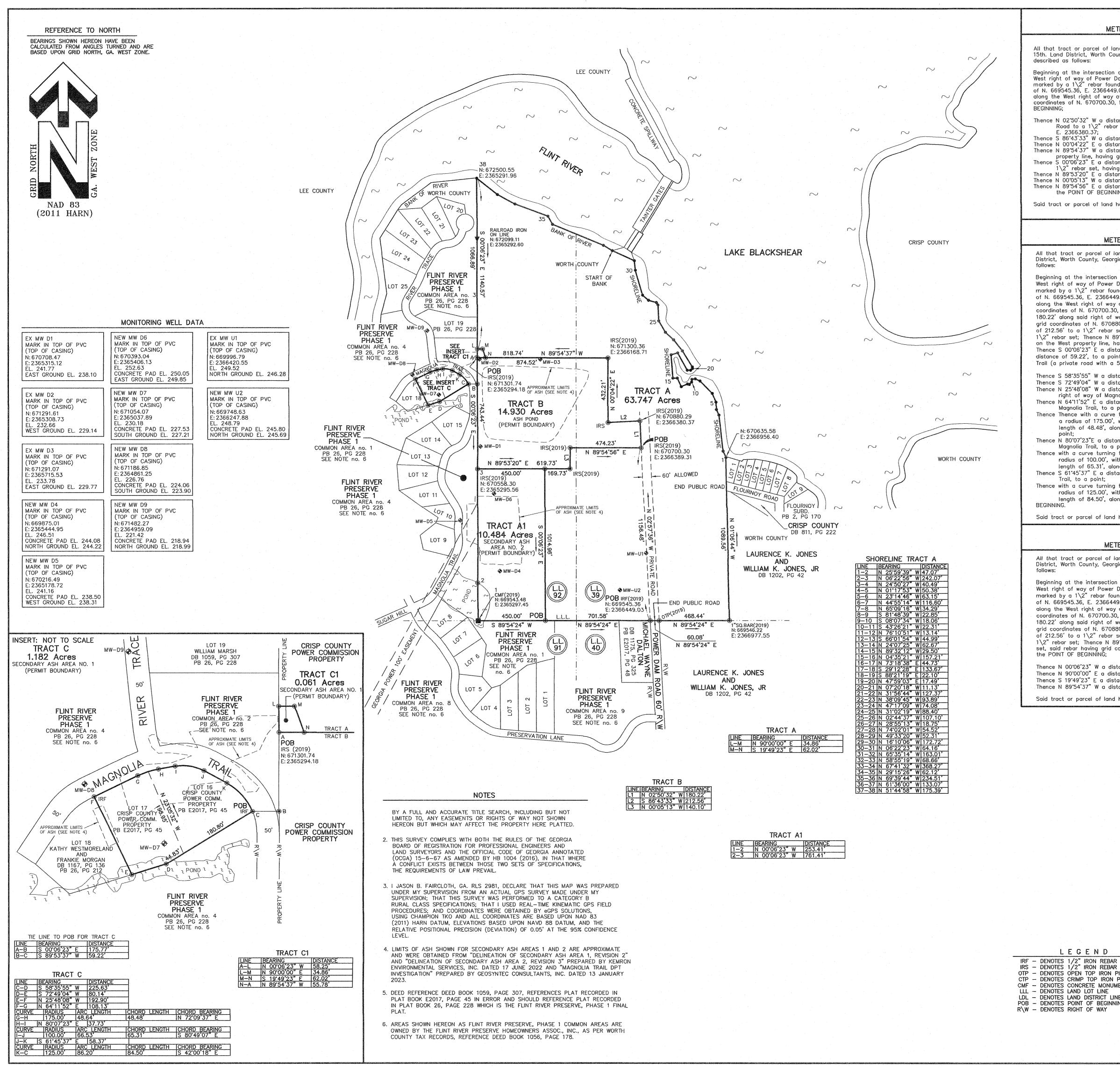






APPENDIX A

Land Surveyor's Certification Drawing



(ASH POND) METES AND BOUNDS DESCRIPTION	TRACT A METES AND BOUNDS DESCRIPTION
rcel of land lying in or being in Land Lots 39 and 92 Worth County, Georgia, and being more particularly	All that tract or parcel of land lying in or being in Land Lots 39 and 92, 15th. Land District, Worth County, Georgia, and being more particularly described as follows:
ersection of the South line Land Lot 39 and the f Power Dam Road (60' R\W), said intersection being ebar found and having Grid North, Ga. West Zone coordinates 2366449.03; Thence N 02'57'36" W s distance of 1156.48' of way of a Private Road, to a 1\2" rebar set, having grid 70700.30, E. 2366389.31, said rebar being the POINT OF	 Beginning at the intersection of the South line of Land Lot 39 and the West right of way of Power Dam Road (60' R\W), said intersection being marked by a 1\2" rebar found and having Grid North Ga. West Zone coordinates of N. 669545.36, E. 2366449.03, and being the POINT OF BEGINNING; Thence N 89'54'24" E a distance of 60.08' along said Land Lot Line to a 1\2" open top pipe, located on the East right of way of Power
W a distance of 180.22' along said right of way of said Private 2" rebar set, having grid coordinates of N. 670880.29,	Dam Road; Thence N 89'54'24" E a distance of 468.44' along said Land Lot Line to a 1" Square Bar, having grid coordinates of N. 669546.22, E. 2366977.55;
37; W a distance of 212.56' to a 1\2" rebar set; E a distance of 432.21' to a 1\2" rebar set; W a distance of 874.52' to a 1\2" rebar set on the West , having grid coordinates of N. 671301.74, E. 2365294.18; E a distance of 743.44' along said West property line to a set, having grid coordinates of N. 670558.30, E. 2365295.56; E a distance of 619.73' to a 1\2" rebar set; W a distance of 140.10' to a 1\2" rebar set; E a distance of 474.23' to a 1\2" rebar set; E a distance of 474.23' to a 1\2" rebar set; B E GINNING. of land having an area of 14.930 Acres.	 Thence N 01'06'44" W a distance of 1089.56' to a point located on the Westerly shoreline of Lake Blackshear, having grid coordinates of N. 670635.58, E. 2366956.40; Thence N 25'59'39" W a distance of 47.07' along said shoreline to a point; Thence N 06'22'56" W a distance of 242.07' along said shoreline to a point; Thence N 06'22'56" W a distance of 40.49' along said shoreline to a point; Thence N 01'17'53" W a distance of 50.38' along said shoreline to a point; Thence N 01'17'53" W a distance of 63.15' along said shoreline to a point; Thence N 23'14'46" W a distance of 116.60' along said shoreline to a point; Thence N 44'55'14" W a distance of 34.29' along said shoreline to a point; Thence S 81'48'39" W a distance of 22.85' along said shoreline to a point; Thence S 08'07'34" W a distance of 22.31' along said shoreline to a point; Thence S 43'26'21" W a distance of 13.14' along said shoreline to a point; Thence S 66'01'54" W a distance of 44.99' along said shoreline to a point;
TRACT C (SECONDARY ASH AREA NO. 1) METES AND BOUNDS DESCRIPTION	Thence N 24'07'25" W a distance of 62.67' along said shoreline to a point; Thence N 89'32'12" W a distance of 29.50' along said shoreline to a point; Thence N 04'35'21' W a distance of 157.21' along said shoreline to a point; Thence N 73'18'38" E a distance of 44.73' along said shoreline to a point;
arcel of land Iting in or being in Land Lot 92, 15th. Land Ity, Georgia, and being more particularly described as	Thence S 29'12'28" E a distance of 133.67' along said shoreline to a point; Thence S 88'21'19" E a distance of 22.10' along said shoreline to a point; Thence N 47'59'03" E a distance of 17.49' along said shoreline to a point; Thence N 07'20'18" W a distance of 11.13' along said shoreline to a point;
tersection of the South line Land Lot 39 and the of Power Dam Road (60' R\W), said intersection being rebar found and having Grid North, Ga. West Zone coordinates . 2366449.03; Thence N 02'57'36" W s distance of 1156.48' tt of way of a Private Road, to a 1\2" rebar set, having grid 70700.30, E. 2366389.31; Thence N 02'50'32" W a distance of right of way of said Private Road to a 1\2" rebar set, having N. 670880.29, E. 2366380.37; Thence S 86'43'33" W a distance 2" rebar set; Thence N 00'04'22" E a distance of 432.21' to a ance N 89'54'37" W a distance of 874.52' to a 1\2" rebar set ty line, having grid coordinates of N. 671301.74, E. 2365294.18; E a distance of 175.77', to a point; Thence S 89'53'37" W a to a point located on the Westerly right of way of Magnolia d with a 50' R\W), said point being the POINT OF BEGINNING; W a distance of 80.14', to a point; W a distance of 192.90', to a point; W a distance of 108.13', along said right of way of said all, to a point; a curve turning to the right with an arc length of 48.64', with 175.00', with a chord bearing of N 72'09'37" E, with a chord 8.48', along said right of way of said all, to a point; e turning to the right with an arc length of 66.53', with a 20.000', with a chord bearing of S 80'49'07" E, with a chord 5.31', along said right of way of Magnolia fill, to a point; e turning to the right with an arc length of 66.53', with a 20.000', with a chord bearing of S 80'49'07" E, with a chord 5.31', along said right of way of Magnolia Trial, to a point; E a distance of 58.37', along said right of way of Magnolia point; e turning to the right with an arc length of 86.20', with a 25.00', with a chord bearing of S 42'00'18" E, with a chord 4.50', along said right of way of Magnolia Trial, to POINT OF	 Thence N 31'56'44" W a distance of 127.37' along said shoreline to a point; Thence N 38'09'45" W a distance of 93.89' along said shoreline to a point; Thence N 47'17'09" W a distance of 74.08' along said shoreline to a point; Thence N 02'44'37" W a distance of 107.10' along said shoreline to a point; Thence N 02'44'37" W a distance of 107.10' along said shoreline to a point; Thence N 02'44'37" W a distance of 107.10' along said shoreline to a point; Thence N 02'44'37" W a distance of 12.72' along said shoreline to a point; Thence N 49'33'20" W a distance of 54.52' along said shoreline to a point; Thence N 16'10'06" W a distance of 52.31' along said shoreline to a point; Thence N 16'10'06" W a distance of 163.01' along said shoreline to a point; Thence N 16'22'23" W a distance of 163.01' along said shoreline to a point; Thence N 65'35'14" W a distance of 68.66' along said bank to a point; Thence N 65'35'14" W a distance of 234.51' along said bank to a point; Thence N 67'41'32" W a distance of 234.51' along said bank to a point; Thence N 67'36'00" W a distance of 234.51' along said bank to a point; Thence N 61'36'00" W a distance of 133.07' along said bank to a point; Thence N 61'36'00" W a distance of 134.07' along said bank to a point; Thence N 51'44'58" W a distance of 134.07' along said bank to a point; Thence N 51'44'58" W a distance of 140.57' along said bank to a point; Thence N 90'00'0" E a distance of 62.02' to a point; Thence S 19'49'23" E a distance of 618.74' to a 1\2" rebar set; Thence S 19'49'23" E a distance of 618.74' to a 1\2" rebar set; Thence N 86'43'33" E a distance of 140.10' to a 1\2" rebar set; Thence S 00'06'27" W a distance of 140.10' to a 1\2" rebar set; Thence S 00'06'27" E a distance of 180.22' along said right of way of said Private Road; Thence S 00'05'37" E a distance of 140.10' to a 1\2" rebar set; Thence S 00'05'37" E a distance of 140.10' to a 1\2" rebar set; Thence S 00'05'37" E a distance of 140.10' to a 1\2" rebar set; Thence S 00'05'3
l of land having an area of 1.182 Acres. TRACT C1	(SECUNDARY ASH AREA NO. 2) METES AND BOUNDS DESCRIPTION
(SECONDARY ASH AREA NO. 1) METES AND BOUNDS DESCRIPTION	All that tract or parcel of land lying in or being in Land Lot 92, 15th. Land District, Worth County, Georgia, and being more particularly described as follows:
 brcel of land Iting in or being in Land Lot 92, 15th. Land hty, Georgia, and being more particularly described as betresection of the South line Land Lot 39 and the of Power Dam Road (60' R\W), said intersection being rebar found and having Grid North, Ga. West Zone coordinates c. 2366449.03; Thence N 02'57'36" W s distance of 1156.48' at of way of a Private Road, to a 1\2" rebar set, having grid c. 70700.30, E. 2366389.31; Thence N 02'50'32" W a distance of right of way of said Private Road to a 1\2" rebar set, having N. 670880.29, E. 2366380.37; Thence S 86'43'33" W a distance 2" rebar set; Thence N 00'04'22" E a distance of 432.21' to a ence N 89'54'37" W a distance of 874.52' to a 1\2" iron rebar ing grid coordinates of N. 671301.74, E. 2365294.18 and being NNING; W a distance of 58.25', to a point; E a distance of 62.02', to a point; 	 Beginning at the intersection of the South line of Land Lots 39 & 92 and the West right of way of Power Dam Road (60' R\W), said intersection being marked by a 1\2" rebar found and having Grid North Ga. West Zone coordinates of N. 669545.36, E. 2366449.03, Thence S 89'54'24" W a distance of 701.58' along said line of said Land Lots to the POINT OF BEGINNING; Thence S 89'54'24" W a distance of 450.00' along said line of said Land Lots, to a concrete monument; Thence N 00'06'23" W a distance of 253.41', to a point; Thence N 00'06'23" W a distance of 761.41', to a point; Thence N 89'53'20" E a distance of 450.00', to a point; Thence S 00'06'23" E a distance of 1014.96', to the POINT OF BEGINNING. Said tract or parcel of land having an area of 10.484 Acres.
W a distance of 55.78', to the POINT OF BEGINNING.	

	GRAPHIC SCALE
	300 0 150 300 600 1200
	(IN FEET) 1 inch = 300 ft.
	REVISION no. 7, AUG. 28, 2023, ADDRESSED RED LINE COMMENTS.
	REVISION no. 6, JUNE 19, 2023, ADDRESSED RED LINE COMMENTS.
	REVISION no. 5, JUNE 2, 2023, ADDRESSED RED LINE COMMENTS.
	REVISION no. 4, AUG. 5, 2022, ADDRESSED RED LINE COMMENTS.
	REVISION no. 3, JUNE 8, 2022, TO SHOW LOCATION OF NEW MONITORING WELLS AND TO SHOW LIDAR TOPOGRAPHIC SURVEY.
	* SURVEY FOR *
	CRISP COUNTY POWER COMMISSION
	PART OF LAND LOTS 92 & 39, 15th. LAND DISTRICT, WORTH COUNTY, GEORGIA
FOUND	SCALE: 1 INCH REPRESENTS 300 FEETDATE OF SURVEY: DATE OF SURVEY: DATE OF PLAT:OCT. 15, 2018THIS PLAT HAS BEEN CALCULATED FOR CLOSURE AND IS FOUND TO BE ACCURATE LINEAR PRECISION - 1' IN 42,366,456'SCALE: 1 INCH REPRESENTS 300 FEETDATE OF PLAT: OCT. 25, 2018OCT. 25, 2018THIS PLAT HAS BEEN CALCULATED FOR CLOSURE AND IS FOUND TO BE ACCURATE
PIPE FOUND PIPE FOUND ENT FOUND	THE FIELD DATA UPON WHICH THIS PLAT IS BASED HAS A CLOSURE PRECISION OF ONE FOOT IN FEET AND AN ANGULAR ERROR OF PER ANGLE POINT,
E NG	EQUIPMENT USED: SEE NOTE no. 3
	PROJECT: C: \CARLSON PORJECTS\2017\CCPAshPond\CCPD Boundary Plat 2022 REV(KEMRON)6-02-2023.DWG DRAWN BY: SMK FILE NO. 4137 PLAT NO. 1456 A DATE OF ISSUANCE:
	J.B. FAIRCLOTH & ASSOCIATES, P.C. LAND SURVEYING, PLANNING AND MAPPING FIRM CERTIFICATE OF AUTHORIZATION NO. LSF00031
	FAIL FIRM CERTIFICATE OF AUTHORIZATION NO. LSPOUDST

PHONE (229)-273-1282

FAX (229)-273-2340

8-30-23

1109 EAST 13th. AVE.

CORDELE, GEORGIA 31015

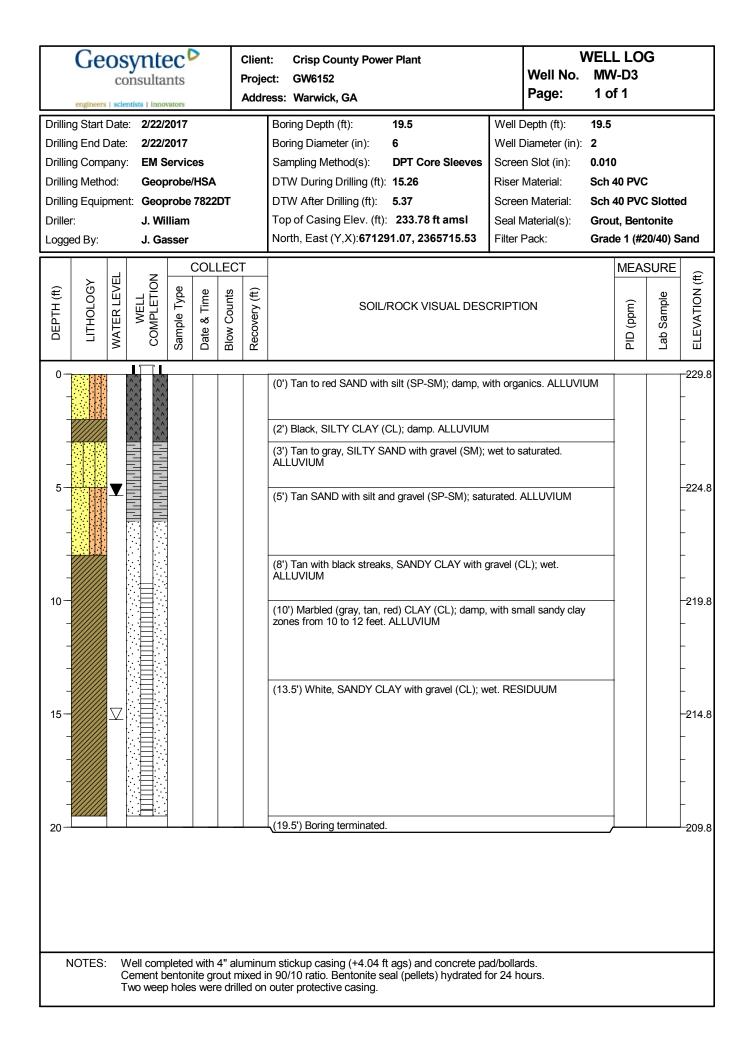
APPENDIX B

Boring Logs and Well Construction Diagrams

C engineers sc	synte consulta		BORING AND WELL LOG LEGEND						
LITHOLOGY WATER LEVEL	WELL/BORING COMPLETION	SAMPLE TYPE	DESCRIPTION						
		SH CO DP	Encore Split Spoon Shelby Tube Core Barrel						

	consultants Proj						Clien Proje Addr						
Drillin Drillin Drillin Drillin Drille	Drilling Start Date:2/22/2017Drilling End Date:2/22/2017Drilling Company:EM ServicesDrilling Method:Geoprobe/HSADrilling Equipment:Geoprobe 7822DTDriller:J. WilliamLogged By:J. Gasser							Boring Depth (ft):20Well Depth (ft):19.5Boring Diameter (in):6Well Diameter (in):2Sampling Method(s):DPT Core SleevesScreen Slot (in):0.010DTW During Drilling (ft):13.36Riser Material:Sch 40 PVCDTW After Drilling (ft):13.42Screen Material:Sch 40 PVCTop of Casing Elev. (ft):241.77 ft amslSeal Material(s):Grout, BentoNorth, East (Y,X):670708.47, 2365315.12Filter Pack:Grade 1 (#20.			C Slotted tonite		
DEPTH (ft)	ГІТНОГОСУ	WATER LEVEL	WELL	Sample Type	Date & Time	Blow Counts J	Recovery (ft)	SOIL/ROCK VISUAL DESCRIPTION				ELEVATION (ft)	
0								(0') Dark brown, SILTY SAND (SM); damp. ALLUVIUM (1.5') Red, CLAYEY SAND (SC); damp. ALLUVIUM		-		-238.1 - - -	
5								(5') Red, CLAYEY SAND with gravel (SC). ALLUVIUM (7.8') Gravel layer from 7.8-8.0 feet. ALLUVIUM (8') Brown, CLAYEY SAND with gravel (SC); damp. ALLUVIUM (9') Brown SAND with clay and gravel (SP-SC); saturated. ALLUVIUM	, ,	r r		-233.1 - - - -228.1	
- - - 15		▼						(12') Marbled (tan, gray, red, black,) CLAY (CL); damp, compact, with some sand and gravel decreasing with depth. ALLUVIUM (15') Same as above.		-		_ - - -223.1	
								(17') White, SANDY CLAY (CL); wet. RESIDUUM (20') Boring terminated.		-		- - 218.1	
												- - - -213.1	
	IOTES:	C	ement b	enton	ite gr	out m	ixed i	m stickup casing (+3.66 ft ags) and concrete pad/bollards. n 90/10 ratio. Bentonite seal (pellets) hydrated for 24 hours. outer protective casing.				-213.1	

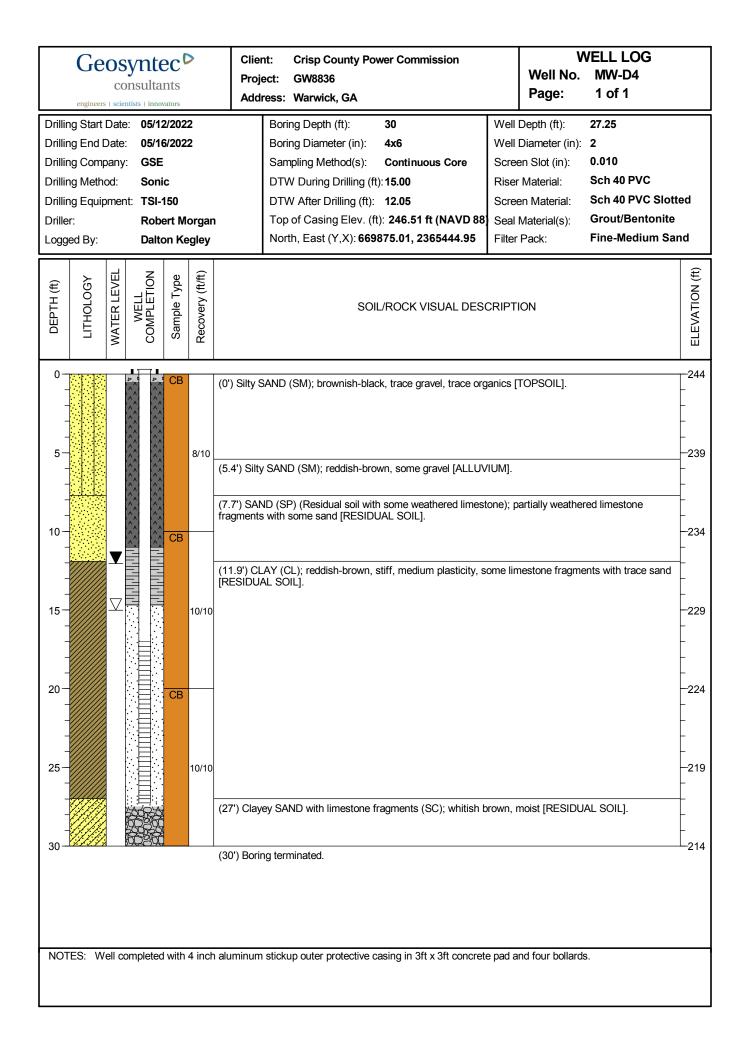
Drilling Start Date: 2/21/2017 Drilling End Date: 2/21/2017 Drilling Company: EM Servir Drilling Method: Geoprobe Drilling Equipment: Geoprobe Driller: J. William Logged By: J. Gasser	ces e/HSA e 7822D i	DTW After Drilling (ft): 11.7 Screen Material: Sch Top of Casing Elev. (ft): 232.66 ft amsl Seal Material(s): Gro	0 40 PVC 40 PVC ut, Bent de 1 (#2	Slotted onite 0/40) S OURE	and
		SOIL/ROCK VISUAL DESCRIPTION			N (ft)
			PID (ppm)	Lab Sample	ELEVATION (ft)
10 10 15 20 20 - 25 NOTES: Well complete		(0') Dark brown/red, ORGANIC SOIL with silt (OL); dry, topsoil. (4') Brown, SANDY SILT (ML); dry. ALLUVIUM (5') Tan SAND (SP); damp, fine-grained with trace clay. ALLUVIUM (6') Saturated from 5-6 feet. (7.5') Gray CLAY (CL); damp, very firm/compact, with trace sand and two thin bands of gravel. ALLUVIUM (12') Gray blue CLAY (CL); moist, soft, with trace sand. ALLUVIUM (14') White/gray SAND with gravel (SP); wet, trace clay. RESIDUUM (20') Boring terminated.			-229.1 - -



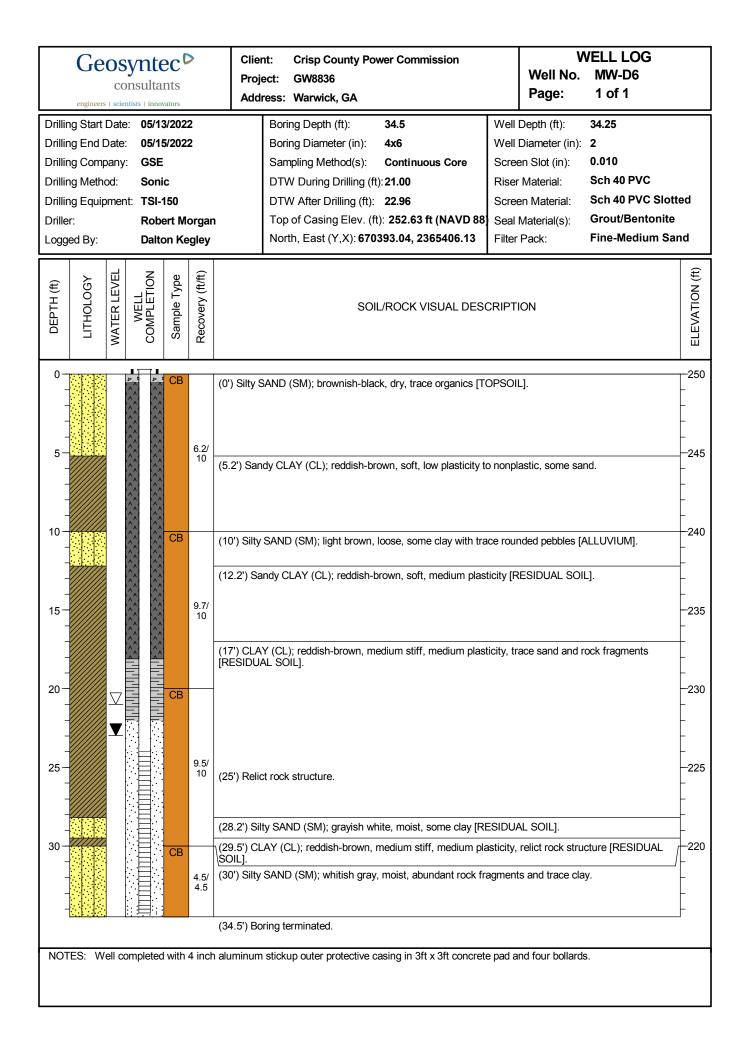
	Clier consultants engineers scientists innovators						Proje					
Drilling Start Date:2/21/2017Drilling End Date:2/23/2017Drilling Company:EM ServicesDrilling Method:Geoprobe/HSADrilling Equipment:Geoprobe 7822DTDriller:J. WilliamLogged By:J. Gasser								Boring Depth (ft):40Well Depth (ft):Boring Diameter (in):6Well Diameter (in):Sampling Method(s):DPT Core SleevesScreen Slot (in):DTW During Drilling (ft):11Riser Material:DTW After Drilling (ft):9.01Screen Material:Top of Casing Elev. (ft):249.52 ft amslSeal Material(s):North, East (Y,X):669996.79, 2366420.55Filter Pack:	0.010 Sch Sch Grou		Slotte	
DEPTH (ft)	ГІТНОГОСУ	WATER LEVEL	WELL	Sample Type	Date & Time	Blow Counts	Recovery (ft)	SOIL/ROCK VISUAL DESCRIPTION				ELEVATION (ft)
0								(0') Dark brown SILT with sand (ML); organics, topsoil. (3') Orange/red CLAY with sand (CL); slightly moist. ALLUVIUM				246.3
5		▼						(5') Tan, SANDY CLAY (CL); moist. ALLUVIUM		-		- -241.3 - - -
10		∇						(10') Same as above. (12.5') Marbled (tan, red), SANDY CLAY (CL); dry, compact, trace gra ALLUVIUM	avel.			-236.3 - - -
15 — - - -								(15') Marbled (red, white, tan) CLAY (CL); trace water, very hard/com some sand and trace gravel. ALLUVIUM	pact,	-		-231.3 - - -
20								(20') Same as above. (21') Dark brown, ORGANIC SOIL (OL); with wood. ALLUVIUM (22') Tan/dark brown CLAY with sand and gravel (CL); moist. ALLUVI	UM			-226.3 - - - -
25-	IOTES:	C T	ement b	enton hole	ite gro s were	out m e drille	ixed i ed on	m stickup casing (+3.20 ft ags) and concrete pad/bollards. n 90/10 ratio. Bentonite seal (pellets) hydrated for 24 hours. outer protective casing. and 40 ft depth was filled with clay collapsed from the borehole.		-		-221.3

	consultants Proje						Clien Proje Addre	ct: GW6152 Well No. M				
Drillin Drillin Drillin Drillin Drille	Drilling Start Date: 2/21/2017 Drilling End Date: 2/23/2017 Drilling Company: EM Services Drilling Method: Geoprobe/HSA Drilling Equipment: Geoprobe 7822DT Driller: J. William Logged By: J. Gasser							Boring Diameter (in):6Well Diameter (in):2Sampling Method(s):DPT Core SleevesScreen Slot (in):0.0DTW During Drilling (ft):11Riser Material:SciDTW After Drilling (ft):9.01Screen Material:SciTop of Casing Elev. (ft):249.52 ft amslSeal Material(s):Green	Diameter (in):2en Slot (in):0.010Material:Sch 40 PVCen Material:Sch 40 PVC SlottedMaterial(s):Grout, Bentonite			
DEPTH (ft)	ГІТНОГОСУ	WATER LEVEL	WELL	Sample Type	Date & Time	Blow Counts	Recovery (ft)	SOIL/ROCK VISUAL DESCRIPTION	LE (mdd) OIA	Lab Sample	ELEVATION (ft)	
25 								 (25') Dark brown CLAY (CL); moist, sticky, very trace sand with one to two small sections of gravel. ALLUVIUM (29') Same as above, but more moist and soft. (30') Dark tan/brown CLAY with sand and gravel (CL); wet/saturated. RESIDUUM (35') White, SANDY CLAY (CL); saturated, and mostly sand at 40 feet. RESIDUUM (40') Boring terminated. 			-221.3 - - -216.3 - - - - - - - - - - - - - - - - - - -	
45-	NOTES: Well completed with 4" aluminum stickup casing (+3.20 ft ags) and concrete pad/bollards. Cement bentonite grout mixed in 90/10 ratio. Bentonite seal (pellets) hydrated for 24 hours. Two weep holes were drilled on outer protective casing. DPT borehole between 33.75 ft and 40 ft depth was filled with clay collapsed from the borehole.											

Geosyntec consultants engineers scientists innovators						BORING AND WELL LOG LEGEND					
	_	() –		COL	LEC	Ţ		MEASU			
ГІТНОГОСУ	WATER LEVEL	WELL/BORING COMPLETION	Sample Type	Date & Time	Blow Counts	Recovery (ft)	SOIL/ROCK VISUAL DESCRIPTION	(mqq) OIP	Lab Sample		
			GR EN SS ST CO DP				ASPHALT CONCRETE FILL TOPSOL COBBLES IGNEOUS Rock METAMORPHIC Rock SEDIMENTARY Rock Well-graded GRAVEL (GW) Poorly graded GRAVEL (GP) Silty GRAVEL (GC) Well-graded GRAVEL (GP) Silty GRAVEL (GC) Well-graded GRAVEL (GP) Silty GRAVEL (GC) Well-graded GRAVEL with silt (GP-GM) Well-graded GRAVEL with silt (GP-GC) Poorly graded GRAVEL with clay (GP-GC) Poorly graded GRAVEL with silt (GP-GN) Well-graded GRAVEL with silt (SW-SC) Poorly graded SAND (SP) Silty SAND (SC) Well-graded SAND with silt (SW-SM) Poorly graded SAND with silt (SW-SC) Poorly graded SAND with silt (SW-SC) Poorly graded SAND with silt (SW-SC) Poorly graded SAND with clay (SP-SC) SILT (ML) Lean CLAY (CL) Organic SOIL (OL) Elastic SILT (MH) Fat CLAY (CH) Organic SOIL (OH) PEAT SS Some 3:0:45% M	0.0	ID		
NOTE	S:										

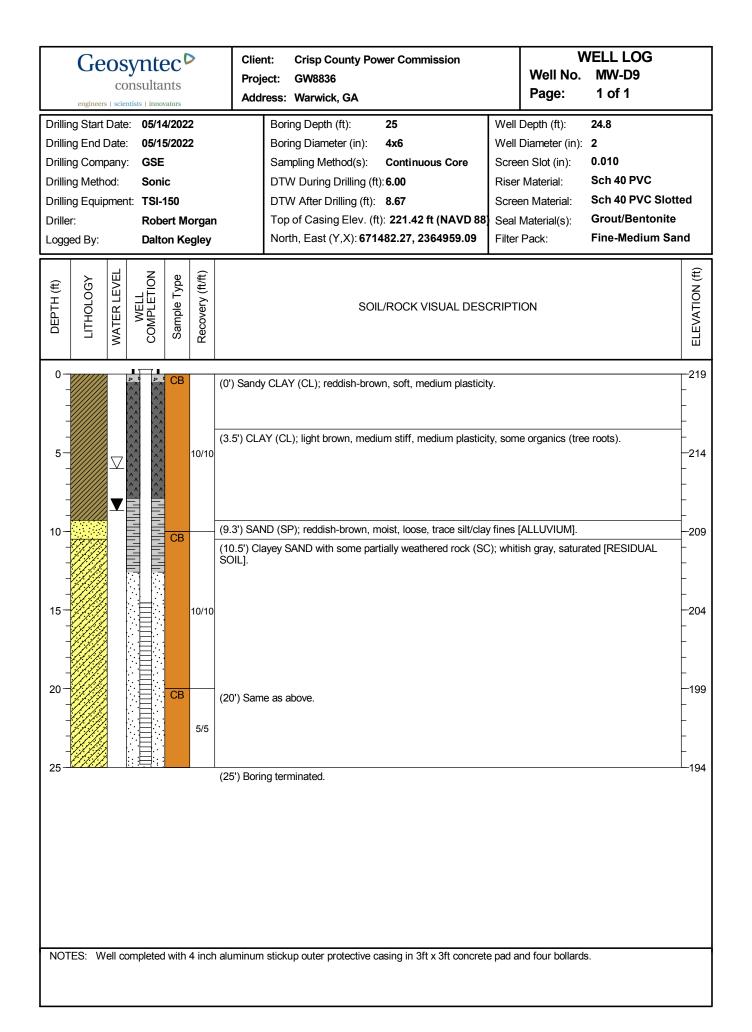


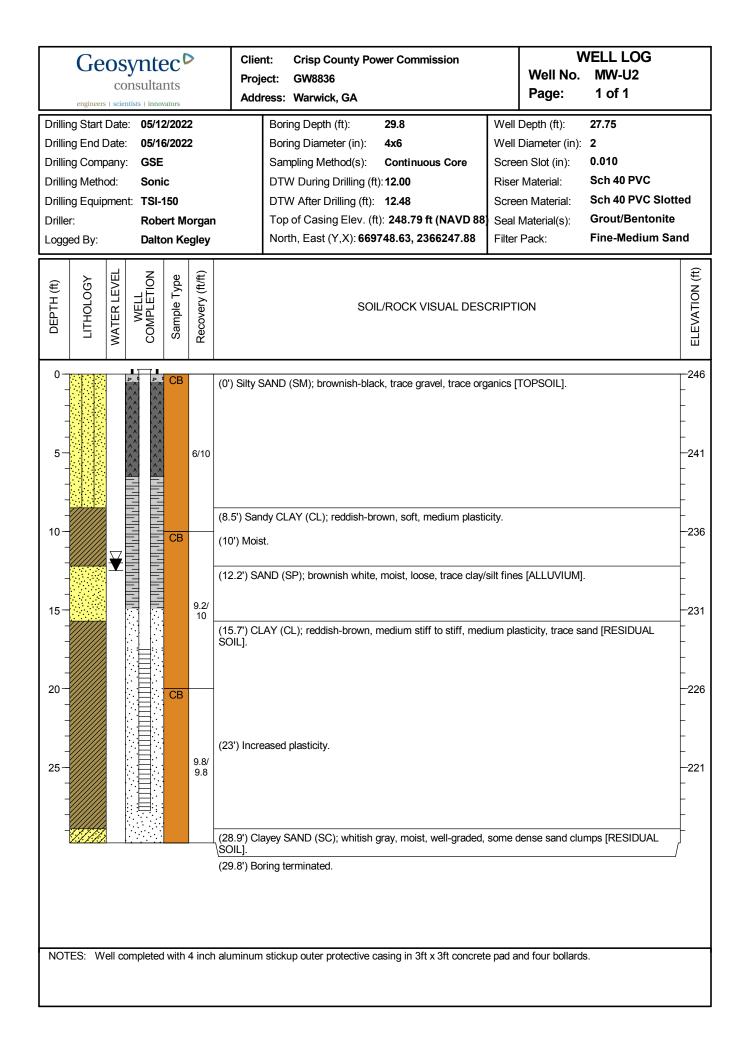
Geosyntec consultants engineers scientists innovators	>	Client:Crisp County Power CommissionWELL LOGProject:GW8836Well No.MW-D5Address:Warwick, GAPage:1 of 1	
Drilling Start Date:05/16/2022Drilling End Date:05/18/2022Drilling Company:GSEDrilling Method:SonicDrilling Equipment:TSI-150Driller:Robert MethodLogged By:Dalton Ke	2 organ	Boring Depth (ft):35Well Depth (ft):33Boring Diameter (in):4x6Well Diameter (in):2Sampling Method(s):Continuous CoreScreen Slot (in):0.010DTW During Drilling (ft):19.00Riser Material:Sch 40 PVCDTW After Drilling (ft):NAScreen Material:Sch 40 PVC StTop of Casing Elev. (ft):241.16 ft (NAVD 88Seal Material(s):Grout/BentonNorth, East (Y,X):670216.49, 2365178.72Filter Pack:Fine-Medium	ite
DEPTH (ft) LITHOLOGY WATER LEVEL COMPLETION Sample Type	Recovery (ft/ft)	SOIL/ROCK VISUAL DESCRIPTION	ELEVATION (ft)
	(0') Silty SAND (SM); brownish-black, trace organics [TOPSOIL].	238
	7/10	 (3.7') Silty SAND to sandy clay (SM); reddish-brown, dry, loose, poorly graded [ALLUVIUM]. (8') CLAY (CL); reddish-brown, medium stiff, medium plasticity, some rock fragments, relic rock structure [RESIDUAL SOIL]. 	- 233 - - - -
	8.5/ 10		-228 - - - - - -223 - -
		(18.2') Silty SAND and clay (SC-SM); reddish-brown, abundant rock fragments. (19') Moist.	
	10/10	(20') Silty SAND and clay (SC-SM); whitish brown, saturated, loose, abundant rock fragments.	
30 CB	0/5	(30') No recovery.	208
35		(35') Boring terminated.	
NOTES: Well completed with		aluminum stickup outer protective casing in 3ft x 3ft concrete pad and four bollards.	



Geosynt consult engineers scientists inr	ants	>	Clier Proje Addı	ct: GW8836	WELL LOG Well No. MW-D7 Page: 1 of 1			
Drilling Company: GS Drilling Method: Son Drilling Equipment: TSI Driller: Rol	15/2022 E nic	2 organ		Sampling Method(s):Continuous CoreScreen SDTW During Drilling (ft):5.50Riser Ma	ameter (in): Slot (in): laterial: Material: aterial(s):	24.4 2 0.010 Sch 40 PVC Sch 40 PVC Slotted Grout/Bentonite Fine-Medium Sand		
DEPTH (ft) LITHOLOGY WATER LEVEL VVELL	Sample Type	Recovery (ft/ft)		SOIL/ROCK VISUAL DESCRIPTION				
		9/10	(4.5') San [ALLUVIU	- y CLAY and partially weathered rock (CL); reddish-brown to	plasticity, so	ragments		
		10/10	(10') Clay SOIL].	y SAND and partially weathered rock fragments (SC); whitis	sh gray, satu	- - - - -21 - - - -		
	СВ	5/5	(20') Sano medium p	CLAY and partially weathered rock fragments (CL); whitish sticity [RESIDUAL SOIL].	h gray, moist	-		
25			(25') Borir	terminated.		20		
NOTES: Well complete	ed with 4	4 inch	aluminum	stickup outer protective casing in 3ft x 3ft concrete pad and f	four bollards			

Geosyntec consultants engineers scientists innovators	>	Client: Crisp County Power Commission Project: GW8836 Address: Warwick, GA	Well No. Page:	/ELL LOG MW-D8 1 of 1				
Drilling Start Date:05/13/2021Drilling End Date:05/15/2021Drilling Company:GSEDrilling Method:SonicDrilling Equipment:TSI-150Driller:Robert Method:Logged By:Dalton Keto	2 organ	Boring Diameter (in): 4x6 WSampling Method(s):Continuous CoreSiDTW During Drilling (ft): 5.50 RDTW After Drilling (ft): 8.61 SiTop of Casing Elev. (ft): 226.76 ft (NAVD 88 Si	Vell Depth (ft): Vell Diameter (in): creen Slot (in): iser Material: creen Material: eal Material(s): ilter Pack:	25 2 0.010 Sch 40 PVC Sch 40 PVC Slotted Grout/Bentonite Fine-Medium Sand				
DEPTH (ft) LITHOLOGY WATER LEVEL COMPLETION Sample Type	Recovery (ft/ft)	SOIL/ROCK VISUAL DESCRI	SOIL/ROCK VISUAL DESCRIPTION					
0 - CB 5 - ∇ M	8/10	(0') Silty SAND (SM); brownish-black, some clay/fines, trace org	ganics [TOPSOIL].					
		 (7.4') Sandy CLAY (CL); reddish-brown, medium stiff, low plasticity to nonplastic, trace rock fragments, relic rock structure [RESIDUAL SOIL]. (10') Clayey SAND with partially weathered rock fragments (SC); whitish gray, saturated [RESIDUAL 						
	10/10	(10) Clayey SAND with partially weathered rock fragments (SC, SOIL].); whitish gray, satu	Irated [RESIDUAL				
20 	0/5.2	(19') Some harder sections. (20') No recovery.		204 				
25 !: !!!		(25.2') Boring terminated.						
NOTES: Well completed with	4 inch	aluminum stickup outer protective casing in 3ft x 3ft concrete pa	ad and four bollards					





Site Name: CRISP COUNTY	Project Number:					
Well Name: MW-DI	Date Installed:	2/22/17				
	Date Developed:	2/24/17				
Depth To Bottom:						
(Initial)	Pump (Type)	JUBMERSIBLE				
(Final)	(Capacity)					
DTW-13.42 TOC	TOC - PAD 417/8"					
TPW - 22.95 TOC						
Field Cleaning of Equip:						
Save Purge Water:	Purge Water Conta	aiment Method: 5 GAL, BUCKETS				
Measuring Point:	GeoSyntec Representative:					
Casing I.D.:	Drilling Firm Representative:					

Time	Volume Removed (gal)	pН	Temp (°C)	Conductance (µS/cm)	Turbidity (NTU)	Salinity (ppm)	ORP (mV)	Comments
1630	Ø	6.82	21.5	180.0	571			
1637	5	7.02	22.3	184.9	319			
1657	10	7.90	23.2	279	999			
1710	12.5	7.42	23.1	252	91			
1723	15	7.36	22.8	216	148	•		
1736	17.5	7,22	22.7	217	109			
1750	20	7.21	21.4	199.4	8			
1805	22.5	7.19	21.4	204	13			
1820	25	7.20	21.6	206	8		,	
[
L								

PUMP PLACED WITHIN 6" FROM BOTTOM OF WELL SCREEN. WELL PRODUCED A CONSTANT SLOW FLOW. WELL DID NOT DRY.

Site Name: CRISP COUNTY	Project Number:
Well Name: MW-DZ	Date Installed: 2/22 17
	Date Developed: 2/24/17
Depth To Bottom:	
(Initial)	Pump (Type) SUBMERSIBLE
(Final)	(Capacity)
DTW- 11.7 TOC	TOC- PAD 41.5"
Field Cleaning of Equip:	1 A A A A A A A A A A A A A A A A A A A
Save Purge Water:	Purge Water Contaiment Method: 5 GAL BUCKETS
Measuring Point:	GeoSyntec Representative:
Casing I.D.:	Drilling Firm Representative:

Time	Volume Removed (gal)	pН	Temp (°C)	Conductance (µS/cm)	Turbidity (NTU)	Salinity (ppm)	ORP (mV)	Comments
1110	Ø	7.70	22.7	6.45	999			
1120	3	7,34	22.6	6.47	999			
1130	2	7,36	23.5	4.52	999			
1135	3	7.42	23.6	6,54	999			
1140	2	7.51	23.7	6.62	999			
1150	3	7.25	23.7	6.41	999			
1200	Z	7,33	23.6	6.52	999			WELL DRY
12.30		7.37	23.3	6.43	999			PUMP ON
1250	2	7.36	23.8	6.51	999		,	WELL DRY
	17.0	TOTAL	PURGED					

WATER COLUMN DOWN QUICKLY. PUMP PLACED WITHIN 6" FROM BOTTOM OF SCREEN. WELL WILL NOT RECOVER TO ALLOW CONSTANT FLOW WITH SUBMERSIBLE PUMP. 30

2/27/17 Site Name: CRISP COUNTY Project Number: Well Name: MW-D2 Date Installed: 2127/17 Date Developed: Depth To Bottom: SUBMERSIBLE (Initial)_____ (Final)_____ Pump (Type) (Capacity) PTW 11.84' TOC Field Cleaning of Equip: Save Purge Water: Purge Water Contaiment Method: Measuring Point: GeoSyntec Representative: Casing I.D.: Drilling Firm Representative: Volume Temp Conductance Turbidity ORP Removed Salinity (°C) $(\mu S/cm)$ (gal) (NTU) (mV)Time pН (ppm) Comments 715 999 ø 103Z 7.29 18,6 1043 2.5 688 7.32 19.8 999 95 5.0 7,28 21.3 693 1102 7.29 21.6 695 94 1110 6.0 688 26 7.5 7,19 23.8 121 9 7.16 22.7 693 1141 10.0 12.5 7-10 24.7 677 1201 11 23.3 673 1221 15.0 7.13 7 1

1036 - SURGED PUMP. PUMP NOW APPROX "" FROM BOTTOM OF WELL SCREEN. SLOW FLOWBUT CONSTANT.

WELL DEVELOPMENT DATA FORM

Site Name: CRISP COUNTY	Project Number:
Well Name: MW - D3	Date Installed: 2/23/17
	Date Developed: 2/24/17
Depth To Bottom:	
(Initial)	Pump (Type) JUBMERSIBLE
(Final)	(Capacity)
DTW - 5.37 - TOC TDW - 23.8 - TOC	Toc - PAD 43.75"
Field Cleaning of Equip: Save Purge Water:	Purge Water Contaiment Method: 5 GAL BUCKETS
Measuring Point:	GeoSyntec Representative:
Casing I.D.:	Drilling Firm Representative:

Time	Volume Removed (gal)	pН	Temp (°C)	Conductance (µS/cm)	Turbidity (NTU)	Salinity (ppm)	ORP (mV)	Comments
1310	Ø	7.15	22.8	6.25	999			
1319	5	7.19	24.7	6.20	999			
1330	10	7.25	23.8	6.33	999			
1340	15	7.28	23.9	6.10	999			
1351	20	7.20	23.9	6.13	999			
1402	25	7.21	24.2	6.16	999			
1415	30	7.23	24.1	6.15	961			
1429	35	7.22	24.3	6.13	415			
1442	40	7.21	24.2	6.14	71		,	
1455	45	7,21	24.1	6.13	78			
1509	50	7.22	24.1	6.13	39	1		
1521	55	7.22	24.0	6.14	34			
1533	60	7.22	24.1	6.14	44			
1547	65	7.22	24.1	6.13	43			
1603	70	7.21	23.8	6.13	31			

PUMP PLACEMENT WITHIN 6" FROM BOTTOM OF WELL SCREEN. WAS TOLDBY JEREMY 3 READINGS BELOW SO NTU AFTER SO GALS PURGED WAS SUFFICIENT. WELL DID NOT RUN DRY.

PAGE 1 OF 2

WELL DEVELOPMENT DATA FORM

Site Name: Well Name:	ORISP C.	OUNTY		Project Number: Date Installed:	2	123/17		
well Mattic.	<u> </u>			Date Developed:		127/17		
Depth To B				Pump (Type) (Capacity)	SUBMI	ERSIBL	E	
D	TW - 9.		<u>د</u>	TD	w- 37.	8 70	C	
Field Clean Save Purge Measuring Casing I.D.	Point:	:		Purge Water Cont GeoSyntec Repres Drilling Firm Repr	entative:	od: .		
Time	Volume Removed (gal)	pН	Temp (°C)	Conductance (µS/cm)	Turbidity (NTU)	Salinity (ppm)	ORP (mV)	Comments
12.50	Ø	דר, ך	21.0	354	999	NA 4 177	<u>`</u>	
1259	5.0	7.87	22,4	344	999			······
1309	10.0	7.88	23.1	340	999			
/314	15.0	7.76	21.9	256	999			
1322	20.0	7.96	22.4	237	999			
1331	25.0	7.83	23.7	245	999			
1341	30.0	7.99	24.0	233	999			
1349	35.0	7.92	24.6	237	999			
1400	40.0	7.98	23.8	235	999			
1409	45.0	7.92	23.1	236	ବିକ୍ୟ			
1419	50.0	8.01	21.8	222	999			
1428	55.0	7.95	22,4	216	999			
1438	60.0	7.96	Z2.9	209	999			
1447	65.0	7.95	22.5	210	599			
1457	70.0	7.83		Z10	999			
150 5	75.0	7.87	23.3	200	999			
1515	80.0	8.00	22.3	196.2	999			
1524	85.0	7.91	22.4	194.8	999			
1532	90.0	7.98		190.8	668			
1541	95.0	7.96		200.8	999			
1551	100-00	8.00	21.2	190.1	999			

:

Site Name: CRISP COUNTY	Project Number:
Well Name: MW-UI	Date Installed: 2 23 17
	Date Developed: 2/27/17
Depth To Bottom:	_
(Initial)	Pump (Type) SUBMERSIBLE
(Final)	(Capacity)
DTW- 9.01 TOC	TOW-37.8 TOC
Field Cleaning of Equip:	
Save Purge Water:	Purge Water Contaiment Method:
Measuring Point:	GeoSyntec Representative:
Casing I.D.:	Drilling Firm Representative:

Time	Volume Removed (gal)	pН	Temp (°C)	Conductance (µS/cm)	Turbidity (NTU)	Salinity (ppm)	ORP (mV)	Comments
1601	(gai)	7.93	22,3	192.4	999	(ppm)	()	Commons
1610	110	7.95	21.9	193.5	999			
1619	115	7.96	21.8	194.6	788			
1628	120	7.96	21.7	195.4	999			
1637	125	7.95	21.2	195.3	999	·		
1646	130	7.96	Z1.3	195.6	999			
1655	135	7.96	21.3	196.4	658			
1704	ાન૦	7.95	21.7	195.8	557			
1714	145	7.96	21.2	195.4	512			
1724	150	7.95	21.2	196.7	319		,	
1733	155	7.95	21,1	196.8	862			CHANGED BATERIES
1743	160	7.94	21.9	196.2	999			
1753	165	7.95	20.9	195.3	915			715 JURB
1803	170	7.94	Z0,8	195.1	408			
1813	175	7.95	20,8	196.2	3716			
1822	180	7.95	20.4	197.1	999			
1831	185	7,95	20.4	196.7	910			
1840	190	7.95	20:1	195.8	999			
					•			

PAGE Z OF 2

WELL DEVELOPMENT LOG SHEET	Project No Development Date Location. Location. Pump Type/Model: Ereld Personnel Name Autorial Pump Intake Depth (ft): Ereld Personnel Name Autorial Pump Intake Volume (L) Ereld Personnel Name Autorial	Temp. (°C) Turbidity (NTUs) DTW (ft bloc) Purged Volume (mL/min) Purged Volume (mL/min) ••• •• •• •• • • •• • • •• • • •• • • •• • • • • • •
	11035	3
r Log Shife	SCAL SCAL	201W (ff broc
LL DEVELOPMEN	Project No Location Pump Type/Model: Tubing Material mp Intake Depth (ft) Purge Rate (mL/min): Purge Rate (mL/min): tal Purge Volume (L)	
WEI	Jo R R	Temp. (°C)
		DO (mg/L)
	nm (feet)	d. ORP (mV)
	CCPC MW-U Pul. 92 Stick Up No Replace No	Spec. Cond. (µS/cm)
	purge): 041d ₂ h 1*3 785 <i>hesy: h = leng</i> Flush Yes 1 Yes 1	(US) Hq
Geosyntec ⁽² consultants	Client:CCOCSite:Site:Well ID:Well ID:Total Depth (tt) (after purge): $\overline{MM^-U2}$ Total Depth to Water (ft) $\overline{MM^-U2}$ Depth to Water (ft) $\overline{MM^-U2}$ Well Volume (gal) = 0 041d_2h \overline{MU} Well Uotree (finches): $h = length of water column (feet)Well TypeFlushWell LockYesWell Cap ConditionGuodWell Tag PresentYesNo$	Time pH (SU)

Geosyntec ⁽²⁾ consultants					WEL	WELL DEVELOPMENT LOG SHEET	IT LOG SHEET			
Client CCOC Site CCOC Site MUU-U2 Well ID: Total Depth (th) (after purge): Total Depth to Water (ft) Total Depth to Water (ft) Depth to Water (in) Vell Volume (gal) = 0 041d ₂ h Well Volume (L) = gal * 3 785 Increase of the of water column (feet) d = well diameter (inches): h = length of water column (feet) Well Type Flush	purge): 041d h 1 * 3 782 fesy: h = len Flush	CCOC MWJJ2 12.34 12.34 Stok Up	7 mn (feet)		Pun Torr	Project No Location Pump Type/Model: Tubing Material Pump Intake Depth (ft): Start/Stop Purge Time Purge Rate (mL/min): Jeso Total Purge Volume (L):	1:55 /	08.20	e	Development Date 1/19/23 Field Personnel Name 1. Neers
Well Lock Well Cap Condition Well Tag Present.	Yes Guod Yes	No Replace No			-					97
Time St		Spec. Coad. (IS/cm) CC1 CM	ORP (mV)		(C) (C) (C)	Turbidity (NTUs)	DTW (ft bloc)	Purge Rate (mL/min)	Purged Valume (L)	Notes (Furge method, water clarify, odor, purge rate, issues with pump/welt/weather/etc.)
Stabilizing Criteria	+/- 0.1 SU	+/- 5%		DO>0 5 mg/l (whicheren is greater)		< 5 NTUS				

.

	Field Personnel Name A. NCCV	Notes (Purge metbod, water clarity, odor, purge rate, issues with pump/well/weather/etc.)	
		Purged Volume Notes (L)	
	1120	Purge Rate	
VT LOG SHEET		DTW (ft bloc)	
MELL DEVELOPMENT LOG SHEET	Project No Location Pump Type/Model: Tubing Material Pump Intake Depth (ft): Start/Stop Purge Time: Purge Rate (mL/min): Total Purge Volume (L):	Turbidity (NTUs)	< 5 NTUS
- ME	μ N N L	Temp. (°C)	
		DO (mg/L) 4.1.2 6.35 6.35 1.01 mg/L on 10%: fou	DO>05 angd. (whicheser is greater)
	um (feet)	ORP (mV)	
	CCPC MW 12.34 12.34 12.34 No No No		+/- 5%
	purge): 0.041d h 1 * 3 785 <i>thes</i>): <i>h</i> = <i>leng</i> Yes Good Yes	pH (SU)	+/- 0.1 SU
Geosyntec ⁽⁾ consultants	Client:CLOCSite:Site:Well ID:Total Depth (th) (after purge):Total Depth to Water (ft)Depth to Water (ft)Well Diameter (in)Well Volume (gal) = 0.04 ld hWell Volume (gal) = 0.04 ld h 12.34 Well Volume (gal) = 0.04 ld h 12.34 Well Volume (ft)Stack UpWell TypeFlushWell UcckYesWell Cap Condition:GoodWell Tap Present:YesWell Tap Present:Yes	Time 1135 1140,145 1200,020	Stabilizing Criteria +/- 0.1 SU

Geosyntec ⁽⁾ consultants	Ť.				WEI	WELL DEVELOPMENT LOG SHEET	T LOG SHEET		States -	
Client:CCPCSite:Site:Well ID:Total Depth (tt) (after purge):Total Depth (tt) (after purge): $\boxed{\bef{mmeddef}}$ Total Depth to Water (ft) $\boxed{\bef{mmeddef}}$ Depth to Water (ft) $\boxed{\bef{mmeddef}}$ Well Dnameter (in) $\boxed{\bef{mmeddef}}$ Well Volume (gal) = 0 04 i d_2 hWell Volume (L) = gal * 3785Well Volume (L) = gal * 3785Well Volume (L) = gal * 3785Well TypeFlushWell LockWell Cap ConditionWell Cap ConditionWell Tag Present:YesWell Tag Present:	purge): 04 id h 1 * 3 785 hey): h = len Flush Yes Yes	CCPC MM-1 28 83 Stick Up No No No	umn (feet)		J E S E	Project No Location Pump Type/Model: Tubing Material Purnp Intake Depth (ft): Start/Stop Purge Time: Purge Rate (mL/min): Total Purge Volume (L)	08	/1325		Field Personnel Name A New A
Time 1335 1335 1335 1335 1335 1335 1335 133	(NS) Hd	Spec. Cond. (µS/cm)	ORP (mV)		Temp. (°C) 22.23 27.89	Tarbidity (NTUs)	DTW (ft bloc)	Purge Rate (mL/min) //000	Purged Volume (L)	Notes (Purge metbod, water clarify, odor, purge rate, issues with pump/well/weather/etc.)
Stabilizing Criteria +/- 0.1 SU	+/- 0.1 SU	+/- 5%		0.2 mg/L (n 10% for DO > υ 5 mg/L (whiches et is greater)		< 5 NTUs				

					WE	LL DEVELOPMEN	T LOG SHEET			
Client:		CCPC				Project No :	GW8830			Development Date 515122
ite:		Plant (Leiso			Location:	MANA	k Warwick	GA	Field Personnel Name Dalton Keele
ell ID:		MW-42				Pump Type/Model:	HUTTICAL	e	,	
otal Depth (ft) (after	purge)	30.06				Tubing Material:				
epth to Water (ft):		12.0)			Pı	ump Intake Depth (ft):	Toronte		56 65	
ell Diameter (in):		2			S	tart/Stop Purge Time:	4:34/	11:09		
vell Volume (gal) = () 041d h:	Can a	3.11			Purge Rate (mL/min):	500	11.2	•.\	
ell Volume (L) = ga	2	and the	11.76)		tal Purge Volume (L)		5	9. 	
= well diameter (inc		-	110 100	ŧ.						
ell Type:	1	Stick Up								
ell Lock:	Tres	No								
	Good									
Vell Cap Condition:		Replace								
ell Tag Present:	Yes (No					7			
Time	pH (SU)	Spec, Con d.	ORP (mV)	DO (mg/L)	Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)	Purge Rate (mL/min)	Purged Volume (L)	Notes (Purge method, water clarity, odor, pur rate, issues with pump/well/weather/etc.)
46:34	7.3.6	0.231	.31	7.60	75.62	2122 ATU	12.01	3400/10:0		
4:39	7.49	0.247	24	7.09	25.4	QUES SAAR	23.46	3900/min	14.9	
8:44	7.62	0.24	351	7.04	25,52	3474 AN	23.52	900	23.4	
8:49	7.50	2. 2.53	34	7.16	25.62	3415 AM	23.46	400	27.4	
2:59	1.7	0.271	35	7.19	25.74	3372.44	24.64	SOD	37.4	
9:09	7.8%	0.240	34	7.70	25.71	1324 AM	27.21	500	41.4	
9119	4.00		357	7.12 7	193	Over rand	27.72	500	47.46	
9:24	8.07	0.237	3/		25	Der const	28.21	500	51.4	
	4.10	0.253	59	7.17	25.10	Cyli Saral	24.13	500	57.4	
9:49	46.05	0.754	53	7.24	2100	23.15	24.30	500	62.9	
4:59	4.17	0.258	47	7.74	27.40	23 3.3	28.31	450	67.3	
10:09	-6194	O. LOL	41	1.15	24.58	20.10	24.33	450	7.4	The Recharge
10139	0.22	D. U56		7.77	76.86	Ø 45.4	27,11	450	74.3	Dy Recharge
	8.33	0.257	53	7.57	74.47					
10159	4.29	0.257	34	7.59	76.79	17.3	28.31	450	50.4	
Niog	4.39	2255	40		26.98	10.73	28.50	450	49.4	/
H.04	2027	0.60	-7 10	7.54	Llg. 1 ·	(0,1)	60.00	420	37.8	
						•				
				0 2 mg/L or 10% for						
	1/ 01 611	+/- 5%		DO > 0 5 mg/L		< 5 NTUS				
Stabilizing Criteria	T/- 0.1 SU	.7 570		(whichever is greater)						

Client:		2922				Project No :	(3WH1210			Development Date: 5/15/22-
Site:		Plant (5.60				Warwick	/****	-	Field Personnel Name: Dellas Keol
Well ID:		MW-D4	`			Pump Type/Model:		10.11		Theid Telsonnel Traine La tran Por
Total Depth (ft) (after	purge).	29.91				Tubing Material:	13 X2		-	
Depth to Water (ft):	purge).	11.4(0			D	imp Intake Depth, (ft):	Tolyeth 79	Fienc	-	
Well Diameter (in):		7.40				start/Stop Purge Time:	11:45	14:30	<117	
	9 0 0 4 1 4 1-1	20	3.03			(D) 677 (1 5.5	2/11	
Well Volume (gal) = (2	TOP	1111			Purge Rate (mL/min):	<u></u>	*	-:	· · ·
Well Volume $(L) = ga$			11.42		10	otal Purge Volume (L)	11103			
d = well diameter (inc			ımn (feet)		3					
Well Type:	-	Stick Up			, e					
Well Lock:	Yes	No								
Well Cap Condition:	Good	Replace								
Well Tag Present:	Yes (No								
		Spec. Cond.	ORP (mV)	DO	Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)	Purge Rate	Purged Volume	Notes (Purge method, water clarity, odor, p
Time	pH (SU)	Spec. Cond.		(mg/L)		Turbiany (1103)		(mL/min)	(L)	rate, issues with pump/well/weather/etc.
11:45		(2)/cm)	-29	4.01	26.31	Overange	11.46	1000000	D	
11:45 11:55	4443	0.240	-29 -118	4.01	26.37	Overange	11.46	3500	28.36	
11:45	443	0.240	-29	4.01	26.31	Overanoe	11.46	1000000	D	
1/:43 11:35 12:05	46.43 46.16 46.07	0.250 0.250 0.295	-29 -118 -142	4.01 7.73 4.17	26.37 25.83 24.70	Overange Overange Overange	11.46 76.90 79.7	1000	28.36 Sce	
1/:43 11:35 12:05	46H3 46.14 46.07 46.25	0.240	-29 -118 -142 -35	46.01 7.73 4.17 9.06	26.37 25.83 24.70 23.96	Overange	11.46 76.90 79.7 76.13	1000 500 500	28.367 Sle 41	rate, issues with pump/well/weather/etc.
1/:45 /1:55 /2:05	46.43 46.16 46.07	0.250 0.250 0.295	-29 -118 -142	4.01 7.73 4.17	26.37 25.83 24.70	Overange Overange Overange	11.46 76.90 79.7	1000	28.36 Sce	
1/:45 11:55 12:05 11:25 13:00	48.83 48.16 48.07 48.25 48.31	0.240 2.240 2.245 2.245	-29 -118 -142 -35 -7@	46.01 7.73 4.17 9.06 7.74	26.37 25.83 24.70 23.96 74.57	Overange Overange Overange Overange Overange	11.46 76.90 79.7 76.13 75.35	1000 3500 1000 500	28.367 S(e 41 41	
1/:45 1:55 12:05 12:25 13:00 14:20	46.13 46.07 46.25 46.31 46.70	0.240 0.240 0.245 0.245 0.243 0.243 0.246	-29 -118 -142 -35 -76 -24	46.01 7.73 4.17 9.06 7.74 6.96	26.37 25.83 24.70 23.96 24.57 24.57 25.31	Overage Overage Overage Overage Overage	11.46 26.90 29.7 76.13 75.35	600 3500 500 500	28.361 SLe 41 42	
1/:45 11:55 12:05 11:25 13:00	48.83 48.16 48.07 48.25 48.31	0.240 2.240 2.245 2.245	-29 -118 -142 -35 -7@	46.01 7.73 4.17 9.06 7.74	26.37 25.83 24.70 23.96 74.57	Overange Overange Overange Overange Overange	11.46 76.90 79.7 76.13 75.35	500 (3500 (3500 (3500 (3500)	28.367 Sce 41 42 44 46 74	
1/:45 1:55 12:05 12:25 13:00 14:20 14:20 14:30 14:40	46.13 46.25 46.25 46.31 46.70 46.70 46.70 46.70 46.70 46.70 46.70 46.70 46.70	0.245 0.245 0.245 0.245 0.243 0.243 0.246 0.251 0.262	-29 -118 -142 -35 -76 -21 -41 -35	46.01 7.73 4.17 9.06 7.74 6.96 6.46 10.464 7.07	26.37 25.83 24.70 23.96 24.57 25.31 25.31 25.71 2.5.44	Overanne Overanne Overanne Overanne Overanne Overanne Overanne Overanne Overanne	11.46 26.90 29.7 76.13 75.35 25.35 25.90 29.90 29.6	500 500 (200 500 (200 3500 1000	28.367 S(e 41 42 42	
1/:45 11:55 12:05 12:25 13:00 14:20 14:20 14:30 16:40 16:40	48.H3 48.07 48.25 48.25 48.31 48.76 41.83 8.31 48.53	0.250 0.250 0.255 0.245 0.243 0.243 0.246 0.251 0.262 0.223	-29 -118 -142 -35 -76 -21 -41 -35 47	46.01 7.73 4.17 9.06 7.74 6.96 6.44 1.07 5.18	26.37 25.83 24.70 23.96 24.57 25.31 25.31 2.5.44 22.48	Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance	11.46 76.90 29,7 76.13 75.35 75.35 25.90 29.60 29.60	(1200 3500 1000 500 500 (1200 3500 1000	28.387 3(e 41 42 42 42	S Dry Recharging Dry Recharging Dry Recharging
1/:45 1:55 12:05 12:25 13:00 14:20 14:20 14:30 14:30 14:40 14:40 14:40 14:50 4:00	4.14 4.14 4.07 4.25 4.25 4.31 4.76 4.76 4.76 4.73 4.53 4.43	0.250 0.250 0.255 0.245 0.245 0.243 0.246 0.251 0.262 0.223 0.234	-29 -118 -142 -35 -76 -21 -41 -35 47 23	46.01 7.73 4.17 9.06 7.74 6.96 6.44 1.07 5.18 4.02	26.37 25.83 24.70 23.96 24.57 25.31 25.31 25.71 25.44 22.44 22.44 22.55	Overange Overange Overange Overange Overange Overange Overange Sog Zuto AN 953 AN	11.46 26.90 29.7 76.13 75.35 25.35 25.90 29.00 21.6 11.57 25.64	(1200) 3500 1000 500 500 (.200 3500 1000 (.300 3500	28.387 S(e 41 42 74 42 100	S Dry Recharging Dry Recharging Dry Rechargeng Dry Recharge
1/:45 11:55 12:05 12:25 13:00 14:20 14:20 14:30 15	4,143 4,14 4,07 4,25 4,25 4,25 4,25 4,76 4,76 4,76 4,76 4,76 4,75 4,93	0.250 2.250 2.250 2.255 2.245 2.243 2.243 2.243 2.251 2.262 2.252 0.254 0.231	-29 -118 -142 -35 -76 -21 -41 -35 47 23 (4	46.01 7.73 4.17 9.06 7.74 6.96 6.464 7.07 5.18 4.02 7.84	26.37 25.83 24.70 23.96 24.57 25.31 2.5.31 2.5.44 22.44 22.44 22.55 22.77	Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance	11.46 26.90 29.7 26.13 25.35 25.35 25.90 29.6 11.57 23.64 29.6	6300 3500 1000 500 500 1000 3500 1000 6300 3500 4000 500	28.387 S(e 41 42 74 42 100 661025	S Dry Recharging Dry Recharging Dry Rechargeng Dry Recharge
1/:45 11:55 12:05 12:25 13:00 14:20 14:30 15:30 15	4,143 4,14 4,25 4,25 4,25 4,25 4,76 4,76 4,76 4,76 4,76 4,76 4,75 4,43 4,45 4,49 5 4,49	0.250 2.250 2.250 2.250 2.255 2.265 2.243 2.243 2.251 2.262 2.252 0.254 0.231 0.231 0.226	-29 -118 -142 -35 -76 -21 -41 -35 47 23 14 19	46.01 7.73 4.17 9.06 7.74 6.96 6.464 7.07 5.18 4.02 7.84 7.84 7.29	26.37 25.83 24.70 73.96 74.57 25.31 25.71 25.71 25.44 22.55 22.55 22.77 22.94	Overage Overage Overage Overage Overage Overage Sog Zito AN 953 AN 219 MTLA 31.8	11.46 26.90 29.7 26.13 25.35 25.35 25.90 29.0 29.0 29.0 28.42	6300 3500 1000 500 500 1000 3500 1000 6300 3500 500 500	28.36) 28.36) S(e 41 42 42 100 25.1025 105	S Dry Recharging Dry Recharging Dry Rechargeng Dry Recharge
1/:45 11:55 12:05 12:25 13:00 14:20 14:20 14:30 15	4,143 4,14 4,07 4,25 4,25 4,25 4,25 4,76 4,76 4,76 4,76 4,76 4,75 4,93	0.250 2.250 2.250 2.250 2.255 2.243 2.243 2.243 2.243 2.251 2.262 0.234 0.234 0.234 0.234 0.235 0.223	-29 -118 -142 -35 -76 -21 -41 -35 47 23 (4	46.01 7.73 4.17 9.06 7.74 6.96 6.464 7.07 5.18 4.02 7.84	26.37 25.83 24.70 23.96 24.57 25.31 2.5.71 2.5.44 22.55 22.77 22.96 23.60	Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance Overance	11.46 26.90 29.7 25.35 25.35 25.35 25.90 29.0 29.0 29.0 28.42 24.05	6300 3500 1000 500 500 1000 3500 1000 6300 3500 4000 500	28.36) 28.36) S(e 41 42 42 100 100 100 100 100 100 100 10	S Dry Recharging Dry Recharging Dry Rechargeng Dry Recharge
1/:45 1:55 12:25 12:25 13:00 14:20 14:30 15:30 15:	4,43 4,14 4,25 4,25 4,25 4,25 4,25 4,25 4,43 4,45 4,45 4,45 4,49 4,45	0.250 2.250 2.250 2.250 2.255 2.265 2.243 2.243 2.251 2.262 2.252 0.254 0.231 0.231 0.226	-29 -118 -142 -35 -76 -21 -41 -35 47 -35 47 23 14 19 (7	46.01 7.73 4.17 9.06 7.74 6.96 6.464 7.07 5.18 4.02 7.84 7.84 7.71	26.37 25.83 24.70 73.96 74.57 25.31 25.71 25.71 25.44 22.55 22.55 22.77 22.94	Overage Overage Overage Overage Overage Overage Overage Sog ZJ TO AN 953 AN 219 MTL 31.8 22.3	11.46 26.90 29.7 26.13 25.35 25.35 25.90 29.0 29.0 29.0 28.42	(1200 3500 1000 500 500 1000 3500 1000 (.200 3500 1000 (.200 3500 1000 400 500 400 500 400 500	28.36) 28.36) S(e 41 42 42 100 25.1025 105	S Dry Recharging Dry Recharging Dry Rechargeng Dry Recharge

Client:		2903				Project No.:	64863	36		Development Date: 5/14/22
Site:		Plant Co	158	2		Location:	Warnic	K. 68	2	Field Personnel Name: Dalton K
Well ID:		MW-D				Pump Type/Model:			-	
Fotal Depth (ft) (after	purge):	361!				Tubing Material:			•>	
Depth to Water (ft):		9.5-	1		P		20	1000	-	
Well Diameter (in):		-1-	<u> </u>			ump Intake Depth (ft): Start/Stop Purge Time:	17:50	1 14:35 -	5126	i.
Well Volume (gal) = (0.0414 h	4.3		5					-	
	2					Purge Rate (mL/min):		•	5	
Well Volume (L) = ga		16.7	1		То	otal Purge Volume (L)	- 93	2		
d = well diameter (inc		gth of water colu	mn (feet)							
Well Type:	-	Stick Up		-2						
Well Lock:	Yes	No								
Well Cap Condition:	Good	Replace								
Well Tag Present:	Yes	No								
	1			DO				Purge Rate	Purged Volume	Notes (Purge method, water clarity, odor, pur
Time	pH (SU)	Spec. Cond.	ORP (mV)	(mg/L)	Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)	(mL/min)	(L)	rate, issues with pump/well/weather/etc.)
12:50	48.51	0.291	191	7.76	27.29	Overange	\$9.57	6300	0	
13:00	4.53	0,244	201	3,469	74.95	4049 AL	32.12	3400	20	
13:10	3.48	3.793	214	4.63	23.96	Querange	33.12	3400	38	
13:10	95.48 4.45	0.245	229	4.63	24.86	Querance 2423 AU	33.14	3400	38	
13:10	4.45	2.793 0.265 0.2%	229	4.63	24.86	2423 AU 1422 AV	33.14 33.13	3400 3400 3400	38 172 24Ce	
13:10 13:40 14:10 14:10	4.45	2.793 0.265 0.265 0.260 0.260	229 7.39 210	4.63	24.86	2423 AU 1422 AU 1249 AU	33.14 33.13 23.14	3400 3400 3400 3400	3 8 172 24(e 400	
13:40 13:40 14:10 14:10 14:10	4.45	2.793 0.265 0.260 0.240 0.279 0.267	229 739 210 214	4.63 7.92 9.55 9.32 9.32	24.86 25.45 25.74 25.74	2423 AU 1422 AU 1249 AU 1249 AU	33.14 33.13 23.14 33.14 33.12	3400 3400 3400 3400	3 8 172 24(e 400 5 14	
13:40 13:40 14:10 14:10 15:10 15:40	4.45	2.793 2.265 2.265 2.260 2.279 0.267 0.767	229 739 710 214 214 204	4.63 7.92 9.55 9.32 9.32 4.07	24.86 25.45 25.74 25.74 27.12	2423 AU 1422 AU 1249 AU 1249 AU (15 AU 175	33.14 33.13 23.14 33.14 33.12 33.14 33.14	3400 3400 3400 3400 3400 3400	3 8 172 24(e 400 5 14 (24	
13:40 14:10 14:10 15:10 15:40 15:40	4.45 48.51 48.51 48.48 48.48 41.55	3.793 0.265 0.260 0.260 0.267 0.267 0.267 0.267	229 739 710 714 704 704	4.03 7.92 9.55 9.32 9.32 4.07 7.60	24.86 25.45 25.74 25.74 27.12 25.74	2423 AU 1422 AU 1422 AV 1249 AU (15 AU 175 93.2	53.14 33.13 33.14 34.141	3400 3400 3400 3400 3400 3400 3400 3400	3 8 172 240 400 9 514 424 792	
13:40 13:40 14:10 14:10 15:10 15:40	4.45	2.793 2.265 0.260 2.79 0.767 0.767 0.771 0.280	229 739 710 214 214 204	4.63 7.92 9.55 9.32 9.32 4.07	24.86 25.45 25.74 25.74 27.12 25.74	2423 AU 1422 AU 1249 AU 1249 AU (15 AU 175	33.14 33.13 23.14 33.14 33.12 33.14 33.14	3400 3400 3400 3400 3400 3400	3 8 172 24(e 400 5 14 (24	
13:40 14:10 14:10 15:10 15:40 15:40	4.45 48.51 48.51 48.48 48.48 41.55	3.793 0.265 0.260 0.260 0.267 0.267 0.267 0.267	229 739 710 714 704 704	4.63 7.92 9.55 9.32 4.67 4.67 4.67 4.67 4.67 4.67 4.67 4.67	24.86 25.45 25.74 25.74 27.12 26.49 727.82	2423 AU 1422 AU 1422 AV 1249 AU 125 93.2 221.0	33.14 33.13 33.14 33.14 33.14 33.14 33.15 33.15	3400 3400 3400 3400 3400 3400 3400 3400	3 8 172 240 400 9 514 424 7142 856	ío
13:40 14:10 14:10 14:10 15:10 15:40 15:40 16:40	4.45 48.51 56.55 56.55 56.48 55 56.55 57.5	2.793 0.265 0.260 0.260 0.260 0.267 0.267 0.260 0.260	229 739 710 714 704 704 704 704 704 704 704 704	4.63 7.92 8.55 9.55 9.32 4.67 9.20 4.67 9.20 4.97 9.20	24.86 25.45 25.74 25.74 27.12 25.74	2423 AU 1422 AU 1422 AU 1249 AU 125 93.2 221.0	33.14 33.13 33.14 33.14 33.14 33.14 33.15 33.15	3400 3400 3400 3400 3400 3400 3400 3400	58 172 240 400 514 (124 792 456 6	
13:40 14:10 14:10 14:10 15:10 15:40 15:40 16:10 16:40 12:30	4.45 4.51 5.55 5.48 5.48 5.48 5.45 28,45 28,45 28,45 28,72	2.793 0.2465 0.2465 0.2465 0.2467 0.247 0.245 0.260 0.260 0.245	229 739 7210 214 704 204 213 213	4.63 7.92 8.55 9.32 4.07 4.07 7.66 9.23 4.97	24.86 25.45 25.74 27.12 25.74 27.12 25.49 27.82	2423 AU 1422 AU 1422 AU 1249 AU 125 93.2 221.0 CNECA NOP 22349 At	33.14 33.13 33.14 33.14 33.14 33.14 33.15 33.15 8.27	3400 3400 3400 3400 3400 3400 3400 3400	3 8 172 240 400 9 514 6724 7192 4356 4 20 85 856	
13:40 14:10 14:10 15:10 15:40 16:10 16:40 12:30 12:35	4.45 4.45 5.51 5.55 5.48 4.55 4.45 4.55 4.45 7.46 7.46 7.46 7.46 7.46 7.46	2.793 0.2465 0.2465 0.2465 0.2467 0.247 0.245 0.260 0.260 0.245	229 239 739 710 214 204 214 204 214 204 213 197 199 199 199	4.63 7.92 8.55 9.55 9.55 4.57 4.67 7.66 7.70 4.36 4.58	24.86 25.45 25.74 27.12 24.49 27.12 24.49 23.49 23.49 23.49 23.49	2423 AU 1422 AU 1422 AU 122 AU 175 93.2 221.0 0 0 221.0 0 0 2349 AH 243	33.14 33.13 33.14 33.14 33.12 33.12 33.15 33.15 48.27 27.19 22.14 22.14	3400 3400 3400 3400 3400 3400 3400 3400	3 8 172 24(e 400 9 514 (124 7192 856 9 20 85 85 85 85 85 85 85 85 85 85 85 85 85 8	
13:40 14:10 14:10 15:40 15:40 15:40 16:10 16:40 12:30	4.45 4.45 5.51 5.55 5.48 4.55 4.45 4.55 4.45 7.46	2.793 2.265 0.250 0.250 0.257 0.250 0.250 0.250 0.250 0.245 0.245 0.245	229 239 739 727 279 279 202 202 202 202 202 202 202 202 202 20	4.63 7.92 8.55 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.97 9.36 9.32 4.97 9.36 9.32 4.97 8.35 9.32 4.97 8.35 9.32 9.32 9.32 9.32 9.32 9.32 9.32 9.32	24.86 25.45 25.74 25.74 27.12 27.12 27.49 27.49 27.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49	2423 AU 1422 AU 1422 AU 1249 AU 175 93.2 221.0 0214 AU 22349 AU 22349 AU 243 265 150	33.14 33.13 33.14 33.14 33.12 33.15 33.15 33.15 33.15 48.77 27.19 27.19 22.17 22.19 22.17	3400 3400 3400 3400 3400 3400 3400 3400	3 8 172 24(e 400 9 514 (224 7142 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 857 857 856 856 856 856 856 857 857 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 857 857 857 857 856 856 856 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 1	
12:10 14:10 14:10 14:10 15:10 15:40 16:40 12:30 12:30 12:30 12:35 12:40 12:35 12:40 12:35 12:40 12:35 12:40 12:50 12:50	4.45 4.45 5.51 5.55 5.48 4.45 4.45 7.40 7.40 7.40 7.40 7.44	2.793 0.256 0.256 0.256 0.257 0.257 0.250 0.250 0.250 0.245 0.245 0.245 0.245 0.255	229 239 739 739 739 739 739 739 739 739 739 7	4.03 7.92 8.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55	24.86 25.45 25.74 25.74 25.74 27.12 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49	2423 AU 1422 AU 1422 AU 1249 AU 175 93.2 221.0 02614 AU 22349 AH 243 265 150 150	33.14 33.13 33.14 33.14 33.12 33.15 33.15 33.15 48.27 27.19 22.19 22.19 22.19 22.19 22.19	3400 3400 3400 3400 3400 3400 3400 3400	3 8 172 24(e 400 5 14 (224 7142 5 6 6 56 6 56 6 56 6 56 6 56 6 56 6 56 6 56 6 57 6 577 6 577 6 577 6 577 6 577 6 577 6 577 6 577 6 577 6 5777 6 5777 6 57777 6 5777777777777777777777777777777777777	
13:40 14:10 14:10 15:40 15:40 15:40 16:10 16:40 12:30	4.45 4.45 5.51 5.55 5.48 4.55 4.45 4.55 4.45 7.46	3.793 0.2465 0.2465 0.2465 0.2479 0.247 0.245	229 239 739 727 279 279 202 202 202 202 202 202 202 202 202 20	4.63 7.92 8.55 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.07 7.66 9.32 4.97 9.36 9.32 4.97 9.36 9.32 4.97 8.35 9.32 4.97 8.35 9.32 9.32 9.32 9.32 9.32 9.32 9.32 9.32	24.86 25.45 25.74 25.74 27.12 27.12 27.49 27.49 27.49 23.49 23.49 23.49 23.49 23.49 23.49 23.49	2423 AU 1422 AU 1422 AU 1249 AU 175 93.2 221.0 0214 AU 22349 AU 22349 AU 243 265 150	33.14 33.13 33.14 33.14 33.12 33.15 33.15 33.15 33.15 48.77 27.19 27.19 22.17 22.19 22.17	3400 3400 3400 3400 3400 3400 3400 3400	3 8 172 24(e 400 9 514 (224 7142 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 857 857 856 856 856 856 856 857 857 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 856 857 857 857 857 856 856 856 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 857 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 187 1	

Geosyntec[▷] consultants WELL DEVELOPMENT LOG SHEET GCPC

Plotot Grisp

MW-DS

36.11

9.57

7

4.35

11.47

Client:

Well ID:

Well Type:

Well Lock:

Well Cap Condition:

Well Tag Present:

Total Depth (ft) (after purge):

Well Volume (gal) = 0.041d_h:

Well Volume (L) = gal * 3.785:

d = well diameter (inches); h = length of water column (feet)

Yes

Good

Flush Stick Up

Yes No

No

Replace

Depth to Water (ft):

Well Diameter (in):

Site:

GW8436 Development Date: Field Personnel Name: Dalton Kegle Warwick. 17A Pump Type/Model: Monson Polvethviene 31 14:35 -5/26 12:50

512612

Time	pH (SU)	Spec, Cond.	ORP (mV)	DO (mg/L)	Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)	Purge Rate (mL/min)	Purged Volume (L)	Notes (Purge method, water clarity, odor, purge rate, issues with pump/well/weather/etc.)
13:10	7.65	0246	232	9.16	23.89	47,0	22.19	500	904.5	
13:15	7-70	0,2564	236	5.10	7338		22.14	Seo	907	
13:20	7.68			7.79	23.01		22,16	500	909.5	
13:25	7,72	0.289	2.36	7.9	23.25		22.13	500	912	
13:30	7.67		239	7.84	Z3 51	24.8	21.62	500	914.5	10 -1 0:000 1: 711
13:35	7.05	0.244	248	7:85	23.72	446.3	21-62	500	917 919,5	Moved pump to 31'
13:55	7,67	0290	754	7.60	23:79	29.4	20.42	500	922	
14:05	5 100	0.792	258	1.73	7260	13.5	70.71	500	974-5	
14215	7.64	0,241	255	7.74	23,72		20,12	500	977	
	7.09	0.292		7:75	23.81	11.3	20.12	500	9295	
	7.46		254	7.77	23,961		20.11	500	932	
25 F	÷					2				
						VIC				
•										
Stabilizing Criteria	+/- 0.1 SU	+/- 5%		0.2 mg/L or 10% for DO > 0.5 mg/L (whichever is greater)		< 5 NTUs				

Project No.

Tubing Material:

Pump Intake Depth (ft):

Start/Stop Purge Tim

Purge Rate (mL/min):

Total Purge Volume (L):

Location:

500

15:45 4.00 15:55 4.00 RAOS 4.0	5: = length of water col Stick Up No Replace Spec. Cond.	CRP (mV)	DO (mg/L)	S To To		Polyety 36 -13:55 / -2 -11	10:25-5	Purged Volume	Development Date: Field Personnel Name: Notes (Purge method, warrate, issues with num	ater clarity, odor, purg	
Well ID:Total Depth (ft) (after purge):Depth to Water (ft):Well Diameter (in):Well Volume (gal) = $0.041d_2h$:Well Volume (L) = gal * 3.785: $d = well diameter (inches): h = lee$ Well Type:Well Lock:Well Cap Condition:Well Tag Present:YesTimepH (SU)13:5514:5514:5515:5515:35	37.40 22 7 2 5: 25 5: 94 = length of water coll No Replace No Suck Up No Replace	CRP (mV)	(mg/L)	S To To	Pump Type/Model: Tubing Material: ump Intake Depth (ft) tart/Stop Purge Time Purge Rate (mL/min): tal Purge Volume (L):	Hurelea Polyety 26. -13:55 / -13:55 / -110:0000000000000000000000000000000000	<u>Purge Rate</u>	Purged Volume	Notes (Purge method, wa	ater clarity, odor, purg	
Total Depth (ft) (after purge):Depth to Water (ft):Well Diameter (in):Well Volume (gal) = $0.041d_2h$:Well Volume (L) = gal * 3.785 :d = well diameter (inches): $h = le$ Well Type:FlushWell Cap Condition:Well Tag Present:YesTimepH (SU)13:5545:0013:5545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:0545:0015:05 <td c<="" td=""><td>37.40 22 7 2 5: 25 5: 94 = length of water coll No Replace No Suck Up No Replace</td><td>CRP (mV)</td><td>(mg/L)</td><td>S To To</td><td>Tubing Material: Imp Intake Depth (ft) tart/Stop Purge Time Purge Rate (mL/min): tal Purge Volume (L):</td><td>Polyety 36 -13:55 / -2 -11</td><td>ylene 10: 25 - 5 30 36 Purge Rate</td><td>Purged Volume</td><td></td><td></td></td>	<td>37.40 22 7 2 5: 25 5: 94 = length of water coll No Replace No Suck Up No Replace</td> <td>CRP (mV)</td> <td>(mg/L)</td> <td>S To To</td> <td>Tubing Material: Imp Intake Depth (ft) tart/Stop Purge Time Purge Rate (mL/min): tal Purge Volume (L):</td> <td>Polyety 36 -13:55 / -2 -11</td> <td>ylene 10: 25 - 5 30 36 Purge Rate</td> <td>Purged Volume</td> <td></td> <td></td>	37.40 22 7 2 5: 25 5: 94 = length of water coll No Replace No Suck Up No Replace	CRP (mV)	(mg/L)	S To To	Tubing Material: Imp Intake Depth (ft) tart/Stop Purge Time Purge Rate (mL/min): tal Purge Volume (L):	Polyety 36 -13:55 / -2 -11	ylene 10: 25 - 5 30 36 Purge Rate	Purged Volume		
Depth to Water (ft): Well Diameter (in): Well Volume (gal) = $0.041d_2h$: Well Volume (L) = gal * 3.785: H = well diameter (inches); h = le Well Type: Well Cap Condition: Well Cap Condition: Well Tag Present: Yes Time pH (SU) 13:55 4:56 4:55 4:56 4:55 4:56 5:75	2.5 5: Q.14 = length of water col No Replace No Stick Up No Stick Up No Stick Up No Stick Cond.	Correction of the second secon	(mg/L)	S To To	ump Intake Depth (ft) tart/Stop Purge Time Purge Rate (mL/min): tal Purge Volume (L):	26. -13:55 / 2.7 -11 DTW (ft btoc)	10: 95 - 5. 36 Purge Rate	Purged Volume			
Depth to Water (ft): Well Diameter (in): Well Volume (gal) = $0.041d_2h$: Well Volume (L) = gal * 3.785: H = well diameter (inches); h = le Well Type: Well Cap Condition: Well Cap Condition: Well Tag Present: Yes Time pH (SU) 13:55 4:56 4:55 4:56 4:55 4:56 5:75	2.5 5: Q.14 = length of water col No Replace No Stick Up No Stick Up No Stick Up No Stick Cond.	Correction of the second secon	(mg/L)	S To To	tart/Stop Purge Time Purge Rate (mL/min): tal Purge Volume (L):	DTW (ft btoc)	3 B Purge Rate	Purged Volume			
Vell Diameter (in):Vell Volume (gal) = $0.041d_{2}h$:Vell Volume (L) = gal * 3.785:I = well diameter (inches); h = letVell Type:Vell Lock:Vell Cap Condition:Vell Tag Present:Vell Tag Present:	2.5 5: Q.14 = length of water col No Replace No Stick Up No Stick Up No Stick Up No Stick Cond.	Correction of the second secon	(mg/L)	S To To	tart/Stop Purge Time Purge Rate (mL/min): tal Purge Volume (L):	DTW (ft btoc)	3 B Purge Rate	Purged Volume			
Vell Volume (gal) = $0.041d_{2}h$:Vell Volume (L) = gal * 3.785 : $r = well diameter (inches); h = letVell Type:Vell Type:Vell Lock:Vell Cap Condition:Vell Tag Present:Vell Tag Present:$	E Z - S E elength of water coll No Replace Suck Up No Suck Up No Suck Up No Replace	S Jumn (feet) ORP (mV)	(mg/L)	To To	Purge Rate (mL/min): tal Purge Volume (L):	DTW (ft btoc)	3 B Purge Rate	Purged Volume			
Vell Volume (L) = gal * 3.785: $I = well diameter (inches); h = leVell Type:FlushVell Lock:YesVell Cap Condition:GoodVell Tag Present:YesVell Tag Present:Yes$	5: = length of water col No Replace Spec. Cond.	S Jumn (feet) ORP (mV)	(mg/L)	To Temp. (°C)	tal Purge Volume (L):	DTW (ft btoc)	3-6 Purge Rate				
i = well diameter (inches); h = letVell Type:FlushVell Lock:YesVell Cap Condition:GoodVell Tag Present:YesVell Tag Present:YesTimepH (SU)13:55\$.5414:05\$.5414:05\$.5414:35\$.5414:35\$.5514:35\$.5514:35\$.5515:05\$.5515:05\$.5515:05\$.5515:35\$.0016:35\$.0016:35\$.0016:35\$.0016:35\$.0016:35\$.00	e length of water col No Replace Spec. Cond.	order (feet)	(mg/L)	Temp. (°C)		DTW (ft btoc)	Purge Rate				
Well Type: Flush Well Lock: Yes Well Cap Condition: Good Well Tag Present: Yes Time pH (SU) 13:55 3:54 14:05 3:54 14:05 3:54 14:35 4:57 14:35 4:57 14:35 4:57 15:05 4:37 15:05 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37 15:35 4:37	No Replace StD Spec. Cond.	ORP (mV)	(mg/L)		Turbidity (NTUs)						
Well Lock: Yes Well Cap Condition: Good Well Tag Present: Yes Time pH (SU) 13:55 9:54 14:05 5:54 14:05 5:54 14:35 4:57 14:35 4:57 14:35 4:57 14:35 4:57 15:05 5:35 15:35 4:37 15:3	No Replace		(mg/L)		Turbidity (NTUs)						
Vell Cap Condition: Good Vell Tag Present: Yes Time pH (SU) 13:55 #.54 14:05 #.54 14:05 #.54 14:25 #.54 14:35 #.54 14:35 #.54 14:35 #.54 14:35 #.54 14:35 #.54 15:05 #.54 15:05 #.54 15:05 #.54 15:05 #.54 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 #.60 15:05 <td>Replace</td> <td></td> <td>(mg/L)</td> <td></td> <td>Turbidity (NTUs)</td> <td></td> <td></td> <td></td> <td></td> <td></td>	Replace		(mg/L)		Turbidity (NTUs)						
Vell Tag Present: Yes C Time pH (SU) 13:55 3:54 14:05 3:54 14:05 3:54 14:15 4:55 14:25 4:57 14:35 4:57 14:35 4:57 14:35 4:57 14:35 4:57 14:35 4:57 14:35 4:57 14:35 4:57 15:05 4:37 15:05 4:37 15:05 4:37 15:05 4:37 15:35 4:30 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4:07 15:35 4	Spec. Cond.		(mg/L)		Turbidity (NTUs)						
Time pH (SU) [3:55 \$:56 [4:05 \$:56 [4:05 \$:54 [4:05 \$:54 [4:25 \$:54 [4:35 \$:57 [4:35 \$:57 [4:35 \$:57 [4:35 \$:57 [4:35 \$:57 [4:35 \$:57 [4:55 \$:637 [5:05 \$:637 [5:05 \$:637 [5:15 \$:627 [5:25 \$:607 [5:35 \$:607 [5:55 \$:607 [5:55 \$:607 [5:55 \$:607 [6:35 \$:607 [6:35 \$:607	Spec. Cond.		(mg/L)		Turbidity (NTUs)						
13:55 \$54 14:05 \$5.54 14:16 4.55 14:16 4.55 14:125 \$5.51 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.57 15:05 4.31 15:05 4.31 15:35 4.0 15:35 4.0 15:55 8.0 15:55 8.	ID Spec, Cond.		(mg/L)		Turbidity (NTUs)						
13:55 \$54 14:05 \$5.54 14:16 4.5 14:16 4.5 14:25 5.51 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.57 14:55 4.97 15:05 4.31 15:05 4.31 15:35 4.0 15:35 4.0 15:55 8.0 15:55 8.0 1					Turbidity (11103)		(mL/min)		rate, issues with num		
14:05 \$.54 14:16 4.55 14:15 4.57 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.57 15:05 4.31 15:05 4.31 15:35 4.0 15:35 4.0 15:55 4.0	(% / % /Cm)				- 4.1				rate, issues with putt	p/well/weather/etc.)	
14:16 4.5 14:125 8.51 14:35 4.57 14:35 4.57 14:35 4.57 14:35 4.67 14:35 4.40 15:05 4.31 15:05 4.31 15:35 4.27 15:35 4.00 15:35 4.00 15:35 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 16:155 4.00 16:155 4.00 16:155 4.00		174	7.81	20.19	Overrange	22.24	6300	75			
Hy125 S.S. 14:35 4.57 14:35 4.57 14:35 4.57 14:45 4.40 15:05 4.31 15:05 4.31 15:05 4.31 15:05 4.31 15:35 4.27 15:35 4.00 15:35 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 15:55 4.00 16:155 4.00 16:155 4.00		107	1015	75.50	Diecconde	33.91	(300)	KO			
14:45 4.40 14:45 4.40 15:05 4.31 15:05 4.31 15:15 4.27 15:25 4.17 15:35 4.0 15:35 4.0 15:55 4.0 16:55	51 0.782		4.24	75.39	DIRCOMPR	32,70	6300	225			
14:55 4.40 15:05 4.31 15:15 4.27 15:25 4.13 15:35 4.0 15:35 4.0 15:55 4	7 0.212	161	8.52	26.04	4093 Auh	\$2.30	4300	300			
15:05 46.31 15:15 427 15:25 46.17 15:35 46.0 15:35 46.0 15:45 46.0 15:55 46.0 16:55		162	4.70	24.51	2941 Au	33.92	6300	375			
15:15 4.27 15:25 4.13 15:35 4.0 15:35 4.0 15:45 4.0 15:55 4.0 15:55 4.0 15:55 4.0 15:55 4.0 15:55 4.0 15:55 4.0 16:55 4.0 16:56 4.0 16:55 4.0 16:56 4.0		167	4.09	25.83	1152 AM	33.8%	6300	450			
15:25 4.13 15:35 4.0 15:35 4.0 15:45 4.0 15:55 4.0 15:55 4.0 15:55 4.0 15:55 4.0 15:55 4.0 15:55 4.0 15:55 4.0 16:25 4.0 16:00 100 100 100 100 100 100 100 100 100		162	7.82	26.51	1355 AU	33.91	(200	525			
15:35 4.00 15:35 4.00 15:55 4.00 15:55 4.00 16:05 4.00 16:25 4.00 16:25 4.00 16:25 4.00 16:25 4.00	13 0.205	173	4.68	27.75	329	33.87	6300	600			
15:45 4.00 15:55 4.00 RAOS 4.0 No?SE 4.0 No?SE 4.0 14:25 8.02	01-12 202		8.04	79.95	303	33.92	(200	750			
13:55 4.00 12:55 4.00 16:55 4.00 No?55 4.00 14:25 8.00		144	4.85	77.73	233	33.93	4300	425			
No155 4.0 16:25 0.02	05 0.201		4.45	28.42	228	33.91	(300	900			
14:25 0.02	01 0.202	190	7.15	28.55	182	33.93	(1300	975			
	25 0.196	194	4.84	77.01	163	33.92	6300	1050			
10.25 3.14	52 A.ZOS	201	3.74	27.32	-150	33.89	(300	1125	Z		
1 selles		199	7.00	27.49	2446An	31.40	2300	1200	Surged	5/15/2-	
- Martin	14 2.219									STUC	
C I	14 2.219									Shell	
Stabilizing Criteria +/- 0.1 SI	14 8.219		0 2 mg/L or 10% for		< 5 NTUs					1427	

					WE	LL DEVELOPMEN	T LOG SHEET			
Client:	-	CCPC				Project No.:	GW863			Development Date: 5/14/2
Site:		Plant	Crisp			Location:	Warw.	K GA	_	Field Personnel Name
Well ID:		MW-D	6			Pump Type/Model:	Hurri	cane		
Total Depth (ft) (after	- purge):	37.40				Tubing Material	Paleth	viene		
Depth to Water (ft):		22.32	1		Pu	imp Intake Depth (ft):		,		
Well Diameter (in):		Z				tart/Stop Purge Time:		45/ 10:25	-5117	
• /	-	2.50						300		
Well Volume (gal) = 0	2					Purge Rate (mL/min):	11 -		15 E	NV .
Well Volume (L) = gal	1 * 3 785	9.45			To	tal Purge Volume (L)	413-	8	-	
d = well diameter (incl	hes); h = leng	th of water colu	mn (feet)							
Well Type	Flush	Stick Lip								
Well Lock:	Tes	No								
Well Cap Condition:	>	Replace								
		No								
Well Tag Present:	Yes	NO)								
	<u> </u>	-							1	
Time	pH (SU)	-	ORP (mV)	DO (mg/l)	Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)	Purge Rate	Purged Volume	
Time	pH (SU)	Spec. Cond.		(mg/L)	the second s	have a second and the		(mL/min)	(L)	
Time 46:20	pH (SU)	Spec. Cond. (m/cm) 0.245	162	(mg/L)	24.98	1098 AU	22.32	(mL/min)	(L) /200	
Time	pH (SU) 7.7%	Spec. Cond.		(mg/L)	the second s	1098 AU		(mL/min)	(L)	
Time 46:2-0 46:30 46:40 46:40	pH (SU)	Spec. Cond. H(H/cm) O.ZYS D.ZoZ	162 202	(mg/L) 9,87 9,29 9,29 9,29	24.98 24.55 24.19 24.19	1098 AU 1419 AU 345 AUTU 335	22.32 33.42 33.45 32.45 32.50	(mL/min) (2300 (2300 (2300 (2300	(L) /200 /275 /350 /425	
Time 46:2-0 46:30 46:40 46:40 46:40 46:50 9:00	рН (SU) 7.7% 7.7% 7.7%	Spec. Cond. 4(2)/cm) 0.245 0.202 0.195 0.202 0.202 0.202	162 202 707 223 225	(mg/L) 9,87 9.25 9,29 9,29 4,02 4,02	24.98	1099 AU 1419 AU 345 AUTA \$35 363	22.32 33.42 33.45 32.45 32.50 32.71	(mL/min) (2300 (300 (300 (300 (300 (1300	(L) /200 /275 /350 /425 /500	
Time 46:20 46:20 46:40 46:40 46:40 46:40 9:00 9:00 9:00	PH (SU) 7.7% 7.7% 7.% 7.% 7.% 7.% 7.% 7.%	Spec. Cond. 4(2)(m) 0.245 0.252 0.202 0.202 0.202 0.202 0.202 0.202	162 202 207 223 225 223	(mg/L) 9,87 9,29 9,29 4,02 9,41 7,99	24.98 24.55 24.19 24.68 24.72 24.72 25.97	1099 AU 1419 AU 345 ATTA 335 363 352	22.32 33.42 33.45 32.45 32.50 32.71 32.51	(mL/min) (2300 (2300 (2300 (2300 (2300 (2300 (2300 (2300)	(L) /200 /275 /350 /425 /575	
Time 46:2_0 45:30 46:40 46:40 46:40 46:40 9:00 9:00 9:10 9:10 9:10	pH (SU) 7.7% 7.7% 7.% 7.% 7.% 7.% 7.% 7.% 7.% 7	Spec. Cond. 4(2)(m) 0.245 0.25 0.202 0.202 0.202 0.202 0.204 0.204 0.204 0.204 0.204	(62 202 207 223 223 223 223	(mg/L) 9,87 9,29 9,29 4,29 4,29 4,30 4,30 9,31 7,99 7,49 7,49	24.98 24.55 24.19 24.68 24.72 25.97 26.36	1099 AU 1419 AU 345 ATTA 355 363 352 348	22.32 33.42 33.45 32.50 32.71 37.51 32.71	(mL/min) (300 (300 (300 (300 (1300 (1300 (1300 (1300)	(L) /200 /275 /350 /425 /425 /575 /650	
Time 46:20 46:40 46:40 46:40 9:00 9:	PH (SU) 7.7% 7.7% 7.% 7.% 7.% 7.% 7.% 7.% 7.% 7	Spec. Cond. 4(2/cm) 0.245 D202 D202 D.195 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.255 0.2	162 207 207 223 223 223 223 225 225	(mg/L) 9,87 9,29 9,29 4,02 9,29 7,29 7,41 7,99 7,29 7,29 7,29 7,29 7,29 7,29 7,29	24.98 24.55 24.19 24.98 24.72 24.72 25.97 26.36 26.11	1099 AU 1419 AU 345 ATTA 355 3403 352 348 239 239	22.32 33.42 33.45 32.50 32.71 32.71 32.71 32.71	(mL/min) (2300 (2300 (2300 (2300 (2300 (2300 (2300 (2300 (2300)	(L) /200 /275 /350 /428 /428 /575 /656 /875	
Time 46:2_0 40:40 46:40 46:40 46:40 46:40 9:000	PH (SU) 7.7% 7.7% 7.8(e 7.80 7.80 7.80 7.80 7.80 7.80 7.80 7.80	Spec. Cond. 4(2/cm) 0.245 D202 D	162 202 207 223 223 223 223 223 225 225 225 225	(mg/L) 9,87 9,29 9,29 28,02 4,31 7,99 7,39 7,39 7,39 7,30 7,30 7,30 7,30 7,30 7,30 7,30 7,30	24.98 24.55 24.19 24.72 24.72 24.72 24.72 24.72 25.97 26.11 26.11 76.71	1099 AU 1419 AU 345 ATTA 355 3403 352 348 230 1403	22.32 33.42 33.45 32.50 32.71 32.71 32.71 32.71 32.84 22.4.1	(mL/min) (.300 (.300 (.300 (.300 (.300 (.300 (.300	(L) /200 /275 /350 /425 /425 /575 /65 /675 2/00	
Time 46:20 46:40 46:40 46:40 46:40 46:40 9:00 9:10 9:10 9:10 9:10 9:10 9:10 9:20 10:20 10:50	PH (SU) 7.7% 7.7% 7.8/2 7.80 7.80 7.80 7.87 7.46 7.90 7.90 7.91	Spec. Cond. 4 (2 / cm) 0.245 D202 D20	162 207 207 223 223 223 223 225 225	(mg/L) 9,87 9,29 9,29 28,02 9,41 7,99 7,49 7,49 7,49 7,49 7,49 7,49 7,49	24.98 24.55 24.19 24.98 24.72 24.72 24.72 24.72 25.97 26.11 76.71 25.66	1099 AU 1419 AU 345 ATTA 935 352 348 230 1453 1463 1463	22.32 33.42 33.45 32.50 32.71 32.71 32.71 32.71	(mL/min) (300 (300 (300 (300 (300 (300 (300 (300 (300	(L) /200 /275 /350 /425 /425 /575 /65 /65 2100 72,25	
Time 46:20 46:40 46:40 46:40 46:40 46:40 9:00	PH (SU) 7.7% 7.7% 7.8(e 7.80 7.80 7.80 7.80 7.80 7.80 7.80 7.80	Spec. Cond. 4 (2 / cm) 0.245 D202 D20	162 202 207 223 223 223 223 223 225 225 225 225 225	(mg/L) 9,87 9,29 9,29 28,02 4,31 7,99 7,39 7,39 7,39 7,30 7,30 7,30 7,30 7,30 7,30 7,30 7,30	24.98 24.55 24.19 24.72 24.72 24.72 24.72 24.72 25.97 26.11 26.11 76.71	1099 AU 1419 AU 345 ATTA 355 3403 352 348 230 1403	22.32 33.42 53.45 32.50 32.71 32.71 32.71 32.71 32.84 72.4.1 22.72	(mL/min) (300 (300 (300 (300 (300 (300 (300 (300	(L) /200 /275 /350 /425 /425 /575 /65 /675 2/00	
Time 46:2_0 46:40 46:40 46:40 46:40 46:40 9:00 9:10 9:10 9:10 9:10 9:20 10:20 10:50	PH (SU) 7.7% 7.7% 7.8/2 7.80 7.80 7.80 7.80 7.80 7.90 7.90 7.91 8.00	Spec. Cond. 4 (2 / cm) 0.245 D202 D20	162 202 207 223 225 223 223 225 225 225 225 225 225	(mg/L) 9,87 9,29 4,25 9,29 4,29 7,41 7,99 7,41 7,99 7,41 7,99 7,41 7,99 7,41 7,99 7,41 7,99 7,41 7,99 7,41 7,99 7,41 7,02 4,01 0,12 0,12 0,12 0,12 0,12 0,12 0,12 0	24.98 24.55 24.19 24.38 24.72 24.72 24.72 25.97 26.11 76.71 25.66 26.50	1099 AU 1419 AU 345 ATTA 335 3423 352 3428 230 1453 1453 1453 1453 1453 1453 1453 1453	22.32 33.42 33.45 32.50 32.71 32.71 32.71 32.84 27.4.1 27.72 32.84 27.4.1 27.72	(mL/min) (300) (300 (300 (300) (300 (300) (300 (300) (300) (300) (300 (300) (30	(L) /200 /275 /350 /425 /425 /575 /656 /875 2100 7125 2100 7125 2450	
Time 46:20 46:40 46:40 46:40 46:40 46:40 9:60 9:70	PH (SU) 7.7% 7.7% 7.%0 7.%0 7.%0 7.%0 7.%0 7.%0	Spec. Cond. 4 (2 / cm) 0.245 D.207 D.707 D.707 0.707	162 202 207 223 223 223 223 223 225 225 225 238 238 238 238 238 238 238 238 238 238	(mg/L) 9,87 9,29 9,29 4,02 9,41 7,99 7,49 7,49 7,49 7,49 7,49 7,49 7,49	24.98 24.55 24.19 24.38 24.72 24.72 24.72 25.97 26.80 26.11 25.66 26.07 26.07 26.12	1099 AU 1419 AU 345 ATTA 335 3423 352 3428 230 1453 1453 1453 1453 1453 1453 1453 1453	22.32 33.42 53.45 32.50 32.71 32.71 32.71 32.71 32.84 72.4.1 72.71 32.84 72.4.1 72.71 32.74 32.74 32.74 32.74	(mL/min) (300) (300 (300 (300) (300 (300) (300 (300)	(L) /200 /275 /350 /425 /425 /575 /656 /875 2100 72,25 2450 2450 2450 3125	
Time 46:20 46:40 46:40 46:40 46:40 9:00 9	PH (SU) 7.7% 7.7% 7.%0 7.%0 7.%0 7.%0 7.%0 7.%0	Spec. Cond. 4 (2 / cm) 0.245 D.207 D.707 D.707 0.707	162 207 207 223 223 223 223 223 225 225 239 239 239 239 239 239 239 235	(mg/L) 9.87 9.29 9.29 4.02 4.02 9.41 7.99 7.49 7.49 7.49 7.49 7.49 7.49 7.49	24.98 24.55 24.19 24.35 24.19 24.72 24.72 25.97 26.80 26.11 25.66 26.07 26.07 26.17 26.17 26.77	1099 AU 1419 AU 345 ATTA 335 3423 352 3478 230 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 145 145 145 145 145 145 145 145	22.32 33.42 33.45 32.50 32.71 32.71 32.71 32.84 72.41 72.72 32.84 72.72 32.74 32.74 32.52 32.43 32.43	(mL/min) (300) (300 (300) (300 (300) (30) (300)	(L) /200 /275 /350 /425 /425 /425 /575 /656 /875 2100 7215 2450 2450 2455 2450 3125 3575	
Time 26:20 46:40 46:40 46:40 46:40 9:00 9	PH (SU) 7.78 7.86 7.80 7.80 7.80 7.80 7.80 7.90 7.90 7.90 7.90 7.91 8.00 7.91 8.00 7.91 8.00 7.91 7.40 7.63 7.60	Spec. Cond. 4 (2 / cm) D. 7 45 D. 7 57 D. 7	162 207 207 223 223 223 223 223 223 225 239 239 239 239 239 239 239 239 239 239	(mg/L) 9.87 9.29 9.29 4.02 7.99 7.41 7.99 7.49 7.49 7.49 7.49 7.49 7.49 7.49	24.98 24.55 24.19 24.58 24.72 25.97 26.30 26.11 25.66 26.07 26.12 26.12 26.12 26.12 26.12 26.12 26.12	1099 AU 1419 AU 345 ATTA 335 3423 352 348 230 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 145 230 1453 145 230 1453 145 230 1453 145 230 1453 145 230 1453 145 230 1453 145 230 1453 145 230 1453 145 230 1453 145 230 1453 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 230 230 230 230 230 230 230	22.32 33.42 53.45 52.50 32.71 32.71 32.71 32.71 32.71 32.74 32.74 32.74 32.74 32.74 32.74 32.52 32.43 32.41 32.12	(mL/min) (2300 (300) (300 (300 (300) (300 (300)	(L) /200 /275 /350 /425 /425 /575 /656 /875 2100 79,25 2450 2450 2450 3125 3575 Uo25	
Time 24:20 4:20 4:30 4:40 4:30 9:00 9:00 9:00 9:00 9:00 9:00 10:20	PH (SU) 7.78 7.86 7.80 7.80 7.80 7.80 7.80 7.80 7.90 7.90 7.90 7.90 7.90 7.91 8.00 7.91 8.00 7.91 8.00 7.91 8.00 7.91 7.40 7.40 7.63 7.60 7.63 7.60 7.63	Spec. Cond. 4 (2 / cm) D. 7 45 D. 7 57 D. 7	162 207 207 223 223 223 223 223 225 225 239 239 239 239 239 239 239 239 239 239	(mg/L) 9.87 9.29 9.29 9.29 9.02 9.31 7.99 7.49 7.49 7.49 7.49 7.49 9.01 9.42 4.02 4.02 4.02 4.02 4.02 7.43 4.02 7.43 4.25 9.29 7.29 7.29 7.29 7.29 7.29 7.29 7.29	24.98 24.55 24.19 24.58 24.72 25.97 26.30 26.11 25.66 26.50 26.02 26.02 26.12 26.12 26.12 26.12 26.12 26.12 26.12 26.12 26.12 26.12 26.12 26.12 26.12	1099 AU 1419 AU 345 ATTU 335 3423 352 348 230 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 1453 145 23,52 348 230 1453 145 23,52 348 230 1453 145 23,52 348 230 1453 145 23,52 348 230 1453 145 230 1453 145 230 1453 145 230 1453 1453 145 230 1453 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1453 1455 230 1453 1453 1455 230 1453 1453 1453 1455 230 1453 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 230 1453 1455 235 235 235 235 235 235 235 2	22.32 33.42 53.45 32.50 32.71 32.71 32.71 32.71 32.84 72.4.1 72.4.1 72.4.1 72.4.1 72.4.1 72.4.1 72.72 32.49 32.74 32.52 32.43 32.52 32.43	(mL/min) (2300) (2300 (2300) (2300 (2300) (2300) (2300 (2300) (230) (2300)	(L) /200 /275 /350 /425 /425 /575 /656 /875 2100 79,25 2450 2450 2450 3125 3575 4025 4025	Notes (Purge method, water clarity, odor, purate, issues with pump/well/weather/etc.)
Time 46:20 46:40 46:40 46:40 46:40 9:00 9:00 9:00 9:00 9:00 10:20 1	PH (SU) 7.78 7.80 7.80 7.80 7.80 7.80 7.80 7.80	Spec. Cond. 4 (2 / cm) D. 7 45 D. 7 57 D. 7	162 202 207 223 223 223 225 225 225 238 238 238 238 238 238 238 238	(mg/L) 9.87 9.29 9.29 4.02 4.02 7.99 7.49 7.49 7.49 7.49 7.49 7.49 7.49	24.98 24.55 24.19 24.36 24.72 25.97 26.11 76.71 25.66 26.07 26.07 26.17 26.17 26.17 26.77 76.77 76.77 76.77 76.77 76.77	1099 AVA 1419 AU 345 ATTU 935 352 348 230 1453 1453 1453 1453 1453 1453 1453 1453	22.32 33.42 53.45 32.50 32.71 32.71 32.71 32.71 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.52 32.43 32.41 32.72 32.43	(mL/min) (300) (300 (300 (300) (300) (300 (300) (300) (300 (300) (300) (300 (300) (30) (300)	(L) /200 /275 /350 /425 /425 /575 /650 /575 /650 /875 2100 79,25 2450 2450 3125 3575 4025 4025	
Time 46:20 46:40 46:40 46:40 46:40 9:60 9:70 9	PH (SU) 7.78 7.80 7.80 7.80 7.80 7.80 7.80 7.80	Spec. Cond. 4 (2 / cm) D. 7 45 D. 7 57 D. 7	162 202 207 223 223 223 225 225 225 225 238 238 238 238 238 238 238 238	(mg/L) 9.87 9.29 9.29 4.02 4.02 4.02 7.99 7.49 7.49 7.49 7.49 7.49 7.49 4.01 0.02 4.02 4.02 4.02 7.43 4.02 7.43 4.02 7.43 4.02 7.43 4.02 7.43 4.02 7.43 4.02 7.43 4.02 7.43 7.49 7.40 7.40 7.40 7.40 7.40 7.40 7.40 7.40	24.98 24.55 24.19 24.55 24.19 24.38 24.72 25.97 26.71 25.46 26.11 26.07 26.17 26.77 26.77 26.77 76.77 76.77 76.77 76.77 76.77 26.97 26.71 26.97 26.71 26.97 26.71 27 26.71 27 26.97 26.97 26.97 26.97 26.97 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 27 26.71 27 26.71 27 26.71 26.71 26.71 26.71 26.71 26.71 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 27 26.77 27 26.77 27 26.77 27 26.77 27 26.77 27 27 27 27 27 27 27 27 27 27 27 27 2	1099 AVA 1419 AU 345 ATTU 335 3423 352 348 230 1453 1455 1557 1559	22.32 33.42 53.45 32.50 32.71 37.51 32.77 32.84 72.4.1 72.4.1 72.71 32.84 32.74 32.74 32.74 32.74 32.74 32.74 32.52 32.43 32.41 32.12 72.34 32.51	(mL/min) (.2300 (.300)	(L) /200 /275 /350 /425 /425 /575 /65 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 7125 2/00 71275 /65 75 /65 75 2/00 71275 /65 75 75 75 75 75 75 75 75 75 7	
Time 46:20 46:40 46:40 46:40 46:40 9:00 9:00 9:00 9:00 9:00 10:20 1	PH (SU) 7.7% 7.7% 7.80 7.80 7.80 7.80 7.80 7.80 7.80 7.80	Spec. Cond. 4 (2 / cm) D. 7 45 D. 7 57 D. 7	162 202 207 223 223 223 225 225 225 238 238 238 238 238 238 238 238	(mg/L) 9.87 9.29 9.29 4.02 4.02 7.99 7.49 7.49 7.49 7.49 7.49 7.49 7.49	24.98 24.55 24.19 24.55 24.19 24.38 24.72 25.97 26.71 25.46 26.11 26.07 26.17 26.77 26.77 26.77 76.77 76.77 76.77 76.77 76.77 26.97 26.71 26.97 26.71 26.97 26.71 27 26.71 27 26.97 26.97 26.97 26.97 26.97 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 26.71 27 26.71 27 26.71 27 26.71 26.71 26.71 26.71 26.71 26.71 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 26.77 27 26.77 27 26.77 27 26.77 27 26.77 27 26.77 27 26.77 27 27 27 27 27 27 27 27 27 27 27 27 2	1099 AVA 1419 AU 345 ATTU 935 352 348 230 1453 1453 1453 1453 1453 1453 1453 1453	22.32 33.42 53.45 32.50 32.71 32.71 32.71 32.71 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.74 32.52 32.43 32.41 32.72 32.43	(mL/min) (300) (300 (300 (300) (300) (300 (300) (300) (300 (300) (300) (300 (300) (30) (300)	(L) /200 /275 /350 /425 /425 /575 /650 /575 /650 /875 2100 79,25 2450 2450 3125 3575 4025 4025	

Net Pack Crise Location: Marcuil (. Ich Field Personal Name: Dather Vell 10 * MAN - DT Pump Type/Model: Marcuil (. Ich Field Personal Name: Dather Depth to Water (fi): 4.33 Tobis Marcuil (. Ich Pump Type/Model: Marcuil (. Ich Field Personal Name: Dather Well Volume (gal) = 0014 dp: 3.07 Tobis Marcuil (. Ich Tables Marcuil (. Ich Field Personal Name: Dather Well Volume (gal) = 0014 dp: 3.07 Tobis Marcuil (. Ich Tables Marcuil (. Ich Tables Marcuil (. Ich Well Volume (gal) = 0014 dp: 3.07 Tobis Marcuil (. Ich Tables Marcuil (. Ich Tables Marcuil (. Ich Well Volume (gal) = 0014 dp: Societ Um Societ Um Societ Um Societ Um Well Type: Tobis Marcuil (. Ich Tables Marcuil (. Ich) Tables Marcuil (. Ich) Tables Marcuil (. Ich) Yell Deci Marcuil (. Ich) No Replace Tables Marcuil (. Ich) Dots (Parge method, water clarity, or tac, issues with pump/well/weath Yell Deci Marcuil (. Ich) No No No Parged Volum: Notes (Parge method, water clarity, or tac, issues with pump/well/weath Yell Decis Societ (. Ich) Yociet (. Ich)	Client	VI. 11	CCPC				Project No.:	GWKK	36	_	Development Date: 5/17/22
Well ID: Avel - D* Total Depth (0) (after purge): 9.33 Depth to Water (ft): 9.33 Well Diameter (in) 3.07 Well Volume (ab) = 0.04 d, b; 3.07 Mell Diameter (in) 3.07 Well Volume (b) = 0.04 d, b; 3.07 Mell Volume (b) = 0.04 d, b; 5.07 Mell Volume (b) = 0.04 d, b; 5.07 Mell States: Yes Well States: Yes Well States: Yes Yes No Well States: Yes Yes Yes Yes No Yes Yes Yes<				rise						_	Field Personnel Name: Dalton Ke
Total Depth (II) (after purge) Yes	2										
Depth to Water (ft): Image: Signal Signa	Total Depth (ft) (after				4		Tubing Material:	Poivethe	ene	_	
Well Diameter (in): 2 Start/Stop Purge Time: 12:45 13:45 Well Volume (L) = gal * 37.85: II. (L.G.S. Purge Rate (nL/min): 4000 Well Volume (L) = gal * 37.85: II. (L.G.S. Purge Rate (nL/min): 4000 Well Volume (L) = gal * 37.85: II. (L.G.S. Purge Rate (nL/min): 4000 Well Volume (L): Fush function Fush function 4000 Well Volume (L): Fush function Fush function Fush function Well Volume (L): Fush function Fush function Fush function Well Condition: Fush function Fush function Fush function Fush function Well Tage Present: Yes Fush function Fush function Fush function Fush function Time pl (SU) Step Condition: Fush function Fush function Fush function Fush function Time pl (SU) Step Condition: Fush function Fush function Fush function Fush function Time pl (SU) Step Condition: Fush function Fush function Fush function Fush function Fush function Time<			8.33			Pu				-	
Well Volume (ga) = 0.041d; h: 3.07 Purge Rate (mL/min): You Well Volume (L) = gal * 3.785; 11.6.3 Total Purge Volume (L) 52 d = well diameter (mckes); h = length of water column (feet); Well Volume (L) 52 Well Volume (mckes); h = length of water column (feet); Well Volume (mckes); h = length of water column (feet); Well Volume (mckes); h = length of water column (feet); Well Lock Yets No Replace Well Tage Presen: Yes No Time pH (SU) Step Cond, ORP (mV) DO (mg(1), Temp. (*C) Turbidity (NTUs) DTW (ft boo Purge Rate (mL/min): Notes (Purge method, water clarity, o rate, issues with pump/well/weath (L) 17:05 51:35 0:32:1 74:35 24:41 51:7 24:631 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24:641 51:7 24		1.00	2			s	tart/Stop Purge Time:			-	
Total Purge Volume (L)		.041d h:	3.0	7						-	
d = well diameter (inclus); h = length of water column (feet) Well Type: Flush Suck U Well Lock: Yes No Well Cap Condition: Good Replace Well Tag Presen: Yes No Yes No DO (mg/m) Temp. (%C) Turbidity (NTUs) DTW (ft bloc) Purge Rate (nL/min) Notes (Purge method, water clarity, o rate, issues with pump/well/weath (L) Ymme PH (SU) Stype Cond (ms/m) ORP (mV) DO (mg/m) Temp. (%C) Turbidity (NTUs) DTW (ft bloc) Purge Rate (nL/min) Notes (Purge method, water clarity, o rate, issues with pump/well/weath (L) Ymme PH (SU) Stype Cond (ms/m) ORP (mV) DO (mg/m) Temp. (%C) Turbidity (NTUs) DTW (ft bloc) Purge Rate (nL/min) Notes (Purge method, water clarity, o rate, issues with pump/well/weath (L) Ymme PH (SU) Stype Cond Stype Co		Z 58									
Well Type: Flush Stack UP Well Lock: Yes No Well Cap Condition: Replace Well Type: Yes No Replace Spsc. Cond. ORP (mV) DO (mg/L) Temp. (°C) Turbidity (NTUs) DTW (ft btoc) Purge Rate (ml.min) Purge Rate (L) Notes (Purge method, water clarify, or rate, issues with pump/well/weath Time Pfl (SU) Spsc. Cond. (mg/L) ORP (mV) DO (mg/L) Temp. (°C) Turbidity (NTUs) DTW (ft btoc) Purge Rate (ml.min) Purge Q Volume (L) Notes (Purge method, water clarify, or rate, issues with pump/well/weath 172: 55 57: 32 57: 32 77: 32 72: 63: 32 23: 32 24: 4 49: 00 34: 4 13: 15 41:32 53: 72 74: 55: 72 74: 72 74: 74 <th74: 74<="" th=""> <th74: 74<="" th=""> 74: 74</th74:></th74:>							5				
Well Lock: Yis No Well Cap Condition: Good Replace Well Tag Present: Yes No Time pH (8U) Size Cond. (mL/min) ORP (mV) DO (mg/L) Temp. (°C) Turbidity (NTUs) DTW (ft broc) Purge Rate (mL/min) Purge Ato (mL/min) Notes (Purge method, water clarity, o rate, issues with pump/well/weath (L) rates 12:45 70,42 72.91 -12.2 7.665 27.70 Over a tope 52.33 67.900 0 rate, issues with pump/well/weath 13:05 41.30 0.32.52 57.71 2.665 27.82 27.82 24.24 49.00 54.4 4 -		and the second		0000							
Well Cap Condition: Good Replace Well Tag Present: Yes No Time pH (SU) Sigs Cond. Green) ORP (mV) DO (mg/L) Temp. (°C) Turbidity (NTUs) DTW (ft bloc) Purge Rate (mL/min) Purge Volum (L) Notes (Purge method, water clarity, o rate, issues with pump/well/weath 12:55 5:25 5:25 7:22 7:45 2:4:31 0.12:25 7:45 2:4:41 57:7 2:4:32 2:5:42 5*** 2:4:4 13:1:25 4:2:32 5:7 7:4:55 2:5:27 7:4:55 19:27 19:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00 3:4:4 40:00		-									
Well Tag Present: Yes Notes ORP (mV) DO (mg/L) Temp. (°C) Turbidity (NTUs) DTW (ft btoo) Purge Rate (mL/min) Purge Volume (L) Notes (Purge method, water clarity, o rate, issues with pump/well/weath (mL/min) 12:45 5/4:35 5/3:2-1 -1/2-2 7.455 2/4:5 3/3 4/300 0 13:05 4:31 0.32:25 5.7 7.455 2/4:51 57.7 2/4:52 5/9 2/4 - 13:05 4:31 0.32:25 5.7 7.455 2/4:51 57.7 2/4:52 5/9 2/4 -	(1117								
Time pH (8U) SEC Cond. (m/min) ORP (mV) DO (mg/L) Temp. (°C) Turbidity (NTUs) DTW (ft btoc) Purge Rate (mL/min) Purge Volume (L) Notes (Purge method, water clarity, o rate, issues with pump/well/weath (L) 172:55 5:35 0:3-27 7:45 27:70 Over 4:002 3:53 0:3-27 7:45 2:5:32 5:62 0 13:05 1:3:1 0:3-27 7:455 2:6:31 57.7 2:6:32 5:62 5:62 0 13:15 4:79 0:3-27 7:455 2:6:71 2:6:72 1/2:72 2/6:72 1/2:72 2/6:74 1/2:7 2/6:74 1/2:7 2/6:74 1/2:7 2/6:74 1/2:7 2/6:74 1/2:7 2/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:72 1/6:74 1/2:74 1/6:74 1/2:74 1			-								
Time pH (SU) Water (SU) ORP (mV) Temp. (°C) Turbidity (NTUs) DTW (ft btee) (mL/min) "(L) rate, issues with pump/well/weath 12:45 75, YZ 02.92 -12.2 7.65 27.70 Over 40.06 53.3 67.800 0 12:55 76.35 03.32 YB 5.4V 75.8V Over 40.06 25.82 570 2.4 - <td< th=""><th>Well Tag Present:</th><th>Yes C</th><th></th><th></th><th></th><th>-</th><th></th><th></th><th></th><th></th><th>Notes (Durgs mothed water electity ador pu</th></td<>	Well Tag Present:	Yes C				-					Notes (Durgs mothed water electity ador pu
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Time	pH (SU)	Spec. Cond.	ORP (mV)		Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)			rate, issues with pump/well/weather/etc.)
$12i \leq 5$ 9.35 0.327 478 5.44 28.44 $0.4ccode$ 25.82 57 24_{0} $13:05$ 4.31 0.325 57 7.55 24.51 57.7 24.34 400 34_{0} 54_{0} $13:15$ 4.79 0.321 53 7.43 26.43 14.4 24.14 400 40 $13:15$ 4.79 0.321 53 7.42 15.27 12.42 400 40 $13:15$ 4.26 0.322 51 1.74 15.27 16.444 400 44 $12:35$ 6.41 0.321 15 12.72 24.12 400 44 $13:45$ 0.323 47 7.87 24.90 9.04 120.32 400 52 $13:45$ 0.323 47 7.87 24.90 9.04 120.32 400 52 $13:45$ 0.323 47 7.87 24.90 52 52 52 52 52	12:45	4.42		-122		29.70	Overande	4.33	usoo		
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13:25 42.23 7.323 ci 5.42 15.25 12.72 26.12 900 44 12:35 49.41 60.377 35 7.714 16.27 16.944 900 4% 13:45 60.323 0.733 49 7.87 74.96 9.04 20.32 920 52 13:45 60.323 0.733 49 7.87 74.96 9.04 20.32 920 52 13:45 60.323 0.733 49 7.87 74.96 9.04 20.32 920 52 13:45 60.323 0.733 49 7.87 74.96 9.04 20.32 920 52 14 14 14.96		4.31									2
12:35 4.41 0.317 33 7.74 25.27 10.44 26.18 4.60 448 13:45 0.733 49 7.87 24.90 9.04 20.32 400 52 13:45 0.733 49 7.87 24.90 9.04 20.32 400 52 13:45 0.733 49 7.87 24.90 9.04 20.32 400 52 13:45 0.733 49 7.87 24.90 9.04 20.32 400 52 13:45 0.733 49 7.87 24.90 9.04 20.32 400 52 13:45 0.733 49 7.87 24.90 9.04 20.32 400 52 13:45 0.733 49 14 14 10 14 100 14 14 14 14 14 14 14 16 14 16 16 14 14 14 14 14 14 16 16 16 16 16 14						The second se			400		
13: 4S 6:73 4q 7.82 24.96 9.04 20.32 400 52 1 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>12.2</td><td></td><td></td><td></td><td></td></t<>							12.2				
Image Image <th< td=""><td></td><td>4.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		4.									
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Stabilizing Criteria +/- 0.1 SU +/- 5% 0.2 mg/L or 10% for DO > 0.3 mg/L <5 NTUs											

					WE	LL DEVELOPMEN	r log sheet			
Client:		CKPC					GW4663		_	Development Date: 5/17/22
Site:		Plant C	risp			Location:	Warwic	K, GA	_	Field Personnel Name: Dalton Keele
Well ID:		MW-D	R'			Pump Type/Model:	Hurric	ane		
Fotal Depth (ft) (after	purge):	27.7				Tubing Material:	Polveth	wiene		
Depth to Water (ft):		4.43			Pi	ump Intake Depth (ft):	27	-5		
Well Diameter (in):		2			S	start/Stop Purge Time:	15:00/11	:20		
Well Volume (gal) = 0	041d h:	3.1	7		1.0	Purge Rate (mL/min):			_	
Well Volume (L) = ga	2	11.90			-	otal Purge Volume (L)	1 4 4	5	_	
l = well diameter (inc						100 100 100 Million				
	Flush	Stick Up	mn (Jeel)							
Well Type: Well Lock:	-	HICK OD								
	Yes	NO								
Well Cap Condition:	Good	Replace								
Well Tag Present:	Yes (No								
Time	pH (SU)	Spec Cond.	ORP (mV)	DO (mg/L)	Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)	Purge Rate (mL/min)	Purged Volume (L)	Notes (Purge method, water clarity, odor, purge rate, issues with pump/well/weather/etc.)
1500	46.60	0.25Ce	-4	4.90	27.46	Overanpe	5.43	1300	0	
1510	4.63	0.256	160	7.46	24.67	2625 AU	26.41	500	20	
1420	4.56	0.249	1500	7.58	25.99	49.0	26.91	500	24	Sucred
1530	40.55	0.312	225	7.04	24.83	144 Z AU	26.72 26.84	500	32	Juipeu
1540	4.54	0326	135	4.33	25.00	17.7	26.95	500	36	
1550	8.43	0.332		7.51	25.02	5.10	27.01	500	40	
1600	9.42	0.33	163	7.39	24.37	3.27	27.09	500	44	
11070	4.43	0.344	(36	7.70	24.27	2.79	27.04	500	46	
1000	242	0.277		-	-		- if the			
6				-	V					
					1-					
					ļ				-	
/				· · · · · ·						
Stabilizing Criteria	+/- 0.1 SU	+/- 5%		0.2 mg/L or 10% for DO > 0.5 mg/L		< 5 NTUs				

Ceosyntec ^D consultants					WE	LL DEVELOPMEN	r log sheet				
Client:		629	C			Project No.:	1-12843	6		Development Date: 5/14	122
Site:		Plent	Crisp			Location:	Marwin	ck (+		Field Personnel Name: Dank	on Keen
Well ID:		MW-5				Pump Type/Model:					
Total Depth (ft) (after	purge):	27.3				Tubing Material:					
Depth to Water (ft):	r0-7	4.(9			P	ump Intake Depth (ft):	27'				
Well Diameter (in):	1. 1	7				Start/Stop Purge Time:	<1:45/1-	1.25			
Vell Volume (gal) = 0	041d b:	3,0	7			Purge Rate (mL/min):	200/4		-2		
	4	 [].6				otal Purge Volume (L)			-3		
Vell Volume (L) = ga					10	otal Purge Volume (L)	24		-		
d = well diameter (incl		-	ımn (feet)								
Well Type:	-	Stick Up									
Well Lock:	Yes	No									
Well Cap Condition:	Good	Replace									
Vell Tag Present:	Yes	No						12			
Time	pH (SU)	Spec. Cond.	ORP (mV)	DO (mg/L)	Temp. (°C)	Turbidity (NTUs)	DTW (ft btoc)	Purge Rate (mL/min)	Purged Volume (L)	Notes (Purge method, water clari rate, issues with pump/well/w	
	4.53	0.257	76	9.51	22.15	845AU	4.61	6300	0		
4:55	4.49	D.256	74	4.05	22.41	Overange	74.91	500	27	Dry Recharge	
10:20	4.52	226	74	10.82	22.81	0.000000	22.51	01000	27	Dry Recharge	
10:20	4.57	0.750		2.94	23.36	Overange 3014 ALA	26.97	YOO	37		
10:40	4.1.0	0.250	127	7.34	24.72		2492	400	40		
10:50	4.63	0,253	126	7.21	25.99	42.2	2094	400	44		
11:00		0.257	129	7.42	75.42	47.3	24.95	400	48	Palana	
				- 10	24		711 01		11/1	Dry Recharge	
11:45	4.61	0,243	90	7.82	25.01	Jol.9	24.01	400 400	48		
11:55	46.64	0.250	115	6.77	27,02	69.7	27.98	200	54		
12:05	3.60		MU	7.91	79.41	10.91	24,99	200	36		
12:23	44		127	779	29.97	9.47	26.93	200	58		
12.23		0.63	100	1 chil				-			
8				TK							
				DR							
3											
Stabilizing Criteria	+/- 0.1 SU	+/- 5%		0.2 mg/L or 10% for DO > 0.5 mg/L		< 5 NTUs					
Seature Criteria		., .,.		(whichever is greater)					(2		