VOLUNTARY COMPLIANCE STATUS REPORT FORMER VULCAN PERFORMANCE CHEMICALS DALTON PLANT

by

Haley & Aldrich, Inc. Greenville, South Carolina

for

Legacy Vulcan Corp. Birmingham, Alabama

File No. 37848-007 15 August 2014



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Georgia Environmental Protection Division Response & Remediation Program 2 Martin Luther King Jr. Drive, SE Suite 1054 Atlanta, Georgia 30334

Attention: Mr. Kevin Collins, Geologist

Subject: Voluntary Compliance Status Report Former Vulcan Performance Chemicals Dalton Plant HSI Site No. 10770

Dear Mr. Collins:

On behalf of Legacy Vulcan Corp. (LVC), Haley & Aldrich, Inc. is submitting this letter and accompanying report for the former Vulcan Performance Chemicals Dalton Plant (Hazardous Site Inventory No. 10770). Enclosed are an original and two (2) CD-ROM copies of the Voluntary Remediation Program Compliance Status Report (CSR). This CSR summarizes the existing groundwater conditions on the subject property and is submitted in lieu of the Third Annual Progress Report and completes the Voluntary Remediation Program corrective action process per the application approved on July 31, 2012.

As stated in the VRP Application, submitted to EPD on 27 January 2012, delineation and remediation at the property is complete. There are no chemicals of concern in soil and the one chemical of concern identified in groundwater (lead) is now below the maximum contaminant level. In general, lead concentrations in groundwater steadily declined following remedial activities in 2008, and, beginning in 2011, lead was reported below the MCL in samples collected from all wells, except MW-21. For the two most recent sampling events, analytical reports of samples collected from MW-21 have included results below the MCL of 0.015 mg/l. As discussed in the meeting with EPD on March 18, 2014, the duplicate sample collected from MW-21 in April 2013, had a reported concentration of lead below the MCL. In April 2014, the annual monitoring was conducted and the analytical report of the sample collected from MW-21 confirmed lead is no longer present in groundwater above the MCL. (Table IV of the attached report)

On behalf of LVC, Haley & Aldrich respectfully requests the EPD delist this site from the Hazardous Site Inventory. If you have any questions regarding this CSR, please contact Carleton Degges/LVC at (205) 298-3063 or myself at (864) 214-8754.

Georgia Environmental Protection Division 15 August 2014 Page 2

Sincerely yours, HALEY & ALDRICH, INC.

Daniel E. McDonnell, P.G. Senior Project Manager

Enclosures

c: Douglas E. Cloud – Kazmarek Mowrey Cloud Laseter LLP Carleton Degges – LVC



COMPLIANCE STATUS CERTIFICATION

I certify under penalty of law that this report and all attachments were prepared under my direction in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Based on my review of the findings of this report with respect to the risk reduction standards of the Rules for Hazardous Site Response, Rule 391-3-19-.07, I have determined that this site/property is in compliance with Type 1 risk reduction standards.

[NAME]

8 114/14

Senior Vice President [TITLE]



PROFESSIONAL GEOLOGIST CERTIFICATION

I certify that I am a qualified groundwater scientist who has received a post-graduate degree in the natural sciences, and have sufficient training and experience in groundwater hydrology and related fields, as demonstrated by state registration and completion of accredited university courses that enable me to make sound professional judgments regarding groundwater monitoring and contaminant fate and transport. I further certify that this Compliance Status Report prepared for Legacy Vulcan Corp. for the former Vulcan Performance Chemicals site, located in Dalton, Georgia, was prepared by myself and appropriate qualified subordinates working under my direction.

McDONNIEL NHELE. M Date Daniel E. McDonnell, P.G. Georgia Professional Geologist Registration * GEORGIA NEGISIE RED 12190 No.PG00208



PRO LIST			i ii iv iv
1.	INTE	RODUCTION	1
	1.1	Objective	1
	1.2	CSR Format	1
2.	FAC	ILITY HISTORY AND PREVIOUS INVESTIGATIONS	2
	2.1	Previous Investigations	2
	2.2	Hydrogeologic Setting	3
	2.3	Source Description	4
	2.4	Extent of Lead in Groundwater	5
3.	HYD	ROGEOLOGIC FRAMEWORK	6
	3.1	Geochemistry	6
		3.1.1 Cation Exchange Capacity	6
		3.1.2 Geochemical Modeling	7
	3.2	Lead Fate and Transport	8
4.	IDEN	TIFICATION OF POTENTIAL RECEPTORS	9
	4.1	Potential Receptors and Exposure Pathways	9
		4.1.1 Environmental Media	9
		4.1.2 Exposure Pathways and Potential Human Receptors	9
		4.1.3 Exposure Pathways and Potential Ecological Receptors	10
	4.2	Point of Exposure and Point of Demonstration Well	10
5.	RISK	K REDUCTION STANDARDS (RRS)	11
6.	SUM	MARY	12

TABLES FIGURES APPENDIX A – Analytical Summary Documents (September 2006) APPENDIX B – Groundwater Sampling Field Notes (April 2014) APPENDIX C – Laboratory Analytical Reports (April 2014)



Page

LIST OF TABLES

Table No.	Title
Ι	Water Level Elevations - April 8, 2014
II	Groundwater Sampling Results - April 2014
III	Summary of Lead Concentrations in Groundwater (1996 - 2007)
IV	Summary of Lead Concentrations in Groundwater (2008 - 2014)

LIST OF FIGURES

Figure No.	Title
1	Site Location Map
2	Monitoring Well Locations
3	Water Table Configuration and Lead Concentration
4	Cross-Sections A - A', B - B'
5	pH vs. Eh Diagram



1. INTRODUCTION

This Voluntary Compliance Status Report (CSR) for the former Vulcan Performance Chemicals Dalton Plant (Hazardous Site Inventory #10770, the Site) is submitted by Haley & Aldrich, Inc. (Haley & Aldrich) on behalf of Legacy Vulcan Corp. (LVC). The Georgia Environmental Protection Division (EPD) formally accepted LVC as a participant in the Georgia Voluntary Remediation Program (VRP) for this qualifying property in the letter dated 31 July 2012.

1.1 Objective

The objective of this CSR is to confirm and document consistency of corrective actions with the provisions, purposes, standards, and policies of the VRP, and to certify compliance of the property with the applicable cleanup standards. The CSR summarizes data obtained from investigations that have been completed since the CSR Addendum was submitted by CH2MHill in November 2008.

1.2 CSR Format

Consistent with EPD Guidance, the format and content of this CSR is as follows:

- **1. Introduction** General introduction to the report and statement of the objective.
- 2. Facility History and Previous Investigation Description of the Site and facility ownership including a summary of previous investigations, hydrogeologic setting, source description, and extent of lead in groundwater.
- **3. Hydrogeologic Framework** Summary of fate and transport of lead in groundwater, including the results of geochemical modeling.
- **4. Identification of Potential Receptors** Discussion of potential receptors and exposure pathways, including point of exposure and point of demonstration.
- 5. **Risk Reduction Standards (RRS)** Comparison of the Type I RRS to current conditions, including certification of compliance with the RRS.
- **6. Summary** Summary of documented findings.



2. FACILITY HISTORY AND PREVIOUS INVESTIGATIONS

The facility was initially developed and owned by Mayo Chemical Company and operated under the name Farm and Industrial Chemical Company. Mayo sold the facility to a business unit of LVC in 1996. In 2003, Lynx Chemical Group purchased the facility and in July 2007, the facility was sold to Harcros Chemicals Inc. (Harcros). The Site continues to be used as a chemical manufacturing facility operated by Harcros.

Harcros' address is as follows:

Harcros Chemicals Inc. 134 Phelps Rd. SE Dalton, GA 30720

The Site is comprised of approximately 27-acres and is located at 134 Phelps Road in the City of Dalton, Whitfield County, Georgia (Figure 1). The Site is bordered to the north by Corporate Drive, to the east by railroad tracks, to the south by undeveloped land, and to the west by South Dixie Road. The Site is zoned for heavy manufacturing and is surrounded by properties that are zoned for either heavy manufacturing or general commercial.

The active manufacturing area of the on-Site facility is located in the northeastern portion of the property and consists of an office building, a maintenance building, warehouses, manufacturing buildings, aboveground tank farms, and two pretreatment lagoons. The developed portion of the property is fenced and access is restricted.

2.1 **Previous Investigations**

The Site underwent a Comprehensive Environmental Response, Compensation, and Liability Information System (CERCLIS) Preliminary Assessment in 1987. Beginning in 1996, environmental assessments associated with property transactions were conducted. Details of the environmental assessments were described in the 2008 CSR Addendum.

Lead was detected at a concentration of 0.044 milligrams per liter (mg/L), which was greater than the Hazardous Site Response Act (HSRA) notification concentration of 0.015 mg/L. A Release Notification was submitted to EPD in June 2003 for lead in groundwater. Based on the Release Notification, the Site was listed on the Hazardous Site Inventory (HSI) in September 2003. EPD notified Lynx Chemical Group LLC of the listing and cited the presence of lead, nickel, and beryllium in groundwater at concentrations above the HSRA notification levels. However, the groundwater pathway score that resulted in the Site being listed was based on the evaluation of lead.

Additional soil and groundwater investigations were conducted in 2006 to support development of a HSRA Corrective Action Plan. In 2006, 14 soil samples were collected at eight boring locations and three new (temporary) monitoring wells were installed and sampled along with four existing monitoring wells. The results of this work were summarized in a report submitted to EPD on 7 September 2006. The summary tables from the September 2006 submittal are included in Appendix A. These summary tables provide a comprehensive overview of metals concentrations in soil and groundwater samples collected onsite from 1996 through 2006. The corresponding data point location map for these samples, also from the September 2006 report, is included in Appendix A.



A HSRA CSR was submitted to EPD on 31 July 2007. An interim corrective action/excavation was completed in July 2008 (information is provided in Section 2.3 of this CSR). Monitoring wells that were abandoned during excavation activities were replaced with MW-17, MW-18, MW-19, and MW-20 in 2008. A CSR Addendum, which included a summary of the interim corrective action, was submitted to EPD on 11 November 2008. That submittal concluded that the Site was in compliance with applicable RRSs for soil but not in compliance with the applicable RRS for lead in groundwater.

Routine groundwater monitoring has been ongoing since 2008. Two monitoring wells were installed in August 2011 to replace destroyed/abandoned wells MW-12 and MW-3D. The replacement wells were designated MW-22D and MW-23 and were installed at the locations shown on Figure 2 to monitor the extent of lead in groundwater. Monitoring well MW-22D was installed adjacent to MW-21 (the only well at the time where lead was detected above RRS) to a depth of approximately 37 feet below ground surface (bgs), 19 feet below auger refusal, to provide vertical delineation data.

Groundwater monitoring results were documented in Annual Reports submitted on 29 October 2009, 29 November 2010, and 30 November 2011. An application requesting that the Site be entered into the VRP was submitted to the EPD on 27 January 2012. EPD reviewed the applications and in a letter dated 31 July 2012 formally approved the application and accepted the Site into the VRP. The approval letter provided a schedule for semi-annual sampling and progress reporting. In January 2013, EPD agreed to reduce the monitoring and reporting frequency from semi-annual to annual.

The first Annual Progress Report was submitted in January 2013 and included a discussion of the analytical results from samples collected in April 2012. A second Annual Progress Report was submitted in January 2014, focusing on the April 2013 sampling event. In accordance with the approved VRP application, the April 2013 groundwater monitoring event included sample collection at monitoring wells MW-19, MW-21, and MW-23, with laboratory analysis for lead.

Groundwater samples were most recently collected in April 2014 and the results are included in this CSR. As in other events, samples were collected using low-flow methods. Prior to sample collection, water levels and field parameters, including pH, temperature, conductivity, turbidity, dissolved oxygen, and oxidation-reduction potential (ORP), were measured and recorded on purge logs (provided in Appendix B). Groundwater samples were submitted to Analytical Environmental Services, Inc. and analyzed for lead by EPA Method 6010C. The analytical results are discussed in Section 2.4 and the laboratory analytical reports are provided in Appendix C.

2.2 Hydrogeologic Setting

The Site is situated in a valley within the Valley and Ridge Physiographic Province. The predominant rocks in the area of the Site are shale and limestone/dolomite of the Conasauga Group (Cambrian). The residual soils present in this area were formed by normal chemical and physical weathering of the parent rock types and are referred to as saprolite. The typical saprolite soil profile consists of clayey soils near the ground surface, transitioning to sandy silts and silty sands that typically contain increasing amounts of rock fragments (shale and limestone) with depth. Depth to the top of rock varies at the Site but generally occurs between 10 and 20 feet. Zones of gravel-sized, partially weathered rock have been observed distributed throughout the otherwise predominantly silty material.

Groundwater occurs under unconfined conditions in the overburden. Although appreciable amounts of groundwater may occur in the limestone/dolomite bedrock units, there is generally minimal flow. Within the water table aquifer, the direction of groundwater flow is controlled by the local topography:



recharge occurs in upland areas with discharge to surface water. Flow within the bedrock (especially the limestone/dolomite units) is controlled to a large degree by fracture systems with recharge of the bedrock units originating from the overlying saprolite.

The developed portion of the Site is relatively flat, with a slight topographic gradient to the south and west. Site surface water includes a stream in the northwest corner of the Site. The stream flows off-Site along the southern boundary of the property.

Groundwater monitoring has been performed at the Site since 1996 with regularly scheduled routine groundwater monitoring events occurring since 2008. A potentiometric surface map based on water level data from the most recent sampling event (April 2014) is included as Figure 3. A summary of April 2014 water level elevations is provided in Table I. Based on these water level data, groundwater flow at the Site is interpreted to be to the south and west.

Hydrogeologic cross sections depicting subsurface hydrogeologic conditions are shown in Figure 4. Cross-section A-A', in Figure 4, is oriented along the groundwater flow path through the area excavated in July 2008. Cross section B-B', in Figure 4, is oriented perpendicular to the flow path, also through the excavated area.

The hydraulic conductivity of the shallow aquifer has been estimated from slug tests conducted at several monitoring wells. The results indicate that the hydraulic conductivity of the shallow aquifer ranges from approximately 1.5×10^{-4} centimeters per second (cm/sec) in silty material to approximately 2.2×10^{-2} cm/sec at wells where gravel zones were encountered. Hydraulic conductivity in bedrock is approximately 1.2×10^{-2} cm/sec. Based on these measurements, estimated values of groundwater flow velocity at the Site range from 11 feet per year (ft/yr) in saprolite to 800 ft/yr in bedrock and more than 1,000 ft/yr in saprolite where zones of gravel are present.

2.3 Source Description

Concentrations of lead in groundwater above the Type 1 RRS were documented at the Site; however, there are no known releases of lead or lead-containing substances. Personnel of a previous Site owner recalled a release of sodium hydroxide, many years ago, that caused a localized, elevated pH in groundwater. The resulting change in geochemical conditions likely induced mobilization of naturally-occurring lead from native soil to groundwater.

The conclusion that lead in groundwater originated from naturally-occurring lead in soil is supported by multiple lines of evidence including analytical results obtained from soil samples taken from borings across the Site, where the average concentration of lead was 12.3 milligrams per kilogram (mg/kg). This average value is consistent with regional studies for Georgia, which reports an average background soil range of lead from 10.3 to 18.7 mg/kg (USGS, 2001¹). In addition, lead was present in groundwater samples collected during the early phases of the investigation at levels above the RRS in a localized area, defined by monitoring wells MW-1, TMW-12, TMW-13, and TMW-14 (these wells have since been abandoned but their locations are shown on the map included in Appendix A).

Following discovery of the elevated groundwater pH, personnel of a previous Site owner reportedly introduced sodium bicarbonate to the subsurface as a buffering agent to neutralize the pH. The

¹ USGS, 2001. Geochemical Landscapes of the Conterminous United States - New Map Presentations for 22 Elements. N. Gustavsson, B. Bølviken, D.B. Smith, and R.C. Severson. U.S. Geological Survey Professional Paper 1648. U.S. Department of the Interior, U.S. Geological Survey. November, 2001.



application of sodium bicarbonate was successful in neutralizing the pH; however, it did not correct all of the geochemical conditions responsible for lead concentrations above the Type 1 RRS in groundwater. Previous soil sampling conducted in this area did not identify a source of lead or exceedances of soil cleanup standards. This appears to verify the report of a sodium hydroxide release as described above, and not of a chemical release containing lead.

To eliminate concerns regarding an ongoing release or a buried source of lead, an interim corrective action was completed in 2008 in the area of the sodium hydroxide release. The interim corrective action consisted of an excavation to a depth of 15 feet bgs at which point bedrock was encountered. Excavated soil was transported directly from the excavation to dump trucks and then transported to the Old Dixie Sanitary Landfill in Whitfield County. In an effort to enhance attenuation of lead in groundwater, a soil amendment (Enviroblend[®]) was added between layers of backfill up to the approximate depth of the water table.

Groundwater sampling conducted later in 2008, indicated lead was present in groundwater above the Type 1 RRS within the excavation area, but only at MW-19. Samples from a downgradient monitoring well installed later in 2008 (MW-21, located approximately 200 feet downgradient from the excavated area) also exceeded the Type 1 RRS for lead.

2.4 Extent of Lead in Groundwater

Analytical results for samples collected in April 2014 are summarized in Table II. Lead was not present above the laboratory detection limit (0.010 mg/L) in any of the samples. The historical concentrations of lead in groundwater samples collected at the Site are summarized in Tables III and IV Lead concentrations are also included on both the potentiometric surface map (Figure 3) and the hydrogeological cross-sections (Figure 4).

The observations and trends in lead concentrations support the conclusion that lead in groundwater, above the MCL, was caused by a change in geochemical conditions following the subsurface introduction of sodium compounds that resulted in an ion exchange of naturally occurring lead from soil, at an elevated pH (a detailed discussion is provided in the following sections). The data support that lead concentrations have attenuated due to natural subsurface geochemical conditions that were enhanced by the application of a soil amendment during the interim corrective action, conducted in 2008. As a result of these processes, analytical results of collected groundwater samples no longer report detections of lead above the Type I RRS.



3. HYDROGEOLOGIC FRAMEWORK

As presented in the VRP Application, a Conceptual Site Model (CSM) developed for the Site portrays the environmental system, including the physical, chemical, and biological processes that affect the source, transport, and fate of lead through the subsurface to potential environmental receptors via potential exposure pathways. The CSM was developed to depict Site geology, hydrogeology, and subsurface geochemical conditions and used to evaluate how these factors affect the environmental fate and transport of lead compounds in groundwater. The CSM illustrates how, over a period of time, lead was mobilized from soil due to the presence of sodium hydroxide. The CSM further depicts lead readsorbing to soil following the buffering of impacted groundwater. A graphical representation of the CSM was included in the VRP application and was updated in previous Annual Progress Reports. The CSM graphic is not included in this CSR as there are no longer any exceedances of the lead RRS.

3.1 Geochemistry

In addition to the metals analyses, samples collected from monitoring wells MW-19, MW-21, and MW-23 during the April 2012 event were analyzed for select indicator parameters (total alkalinity, carbonate/bicarbonate alkalinity, chloride, and sulfate). The results of indicator parameter testing were used in the evaluation of geochemical interactions in Site groundwater that influence or otherwise control the environmental fate and transport of lead. The evaluation included a review of Site-specific data as well as available literature, and the use of geochemical computer modeling software (Geochemist's Workbench Essentials, Version 4.0, Rockware, Inc.) to evaluate the potential for lead compounds to migrate within groundwater. The model output was then used to assess monitored natural attenuation as an appropriate remedial option.

The mobility of lead from soil to groundwater depends on solubility and geochemical form, which is a function of site-specific soil chemistry. Many complex factors affect migration of lead in soils and the key documented factor in determining mobility is the chemical form (speciation). Speciation is affected by a host of site-specific variables including soil acidity (pH), redox potential (Eh), complexation and/or precipitation with natural electrolytes (e.g. sulfate/sulfide, carbonate), co-precipitation with abundantly occurring metal oxides (e.g. Al, Fe, Mn), and the type and amount of organic matter contained in the soil. Soil conditions can vary greatly from location to location, but the primary factor governing the mobility of lead in soil and groundwater (assuming pH ranges typical of natural systems) is its relatively low solubility.

Two non-related evaluation methods were used to investigate mobility of lead at the Site. First, a simple soil adsorption capacity solution was derived, followed by a more sophisticated geochemical model. Both are described below.

3.1.1 Cation Exchange Capacity

The adsorption capacity of a soil, estimated by the number and types of binding sites available, is measured as the "cation exchange capacity" (CEC). The CEC is the capacity of soil to exchange cations between soil and groundwater (soil porewater). CEC is often used as a measure of soil fertility and nutrient retention capacity; however, in environmental chemistry, CEC provides a basic measure of the capacity of the soil to bind cations such as lead.



Researchers have studied many soils and used multivariate regression models in an attempt to predict the ability of soils to bind lead via CEC^2 . A simplified version of the referenced multiple linear regression equation, using pH and CEC, is as follows:

Soil Pb Adsorption Maximum (umol/gram) = 2.81 x CEC (meq/100g) + 10.7 x pH - 49.3

Based on data obtained from the Whitfield County U.S. Department of Agriculture Natural Resources Conservation Service (http://websoilsurvey.nrcs.usda.gov), the soils at the Site are classified as silty loams, with a reported CEC that ranges between 6.9 and 13.1 meq/100 grams. Inserting these values into the above equation, and assuming the soil pH reflects the pH of the groundwater (mean = 6.91 s.u., based on September 2011 groundwater sampling), results in a maximum soil lead absorption capacity ranging from 44 to 61 umol/gram of soil. This absorption capacity equates to a lead concentration in soil of between 9,100 to 12,700 mg/kg. The natural background concentration of lead in soil at the Site is approximately 20 mg/kg and the calculated lead adsorption indicates excess capacity for the soil to adsorb lead from groundwater following pH equilibration. Excess soil binding capacity, calculated as CEC, effectively prevents lead compounds from migrating beyond the Site boundary via groundwater.

3.1.2 Geochemical Modeling

To further evaluate lead mobility, geochemical modeling was performed. Model inputs utilized both the concentration of lead reported from samples collected in September 2011 and the geochemical 'activities' of various groundwater parameters that are known to affect the solubility of lead in aqueous systems. Laboratory data were obtained from wells MW-4, MW-5, MW-18, MW-21, and MW-23 for input into the geochemical model. Analytical results used as input into the model included dissolved lead, alkalinity (total and bicarbonate), chloride, silica, sulfate, and sulfide. Field parameters from the September 2011 sampling event were also used, including temperature, specific conductivity, pH, dissolved oxygen, ORP, and turbidity.

Groundwater pH measured across the Site indicates the geochemistry of the vadose zone soils is within a normal range (6.27 to 7.13 s.u.). Typical for the region, where the parent rocks are shale and limestone/dolomite, the reported bicarbonate alkalinity (HCO_3^{-}) was essentially equivalent to total alkalinity (as calcium carbonate equivalents). Dissolved (or 'free') lead in groundwater (as Pb²⁺) is not expected due to the likelihood of ionic bonding resulting in lead carbonate (PbCO₃). Adjusting for actual concentrations of chloride, carbonate, and sulfate, the geochemical species of lead predicted to be the most stable is PbCO₃. (Figure 5) Lead carbonate is sparingly soluble at pH conditions above 6.5 s.u. (mean for the Site is 6.9 s.u.) and alkalinity is greater than 30 mg/L (mean for the Site is 278 mg/L). This confirms the finding that excess lead (dissolved Pb²⁺) adsorbs to soil as groundwater migrates.

² Hassett, J.J., 1974. Capacity of selected Illinois soils to remove lead from aqueous solutions. Commun. Soil Sci. Plant Anal., 5, 499-505.; Zimdahl, R.L. and Skogerboe, R.K., 1977. Behavior of lead in soil. Environ. Sci. Technol. 11, 1202-1207.



3.2 Lead Fate and Transport

Considering the available information, the geochemical processes that resulted in detections of lead in well MW-21 are likely the result of:

- 1. A historic subsurface release of sodium hydroxide that created a high groundwater pH in a localized area. The alkaline conditions caused desorption of naturally-occurring lead in soil via cation exchange with sodium. This desorption resulted in an imbalance of lead ions in groundwater and the subsequent formation of lead carbonate and/or lead hydroxide as suggested by the geochemical modeling. Lead hydroxide and lead carbonate are slightly soluble under the existing (normal) pH/Eh conditions at the Site.
- 2. The high pH groundwater was discovered years later and groundwater in the immediate area was then buffered with sodium bicarbonate. Although the pH was neutralized, the additional sodium may have caused supplemental dissolution of more lead, again via cation exchange. Additional lead carbonate likely formed when the lead hydroxide reacted with the sodium bicarbonate.
- 3. The contribution of sodium from both the sodium hydroxide (NaOH) and the sodium bicarbonate (NaHCO₃⁻), as well as the presence of lead bound to solubilized (dissolved) organic carbon, held lead in solution as a colloid (USEPA, 2007³).
- 4. As the lead (inorganic and organically bound colloidal) migrated in groundwater, the neutral groundwater pH, combined with the subsurface forces of advection/dispersion, was sufficient to allow the normal cation exchange capacity of the downgradient soils to re-adsorb the lead. This condition is supported by the steady decrease in lead concentration observed at MW-19 and at MW-21.

The geochemical modeling predicted a minimally-soluble form of lead (PbCO₃) in Site groundwater. Geochemical conditions at the Site, combined with a generally low hydraulic conductivity and an abundance of silts and clays with high cation binding capacity in the overburden, support the conclusion that Site soils have re-adsorbed lead thereby restricting movement of dissolved lead in groundwater. As predicted by the model, groundwater with higher than background lead concentrations re-adsorbs to soil, without active remediation. The model accuracy was confirmed at well MW-21 where the detected lead concentration decreased below the RRS without additional remedial activities.

³ USEPA, 2007. Monitored Natural Attenuation of Inorganic Contaminants in Ground Water. Volume 2: Assessment for Non-Radionuclides Including Arsenic, Cadmium, Chromium, Copper, Lead, Nickel, Nitrate, Perchlorate, and Selenium. US Environmental Protection Agency, National Risk Management Research Laboratory, Office of Research and Development, Cincinnati, OH. EPA/600/R-07/140. October 2007.



4. IDENTIFICATION OF POTENTIAL RECEPTORS

4.1 **Potential Receptors and Exposure Pathways**

Land use at the Site and contiguous parcels is classified as industrial and commercial. Dalton Utilities supplies potable water to all developed properties in the area, including the Site. The possible exposure pathways to Site groundwater were evaluated for environmental media, and human and ecological receptors. The results of the evaluation are discussed below.

4.1.1 Environmental Media

- Lead is not present in Site soils above the RRS.
- Soil gas is not a medium of concern for exposure to lead.
- Groundwater is present under unconfined conditions and is controlled by topography. Analytical results from the most recent round of sampling (April 2014) indicate lead is not present above the laboratory reporting limit. Previously, lead concentrations above the RRS were determined to be limited to the uppermost portion of the surficial aquifer and did not migrate downward vertically into the deeper portion of the surficial aquifer.
- Surface water on the Site includes an unnamed small creek that flows northwest to southeast through the undeveloped portion of the property and offsite. The developed portion of the site is primarily paved and stormwater runoff from the production and chemical storage areas is directed into drains that discharge to the facility's pretreatment lagoons and ultimately to the Dalton Utilities sanitary sewer.

4.1.2 Exposure Pathways and Potential Human Receptors

- Dalton Utilities provides water service to the facility. Potable use of groundwater is an incomplete exposure pathway as there is no use of groundwater onsite.
- The nearest groundwater extraction well is more than 3,000 feet, and not downgradient, from the previous lead detections in groundwater. Lead is no longer present in groundwater at concentrations above the RRS. Therefore, migration of lead in groundwater to downgradient receptors is considered an incomplete exposure pathway.
- The water table varies from 4 to 16 feet bgs at the Site. In the localized area where lead has previously been detected in groundwater above the RRS, the depth to water is approximately 10 feet bgs. A future construction worker could be potentially exposed to groundwater through incidental contact (ingestion or dermal contact) should development include the excavation of soil to depths beneath the water table, water is accumulated into the excavation, and construction workers have contact with the accumulated water; however, it is unlikely an excavation in this area would intersect the water table. Regardless, lead is no longer detected in groundwater at concentrations above the RRS. Therefore exposure to future construction workers is considered an incomplete pathway.



• At the Site, there is no complete exposure pathway of groundwater, exhibiting concentrations of lead above the RRS, to surface water. The nearest surface water is approximately 650 feet downgradient from MW-21. Based on groundwater measurements and Site-specific geochemical modeling, dissolved lead has attenuated prior to reaching surface water. Additionally, the onsite creek is located in an undeveloped portion of the site where there is limited possibility of human contact with surface water or sediment.

4.1.3 Exposure Pathways and Potential Ecological Receptors

• Other than native soil, there are no known or documented sources of lead at the Site. Habitat conditions at the Site are, in general, not suitable for the threatened and endangered species for Whitfield County identified by the USFWS. Based on visual assessment of the creek, the quality of the aquatic habitat is moderate. As indicated previously, no complete exposure pathway from groundwater, exhibiting concentrations of lead above the RRS, to surface water occurs at the Site because lead has attenuated prior to reaching the creek, approximately 650 feet down-gradient from MW-21. Therefore, the potential for exposure to lead in groundwater, surface water, and sediments is expected to be minimal because no complete exposure pathway exists.

4.2 Point of Exposure and Point of Demonstration Well

EPD requested a *point of exposure* be identified that is the nearest of the following locations:

- (A) The closest existing downgradient drinking water supply well;
- (B) The likely nearest future location of a downgradient drinking water supply well where public supply water is not currently available and is not likely to be made available within the foreseeable future; or
- (C) The hypothetical point of drinking water exposure located at a distance of 1,000 feet downgradient from the delineated site contamination.

The closest existing water supply well is not directly downgradient, and is approximately 3,000 feet from the Site. This closest water supply well is not known to be a drinking water source as a public water supply is available for the area. As a default, the *point of exposure* for the Site is the property line downgradient/cross gradient of monitoring well MW-21).

EPD also requested a *point of demonstration well* to be identified, consisting of a "monitoring well located between the source of site groundwater contamination and the actual or estimated downgradient point of exposure". Monitoring well MW-23 (Figure 2) is selected as the *point of demonstration well*.

Based on the evaluation presented in Section 4.1, there are no potentially complete exposure pathways at the Site.



5. RISK REDUCTION STANDARDS (RRS)

Soil - There have been no known releases of lead or lead containing substances at the Site. Lead concentrations in soil are within the range of background concentrations

Groundwater - The RRS for the point of exposure and the point of demonstration well is the published (Type 1) RRS value for lead in groundwater (0.015 mg/L). The lead concentration reported at the point of demonstration well (MW-23) is below the MCL and indicates the Site is in compliance with the Type 1 RRS. Consistent with, and as a result of, the fate and transport mechanisms known to effectively attenuate the migration of lead in groundwater, the Site is also in compliance with regard to the point of exposure (the property line).



6. SUMMARY

In summary, and based on the foregoing discussion, the following findings have been documented.

- In isolated areas, concentrations of metals in soil exceed established background concentrations; however, previous investigations indicate no releases exceeding a reportable quantity and no additional work is required.
- Currently there are no regulated substances in Site groundwater above MCLs.
- Lead was previously present in Site groundwater above the MCL and was adequately delineated. Lead concentrations have decreased over time and are no longer present at concentrations above the laboratory reporting limits.
- There have been no known releases of lead or lead containing substances at the Site. The source of lead in groundwater is believed to be related to a sodium hydroxide release that resulted in mobilization of naturally occurring lead from soil to groundwater.
- An interim corrective action was completed to enhance attenuation of lead mobilized by a change in geochemistry.
- The geochemistry of the Site subsurface supports natural attenuation of lead in groundwater. The process resulted in the re-adsorption to soil of naturally occurring lead that had been dissolved in groundwater. The natural attenuation mechanisms were verified by the fate and transport analysis.
- There are no remaining potential exposure pathways for lead in groundwater
- Lead concentrations in groundwater do not exceed the Type 1 RRS at the identified point of exposure and at the point of demonstration well.

In conclusion, this CSR confirms consistency of the corrective actions with the provisions, purposes, standards, and policies of the VRP, and it is certified that the Site is in compliance with applicable RRS.

LVC will comply with the applicable public participation requirements for this CSR within the regulated timeframe. Haley & Aldrich respectfully requests that EPD issue a decision of concurrence with this CSR and that activities for removing the Site from the HSI proceed accordingly.



TABLES



TABLE I SUMMARY OF GROUNDWATER ELEVATIONS April 8, 2014 FORMER VULCAN PERFORMANCE CHEMICALS PLANT - DALTON, GA

Well No.	Top of Casing (ft msl)	Depth to Water (ft below TOC)	Elevation (ft msl)
MW-4	712.26	1.48	710.78
MW-5	713.68	5.40	708.28
MW-6	702.78	1.94	700.84
MW-7	712.69	4.06	708.63
MW-8	711.81	3.65	708.16
MW-13	705.92	2.23	703.69
MW-14	711.05	2.96	708.09
MW-15	710.08	4.30	705.78
MW-16	702.42	1.69	700.73
MW-17	711.95	3.89	708.06
MW-18	711.74	3.65	708.09
MW-19	711.62	3.41	708.21
MW-20	710.91	2.88	708.03
MW-21	709.84	4.53	705.31
MW-22D	710.00	4.74	705.26
MW-23	708.41	5.10	703.31
TMW-19	715.43	14.70	700.73

TABLE II GROUNDWATER SAMPLING RESULTS April 8, 2014 FORMER VULCAN PERFORMANCE CHEMICALS PLANT - DALTON, GA

WELL NO.	Lead (mg/L)	Temp (Deg C)	Conductivity (uS/cm)	pH (SU)	DO (mg/L)	ORP (mV)	Eh** (mV)	Turbidity (NTU)
MW-19	<0.0100	14.42	1113	9.17	0.46	213.6	413.6	3.80
MW-19 DUP	<0.0100	NA	NA	NA	NA	NA	NA	NA
MW-21	<0.0100	15.43	462	6.52	0.76	198.6	398.6	10.10
MW-23	<0.0100	14.68	966	6.82	0.64	50.2	250.2	1.79
RRS*	0.015*	NA	NA	NA	NA	NA	NA	NA

NOTES: MW-19 DUP is a duplicate from MW-19

* Type 1 Risk Reduction Standard

**Eh value calculated by adding 200 mv to the ORP reading.

TABLE III

SUMMARY OF LEAD CONCENTRATIONS IN GROUNDWATER (mg/L) 1996 - 2007

FORMER VULCAN PERFORMANCE CHEMICALS PLANT - DALTON, GA

Well	February-96	April-03	May-03	July-03	March-06	May-06	August-06	July-07
TMW-2	0.088							
TMW-3	BDL							
TMW-5	BDL							
TMW-8	BDL							
TMW-9	BDL							
TMW-10	BDL							
TMW-11	BDL							
TMW-12						<0.010		
TMW-13						<0.010		
TMW-14						<0.010		
TMW-15								<0.001
TMW-16								0.00162
TMW-17								<0.001
TMW-18								<0.001
TMW-21								<0.001
B-1		0.011						
B-2		0.026						
B-6		<0.010						
B-7		<0.010						
B-10		0.095						
B-11		<0.010						
B-12		<0.010						
B-13		<0.010						
B-14		<0.010						
B-15		<0.010						
B-16		<0.010						
B-17		<0.010						
B-18		<0.010						
B-19		<0.010						
MW-1			0.044	0.089	0.199		0.200	0.243
MW-2				<0.001				
MW-3D						<0.010		
MW-4						<0.010		
MW-5						<0.010		
MW-7						<0.001		<0.001
MW-8						<0.001		< 0.001
MW-9								0.0927
MW-10								0.00108
MW-11								< 0.001

NOTE: Shaded cell indicates an exceedance of the Type 1 RRS for lead (0.015 mg/L)

TABLE IV

SUMMARY OF LEAD CONCENTRATIONS IN GROUNDWATER (mg/L)

2008 - 2014

FORMER VULCAN PERFORMANCE CHEMICALS PLANT - DALTON, GA

Well	Oct-08	Oct-08*	Apr-09	Oct-09	Apr-10	Oct-10	Apr-11	Sep-11	Apr-12	Apr-13	Apr-14
MW-5							<0.0100	<0.0100	<0.0100		
MW-12	<0.010										
MW-13	<0.010		<0.0100	<0.0100	<0.0100			<0.0100	<0.0100		
MW-15	<0.010										
MW-16							<0.0100	<0.0100	<0.0100		
MW-17	<0.010		<0.0100	<0.0100	<0.0100	0.143	<0.0100	<0.0100	<0.0100		
MW-18	<0.010		<0.0100	<0.0100	<0.0100	<0.0100	<0.0100	<0.0100	<0.0100		
MW-19	0.103	0.0669	0.0311	0.0523	0.0184	<0.0100	<0.0100	<0.0100	0.0135	<0.0100	<0.0100
MW-20	0.0137	0.0124	<0.0100	<0.0100	<0.0100	<0.0100	0.0027	<0.0100	<0.0100		
MW-21	0.0402	0.0346	0.0284	0.0332	0.0315	0.0361	0.0305	0.0300	0.0239	0.0157 ⁺	<0.0100
MW-22D								<0.0100	<0.0100		
MW-23								<0.0100	<0.0100	<0.0100	<0.0100

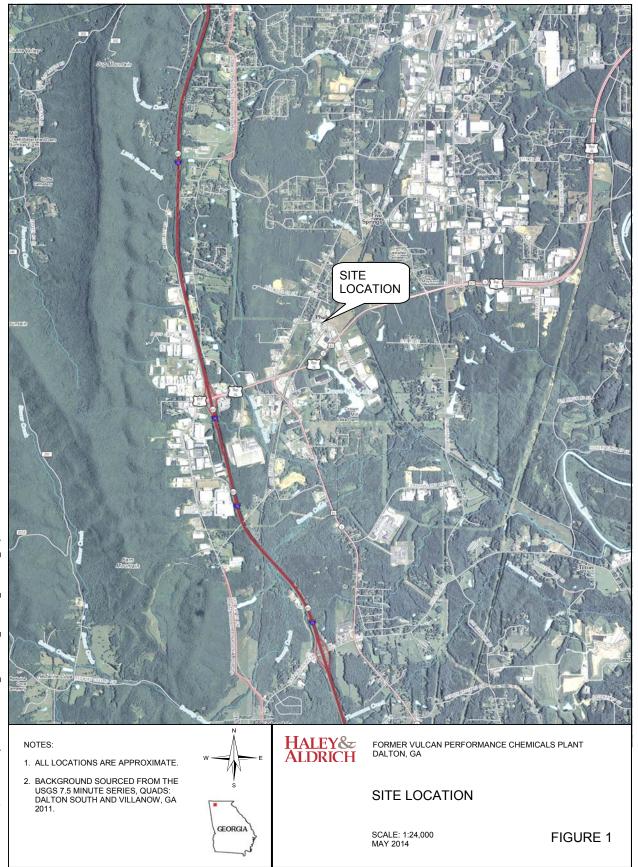
NOTE: Shaded cell indicates an exceedance of the Type 1 RRS for lead (0.015 mg/L)

* Confirmation samples

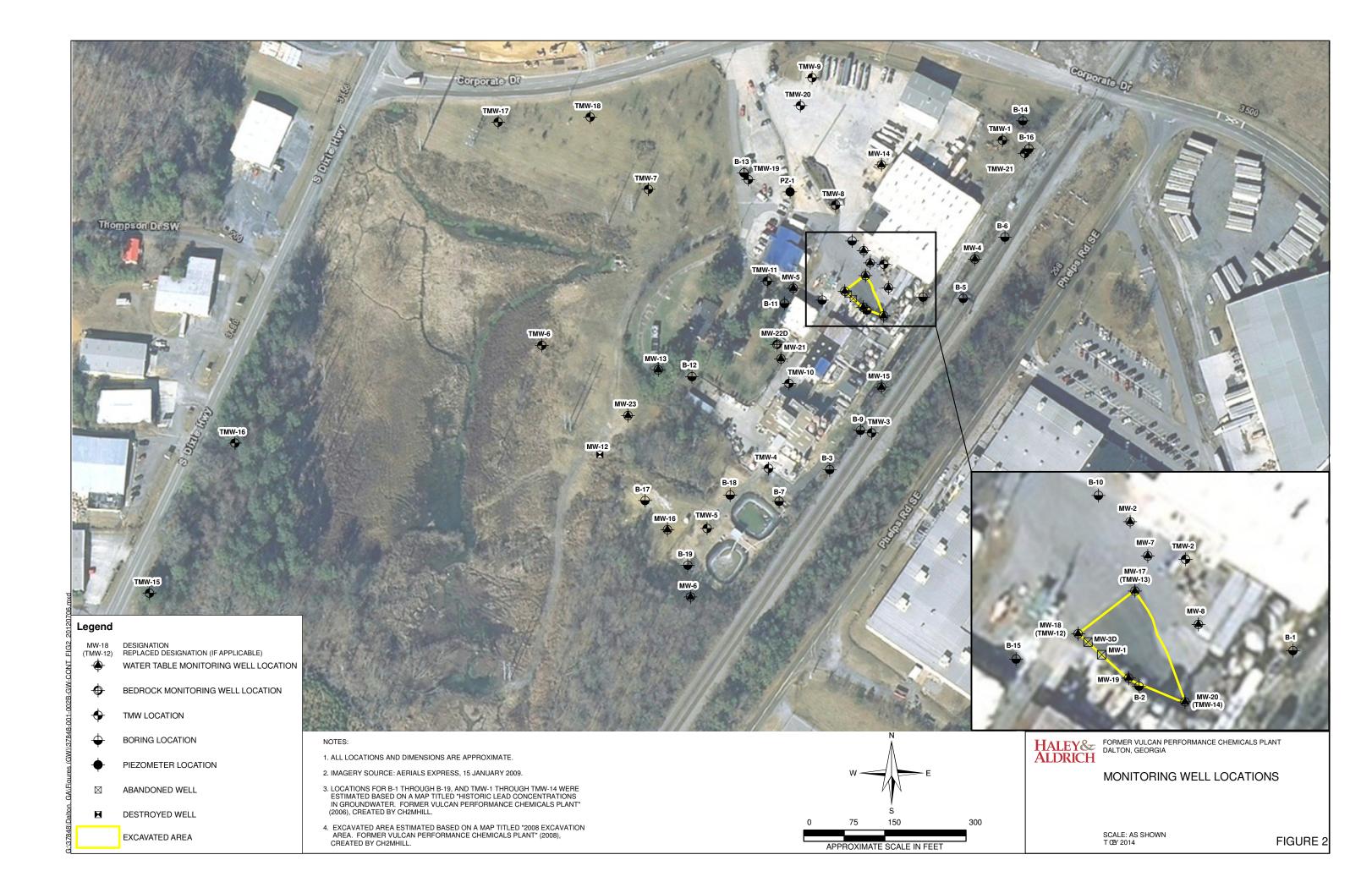
⁺ Duplicate sample collected from MW-21 in April 2013 contained lead at 0.0147 mg/L, below the RRS

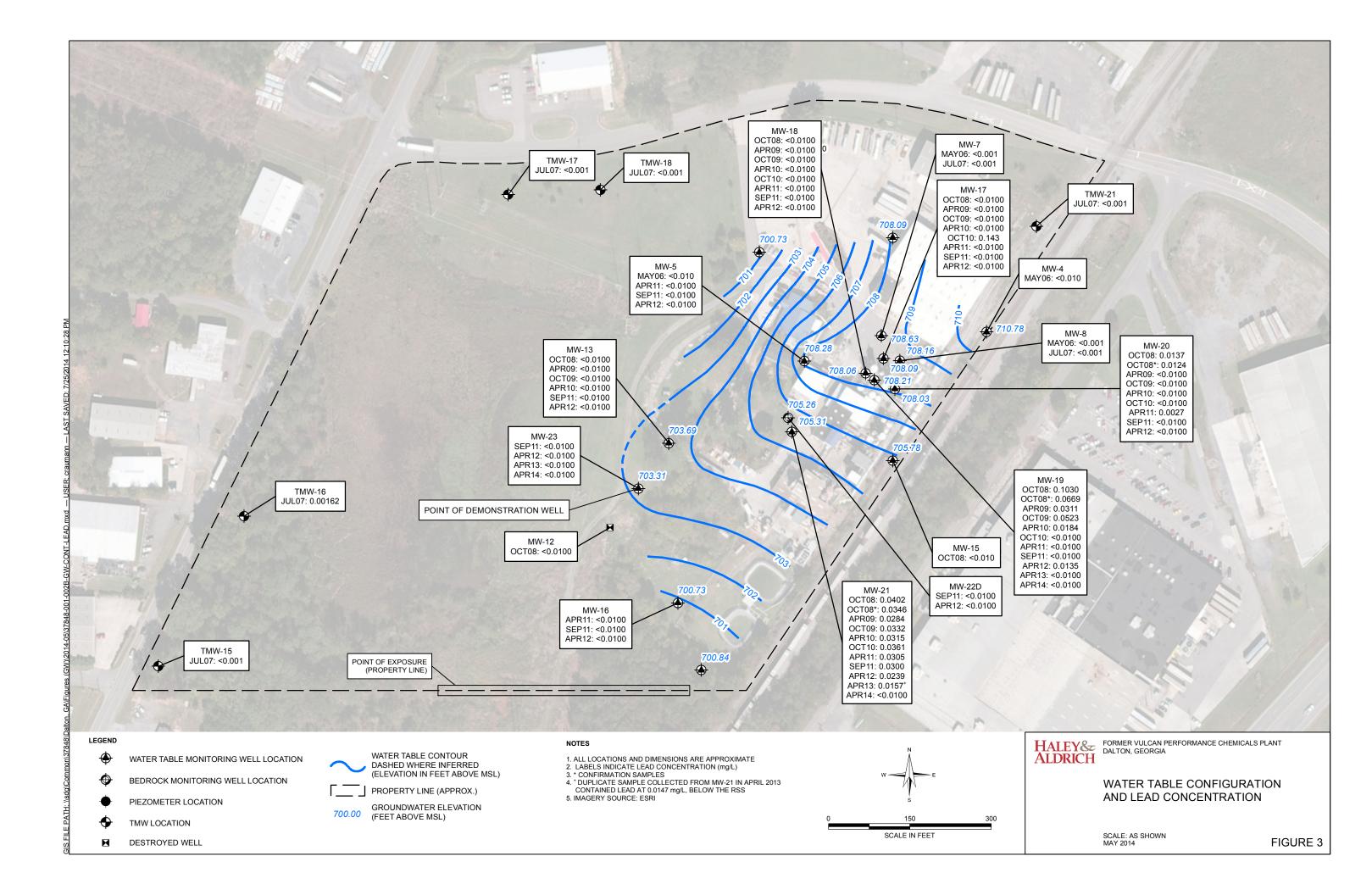
FIGURES

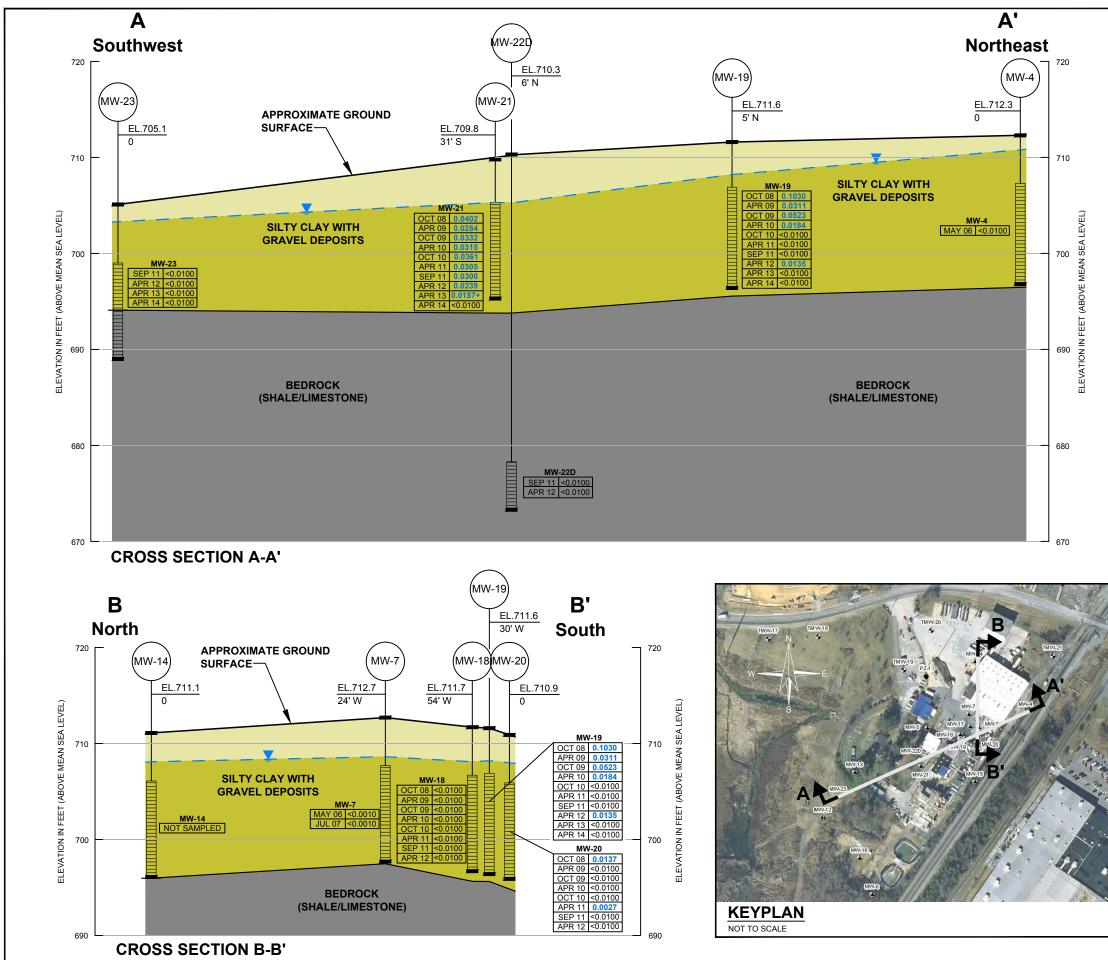




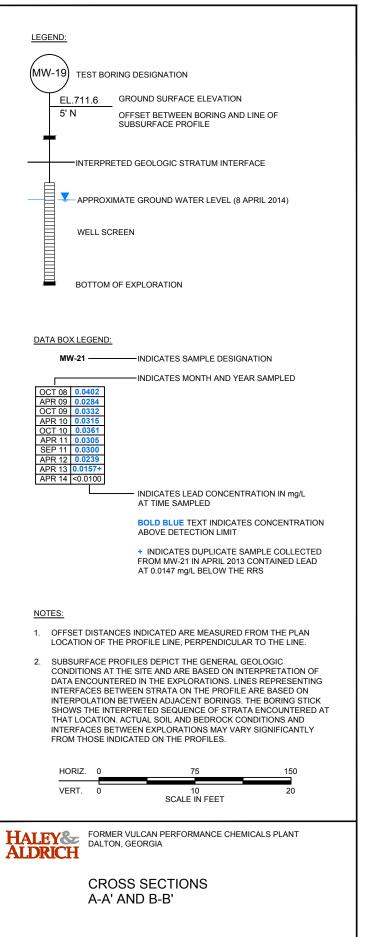
G:\37848\Dalton, GA\Dalton Maps\37848-003-SITE_LOCATION_FIGURE1_01062012_V2.pub







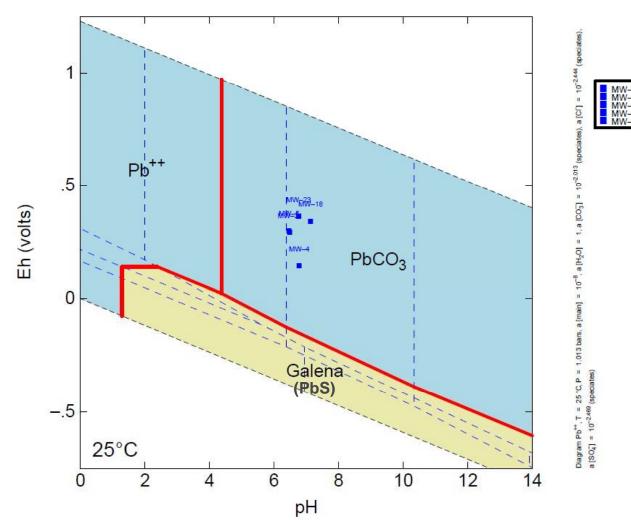
RAPHICS\37848\37848-005-B011.DWG



SCALE: AS SHOWN JULY 2014

FIGURE 4





APPENDIX A

Analytical Summary Documents (September 2006)



Table 1Soil Sampling ResultsMarch 1996 through June 2006Former Vulcan Performance Chemicals Plant, Dalton, Georgia

Analyte (mg/kg):	Antimony	Arsenic	Berylium	Chromium	Chromium (Hexavalent)	Copper	Cyanide	Lead	Nickel	Selenium	Thallium	Zi
HSRA Notification Concentration (mg/kg):	10	41	3	1,200		1,500	10	300	420	36	10 or background if higher	2,8
Sample Location (ft bgs)												
TMW-1 ^a (4'-7')	<5.0	<3.0	<1.0	6.8	<1.0	5.9	NA	<2.5	7.1	<4.0	<5.0	1
TMW-2 ^ª (2'-5')	<5.0	<3.0	<1.0	15.0	<1.0	3.1	<0.25	8.0	<2.0	<4.0	<5.0	5
TMW-3 ^a (3'-6')	<5.0	3.8	<1.0	13.0	<1.0	2.6	<0.25	10.0	<2.0	<4.0	<5.0	1
TMW-5 ^ª (6.9'-15')	6.5	<3.0	1.4	32.0	<1.0	18.0	<0.25	13.0	27.0	<4.0	<5.0	5
TMW-7 (3'-6')	<5.0	<3.0	<1.0	19.0	<1.0	2.1	<0.25	10.0	4.5	<4.0	<5.0	(
TMW8 ^a (5'-8')	5.5	<3.0	1.2	23.0	<1.0	17.0	<0.25	19.0	10.0	<4.0	<5.0	3
B-1 ^b (0'-2')	NA	<4.58	<2.29	20.9	NA	9.37	NA	11.7	7.59	<4.58	<4.58	1
B-2 ^b (4'-6')	NA	<5.54	<2.77	30.5	NA	16.9	NA	11.1	19.2	<5.54	<5.54	
B-3 ^b (2'-4')	NA	<5.95	<2.97	34.7	NA	17.8	NA	11.7	16.6	<5.95	7.32	3
B-5 ^b (4'-6')	NA	<5.45	<2.72	27.8	NA	11.7	NA	9.22	7.85	<5.45	5.77	3
B-6 ^b (2'-4')	NA	3.47	<1.72	35.9	NA	29	NA	11.3	31.8	<3.44	7.64	6
B-7 ^b (4'-6')	NA	<5.98	<2.99	41.5	NA	24.3	NA	12.9	19.4	<5.98	7.06	
B-9 ^b (0'-2')	NA	10.5	<3.00	33.8	NA	30.2	NA	26.2	13.1	<5.99	<5.99	
B-10 ^b (4'-6')	NA	4.43	<1.92	28	NA	11.7	NA	13.4	22.5	<3.84	5.0	3
B-11 ^b (4'-6')	NA	8.41	<1.95	37.7	NA	22.2	NA	10.6	8.25	<3.90	8.25	1
B-12 ^b (9'-10')	NA	4.72	<1.80	23.9	NA	10.4	NA	17.6	23.4	<3.59	4.65	4
B-13 ^b (2'-4') B-14 ^b	NA	<3.95	<1.97	18.5	NA	4.43	NA	9.65	4.53	<3.95	<3.95	g
(4'-6') B-15 ^b	NA	<4.50	<2.25	35.8	NA	19.2	NA	14.3	31.2	<4.50	7.77	5
(2'-4') B-16 ^b	NA	6.82	<2.78	32.9	NA	11	NA	6.9	5.82	<5.57	6.5	1
(9'-11') B-17 ^b	NA	<5.33	<2.67	23.1	NA	17.1	NA	6.38	19.5	<5.33	<5.33	
(4'-6') B-18 ^b	NA	<4.16	<2.08	127	NA	40	NA	66.5	22.2	<4.16	5.96	Ę
(6'-8') B-19 ^b	NA	<3.92	3.5	46.7	NA	34.8	NA	8.73	35	4.69	8.36	5
(10'-12') TMW-12 ^c	NA	<5.43	<2.71	36.3	NA	27.8	NA	13.8	19.3	<5.43	6.23	5
(4'-6') TMW-12 ^c	NA	NA	NA	NA	NA	NA	NA	4.95	NA	NA	NA	
(9'-11') TMW-12 ^c	NA	NA	NA	NA	NA	NA	NA	4.06	NA	NA	NA	
(14'-15') TMW-13 ^c	NA	NA	NA	NA	NA	NA	NA	6.57	NA	NA	NA	
(4'-6') TMW-13 ^c	NA	NA	NA	NA	NA	NA	NA	7.78	NA	NA	NA	
(9'-11') TMW-14 ^c	NA	NA	NA	NA	NA	NA	NA	6.37	NA	NA	NA	
(4'-6') TMW-14 ^c	NA	NA	NA	NA	NA	NA	NA	3.74	NA	NA	NA	l
(9'-11') MW-3D ^d	NA	NA	NA	NA	NA	NA	NA	5.72	NA	NA	NA	١
(4'-6') MW-3D ^d	NA	NA	NA	NA	NA	NA	NA	28.9	NA	NA	NA	I
(9'-11') MW-3D ^d	NA	NA	NA	NA	NA	NA	NA	8.37	NA	NA	NA	
(14'-15.5')	NA	NA	NA	NA	NA	NA	NA	5.73	NA	NA	NA	l
B-20 ^e												

| B-23 ^e
(1'-2') | NA | NA | 1.30J | NA |
|------------------------------|----|----|-------|----|----|----|----|----|----|----|----|----|
| B-22 ^e
(1'-2') | NA | NA | <2.40 | NA |
| (1'-2') | NA | NA | 1.97J | NA |

Notes:

a. TMWs were installed, sampled, and abandoned by CH2M HILL in 1996b. Borings were advanced and sampled by Clayton Group Services in 2003c. TMWs were installed, sampled, and abandoned by CH2M HILL in 2006d. Monitoring wells were installed and sampled by CH2M HILL in 2006

e. Borings were advanced and sampled by CH2M HILL in 2006

f. Yellow highlight indicates an exceedence of HSRA criterion in soil

Legend:

mg/kg	milligram per kilogram
NA	Not Analyzed
TMW	Temporary Monitoring Well
В	Boring
J	Value was below the analytical method detection limit

Analyte	Sample Date				Arsenic Dissolved				Cadmium (Dissolved		Chromium Dissolved								Selenium Dissolved		Silver Dissolved	Thallium Total	Thallium Dissolved	Zinc Total D	Zinc issolved	Mercury Total	Mercury Dissolved	рН Ти	ırbidity
Units		μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	μg/L	SU	NTUs
GA HSRA Appendix III																													
Criteria EPA Drinking		6	NC	50	NC	4	NC	5	NC	100	NC	1,300 ^e	NC	15 ^e	NC	100	NC	50	NC	100	NC	2	2	2,000	NC	2	NC	NC	NC
Water Standards MCL EPA		NC	6	NC	10	NC	4	NC	5	NC	100	NC	TT ^f	NC	TTf	NC	NC	NC	50	NC	NC	NC	2	NC	NC	NC	NC	NC	NC
Region IX PRG		NC	15	NC	0.045	NC	2,600	NC	18	NC	110	NC	1,400	NC	NC	NC	730	NC	180	NC	180	NC	2.4	NC	11,000	NC	11		NC
TMW-2 ^a	03/96	NA	NA	BDL	NA	NA	NA	NA	NA	19	NA	45	NA	88	NA	BDL	NA	NA	NA	NA	NA	NA	NA	1,700	NA	1.2	NA		silty, loudy ^g
TMW-3ª	03/96	NA	NA	BDL	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	BDL	NA	BDL	NA	NA	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	6.9	clear ^g
TMW-4 ^a	03/96	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.3 c	silty,
TMW-5 ^a	03/96	NA	NA	BDL	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	BDL	NA	110	NA	NA	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	6.4 c	loudy ^g
TMW-6 ^a	03/96	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	7.4 c	silty, loudy ^g
TMW8 ^a	03/96	NA	NA	BDL	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	BDL	NA	23	NA	NA	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	7.7 c	silty, loudy ^g
TMW-9 ^ª	03/96	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	BDL	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	10 c	silty, loudy ^g
TMW-10 ^ª	03/96	NA	NA	BDL	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	BDL	NA	98	NA	NA	NA	NA	NA	NA	NA	BDL	NA	BDL	NA	6.5 c	silty, loudy ^g
TMW-11 ^ª	03/96	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	BDL	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.9 c	silty, loudy ^g
B-1 ^b	04/03	NA	<5.00	<5.0	<5.00	<1.0	<1.00	NA	<0.700	15.5	0.58 J	10.4	1.1 J	10.9	0.42 J	17.5	7.90	NA	0.84 J	NA	<5.00	NA	<1.00	45.8	6.2 J	NA	<0.2	6.7	>999
B-2 ^b	04/03	NA	<5.00	<5.0	1.6 J	<1.0	0.052 J	NA	0.095 J	16.9	1.2 J	9.64	1.4 J	26.4	26.80	88.7	75.40	NA	0.65 J	NA	<5.00	NA	<1.00	42	20.30	NA	<0.2	6.77	>999
	05/03	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44	40	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.40	>999
MW-1°	07/03	0.086 J	0.13 J	1.1 J	1.1	<1.0	<1.0	2.06	2.19	<5.0	<5.0	14.6	13.2	88.9	94.7	88.9	94.2	<5.0	<5.00	0.009 J	0.006 J	<1.0	<1.00	30.9	32	NA	NA	6.42	NA
	03/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	199	190	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.49	1.28
	08/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	200	200	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
B-6 ^b	04/03	NA	NA	<5.0	NA	<1.0	NA	NA	NA	<5.0	NA	<5.0	NA	<1.0	NA	10	NA	NA	NA	NA	NA	NA	NA	<10.0	NA	NA	NA	7.4	36
B-7 ^b	04/03	NA	0.18 J	<5.0	1.0 J	<1.0	0.052 J	NA	<0.700	11.1	3.2 J	5.47	6.92	7.01	4.63	25.9	7.13	NA	<5.00	NA	<5.00	NA	0.061 J	<10.0	22.2	NA	<0.5	6.9	619
B-10 ^b	04/03	NA	0.068 J	<5.0	<5.00	8.87	0.028 J	NA	<0.700	77.3	3.3 J	28.7	1.8 J	95.2	0.80 J	64.4	4.9 J	NA	0.79 J	NA	<5.00	NA	<1.00	145	10.2	NA	<0.5	7.4	>999
MW-2 ^d	07/03	0.15 J	0.15 J	0.68 J	0.63 J	<1.0	<1.0	<0.7	<0.7	<5.0	<5.0	1.4 J	1.1 J	0.86 J	0.71 J	3.7 J	3.1 J	1.8 J	1.8 J	0.008 J	0.0040 J	<1.0	<1.0	9.7 J	5.9 J	NA	NA	6.8	NA
B-11 ^b	04/03	NA	0.065 J	<5.0	<5.00	<1.0	1.5	NA	<0.700	<5.0	15.0	<5.0	9.38	3.25	10.7	<5.0	26.5	NA	0.32 J	NA	<5.00	NA	0.083 J	<10.0	31.1	NA	<0.2	6	150
B-12 ^b	04/03	NA	NA	<5.0	NA	<1.0	NA	NA	NA	<5.0	NA	<5.0	NA	1.48	NA	6.02	NA	NA	NA	NA	NA	NA	NA	<10.0	NA	NA	NA	6.7	10
B-13 ^b	04/03	NA	0.12 J	<5.0	0.26 J	<1.0	<1.00	NA	<0.700	<5.0	21.4	<5.0	1.8 J	2.31	0.24 J	<5.0	6.07	NA	<5.00	NA	<5.00	NA	<1.00	<10.0	22.7	NA	<0.5	7.2	192
B-14 ^b	04/03	NA	NA	<5.0	NA	<1.0	NA	NA	NA	<5.0	NA	<5.0	NA	<1.0	NA	<5.0	NA	NA	NA	NA	NA	NA	NA	<10.0	NA	NA	NA	7.7	18
B-15 ^b	04/03	NA	<5.00	<5.0	<5.00	<1.0	<1.00	NA	<0.700	<5.0	0.43 J	<5.0	0.85 J	2.83	0.39 J	6.59	3.9 J	NA	0.48 J	NA	<5.00	NA	<1.00	<10.0	5.1 J	NA	<0.2	6.5	13
B-16 ^b	04/03	NA	NA	<5.0	NA	<1.0	NA	NA	NA	<5.0	NA	<5.0	NA	<1.0	NA	<5.0	NA	NA	NA	NA	NA	NA	NA	<10.0	NA	NA	NA	7.1	8
B-17 ^b	04/03	NA	NA	6.39	NA	<1.0	NA	NA	NA	<5.0	NA	<5.0	NA	2.61	NA	8.63	NA	NA	NA	NA	NA	NA	NA	<10.0	NA	NA	NA	7.1	5
B-18 ^b	04/03	NA	<5.00	<5.0	<5.00	<1.0	0.46 J	NA	<0.700	<5.0	2.5 J	<5.0	2.8 J	4.32	2.47	23.7	18.7	NA	<5.00	NA	<5.00	NA	<1.00	<10.0	8.9 J	NA	<0.5	5.9	38
B-19 ^b	04/03	NA	0.13 J	<5.0	0.43 J	<1.0	0.34 J	NA	<0.700	<5.0	4.7 J	<5.0	5.08	5.85	6.30	284	88.0	NA	0.34 J	NA	<5.00	NA	<1.00	<10.0	24.5	NA	<0.5	6.8	123
MW-3D ^j	05/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.9	5.2	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.7	4.2
MW-4 ^j	05/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	9.2	3.9	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	7.0	3.8
MW-5 ^j	05/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	<0.01	<0.01	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.8	1.7
MW-6 ^j	05/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	<0.2	3.7	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.01	3.7
TMW-12 ⁱ	05/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	<0.01	<0.01	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.72	NA
TMW-13 ⁱ	05/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	BDL	B DL	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.84	850
TMW-14 ⁱ	05/06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.6	3.6	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.98	1,100

в

Notes:

a. TMWs 2-11 were installed, sampled, and abandoned by CH2M HILL in 1996

b. Soil borings were installed, sampled, and abandoned by Clayton Group Services in April 2003

c. MW-1 was installed by CH2M HILL in May 2003 to confirm lead concentrations in B-2

d. MW-2 was installed by CH2M HILL in July 2003 to confirm lead concentrations in B-10 e. Action level

f. Treatment Technique - a required process intended to reduce the level of a contaminant in

drinking water (as defined by US EPA)

g. Visual observation

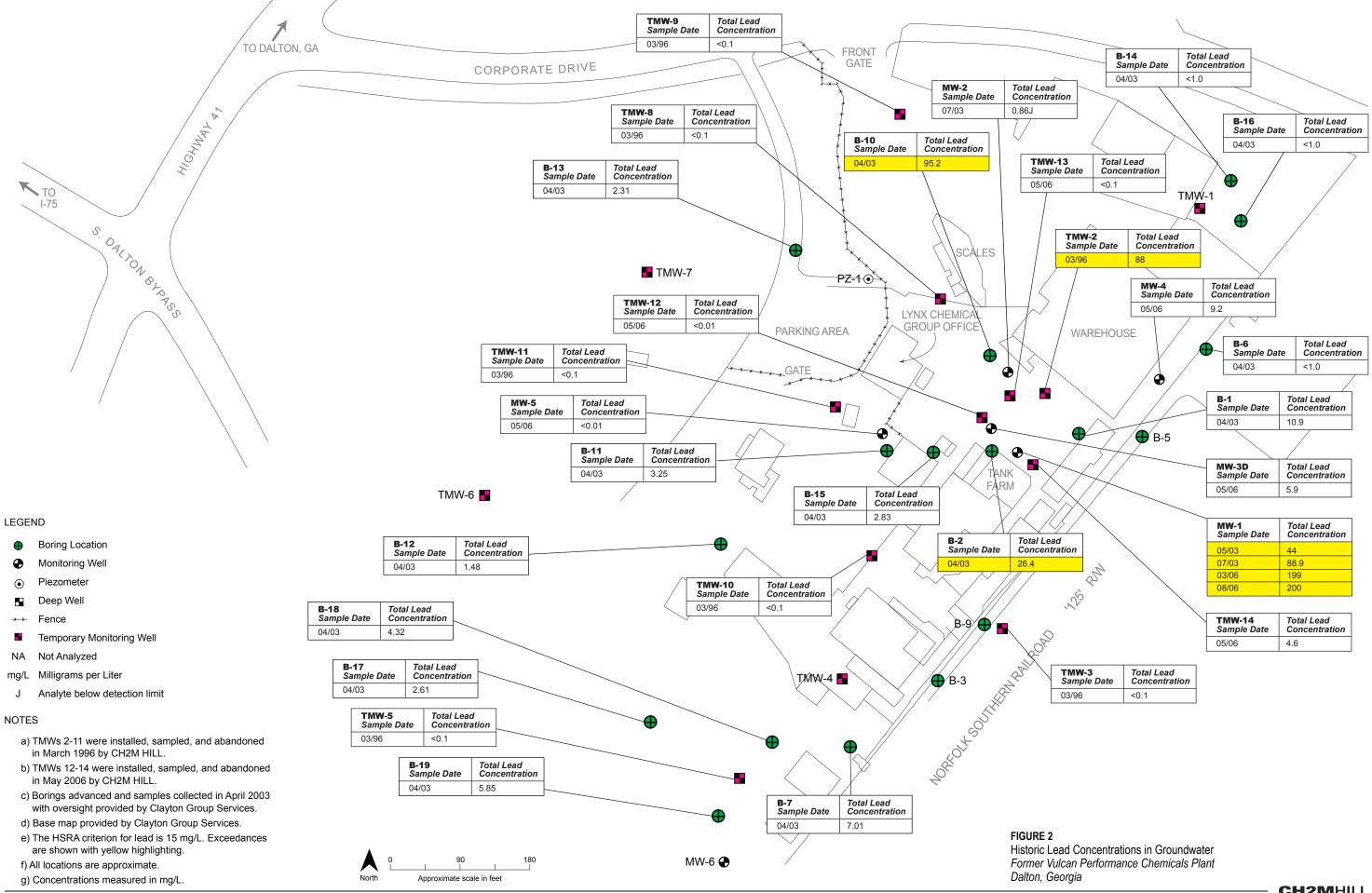
h. Yellow highlighting indicates exceedances of HSRA Appendix III, Table 1 criteria.

i. TMWs 12-14 were installed, sampled, and abandoned by CH2M HILL in 2006

Abbreviations:

Below Detection Limit

- Analyte below detection limits
- Not analyzed
- No criterion established
- Standard units
- microgram per liter
- Temporary Monitoring Well
- Boring
- MW Monitoring Well
- NTUs Nephelometric Turbidity Units



ES072006025ATL Vulcan102.ai

CH2MHILL

APPENDIX B

Groundwater Sampling Field Notes

(April 2014)



AEM Groundwater Sampling Field Log

mpling Personnel: Tor	y Gordon, Cha	d Crumbley			Date:	4-8-20	14
mments:					Time In:	1352 Tim	e Out: 1603
Vell Information		11 - 11				0.04 gal/ft	in 1-inch-ID wel
Well Diameter: ∂ .	() inches	Refe	erence Poir	t Marked: (Yes)	No	0.16 gal/ft	in 2-inch-ID wel
Depth to Water: 3.4		T.O.C. Well	Depth: 1	5_25 feet belo	ow T.O.C.	0.65 gal/ft	in 4-inch-ID wel
Purging Information	Purge			Purging	Equipment and	Calibration Ir	oformation
	Method	I DW STRESS	Micro- purge	Bailer:] Teflon			
Water Column: 11.8					-	-	
1 Well Volume= 1.8		Start Time: 1		Pump Tubing T			
3 Well Volume=5-6.		End Time: 15	549	Meter(s) Used:			
Total Purged: 5.75		1- 1	min	Calibration Date		-8-2014	(1341)
Well Purge Dry (?): ye	s/(no) Purge	Rate: 0-05	gpm	Comments: ()	can pulge la	21	
Groundwater Field Para	meters			Dissolved			
Gallons	Temp.	Cond.	рН	Oxygen	ORP	Turbidity	Water Level
Time Purged	Deg. Cel	µS/cm	SU	mg/L	mV	NTUs	ft. from TO
1425 1.0	13.48	1078	8.84	1.31	219.4	9.43	4.28
440 2.0	13.560	1113	9.14	0.79	270.5	6.35	4.29
50Z 3D	13.1/00	1115	9.1Z	3.13	271.0	5.04	4.32
and the second	13.730	1118	9-16	0.64	216.9	4.29	4.32
533 5-0	13.990	1112	9-21	0.52	718.3	4.18	4.32
549 5.75	14.420	1113	9.17	0.48	213-6	3.80	4:32
······································				-			
				-			
Stabilization Info:	-/- 0.5 deg.	+/- 5%	+/- 0.1 SU	+/- 10%	+/- 10%	<10 NTUs	
		+7- 5%	+7-0.1 30	+7-10%	+7-10%	< TU NT US	
ample Collection Paran							
Sample Collection Met		-		Nethod <u>Pum</u>		acuum Jug	Other
Final Tubing/Pump De		feet below T.(inal Groundwate			eet below T.O.C
Final Sample Turbidity		NTUs	F	errous Iron Cond	centration (if sa	mpled):	NA mg/L
Comments: Oleav	Somple, p	o oden					
aboratory Analytical Int			6	alana ar	D	-	Circa Cara I
Sample ID	Analysi		Cont			ative	Fime Sampled
	otal Lead (6010)	250 mL HD	$\frac{1}{1}$	HNO3 HNUD		1551
MW-19 Up	11 11				HILD)		155
Sample Laboratory (cir	cle): ACL/Yen	COLAFS) Other	-	Delivery Metho	d Hand Deliver	VFed-Fy/III	PS/Other
campic cuboratory (Cli		- Contraction of the	/	Jentery Metho	S. Ciulio Delivel	JICOLATOR	5) Other

1

			lwater San	npling Fiel		×	
-	Aldrich - Former		AEM Job No.	1398-1401	Well No.:		
	ony Gordon, Cl				Date:	4-8-20	
omments: P. (lonen/	Mirt -	51:667 5	14121	Time In:	<u>/6/> 11m</u>	e Out: /9 ù
Well Information						0.04 gal/fi	in 1-inch-ID we
	J.() inches		ference Point A	\sim	No	0.16 gal/ft	in 2-inch-ID we
Depth to Water:	1,33 feet belo	ow T.O.C. We	ell Depth: 1식.	్ర feet below	T.O.C.	0.65 gal/ft	in 4-inch-ID we
Purging Information	Pur	od (LOW Flow-	Micro-	Purging Ec	uipment and (Calibration II	nformation
Water Column: 9	AL ft (chee	1 I OW STRESS	purge Ba	iler: 🛛 Teflon 🛛	Poly. Pump:	Grundfos	Peri. ID# P-
1 Well Volume= \.	5 lo gal Purg	e Start Time:	1622 PU	mp Tubing Typ	e: 🛛 Teflon 🖡	Teflon-Lined Po	oly. 🛛 Polyethy
3 Well Volume= 니	.@Jgal Purg	e End Time:	1845 ME	eter(s) Used:	Hanna 991300 🕅	YSI 556 🗍 Lamo	tte 2020 ID#'s 1
Total Purged: 4	∵γ gal Tota	l Time: 4	3 min Ca	libration Date/	'Time: 4-8	-zoi4 (1341)
Well Purge Dry (?):	yes no Purg	e Rate: 10	} gpm CC	mments:			
Groundwater Field Pa	arameters			Dissolved			
Gallons	Temp.	Cond.	pH	Oxygen	ORP	Turbidity	Water Leve
Time Purged	Deg. Cel	µS/cm	SU	mg/L	mV	NTUs	ft. from TC
165) 1.0	17.24	335	7.29	3.04	196.9	14.4	<u> </u>
1723 20	15.54	349	6.46	2.82	198.6	19.70	4.5
1746 3.0	15.4)	386	6.41	1.63	188.7	15.30	
1809 3.5	15.46	1459	6.46	1.17	192.L	13.90	4.5
1819 40	15.40	4462	6-48 6.52	1.59	195.P 198.6	11.36	4.50
							· · · · · · · · · · · · · · · · · · ·
Stabilization Info: ample Collection Par		+/- 5%	+/- 0.1 SU	+/- 10%	+/- 10%	<10 NTUs	
Sample Collection N						acuum Jug	Other
Final Tubing/Pump				l Groundwater			
Final Sample Turbid Comments:	ity: 135 L	Septilus fi	Ferr	ous Iron Conce	ntration (if sa	mpled): -	NA mg/l
comments.							
aboratory Analytical	Information						
Sample ID	Anal	vcic	Contain	er Qty.	Preserva	ative	Time Sample
	Total Lead (601		250 mL HDPE	<u>(</u>	HNO3	-	1845
MW-21				1			1070
Sample Laboratory (circle): ACL/X	enco(AES)Oth	er De	elivery Method	Hand Deliver	Fed-Ex/U	PS/Other
eld Personnel Signatu		DAT	1				

4/2/2014, 10:21 AM, CurrentSamplingFieldLog, NewSamplingFieldLog (4), Page 1 of 1.

Sangling Personnel: Convents: Dete: 41 (g) (2014) Comments: Time in:1\00 Time in:1\00 Time in:1\00 Time in:1\00 Well Diameter: 2.0 index Reference Point Marked: Image: Imag	AEM Proje	ct: Haley & /	Aldrich - Forme	r Vulcan Site	AEM Job No	o.: 1398-140	1 Well No	.: MW-2	3	
Weil Information Display the Information Display the Information Weil Diameter: 0.0 gal/t in 1-incb: 0 will Display the Information Display the Information Purging Information Mater (S, I) teel below T.O.C. Weil Diameter: Display the Information Water (Summe (S, I) marging information Marging Equipment and Calibration Information Purging Equipment and Calibration Information Water (Summe (S, I) exact (S, I) marging information Purge Start Time: (Id V) Purge Calibration Information Purge Calibration Information Weil Volume: G.I. (Information) Total Time: (Id V) Total Time: (Id V) Purge Calibration Date / Time: IS (Id V) Purge Calibration Date / Time: IS (Id V) Purge Calibration Date / Time: IS (Id V) Time Purge Calibration Date (S, I) marging Calibration Date / Time: IS (Id V) Purge Calibration Date / Time: IS (Id V) Purge Calibration Date / Time: IS (Id V) Purge Calibration Date / Time: IS (Id V) Time Purge Calibration Date / Time: IS (Id V) Immed Purge Calibration Date / Time: IS (Id V) Purge Calibration Date / Time:	Sampling F	Personnel: (ony Gordon, C	had Crumbley	/		Date:	418/2011	+	
Well Diameter: Q. (inclus) Reference Point Marked: No. D. (b gal/t in 2 inclus) well Everying Information Marked (inclus) (inc	Comments	•					Time In	:1400 Tin	ne Out: 1620	_
Depth to Water: 5::0 feet below T.O.C. Data gulf in 4-incl-10 well Purging Information Note: Note: Purging Equipment and Calibration Information Water Column: 13::0:1: Note: Purge Statt Time: [1/2] Purge Statt Time: [1/2] Purge Data Purges Purge Statt Time: [1/2] Purge Tortion [1/2] Purge Data Purges Purge Data Purges 3 Well Volume: -0.:	Well Info	ormation						0.04 gal/f	t in 1-inch-ID well	
Purging Equipment and Calibration InformationWater Column: 13.10 ft.1 Well Volume: 0.2 at3 Well Volume: 0.2 atTotal Ture:1.42.3Purge Start Time:1.42.3Purge Start Time:1.42.3Purge Total Time:1.42.3Purge Start Time:1.42.3Purge Start Time:1.42.3Purge Total Time:1.04.1Well Volume: 0.2 atTotal Purged:Purge Total Time:Purge Start Time:1.04.2Total Time:1.04.2Well Purge Dr. (1): yes(fb)Purge Rate: (5) (6 asConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsStabilizationIntellTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp.ConditionsTemp. <t< td=""><td>Well [</td><td>Diameter:</td><td>)_() inches</td><td>R</td><td>eference Point</td><td>Marked: (res</td><td>) No</td><td>0.16 gal/f</td><td>t in 2-inch-ID well</td><td></td></t<>	Well [Diameter:)_() inches	R	eference Point	Marked: (res) No	0.16 gal/f	t in 2-inch-ID well	
Water Column:Ist (a) (a)Market (a)Description (a)	Depth	to Water: 5	. 10 feet bel	ow T.O.C. W	ell Depth:	9.00 feet bel	ow T.O.C.	0.65 gal/f	t in 4-inch-ID well	
Water Column: [3:7] 0: ft [andif] [andif] purge p	Purging	Information			- Micro-	Purging I	Equipment and	Calibration I	nformation]
3 Well Volume G_{L} as Purge End Time: $ Q Q$ Meter(s) Used: D Haves 99300 V_{125556} D Lamote 2000 $Drs Q_{2N} and V_{2N} andeterm anetreformation and V_{2N} andetereformetric a$	Water	Column: 13			ss purge	Bailer:] Teflon	Poly. Pump	: 🛛 Grundfos	Peri. ID# Port	P-7 20
Total Purged: 7, 0 paiTotal Time: 100 min Purge Rate: $0, 0, 0$ genCalibration Date/Time: 1350 4/8/20/1Well Purge Dry (?): yes (%)Durge Rate: $0, 0, 0$ genDuroleedOutments: $degle, purge Auters, poly of Auters, $	1 Wel	l Volume= Ə	्र gal Purg	e Start Time	1423	Pump Tubing T	ype: 🛛 Teflon	Teflon-Lined P	oly. 🛛 Polyethylene	
Comments: $\mathcal{L}_{q,Q}$ puge $\mathcal{A}_{r}\mathcal{L}_{r_{q}}$ for $\mathcal{L}_{r_{q}}$ for \mathcal{L}	3 Wel	l Volume= 6.	6 gal Purg	e End Time:	1612 1	Meter(s) Used:	Hanna 991300			7
Groundwater Field ParametersDissolvedObjectedDissolved<	Total	Purged: 7.	🗘 gal Tota	l Time: \ ථ	9 min (Calibration Dat	e/Time: 1350	4/8/20	jY	-
GallonsTemp. PurgedCond. psc. CelpHDoygenORP mg/LTurbidityWater LevelTimePurgedDeg. Cel μ /s/cmSumg/LmVNTUsft. from TOC[14]55 $3,0$ 13.68% 978 $6,81$ 3.38 77.2 3.97 $9,81$ [1512] $3,0$ $1/4,926$ 977 $6,83$ $1/2.57$ $4/2.27$ $7/2.8$ $6/2.27$ [157] $4,0$ $1/4,336$ 977 6.84 0.332 51.3 2.437 11.50 [154] 5.0 $1/4,376$ 977 6.84 0.332 51.3 2.437 11.50 [156] 6.20 $1/4,450$ 977 6.852 0.69 48.1 3.13 10.03 1604 6.5 $1/4,450$ 6.83 0.633 491.3 3.10 1233 1604 6.53 0.633 491.3 3.10 1233 1604 6.83 0.633 491.3 3.10 1233 1604 7.6 $1/4.686$ 6.83 0.633 491.3 -10 1624 $1/4.686$ $1/4.686$ $1/4.686$ $1/4.686$ $1/4.686$ $1/4.686$ Sample Collection ParametersSample Collection Rethod (check all):BaillerStraw MethodPump TubingVacuum JugSample Collection ParametersFeet below T.O.CFinal Groundwater Depth(1/4.201): $1/2.22$ feet below T.O.CFinal Sample Collection ParametersSample Collection InformationSample Colle	Well P	Purge Dry (?):	yes/no) Purg	e Rate: نړی	G gpm	Comments: Cl	two purge a	iten, no ode	V	_
TimePurgedDeg. Cel $\mu S/Cm$ SU mg/L mV NTUsft. from TOC1458 $\partial_{-}, 0$ 13. GS^{e} 978 $G_{-}S_{1}$ 3.28 77.2 3.977 9.81 1512 3.0 $17/4.90^{e}$ 978 $G_{-}S_{3}$ 1.554 460.6 3.84 40.227 1527 4.0 $14/4.33^{e}$ 977 $G_{-}S_{3}$ 1.05 57.4 5.30 10.78 1549 5.0 $14/4.37^{e}$ 977 $G_{-}S_{3}$ 0.632 513 2.137 11.52 1554 $G_{-}O$ $14/4.50^{e}$ 972 $G_{-}S_{3}$ 0.697 448.1 3.13 11.03 1604 $G_{-}S_{-}$ $14/4.50^{e}$ $G_{-}G_{-}$ $G_{-}S_{-}$ 0.64^{e} 502^{e} 1.19^{e} 1604 $G_{-}S_{-}$ $14/4.50^{e}$ $G_{-}G_{-}$ $G_{-}S_{-}$ 0.64^{e} 502^{e} 1.19^{e} 1604 $G_{-}S_{-}$ $14/4.50^{e}$ $G_{-}G_{-}$ $G_{-}S_{-}$ 0.64^{e} 502^{e} 1.19^{e} 1604 $G_{-}S_{-}$ $14/4.65^{e}$ $G_{-}G_{-}$ 6.53^{e} 0.64^{e} 502^{e} 1.19^{e} 13.50^{e} 1607 $14/4.65^{e}$ $G_{-}G_{-}$ 6.53^{e} 0.64^{e} 502^{e} 1.19^{e} 13.50^{e} 1607 $14/4.65^{e}$ $16/6^{e}$ 50^{e} 1.19^{e} 10.2^{e} 50^{e} 1.79^{e} 1607 $14/4.65^{e}$ $16/6^{e}$ 50^{e} 1.108^{e} 10.108^{e} </td <td>Groundy</td> <td>vater Field Pa</td> <td>arameters</td> <td></td> <td>d He</td> <td>Dissolved</td> <td></td> <td></td> <td></td> <td>-</td>	Groundy	vater Field Pa	arameters		d He	Dissolved				-
$\frac{ 458}{ 512} = 3.0$ $\frac{ 3.68^{\circ}}{ 7.96^{\circ}} = \frac{978}{978} = \frac{6.81}{6.83} = \frac{3.88}{1.59} = \frac{77.2}{3.82} = \frac{3.97}{9.81} = \frac{9.81}{1.227}$ $\frac{ 525}{ 525} = \frac{4.0}{ 4.0} = \frac{14.33^{\circ}}{9.77} = \frac{9.77}{6.83} = \frac{6.83}{1.05} = \frac{59.4}{5.30} = \frac{10.98}{1.027} = \frac{11.83}{1.55} = \frac{11.83}{1.55} = \frac{11.8}{1.50} = \frac{11.83}{1.50} =$		Gallons	Temp.	Cond.	pН	Oxygen	ORP	Turbidity	Water Level	
$\frac{1512}{1527} \frac{3}{4.0} \frac{14}{9} \frac{\sqrt{9}}{9} \frac{9}{78} \frac{6}{9} \frac{8}{3} \frac{1}{55} \frac{5}{9} \frac{6}{4} \frac{5}{53} \frac{3}{5} \frac{1}{2} \frac{5}{59} \frac{1}{4} \frac{3}{20} \frac{1}{2} \frac{2}{27} \frac{1}{16} \frac{5}{33} \frac{1}{2} \frac{5}{59} \frac{1}{4} \frac{5}{30} \frac{1}{12} \frac{1}{12} $	Time	Purged	Deg. Cel	µS/cm	SU	mg/L	mV	NTUs	ft. from TOC	
$\frac{1529}{1593} \frac{4}{2.0} \frac{14.33}{14.39} \frac{977}{979} \frac{6.53}{6.54} \frac{1.05}{9.32} \frac{59.4}{51.8} \frac{3.30}{9.43} \frac{10.98}{11.50} \frac{11.50}{11.50} \frac{11.50}{11.$	1458	2.0			6.81	2.28		3.97	9,81	
$\frac{1543}{7549} \frac{5 \cdot 0}{6 \cdot 5} \frac{1439^{\circ}}{7463^{\circ}} \frac{979}{972} \frac{6 \cdot 54}{6 \cdot 55} \frac{0 \cdot 32}{5 \cdot 5} \frac{51 \cdot 3}{748 \cdot 3} \frac{51 \cdot 3}{2 \cdot 39} \frac{11 \cdot 52}{11 \cdot 57}$ $\frac{1556}{6 \cdot 6} \frac{6 \cdot 0}{14 \cdot 45^{\circ}} \frac{14 \cdot 69}{6 \cdot 68} \frac{6 \cdot 52}{6 \cdot 52} \frac{0 \cdot 69}{6 \cdot 68} \frac{48 \cdot 1}{9 \cdot 13} \frac{3 \cdot 10}{1232}$ $\frac{1002}{14 \cdot 65^{\circ}} \frac{14 \cdot 59^{\circ}}{14 \cdot 65^{\circ}} \frac{6 \cdot 68}{6 \cdot 68} \frac{0 \cdot 63}{2 \cdot 64} \frac{0 \cdot 63}{49 \cdot 13} \frac{49 \cdot 3}{2 \cdot 10} \frac{3 \cdot 10}{1232}$ $\frac{1232}{1002} \frac{14 \cdot 65^{\circ}}{14 \cdot 65^{\circ}} \frac{91 \cdot 6}{6 \cdot 68} \frac{6 \cdot 52}{6 \cdot 52} \frac{0 \cdot 63}{6 \cdot 63} \frac{49 \cdot 2}{5 \cdot 2} \frac{1 \cdot 79}{1 \cdot 79} \frac{13 \cdot 30}{1232}$ $\frac{11 \cdot 57}{1022} \frac{14 \cdot 65^{\circ}}{14 \cdot 56^{\circ}} \frac{91 \cdot 6}{6 \cdot 68} \frac{6 \cdot 52}{6 \cdot 52} \frac{0 \cdot 63}{6 \cdot 62} \frac{49 \cdot 2}{1 \cdot 79} \frac{13 \cdot 30}{1232}$ $\frac{11 \cdot 57}{1022} \frac{14 \cdot 65^{\circ}}{14 \cdot 56^{\circ}} \frac{91 \cdot 6}{6 \cdot 52} \frac{6 \cdot 52}{6 \cdot 52} \frac{0 \cdot 63}{1 \cdot 79} \frac{49 \cdot 2}{5 \cdot 2} \frac{1 \cdot 79}{1 \cdot 79} \frac{13 \cdot 30}{1232}$ $\frac{11 \cdot 57}{1023} \frac{14 \cdot 65^{\circ}}{5 \cdot 2} \frac{1 \cdot 75^{\circ}}{1 \cdot 75^{\circ}} \frac{1 \cdot 75^{\circ}}{1 \cdot 75^{\circ}} \frac{1 \cdot 75^{\circ}}{1 \cdot 75^{\circ}} \frac{1 \cdot 70^{\circ}}{5 \cdot 2} \frac{1 \cdot 79}{5 \cdot 2} \frac{1 \cdot 79}{1 \cdot 79} \frac{13 \cdot 30}{1 \cdot 79}$ $\frac{5ample Collection Parameters}{Sample Collection Method (check all): Bailer Straw Method (Pump Tubing) Vacuum Jug Other Final Groundwater Depth(if applic.) \frac{13 \cdot 32}{1 \cdot 2} \frac{1 \cdot 79}{1 \cdot 79}$ $\frac{11 \cdot 57}{1023} \frac{11 \cdot 57}{102} \frac{11 \cdot 57}{102} \frac{11 \cdot 57}{102} \frac{11 \cdot 79}{1 \cdot 79} \frac{11 \cdot 57}{102} \frac{11 \cdot 79}{1 \cdot 79}$ $\frac{11 \cdot 57}{102} \frac{11 \cdot 57}{102} \frac{11 \cdot 57}{102} \frac{11 \cdot 79}{1 \cdot 79} \frac{11 \cdot 79}{1 \cdot 79} \frac{11 \cdot 57}{102} \frac{11 \cdot 79}{1 \cdot 79} 11 \cdot$			the second se			()	66.6	-	-	
$\frac{1549}{1556} \underbrace{5.6}_{(14,459)} \underbrace{14.459}_{(16,459)} \underbrace{41.69}_{(16,45)} \underbrace{6.83}_{(16,45)} \underbrace{0.69}_{(48,13)} \underbrace{448.3}_{(16,43)} \underbrace{2.39}_{(14,59)} \underbrace{11.83}_{(16,45)} \underbrace{11.63}_{(16,45)} \underbrace{11.63}_{(16,45)}$				Name and American Street Stree			the second se			
$\frac{1556}{1404} \underbrace{6 \cdot 6}_{0} \underbrace{14.45^{\circ}}_{14.59^{\circ}} \underbrace{6 \cdot 69}_{9 \cdot 68} \underbrace{6 \cdot 83}_{0 \cdot 63} \underbrace{0 \cdot 69}_{49 \cdot 3} \underbrace{49 \cdot 3}_{29 \cdot 3} \underbrace{18 \cdot 03}_{1232} \underbrace{18 \cdot 03}_{1232} \underbrace{14 \cdot 68^{\circ}}_{1232} \underbrace{9 \cdot 6}_{9 \cdot 68} \underbrace{6 \cdot 83}_{0 \cdot 63} \underbrace{0 \cdot 64}_{13 \cdot 3} \underbrace{49 \cdot 3}_{20 \cdot 64} \underbrace{3 \cdot 10}_{1232} \underbrace{1232}_{1232} \underbrace$	and the second s					· · · · · · · · · · · · · · · · · · ·	the second se	0	-	
$\frac{1604}{1402} \underbrace{6.5}_{140} \underbrace{14.59^{\circ}}_{14.65^{\circ}} \underbrace{966}_{166} \underbrace{6.83}_{20.64} \underbrace{0.63}_{20.64} \underbrace{49.3}_{50.62} \underbrace{1.79}_{1.79} \underbrace{12.32}_{12.32}$ $\underbrace{1.79}_{12.32} \underbrace{12.32}_{12.52} \underbrace$	· · · · · · · · · · · · · · · · · · ·				-	· · · · · · · · · · · · · · · · · · ·	-			
$\frac{1612}{1.02} 7.0 14.68^{\circ} 9166 6.83 0.64 50.2 1.79 13.30$ $\frac{14.68^{\circ}}{1.02} 9166 6.83 0.64 50.2 1.79 13.30$ $\frac{14.68^{\circ}}{1.02} 9166 6.83 0.64 50.2 1.79 13.30$ $\frac{14.68^{\circ}}{1.02} 9166 $	100 Jan 100 Ja			and the second second	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				-	
Stabilization Info: +/- 0.5 deg. +/- 5% +/- 10% +/- 10% <10 NTUs	10 million 1		14.37		1	1927 - K. (194		10		
Sample Collection Parameters Sample Collection Method (check all): Bailer Straw Method Pump Tubin Vacuum Jug Other Final Tubing/Pump Depth: j2,5 feet below T.O.C Final Groundwater Depth(if applic.) j2.22 feet below T.O.C Final Sample Turbidity: j. 79 NTUS (2.22 feet below T.O.C Ferrous Iron Concentration (if sampled): NA mg/L Comments: Comments: Ferrous Iron Concentration (if sampled): NA mg/L Laboratory Analytical Information Sample ID Analysis Container Qty. Preservative Time Sampled MW - 23 Total Lead (6010B) 250 mL HDPE j HNO3 I (6 I 5) Sample Laboratory (circle): ACL/Xenco (AES) Other Delivery Method: (Hand Delivery/Fed-Ex/UPS/Other	1012	1:0	19.00	166	6.02	004	20.2	1.17	12.50	
Sample Collection Parameters Sample Collection Method (check all): Bailer Straw Method Pump Tubin Vacuum Jug Other Final Tubing/Pump Depth: j2,5 feet below T.O.C Final Groundwater Depth(if applic.) j2.22 feet below T.O.C Final Sample Turbidity: j. 79 NTUS (2.22 feet below T.O.C Ferrous Iron Concentration (if sampled): NA mg/L Comments: Comments: Ferrous Iron Concentration (if sampled): NA mg/L Laboratory Analytical Information Sample ID Analysis Container Qty. Preservative Time Sampled MW - 23 Total Lead (6010B) 250 mL HDPE j HNO3 I (6 I 5) Sample Laboratory (circle): ACL/Xenco (AES) Other Delivery Method: (Hand Delivery/Fed-Ex/UPS/Other				9			. <u></u> .	· · · · · · · · · · · · · · · · · · ·		
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Sample Collection Parameters Sample Collection Method (check all): Bailer Straw Method Pump Tubin Vacuum Jug Other Final Tubing/Pump Depth: j2,5 feet below T.O.C Final Groundwater Depth(if applic.) j2.22 feet below T.O.C Final Sample Turbidity: j. 79 NTUS (2.22 feet below T.O.C Ferrous Iron Concentration (if sampled): NA mg/L Comments: Comments: Ferrous Iron Concentration (if sampled): NA mg/L Laboratory Analytical Information Sample ID Analysis Container Qty. Preservative Time Sampled MW - 23 Total Lead (6010B) 250 mL HDPE j HNO3 I (6 I 5) Sample Laboratory (circle): ACL/Xenco (AES) Other Delivery Method: (Hand Delivery/Fed-Ex/UPS/Other					% W			hi <u></u>		
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Sample Collection Parameters Sample Collection Method (check all): Bailer Straw Method Pump Tubin Vacuum Jug Other Final Tubing/Pump Depth: j2,5 feet below T.O.C Final Groundwater Depth(if applic.) j2.22 feet below T.O.C Final Sample Turbidity: j. 79 NTUS (2.22 feet below T.O.C Ferrous Iron Concentration (if sampled): NA mg/L Comments: Comments: Ferrous Iron Concentration (if sampled): NA mg/L Laboratory Analytical Information Sample ID Analysis Container Qty. Preservative Time Sampled MW - 23 Total Lead (6010B) 250 mL HDPE j HNO3 I (6 I 5) Sample Laboratory (circle): ACL/Xenco (AES) Other Delivery Method: (Hand Delivery/Fed-Ex/UPS/Other					-				-	
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Sample Collection Method (check all): Bailer Straw Method Pump Tubing Vacuum Jug Other Final Tubing/Pump Depth: 12.5 feet below T.O.C Final Groundwater Depth(if applic.) 12.22 feet below T.O.C Final Sample Turbidity: 1.79 NTUS (2.22 Ptfler Ferrous Iron Concentration (if sampled): NA mg/L Comments:	Stabiliz	ation Info:	+/- 0.5 deg.	+/- 5%	+/- 0.1 SU	+/- 10%	+/- 10%	<10 NTUs		
Final Tubing/Pump Depth: 12,5 feet below T.O.C Final Groundwater Depth(if applic.) 12.22 feet below T.O.C Final Sample Turbidity: 1.79 NTUS (2.22) PC+ler Ferrous Iron Concentration (if sampled): NA mg/L Comments: Malysis Container Qty. Preservative Time Sampled Mui - 23 Total Lead (6010B) 250 mL HDPE I HNO3 1 (a15) Sample Laboratory (circle): ACL/Xenco (AES) Other Delivery Method: (Hand Delivery/Fed-Ex/UPS/Other	Sample C	ollection Par	ameters							
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Comments: Laboratory Analytical Information Sample ID Analysis Container Qty. Preservative Time Sampled $mu - 33$ Total Lead (6010B) 250 mL HDPE J HNO3 1615 Sample Laboratory (circle): ACL/Xenco AES Other Delivery Method: Hand Delivery/Fed-Ex/UPS/Other	-				T.O.C Fir			÷	eet below T.O.C	
Comments: Laboratory Analytical Information Sample ID Analysis Container Qty. Preservative Time Sampled $mu - 33$ Total Lead (6010B) 250 mL HDPE J HNO3 1615 Sample Laboratory (circle): ACL/Xenco AES Other Delivery Method: Hand Delivery/Fed-Ex/UPS/Other	Final S	ample Turbid	ity: 1.79	NTUS (J.J.	1 After) Fe	rrous Iron Cond	centration (if s	ampled):	NA mg/L	
Sample ID Analysis Container Qty. Preservative Time Sampled $mw - 73$ Total Lead (6010B) 250 mL HDPE J HNO3 1615 Sample Laboratory (circle): ACL/Xenco AES Other Delivery Method: Hand Delivery/Fed-Ex/UPS/Other	Comme	ents:								
Sample ID Analysis Container Qty. Preservative Time Sampled $mw - 73$ Total Lead (6010B) 250 mL HDPE J HNO3 1615 Sample Laboratory (circle): ACL/Xenco AES Other Delivery Method: Hand Delivery/Fed-Ex/UPS/Other			110 m 4.1							
mui - 73 Total Lead (6010B) 250 mL HDPE J HNO3 1615 Sample Laboratory (circle): ACL/Xenco(AES)Other Delivery Method: Hand Delivery/Fed-Ex/UPS/Other	Laborator	ry Analytical	Information			K #01 F.				
Sample Laboratory (circle): ACL/Xenco AES Other Delivery Method: Hand Delivery/Fed-Ex/UPS/Other	Sar	nple ID	Anal	ysis	Conta	iner Qty	/. Preser	vative	Time Sampled	
	ти	1-73	Total Lead (60	10B)	250 mL HDP	Ej	HNO ₃		1615	
	Comple	Laborat /	circle): ACL ()	AFF AFF	har	Doliverstaut		VE-JE (III	DC /Other	
Field Personnel Signature: Lony J Gordon	Sample	Laboratory (circle): ACL/X	encor ALS Ot	ner	Delivery Metho	a:(Hand Delive	ery/red-Ex/U	PS/Other	
	Field Perso	nnel Signatu	re: Um	421	prolon					
				100		No. 4				

AEM Groundwater Sampling Field Log

April 2014 Semi-Annual Groundwater Level Measurements Former Vulcan Plant - Dalton, Ga

Estimated	Recorded	Well	Aquifer	Apr-14	Apr-14	Lead
Time	Date	Number	Zone	DTW ¹	DTB ²	(Method 6010B)
1205	4/8/2014	MVV-4	Residuum	1,48	15.10	
1128	4/8/2014	MVV-5	Residuum	5.40	18.42	
1257	4/8/2014	MVV-6	Residuum	1.94	15.26	
1232	4/8/2014	MVV-7	Residuum	4.06	15.73	
1235	4/8/2014	MVV-8	Residuum	3.65	14.70	
1135	4/8/2014	MW-13	Residuum	2.23	11.10	
1158	4/8/2014	MVV-14	Residuum	2.96	15.06	
1210	4/8/2014	MW-15	Residuum	4.30	14.57	
1252	4/8/2014	MW-16	Residuum	1.69	15.09	
1221	4/8/2014	MW-17	Residuum	3.89	14.95	
1228	4/8/2014	MW-18	Residuum	3.65	15.15	
1218	4/8/2014	MW-19	Residuum	3.41	15.25	х
1245	4/8/2014	MVV-20	Residuum	2.88	14.44	
1123	4/8/2014	MW-21	Residuum	4.53	14.05	x
1120	4/8/2014	MW-22D	Residuum	4.74	36.81	
1112	4/8/2014	MVV-23	Residuum	5.10	19.00	х
1150	4/8/2014	TMW-19	Residuum	4.70	15.25	
1155	4/8/2014	TMW-20	Residuum	13.65	15.00	
1142	4/8/2014	PZ-1 (1")	Residuum	15.25	21.50	

¹ - Depth to Water (DTW) measured in feet from Top of Casing (TOC)

² - Depth to Bottom (DTB) measured in feet from Top of Casing

- Well Sampled

Vulcan Dalton, GA

Meter	Date	Time		pH	I	Cor	nd	uctivity (µ	uS/cr	m)	0	RP	D.O. (1	mg/L) /%	Turbidi	ty (NTU)
·15I				Before	After			Before		After	Before	After	Before	After	Before	After
	4/8/14	1341	7	7.27	7-00		1	Temperature	22.0	20	Temperature	22.20	Barometric Pressure			
#12	11-1-1	1741	4	3.99	3.99	1413		1,313	1,4	(13	226-3	2240-1	46.9%	101%	8-68	10-2
Lomolti				Before	After			Before		After	Before	After	Before	After	Before	After
	at her	17/11	7		_			Temperature	-		Temperature		Barometric Pressure	_		-
₽5	418/14	1341	4	-	1	1413		_	-		-	-	_	_	8.68	10.2
YSI				Before	After			Before		After	Before	After	Before	After	Before	After
	1.1.1.11		7	6.98	7.01		- 9	Temperature	18.50	6 "	Temperature	18.56°C	Barometric Pressure	760,00 mmty		
Pental	4/8/14	1150	4 10	3.69	4.00	1413	l	,408	1,	413	238.6	240.0	106.9%	100.0%	-	~
Jaar				Before	After			Before		After	Before	After	Before	After	Before	After
WASTE	1.1.1.1.1		7		_		- 9	Temperature		-7	Temperature	-	Barometric Pressure			
LAMOTTE #7	4/8/14	1150	4	(()	1413		_	-		-	_		_	9.27	9.98
dia				Before	After			Before		After	Before	After	Before	After	Before	After
			7					Temperature			Temperature		Barometric Pressure			
			4			1413										
			10													
				Before	After			Before	100	After	Before	After	Before	After	Before	After
			7					Temperature			Temperature		Barometric Pressure	1		
			4			1413										
			10	-												
			-	Before	After	2	-	Before		After	Before	After	Before	After	Before	After
			7				L	Temperature	1		Temperature	1	Barometric Pressure	2	-	
			4			1413										
	1	L	110	1						ORP Calit	bration Chart	1	1		1	1
Standard	1.5.5.6.00	Lot Numbe	er			Expiration	n			Temp °C	Value, mV	Notes:				
pH 7	23066880/ 22				Jun-15				11	10	250.5		Second .			
pH 4	2301425/27	10176			Dec-14					15	244.0					
					16-Aug-14	110				20	237.5					
ORP	NA/ 4917	ł			NA					25	231.0					
Turbidity	NA				NA		_		┙┣╴	30 35	224.5					
Designation	Matana	Serial #		Designation	Motors	Corial #	1	Designation	, 1	35 Meters	218.0					
Designation 1	Meters Hanna HI 991300	Contraction of the Party of the	-	Designation 4	Meters YSI 556 MPS	Serial # 06L1239AN		Designation 7		otte 2020we	Serial # e 185-3710					
2	LaMotte 2020e			5	LaMotte 2020			8		a HI 991300						
3	Hanna HI 991300		-	6	Hydac	9700142667	-	9	-	a HI 991300		Field Pers	onnel Signature			
		1	_			1			-							

APPENDIX C

Laboratory Analytical Reports

(April 2014)



ANALYTICAL ENVIRONMENTAL SERVICES, INC.



April 16, 2014

Daniel McDonnell Haley & Aldrich 501 River Street, Suite 100 Greenville SC 29601

TEL: (864) 214-8754 FAX:

RE: Former Vulcan Materials (Dalton, GA)

Dear Daniel McDonnell:

Order No: 1404902

Analytical Environmental Services, Inc. received 4 samples on 4/9/2014 8:10:00 AM for the analyses presented in following report.

No problems were encountered during the analyses. Additionally, all results for the associated Quality Control samples were within EPA and/or AES established limits. Any discrepancies associated with the analyses contained herein will be noted and submitted in the form of a project Case Narrative.

AES' certifications are as follows:

-NELAC/Florida Certification number E87582 for analysis of Environmental Water, soil/hazardous waste, and Drinking Water Microbiology, effective 07/01/13-06/30/14. -AIHA-LAP, LLC Laboratory ID: 100671 for Industrial Hygiene samples (Organics, Inorganics), Environmental Lead (Paint, Soil, Dust Wipes, Air), and Environmental Microbiology (Fungal) effective until 09/01/15.

These results relate only to the items tested. This report may only be reproduced in full.

If you have any questions regarding these test results, please feel free to call.

(Kanha)

Chantelle Kanhai Project Manager

o /oo rieshehinai raikway, Ahaina OA 30340-3704		
972-4889 / FAX: (770) 457-8188	D	Date: 4/14 Page 1 of 1
ADDRESS: 501 River street, suite 100	ANALYSIS REQUESTED	Visit our website
الو	,10 g)	www.aesatlanta.com
onnelle		your results, place bottle
signature Lond		orders, etc.
	Tet	No # 0
		NEMIAKAN
4/8/14 1615 X 1	× × × × × × × × × × × × × × × × × × ×	
410114 1845 X 0		1
4)8/14 1551 X 0		
4/8/14 1551 × 0		
	PROJECT NAME:	RECEIPT
KII616 AM	Dalton, Gcu	Total # of Containers
2. Y	PROJECT # 1398-1401 (AGM)	Turnaround Time Request
3:	n GÁ	2 Business Day Rush
· · · · · · · · · · · · · · · · · · ·	SEND REPORT TO: DAN Mc Donnell	O Next Business Day Rush
SHIPMENT N	INVOICE TO: DAM McDomeda (IF DIFFERENT FROM ABOVE)	C Same Day Rush (auth req.)
CLIENT FAREY LIPS MAIL		M (if an
HOUND OTHER	QUOTE #:	DATA PACKAGE: 1 (II) III IV
NSIDERED RECEIVED THE NEXT BUSINESS DA ION UNLESS OTHER ARRANGEMENTS ARE M.	Y. IF TURNAROUND TIME IS NOT INDICATED, AES WILL PROCEEI ADE.) WITH STANDARD TAT OF SAMPLES.
SO = Soil SW = Surface Water W = Water (Bla hly N = Nitric acid S+I = Sulfuric acid + ice S/N	DW = Drinking Water (Blanks) O = Other (specify) WW = Waste Sodium Bisulfate/Methanol + ice O = Other (specify) NA = None	Water
	THEL: (T70) 457-8177 / TOLL-FREE (800) 972-4889 / FAX: (T70) 457-8188 a Ald rich, Fric Sol Kiur Strick, Suith Carelina a $i \in I$ / $I = D$ and I (Second line downell C field Addition b $I = C$ (Lumbley (AEAN) SUBARTURE b $I = C$ (Lumble) Subarture b $I = C$ (Lum	Interime ANALYSIS REQUESTED $n/1/ner m n/1/ner m n/1/ner $

White Copy - Original; Yellow Copy - Client

Work Order: 1404962

Analytical En	vironn	nental Services,	Inc					Da	te:	16-Apr-14	
Client:	2	& Aldrich	Dolton (A)				Sample I on Date			4:15:00 PM	
Lab ID:	140490	Vulcan Materials (I 2-001	Jation, GA)			Matrix:			undwa		
Analyses			Result	Qual	MDL	Reporting Limit	Units	BatchID	DF	Date Analyzed	Analyst
METALS, TO	TAL	SW6010C				G	SW301	DA)			
Lead			0.0013	J	0.0009	0.0100	mg/L	189531	1	04/14/2014 20:04	JL

* Value exceeds maximum contaminant level

BRL Not detected at MDL

- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- NC Not confirmed

- E Estimated value above quantitation range
- S Spike Recovery outside limits due to matrix
- J Estimated value detected below Reporting Limit
- > Greater than Result value
- < Less than Result value
- Narr See case narrative

Analytical En	vironn	nental Services, l	Inc					Da	ite:	16-Apr-14	
Client: Project Name:	5	& Aldrich Vulcan Materials (E	Dalton, GA)			Client S Collecti	•			5:45:00 PM	
Lab ID:	140490	2-002				Matrix		Grou	undwa	ater	
Analyses			Result	Qual	MDL	Reporting Limit	Units	BatchID	DF	Date Analyzed	Analyst
METALS, TO	TAL	SW6010C				G	SW301	0A)			
Lead			0.0048	J	0.0009	0.0100	mg/L	189531	1	04/14/2014 20:08	JL

* Value exceeds maximum contaminant level

BRL Not detected at MDL

- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- NC Not confirmed

- E Estimated value above quantitation range
- S Spike Recovery outside limits due to matrix
- J Estimated value detected below Reporting Limit
- > Greater than Result value
- < Less than Result value
- Narr See case narrative

Analytical En	vironr	nental Services,	Inc					Da	te:	16-Apr-14	
Client:	Haley	& Aldrich				Client S	Sample I	D: MW	7-19 E	DUP	
Project Name:	Forme	Vulcan Materials (Dalton, GA)			Collecti	on Date	4/8/2	2014	3:51:00 PM	
Lab ID:	140490	02-003				Matrix		Grou	undwa	ater	
Analyses			Result	Qual	MDL	Reporting Limit	Units	BatchID	DF	Date Analyzed	Analys
METALS, TO	TAL	SW6010C				6	SW301	DA)			
Lead			BRL		0.0009	0.0100	mg/L	189531	1	04/14/2014 20:12	JL

* Value exceeds maximum contaminant level

BRL Not detected at MDL

- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank

NC Not confirmed

- E Estimated value above quantitation range
- S Spike Recovery outside limits due to matrix
- J Estimated value detected below Reporting Limit
- > Greater than Result value
- < Less than Result value
- Narr See case narrative

Analytical En	vironn	nental Services,	Inc					Da	ite:	16-Apr-14	
Client: Project Name: Lab ID:	5	& Aldrich Vulcan Materials (I 2-004	Dalton, GA)				Sample I on Date	: 4/8/2	- /	3:51:00 PM ater	
Analyses			Result	Qual	MDL	Reporting Limit	Units	BatchID	DF	Date Analyzed	Analyst
METALS, TO	TAL	SW6010C				6	SW301	0A)			
Lead			0.0010	J	0.0009	0.0100	mg/L	189531	1	04/14/2014 20:15	JL

* Value exceeds maximum contaminant level

BRL Not detected at MDL

- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank

NC Not confirmed

- E Estimated value above quantitation range
- S Spike Recovery outside limits due to matrix
- J Estimated value detected below Reporting Limit
- > Greater than Result value
- < Less than Result value
- Narr See case narrative

Analytical Environmental Services, Inc.

Sample/Cooler Receipt Checklist

Client HA/ET & ALDRICH. INC		Work Order	r Number <u>1404902</u>
Checklist completed by <u>Jack 2, c</u> Signature Date	[g]14		
Carrier name: FedEx UPS Courier Client 1/ US	S Mail Other	•	_
Shipping container/cooler in good condition?	Yes _	No	Not Present
Custody seals intact on shipping container/cooler?	Yes	No	Not Present
Custody seals intact on sample bottles?	Yes	No	Not Present
Container/Temp Blank temperature in compliance? (4°C±2)*	Yes i	No	
Cooler #1 4.0 Cooler #2 Cooler #3	_ Cooler #4	Coo	oler#5 Cooler #6
Chain of custody present?	Yes	No	
Chain of custody signed when relinquished and received?	Yes	No	
Chain of custody agrees with sample labels?	Yes 🖌	No	
Samples in proper container/bottle?	Yes 🗹	No	
Sample containers intact?	Yes 🧹	No	· .
Sufficient sample volume for indicated test?	Yes	No	
All samples received within holding time?	Yes	No	
Was TAT marked on the COC?	Yes	No	
Proceed with Standard TAT as per project history?	Yes	No	Not Applicable
Water - VOA vials have zero headspace? No VOA vials su	bmitted	Yes	No
Water - pH acceptable upon receipt?	Yes	No	Not Applicable
Adjusted?	Chec	cked by 🖌	1.1.
Sample Condition: Good Other(Explain)			77
(For diffusive samples or AIHA lead) Is a known blank includ	led? Yes	N	No

See Case Narrative for resolution of the Non-Conformance.

* Samples do not have to comply with the given range for certain parameters.

\L\Quality Assurance\Checklists Procedures Sign-Off Templates\Checklists\Sample Receipt Checklists\Sample_Cooler_Receipt_Checklists

Analytical Environmental Services, Inc

Date: 16-Apr-14

Client:	Haley & Aldrich
Project Name:	Former Vulcan Materials (Dalton, GA)
Workorder:	1404902

ANALYTICAL QC SUMMARY REPORT

BatchID: 189531

Sample ID: MB-189531	Client ID:				Uni	its: mg/L	Prep Dat	e: 04/11/	2014	Run No:	265540
SampleType: MBLK	TestCode:	METALS, TOTAL	SW6010C		Bat	chID: 189531	Analysis	Date: 04/14/	2014	Seq No:	5594779
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit R	PD Ref Val	%RPD	RPD	Limit Qual
Lead	BRL	0.0100									
Sample ID: LCS-189531	Client ID:				Uni	ts: mg/L	Prep Dat	e: 04/11/	2014	Run No:	265540
SampleType: LCS	TestCode:	METALS, TOTAL	SW6010C		Bat	chID: 189531	Analysis	Date: 04/14/	2014	Seq No:	5594778
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit R	PD Ref Val	%RPD	RPD	Limit Qual
Lead	0.9866	0.0100	1.000		98.7	80	120				
Sample ID: 1404509-009BMS	Client ID:				Uni	its: mg/L	Prep Dat	e: 04/11/	2014	Run No:	265540
SampleType: MS	TestCode:	METALS, TOTAL	SW6010C		Bat	chID: 189531	Analysis	Date: 04/14/	2014	Seq No:	5594782
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit R	PD Ref Val	%RPD	RPD	Limit Qual
Lead	1.001	0.0100	1.000		100	75	125				
Sample ID: 1404509-009BMSD	Client ID:				Uni	its: mg/L	Prep Dat	e: 04/11/	2014	Run No:	265540
SampleType: MSD	TestCode:	METALS, TOTAL	SW6010C		Bat	chID: 189531	Analysis	Date: 04/14/	2014	Seq No:	5594787
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit R	PD Ref Val	%RPD	RPD	Limit Qual
Lead	0.9865	0.0100	1.000		98.7	75	125	1.001	1.45	2)

- Qualifiers: > Greater than Result value
 - BRL Below reporting limit
 - J Estimated value detected below Reporting Limit

Rpt Lim Reporting Limit

- < Less than Result value
- E Estimated (value above quantitation range)
- N Analyte not NELAC certified
- S Spike Recovery outside limits due to matrix

- B Analyte detected in the associated method blank
- H Holding times for preparation or analysis exceeded
- R RPD outside limits due to matrix