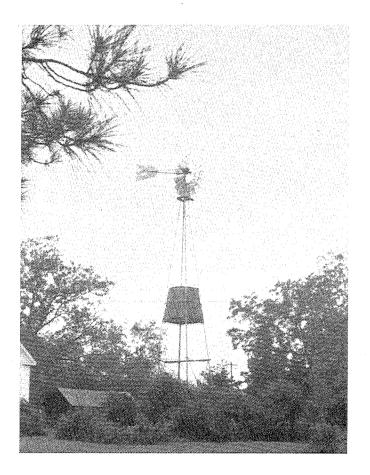
# HYDROGEOLOGY OF THE GULF TROUGH- APALACHICOLA EMBAYMENT AREA, GEORGIA

Madeleine F. Kellam Lee L. Gorday



Georgia Department of Natural Resources Environmental Protection Division Georgia Geologic Survey

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Cover Photo: Windmill on a domestic well in Tarrytown, Montgomery County, Georgia.

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Georgia Department of Natural Resources Lonice C. Barrett, Commissioner

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> Atlanta 1990

# **BULLETIN 94**



M. Wallace Holcombe

# IN MEMORIAM

Wallace Holcombe, the Geologic Survey's Senior Environmental Technician for the last ten years, passed away on October 8, 1990. Wallace was always prepared to go the extra mile to see that the needs of the Geologic Survey staff were met. His diligence in maintaining the geological equipment and field vehicles in proper working condition allowed the staff to maintain their field and laboratory schedules. Wallace's contributions to the success of this report and numerous others over the last ten years will be greatly missed. . .

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# HYDROGEOLOGY OF THE GULF TROUGH -APALACHICOLA EMBAYMENT AREA, GEORGIA

# Madeleine F. Kellam

Lee L. Gorday

# ABSTRACT

The geologic make-up and hydrologic properties of the Floridan aquifer system in the study area are controlled by the presence of the Gulf Trough-Apalachicola Embayment. The Floridan aquifer system, within the trough-embayment, is composed of dense, deep-water limestones; and it is thickly overlain by Miocene and younger sediments.

Throughout the Gulf Trough, and in most of the Apalachicola Embayment, the permeability of the aquifer is lower than that typical of the Floridan system outside the trough-embayment. This is due to a combination of factors, including the low primary permeability of the deep-water limestones of the trough-embayment; limited development of secondary permeability due to thick overburden; and, possibly, a lack of joints or fractures to enhance movement of ground water. However, certain areas within the Apalachicola Embayment and along its south flank are exceptions to this trend. The contact between the Miocene and Oligocene sediments in these areas is a zone of enhanced permeability.

The quality of water from the Floridan aquifer system is reduced in certain parts of the study area. In the Colquitt-Thomas-Grady Counties area, sluggish ground-water flow through the lower parts of the aquifer has inhibited the dissolution of gypsum and the removal of sulfate from the aguifer, causing high sulfate levels. The source of elevated levels of barium in ground water from Ben Hill County is not understood. High concentrations of natural radioactivity (mainly as Radium-226) occur in ground water from the Wheeler-Montgomery and Tift-Berrien Counties areas. The ultimate source is Uranium-238, probably derived from weathered crystalline rocks of the Piedmont. The uranium was incorporated in the crystal structure of the abundant phosphate minerals of the Miocene confining sediments. Oxidizing recharge waters flowing through these sediments dissolved uranium and transported it into the aquifer. The uranium was deposited on the aquifer matrix in areas where reducing conditions were encountered. The pyrite content of the troughembayment limestones provided such reducing conditions, as did decaying organic matter trapped in paleo-sinkholes within the top of the Oligocene strata. Radioactive decay now contributes Radium-226 to ground water in these areas.

### **INTRODUCTION**

#### GENERAL

This investigation is the culmination of a multi-year study by the Georgia Geologic Survey of the geology and ground-water hydrology of the Gulf Trough and Apalachicola Embayment, which are part of a subsurface paleo-marine channel system in the Georgia Coastal Plain. The Floridan aguifer system, the most widely used aguifer in the Coastal Plain, is affected by the presence of the Apalachicola Embayment, and by its northeastward extension, the Gulf Trough. Both the quality and the availability of ground water in and near the trough-embayment are reduced. In view of the continuing water needs of municipal, agricultural, and industrial users of this aquifer, a comprehensive study of the geology and hydrogeology of this area was conducted in order to explain the causes of reduced well yields and water quality.

This study of the Gulf Trough-Apalachicola Embayment includes three reports. A data report (McFadden and others, 1986) presents lithologic logs and a table summarizing stratigraphic data on all wells used in the ensuing geologic and hydrologic investigations. The locations of these wells are displayed on a 1:500,000 scale base map. A geologic report (Huddlestun and others, in preparation) presents the stratigraphic framework for the hydrologic investigation of the Gulf Trough and Apalachicola Embayment. The geologic report contains lithologic and faunal descriptions of stratigraphic units, isopach and structure-contour maps, and discussions of the nature, origin, and geologic history of the troughembayment. The present report, which was completed in 1988, describes the aquifers in the Gulf Trough-Apalachicola Embayment area, presents data on the availability and quality of ground water from the Floridan aquifer system, and makes recommendations for the future development of ground-water resources in the area.

# PURPOSE

The Floridan aquifer system is the most widely used aquifer in Georgia. Potentiometric maps of the Floridan system in Georgia consistently show an anomalous steepening of the potentiometric surface trending northeastward across the Coastal Plain, from Grady County in the southwest, to Bulloch County in the northeast. This anomaly roughly parallels the trend of the Gulf Trough-Apalachicola Embayment. The Floridan aquifer system in the vicinity of this anomaly exhibits poor well yields and locally reduced water quality, including abnormally high concentrations of barium, sulfate, and natural radioactivity. The present study was designed primarily to examine the hydrogeology of the Floridan aquifer system in the Gulf Trough-Apalachicola Embayment area. The goal of this study was to assess the principal controls on the occurrence, availability, and quality of ground water from the Floridan system in the study area. Specifically, the following aspects were to be addressed:

1) the cause of the potentiometric anomaly;

2) ground-water occurrence and movement in the Upper Floridan aquifer; and;

3) water quality, particularly the mechanisms which produce the abnormally high barium, sulfate, and natural radioactivity levels which appear to be associated with the Gulf Trough-Apalachicola Embayment.

# SCOPE

Prior studies of the ground-water hydrology of the Gulf Trough area were hampered by an incomplete understanding of its complex geology. This study used data from approximately 500 wells to define the stratigraphy of the Gulf Trough-Apalachicola Embayment area. The interpretation of the geology of the trough-embayment area which has emerged from this study allows a more comprehensive view of the hydrogeology of the trough-embayment area than had been possible previously. The hydrogeology phase of this study was designed (1) to describe the lithology and extent of aquifers in the vicinity of the troughembayment; (2) to produce new data on the hydraulic characteristics of the Floridan aquifer system in the Gulf Trough and Apalachicola Embayment; (3) to discuss the hydraulic characteristics of the Floridan aquifer system in the area; and (4) to examine the possible causes of the reduced quality and availability of ground water from the Upper Floridan aquifer in and near the trough-embayment.

# SOURCES OF DATA

Data for the hydrogeologic study were gathered from a variety of sources, both published and unpublished. Published sources of lithologic data and stratigraphic data include collections of well logs by Herrick (1961) and Applin and Applin (1964). A summary of petroleum exploration wells in Georgia (Swanson and Gernazian, 1979) provided stratigraphic and well location data. In addition to well logs from these sources, a number of additional wells were examined and five wells were cored and examined specifically for this project. These were all wells for which the Georgia Geologic Survey (GGS) retains cutting or core samples in its cuttings library or wells drilled (cored) specifically for this project. All are assigned a sequential registration number, known as a GGS number, and are available for inspection at the Georgia Geologic Survey in Atlanta. The stratigraphic data obtained from all the above sources have been published in Georgia Geologic Survey Information Circular 56 (McFadden and others. 1986).

Sources of unpublished geologic data include the files of the GGS in Atlanta and those of the U. S. Geological Survey (USGS), Water Resources Division office in Doraville, Georgia. These files include lithologic logs prepared by staff of the GGS and USGS and a small number of logs prepared by the staffs of petroleum exploration companies.

Hydrologic data for this study were obtained primarily from the files of the GGS, the USGS, and the Water Resources Management Branch of the Georgia Environmental Protection Division. These data include well-construction details, production-test data, and water-quality analyses. Published water-quality data were also included in this study (Grantham and Stokes, 1976). Permeability tests were conducted on cores collected during the project, and the results are summarized in Appendix D. The potentiometric maps of the Floridan aquifer used in this report were produced by the Water Resources Division of the USGS (Clarke and others, 1979; Bush and others, 1987).

#### METHODS OF INVESTIGATION

The wells chosen for inclusion in the study were those for which the most complete information was available in the form of lithologic logs or cuttings, well construction data, and verifiable locations. These locations were field checked wherever possible. Geophysical and paleontological logs were also available in some case. In addition, five wells were cored and geophysically logged, specifically, for this study.

The definition of the Floridan aquifer system in the study area was reexamined on the basis of the revised stratigraphic interpretation of the Gulf Trough-Apalachicola Embayment area. Using lithologic and geophysical logs of all wells from the stratigraphic data base, the top and base of the Floridan aquifer system in the study area were determined and its thickness was mapped. The depth to the top of the Upper Floridan aquifer was also calculated and mapped. Appendix A lists the wells used in mapping the aquifer and includes land surface elevations, depth to top of the aquifer, and elevations of its top and base. More complete information on these wells is presented by McFadden and others (1986).

Specific-capacity maps were constructed using data from well production tests. These tests varied greatly in duration, ranging from an hour or less to several days. Construction of the wells also varied widely in such details as diameter, depth, and length of open borehole. Specific-capacity indices were obtained by dividing the specificcapacity values by the length of open borehole of the well; thus, normalizing, in part, the varying well construction. Maps were constructed to show the range and distribution of specific-capacity indices. Appendix B summarizes construction data for these wells.

Time-drawdown data, needed to calculate transmissivity (T), storativity (S), and hydraulic conductivity, are very limited for the study area. However, an estimate of transmissivity can be obtained from the specific capacity (Q/s). Lohman (1979, p. 52) noted a relationship between specific capacity and transmissivity of confined aquifers which can be expressed as:

$$T = \frac{2.3(O/s_w)}{4 \pi}$$
 .  $\log (2.25Tt/r_w^2S)$ 

where pumping rate (Q), drawdown (s), and duration of test (t) are measured during the well production test, and rw is the diameter of the well.This relationship was used to estimate the transmissivity of the aquifer at wells for which time-drawdown data is not available. Pertinent data on these wells is summarized in Appendix B.

Storage cooefficients (S) for the Floridan aquifer system in the study area were, also, not generally available. A S value typical for confined aquifers (0.0001) was used in the transmissivity estimations. The effect of changes in the S on the estimated transmissivity value is relatively small; an order of magnitude change in the S value, typically, produces only an 11 per cent change in the estimated transmissivity. Transmissivity estimates derived using this method agreed well with values obtained using time-drawdown data.

Tests of vertical hydraulic conductivity were conducted on 140 core samples from the five core holes drilled for this study and from two U. S. Gypsum cores. Test samples were selected at intervals of approximately 25 feet Sampling intervals varied, however, where sample gaps occurred or where the core was fragmented. The sides of core samples were sealed by wrapping them tightly with impermeable tape. Polyvinylchloride caps were fitted on the ends of the samples and sealed with silicone sealer. The samples were oriented vertically and saturated with water. Water was introduced from the bottom of the core sample to minimize the possiblity of trapping air in the sample.

Core samples varied greatly in permeabilty, making it neccessary to employ both constant head and falling head tests. Samples with relatively high vertical hydraulic conductivity values were tested using the constant head method. In this method, a constant head gradient was established across the sample while measuring the rate of flow. A constant head was maintained by the use of an overflow tube on the supply side of the sample. The flow rate was measured by noting the time required to fill a known volume. Head gradients used ranged up to approximately 2 feet.

Measurements were made at three or more different gradients for each sample. For each measurement, the flow rate was plotted against the head gradient. If the values plotted on a line that extended through the origin, then laminar flow conditions through the sample were assumed. A non-linear plot of values was assumed to indicate turbulent flow through the sample. These samples were retested at lower head gradients. In several instances, scatter of the head gradient versus flow rate plot could not be attributed to turbulent flow. Measurements repeated several hours later showed a linear plot, suggesting that the saturation of the sample may have caused swelling of clay minerals. A longer interval between saturation and testing eliminated this problem.

When flow through the core sample was too small to be measured readily by timing the filling of a known volume, falling head tests were used. Falling head tests measure the rate at which water enters the sample. Following saturation, a tube of known cross-sectional area, open to the sample, was filled with water. The rate at which the water level in the tube dropped was measured. The initial head gradient (the difference in height between the water level in the supply tube and the discharge point) ranged up to 5.5 feet. The head values were plotted against time to insure that there were no sudden changes in the rate of decline.

Samples of low permeability, typically, required several days to saturate. Those samples which did not saturate after four days or more could not be tested and are assumed to have a vertical hydraulic conductivity of 0.001 ft/day or less. This appears to be a conservative figure, as several samples which did saturate had vertical hydraulic conductivity values lower than 0.001 ft/day.

Hydraulic conductivity values were calculated using readily available equations derived from Darcy's Law (Freeze and Cherry, 1979, p. 335-336). Vertical hydraulic conductivity data are presented in Appendix D.

Water-quality maps were produced using a combination of published and unpublished data. Sequential identification numbers were assigned to the wells and municipal water systems used in the maps, keyed to appendices which list sources of data.

# ACKNOWLEDGEMENTS

The authors would like to thank the many people whose assistance helped make this report possible. Sue Rodenbeck and Susan Mosteller collected and checked much of the data on which this study was based. Stephen McFadden partici-

pated in the early portion of this study and also provided information on research into the occurrence of radionuclides in ground water. John Fernstrom, now retired from the Georgia Environmental Protection Division's Ground-water Program, contributed data on the occurrence of natural radioactivity in the Gulf Trough/Apalachicola Embayment area. Wendell Pope, of Abner Pope and Sons Well Drilling, supplied well data and cooperated with geophysical logging of wells in the vicinity of Alapaha. Grady Thompson, of Bishop Pump and Well Service, provided well data and general observations on the nature of the Gulf Trough/Apalachicola Embayment. He also assisted in repairing a damaged inflatable packer. James Miller and Woody Hicks of the U.S. Geological Survey reviewed the manuscript and made many helpful comments.

# **DESCRIPTION OF STUDY AREA**

#### LOCATION

The 27-county study area is located in the Coastal Plain Province of Georgia. The Coastal Plain covers approximately 60 percent of the state's total area and contains Georgia's major aquifers. The study area extends northeastward from the southwestern corner of the state to the Savannah River, an area of approximately 11,550 square miles (Figure 1). The study area takes in the Apalachicola Embayment and Gulf Trough (Figure 2), as well as adjacent portions of the Coastal Plain. The Apalachicola Embayment occupies the southwestern end of the study area, and the Gulf Trough occupies the central portion.

#### **DEMOGRAPHY AND POPULATION**

The total estimated population of the study area was 492,900 in 1985 (Bachtel, 1987), with a population density of approximately 43 people per square mile. The population is primarily rural, producing agricultural and forest products as the main economic activities. A number of small cities are located in the study area, eight of which have populations in excess of 10,000. These eight cities are: Bainbridge, Douglas, Fitzgerald, Moultrie, Statesboro, Thomasville, Tifton, and Vidalia. Only Moultrie (15,508) and Thomasville (18,352) contain populations greater than 15,000 (Bachtel,

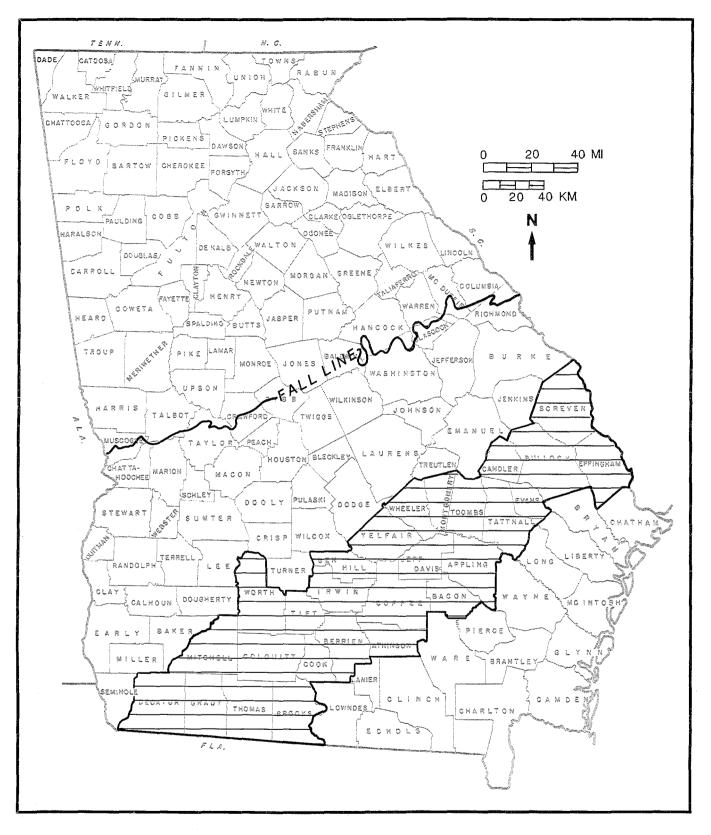


Figure 1. Location of the study area.

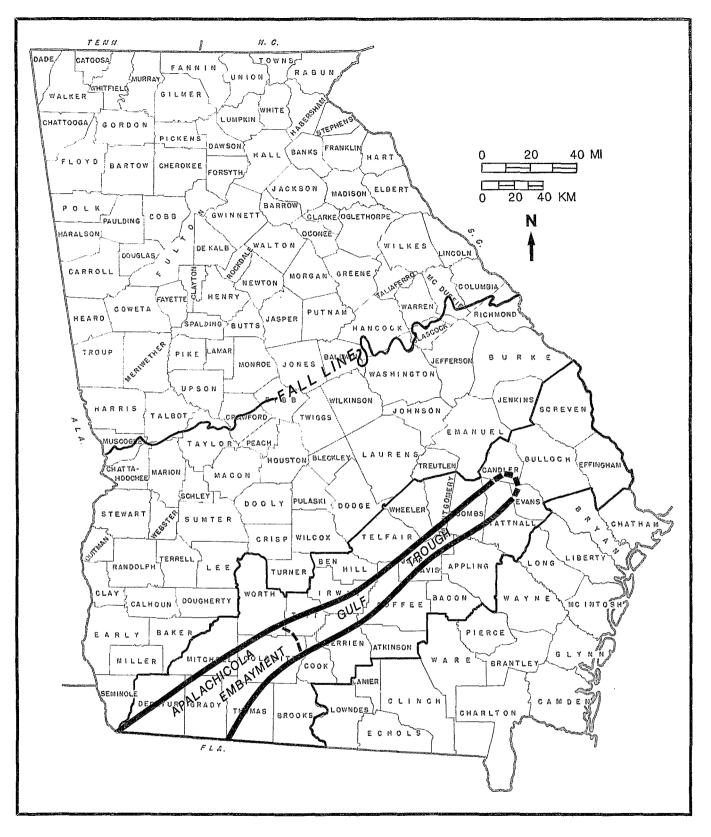


Figure 2. Approximate location of the Gulf Trough and Apalachicola Embayment. (After Huddlestun and others, in prep.)

#### PHYSIOGRAPHY AND DRAINAGE

Portions of five physiographic districts make up the study area: the Tifton Upland, Vidalia Upland, Dougherty Plain, Bacon Terraces, and Barrier Island Sequences Districts (Clark and Zisa, 1976). The Tifton and Vidalia Uplands comprise the majority of the study area (Figure 3). These two districts are topographically high areas, ranging in elevation from about 500 feet above sea level in the north and northeast to about 100 feet above sea level in the southeast. The regional slope is southeastward, towards the Atlantic coast. Drainage in these areas is well developed and dendritic.

The western edge of the study area, including portions of Decatur, Grady, Mitchell, and Worth Counties, lies in the Dougherty Plain, a gentlyrolling karstic lowland. The regional slope of this district is southwestward, towards the Gulf of Mexico. Maximum elevations of about 300 feet above sea level occur in the northeast and a minimum elevation of about 77 feet above sea level in the southwest, at Lake Seminole. The Dougherty Plain contains few surface streams but many sinkhole lakes and marshes.

Portions of Appling, Atkinson, Bacon, Ben Hill, Coffee, Irwin, and Jeff Davis Counties lie in the Bacon Terraces District, an area of subtly dissected terraces, paralleling the present coastline. Terrace levels range in elevation from about 330 to about 160 feet above sea level. Drainage is southeast-trending, dendritic, and extended.

The easternmost end of the study area, including Effingham County and portions of Bulloch and Screven Counties, lies in the Barrier Island Sequence District, an area of abandoned shorelines parallel to the present coast. This area exhibits slight to moderate dissection, with marshes occupying poorly drained lowlands.

The study area is crossed by several of the state's major rivers. The Flint River forms the western boundary of the study area and flows through Decatur County in the extreme southwestern part of the study area. The Ocmulgee and Oconee Rivers join in the vicinity of Jeff Davis, Montgomery, and Toombs Counties to form the Altamaha River. The Savannah River forms the eastern boundary of the study area.

#### CLIMATE

The climate of the study area is influenced in the west by the Gulf of Mexico and in the east by

the Atlantic Ocean. Winters are generally mild, and summers are hot and humid. The mean annual temperature for the period of record, 1951 to 1980, was 65.7° F at the Tifton experiment station of the National Oceanic and Atmospheric Administration (NOAA). Mean annual precipitation for the same period and location was 46.61 inches. March and July are, usually, the wettest months of the year in the study area; while October and November are the driest. Evapotranspiration rates are highest in the spring and summer.

# **PREVIOUS INVESTIGATIONS**

The Floridan aquifer system has been known by a number of names, among them, the principal artesian aquifer, the Tertiary limestone aquifer, the Floridan aquifer, and most recently and formally, the Floridan aquifer system. The large geographic extent of the Floridan aquifer system in Georgia has, until recently, limited the detail of most investigations. Early reports on the hydrogeology of the Floridan in Georgia were of a reconnaissance nature, due to the incompletely understood geology of the Coastal Plain. More detailed work, on a single county or smaller scale, has added to the general understanding of the hydrogeology of the aquifer; and as more detail emerges from these small studies, a larger regional picture of the Floridan aquifer system is being developed. The influence of the Gulf Trough-Apalachicola Embayment on the Floridan aquifer system in Georgia has only recently been studied.

One of the earliest reconnaissance studies of ground water in Georgia was that of McCallie (1908), who described wells and springs throughout Georgia and included many driller's logs and water-quality analyses in his descriptions. He identified the upper Eocene limestone, which he called the Vicksburg-Jackson limestone, as the major water-bearing unit of the Coastal Plain. Stephenson and Veatch (1915) related ground water to stratigraphy, and summarized the geology and water resources of the Coastal Plain by county, including information on well construction, well yields, subsurface geology, and water quality. Meinzer (1923), in his summary of groundwater occurrence in the United States, identified the Eocene and Oligocene formations of Georgia as important water-bearing strata.

In view of the rapid rate at which groundwater resource development was occurring in the Southeast, Warren (1944) published results of investigations of limestone aquifers of the Coastal

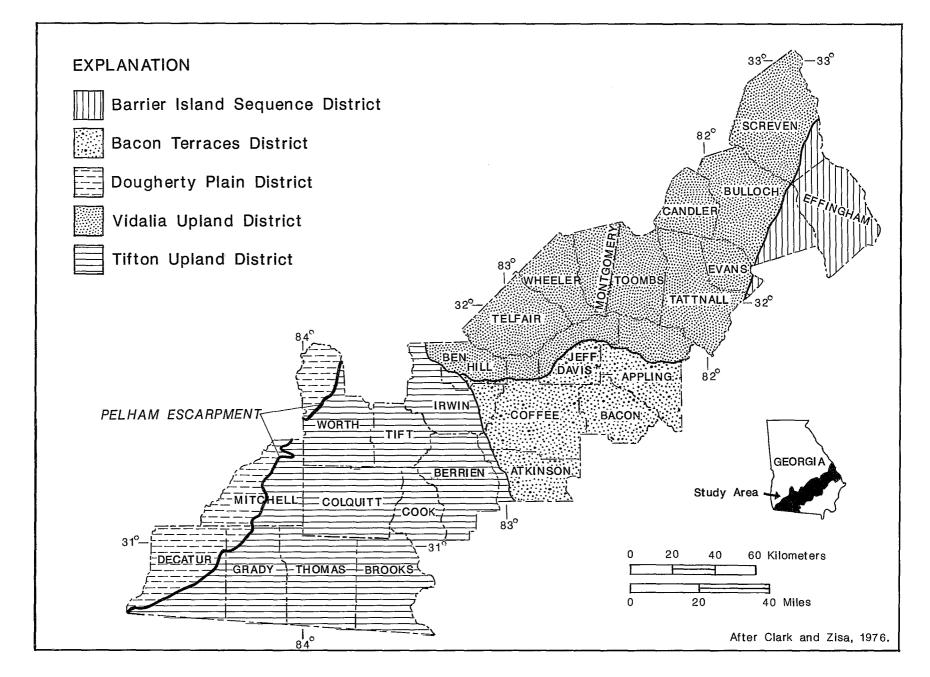


Figure 3. Physiographic districts of the study area.

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Plain. Warren noted that the principal artesian aguifers in the Southeast are limestones of Eocene and Oligocene age, which crop out in a belt extending northeastward from the southwestern corner of Georgia, roughly paralleling the Fall Line. Recharge areas were identified in the area of outcrop, and also in the Valdosta area, where lime sinks allow direct access to the aquifer. Warren included the Oligocene Suwannee Limestone and the Eocene Ocala Limestone in the principal artesian aquifer, and identified the impervious clavs and marls of the Miocene Hawthorne Formation as the upper confining unit. Transmissivity values for the principal artesian aquifer were calculated to range from 100,000 to 1,000,000 square feet per day (ft<sup>2</sup>/d). Herrick and Wait (1956) characterized the availability and quality of ground water from Coastal Plain strata, including the middle Eocene to lower Miocene principal artesian aquifer. They cited dolomitization as the cause of reduced utility of the principal artesian aquifer in the vicinity of Grady, Thomas, and Colquitt Counties, and mentioned the presence of a "subsurface structural trough" in this area as the cause of decreased permeability of the aquifer and increased hardness of the ground water. In a 1960 study, Wait described ground-water quality in the Ocala Limestone, characterizing the water as moderately hard to hard, slightly alkaline, and of calcium bicarbonate type. He noted that in some areas of the Tifton Upland, water from the Ocala Limestone contained elevated levels of sulfate. The principal artesian aquifer was redefined to include limestones of Miocene age. Wait presented water-quality data for southwestern Georgia, and discussed the relationship of structural features and sinkholes to water-quality trends in the area.

In a study that has formed the basis for much of the subsequent geologic and hydrogeologic work in the Coastal Plain, Herrick (1961) published a collection of lithologic logs of wells in the Coastal Plain of Georgia. He described well cuttings from 354 wells, noting possible water-bearing units in each.

Among the reports detailing ground-water resources of single counties in the study area was that of Owen (1963) on the geology and groundwater resources of Mitchell County. Mitchell County was divided into three hydrologic zones, the Dougherty Plain, the solution escarpment, and the Tifton Upland. Mitchell County lies, for the most part, in the Dougherty Plain. In this karstic lowland, the Ocala Limestone is at the land surface, overlain by a blanket of residuum. Water in the Ocala Limestone is under unconfined conditions, except where the overburden of clayey residuum is sufficiently thick to confine it. Wells drilled in the Dougherty Plain often tap the middle Eocene Tallahatta Formation, in addition to the Ocala. Few wells have been drilled in the solution escarpment, probably due to the greater thickness of overburden in this area. In the Tifton Upland, the Ocala Limestone is deeply buried by thick Miocene and Oligocene deposits, which Owen interpreted as evidence of downwarping in the extreme southeastern part of the county. The term principal artesian aquifer was not used in this study because the Oligocene and Eocene limestone are unconfined over most of Mitchell County.

Callahan (1964) attempted to quantify the amount of water available from Coastal Plain aquifers, including the principal artesian aquifer. The principal artesian aquifer was redefined as an aguifer system made up of a number of interconnected water-bearing strata. Aquifer geometry, flow zones, water quality, and recharge were considered. An estimated maximum "safe yield" of the principal artesian aquifer system was calculated, and the probable effects of maximum pumpage on water levels in the aquifer and in streams were assessed. Using potentiometric maps of the principal artesian aquifer, Callahan noted an apparent decrease in transmissivity in the position now identified as the Gulf Trough-Apalachicola Embavment. Two northeast-trending faults, offsetting or constricting the permeable zones of the aquifer, were postulated as the cause of this anomaly.

Sever (1966), in another small-scale study, surveyed the ground water and geology of Thomas County. He identified the Eocene Ocala Limestone and Oligocene Suwannee Limestone as the principal aquifer in the county, excluding the middle Eocene Lisbon Formation due to its highly mineralized waters. Sever noted the wide range of weli yields in Thomas County, from 60 gallons per minute (gal/min) in the northeast, to 3,000 gal/ min in the southeast; and he postulated a fault, the Ochlockonee fault, to explain the steep gradient of the potentiometric surface of the principal artesian aquifer. In addition, certain water-quality anomalies were identified, including elevated levels of sodium chloride and sulfate.

In a paper on the Tertiary limestone aquifers of the southeastern states, Stringfield (1966) identified the Ocala Limestone and the Suwannee Limestone as the major water-bearing units in Georgia, and described the hydraulic properties, recharge, and water quality of these units. The steepening of the hydraulic gradient across the Georgia Coastal Plain was discussed and a number of possible explanations were given. A written communication from H.E. LeGrand (in Stringfield, 1966, p. 123) attributed the anomaly to the proximity of the recharge area. LeGrand's theory was that there was upward leakage from the principal artesian aquifer to the overlying Miocene rocks, which diminished as the water moved under the confining Hawthorne Formation, and as the aquifer became thicker and more permeable. Stringfield (p. 132) attributed the potentiometric anomaly to "recharge and discharge relationships and...changes in the permeability and thickness of the limestone."

Sever and Herrick (1967) discussed the origin of poor-quality ground water, high in sulfate, iron, flouride, and total dissolved solids, derived from wells in the Grady County area. They concluded that this water, formerly thought to be from the Ocala Limestone, was probably being obtained from a limestone of early Oligocene age, never before described in Georgia.

Sever (1969) reported the results of aquifer tests and water-quality analyses at the cities of Alapaha, Coolidge, Fitzgerald, and Thomasville. Transmissivity values calculated for wells tapping the Oligocene and Eocene limestones ranged from 16,000 ft<sup>2</sup>/d at Fitzgerald to as large as 2,700,000 ft<sup>2</sup>/d at Thomasville. The extremely high transmissivity value obtained from the Thomasville test was attributed to solution of the limestone along structurally-produced joints and fractures. In addition to calculations of transmissivity, storage coefficients were derived where possible, and the effects of future pumpage were estimated.

Zimmerman (1977) explained variations in the transmissivity of the principal artesian aquifer in Colquitt County as the result of facies changes across a paleogeographic feature which he identified with the Suwannee Strait. Reduced transmissivity was attributed to deposition of fine-grained clastic sediments within the strait, contrasted with deposition of more permeable carbonates outside the feature. The Ochlockonee fault of Sever (1966) was used to explain such waterquality anomalies as high concentrations of dissolved solids, especially sulfate.

Krause (1979), in a study of the geohydrology of Brooks, Lowndes, and western Echols Counties, described the principal artesian aquifer in Brooks County as containing rocks of the Claiborne Group, the Ocala Limestone, Suwannee Limestone, and limestone of the lower Hawthorne Formation. These limestones are jointed, enhancing solution of the limestone and allowing conduit flow of ground water. Recharge takes place through the area's many sinkholes and permeable lake bottoms and the bed of the Withlacoochee River.

Gelbaum (1978), in a paper on the geology and ground water of the Gulf Trough, extended the trough northeastward into Screven and Effingham Counties on the basis of potentiometric maps of the principal artesian aquifer. She discussed possible causes of low yields from wells in the vicinity of the trough, suggesting that many wells may not penetrate the aquifer very deeply, or at all, due to the greater depth to the top of the aguifer in the Gulf Trough. Another possibility mentioned was a thinning of Oligocene strata in the trough, making the aquifer thinner overall. Faulting parallel to the trough and facies changes across the trough were also considered as possible causes of low well yields. In later work on the Gulf Trough, Gelbaum and Howell (1982) used specific-capacity indices to characterize groundwater flow across different areas of the trough. The potentiometric anomaly which marks the trough was described as the result of a combination of structural and depositional factors. They attributed the reduced transmissivity of the aquifer in the trough to facies changes resulting in denser limestones deposited in the trough, with downfaulted blocks locally forming ground-water flow barriers.

Bush (1982) simulated the predevelopment flow in the Tertiary limestone aquifer. The model revealed that the majority of flow in the aquifer prior to development occurred in the unconfined and thinly confined portions of the aquifer. In these areas, high recharge and discharge produced an active shallow flow zone and a less active deeper zone. Transmissivity values for unconfined and shallowly confined areas commonly exceeded 1,000,000 square feet per day (ft2/d). The thickly confined areas of the aquifer had lower transmissivities, due to the retarded discharge and sluggish ground-water flow.

The geology and configuration of the top of the Floridan aquifer system was mapped by Miller (1986). He followed Gelbaum in attributing the reduced transmissivity of the aquifer in the trough to faulting, stating that extensive graben faulting along the trend of the trough could have dropped low-permeability Miocene clastics into contact with permeable limestones of the aquifer, effectively damming ground-water flow across the trough. In 1986, Miller restated this conclusion in the context of a Regional Aquifer System Analysis (RASA). Although this work is the most complete and comprehensive report on the geology of the Floridan aquifer system to date, it employed relatively few data specific to the Gulf Trough-Apalachicola Embayment area.

An unpublished M. S. thesis by Korosy (1984) delineated ground-water flow patterns in the Ochlockonee River area of northwest Florida and southwest Georgia. Korosy used uranium isotope distributions to identify recharge areas and areas where the development of secondary permeability in the limestones of the Floridan aquifer is inhibited by retarded ground-water flow and thick overburden.

# GEOLOGIC FRAMEWORK

The study area is located in the Coastal Plain geologic province. The Coastal Plain is underlain by a seaward thickening wedge of sediments ranging in age from late Cretaceous to Holocene, resting unconformably on a basement complex of Piedmont crystalline rocks; Triassic grabens filled with red-bed sediments and volcanic rocks; and Paleozoic sedimentary rocks. Coastal Plain sedimentary units generally dip to the southeast and exhibit an outcrop pattern that strikes northeast to southwest. The oldest outcropping sedimentary units of the Coastal Plain are exposed along the Fall Line in southwest Georgia, and the youngest crop out along the coast.

The Apalachicola Embayment along with the Gulf Trough, its narrow northeastward extension, is a linear, subsurface depression continuous with the Gulf of Mexico (Figure 2). The troughembayment exhibits as much as 600 feet of buried relief and varies in width from 35 miles in the extreme southwestern corner of the state to approximately 6 miles at its narrowest in Jeff Davis County. The feature cannot be traced east of central Bulloch County.

The Gulf Trough-Apalachicola Embayment area is distinguished by radical changes in the geometry and lithology of stratigraphic units in the study area (Plate 1). The presence of the Gulf Trough is first apparent in Claibornian-age sediments, which show a facies boundary between clastic and carbonate sedimentation which approximates the position of the trough-embayment. Claibornian sediments are also anomalously thin in the vicinity of the feature. The Upper Eocene in the trough-embayment is represented by a dense, fine-grained, relatively deep-water limestone that is thinner than the adjacent Upper Eocene Ocala Limestone. The boundary between Eocene and Oligocene sediments is difficult to distinguish in well cuttings from the trough-embayment, due to their lithologic similarity. The Lower Oligocene Ochlockonee Formation of the trough-embayment is a dense, fine-grained limestone. There is no typical Suwannee Limestone in the troughembayment. The Okapilco Member of the Suwannee, a coarser-grained, more variable, coralline limestone, occupies its stratigraphic position. In general, the Oligocene section in the trough-embayment is thicker than normal and contains a deeper-water faunal assemblage. Lower Miocene sediments in the trough-embayment are also unusually thick, particularly the Parachucla Formation of Aquitanian age.

The Apalachicola Embayment and Gulf Trough are interpreted to have been produced by the Suwannee Current which flowed from the Gulf of Mexico to the Atlantic Ocean and inhibited sedimentation in the trough-embayment during the middle and upper Eocene (Huddlestun and others, in preparation). Falling sea level during the Early Oligocene probably initiated the cessation of the current. The filling of the troughembayment began, continuing into the lower Miocene.

Plate 1 shows generalized stratigraphic columns for representative parts of the study area. The stratigraphy and geologic history of the Gulf Trough and Apalachicola Embayment are complex, and this report addresses only those aspects pertinent to a discussion of the hydrogeology of the area. For a more thorough treatment of the geology of the Gulf Trough-Apalachicola Embayment area, the reader is referred to Huddlestun and others (in preparation).

# HYDROLOGIC FRAMEWORK

#### GENERAL

Aquifers are rock units which store significant quantities of water and transmit that water to wells which tap the rock units. The amount of water considered to be significant varies with the water needs and water availability of an area. A confined, or artesian, aquifer is one which is overlain by a layer of relatively impermeable material. Pressure in the aquifer exceeds atmospheric pressure, causing water to rise above the level of the aquifer in tightly cased wells tapping the aquifer. The imaginary surface, coinciding with the level to which water from the aquifer will rise in artesian wells is called the potentiometric surface. An unconfined aquifer is one which contains water in contact with the atmosphere by way of the open spaces in the permeable material. The upper surface of water in an unconfined aquifer is called the water table. For this reason, unconfined aquifers are also called water-table aquifers. Water in unconfined aquifers is at atmospheric pressure at the water table. The configuration of the water table is usually a subdued replica of the land surface.

The Coastal Plain province of Georgia contains the State's major aquifers. Of these, the Upper Floridan aquifer, a confined carbonate aquifer of Middle Eocene to Oligocene age, is the most widely used. In much of the study area, the Floridan is overlain by sediments of Miocene and younger age, which are sufficiently permeable to form an unconfined surficial aquifer. The surficial aquifer in the study area locally yields quantities of water sufficient for domestic supply.

Other major aquifers which extend into the study area include the Clayton, Claiborne, and Providence aquifers and the Cretaceous aquifer system. All are confined aquifers. Because these aquifers are more deeply buried than the Floridan aquifer system, they are used extensively only in areas where the Floridan system is absent or yields insufficient water. Increased costs associated with the drilling of deep wells make use of the Floridan aquifer system the most practical in areas where it yields sufficient water.

#### SURFICIAL AQUIFER

Miller (1986) noted that the Floridan aquifer system in most places is overlain by an unconfined surficial aquifer (Figure 4). In the study area, the surficial aquifer is composed of sediments of Miocene to Holocene age, which vary greatly in thickness and permeability. In areas where the Upper Floridan aquifer or its upper confining unit crop out, such as the Dougherty Plain (Figure 4) no surficial aquifer is present.

The surficial aquifer in the majority of the study area is made up primarily of unconsolidated clastic sediments of the Miocene Hawthorne Group. Although the Hawthorne Group sediments are characteristically high in clay content and act as the upper confining unit for much of the Floridan aquifer, they vary greatly in lithology over the study area. Beds of coarser material locally yield supplies of water adequate for domestic supply. The Hawthorne Group also varies greatly in thickness in the study area, due to the presence of the Gulf Trough-Apalachicola Embayment. Deposition of the Hawthorne Group sediments completed the majority of infilling of the trough, primarily through deposition of the limestones of the lower Miocene Parachucla Formation.

Areal variations in lithology produce widely different well yields over the study area, even in wells drilled to the same depths, or in the same formations. Although the Parachucla Formation contains considerable amounts of dense dolomite, it may locally yield adequate amounts of water for domestic supply, particularly in areas where it contains beds of coquinoid limestone. Seasonal variations in water levels and well yields may also be extreme, as water-table aquifers respond quickly to fluctuations in precipitation. The surficial aquifer is used primarily for domestic supply because of its small and variable well vields. Locally, the surficial aquifer may yield adequate water for other purposes, but in drought years water supplies from this aguifer often prove to be unreliable. Even in areas where it is not used to supply water to wells, the surficial aquifer is important as a source of recharge to the Upper Floridan aquifer.

#### FLORIDAN AQUIFER SYSTEM

The Floridan aquifer system is a thick sequence of permeable carbonate rocks, ranging in age from Paleocene to Miocene, which are in some degree of hydraulic connection. The Floridan aquifer system blankets all of Florida, most of the Coastal Plain of Georgia (Figure 5), and adjacent portions of South Carolina and Alabama. The Floridan aquifer system consists of a single permeable zone in its updip regions, confined by less permeable sediments. Downdip, the aquifer system contains two permeable zones, the Upper and Lower Floridan aquifers, separated by one of a number of local confining units designated by Miller (1986) as middle confining units I-VIII. The Floridan aguifer system is represented only by the Upper Floridan aguifer throughout most of the study area. Although Miller (1986) and Bush (1982) mapped an intra-aquifer low permeability zone in the area southeast of the Apalachicola Embayment, this study did not divide the aquifer system into upper and lower permeable zones. The Floridan aquifer system is separated from the surficial aquifer by a relatively impermeable confining unit. This upper confining unit varies considerably in age, lithology, thickness, and permeability. The interbedded clays and sands of the Miocene Hawthorne Group form the confining unit for the Floridan aquifer system over most of the Coastal Plain of Georgia. Locally, however, the Miocene section also contains dense dolomites or other carbonate layers which form a portion of the confining unit. The Suwannee Limestone, a major component of the Upper Floridan aquifer, locally

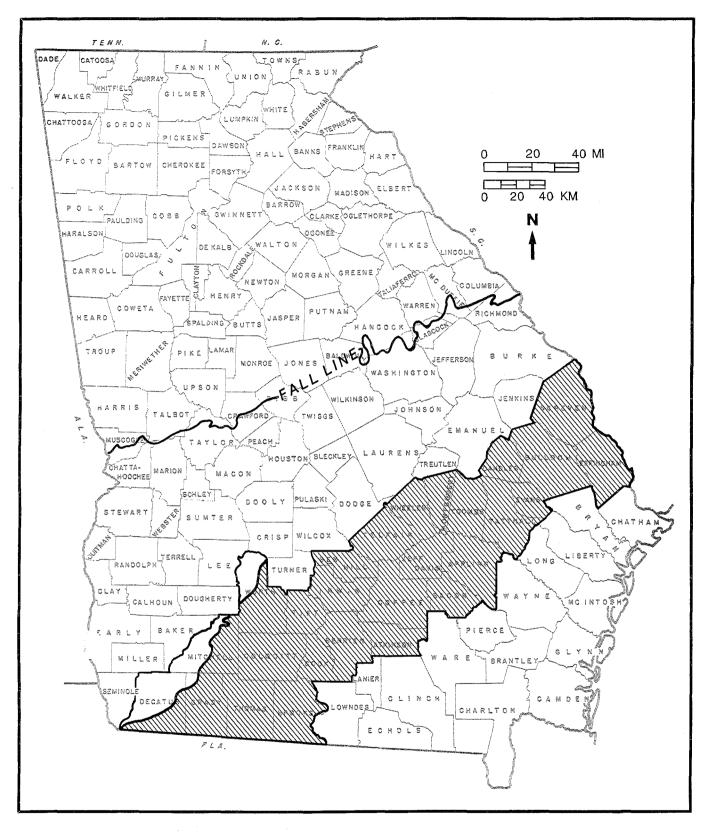


Figure 4. Geographic extent of the surficial aquifer in the study area. Shaded area indicates aquifer. (After Miller, 1986.)

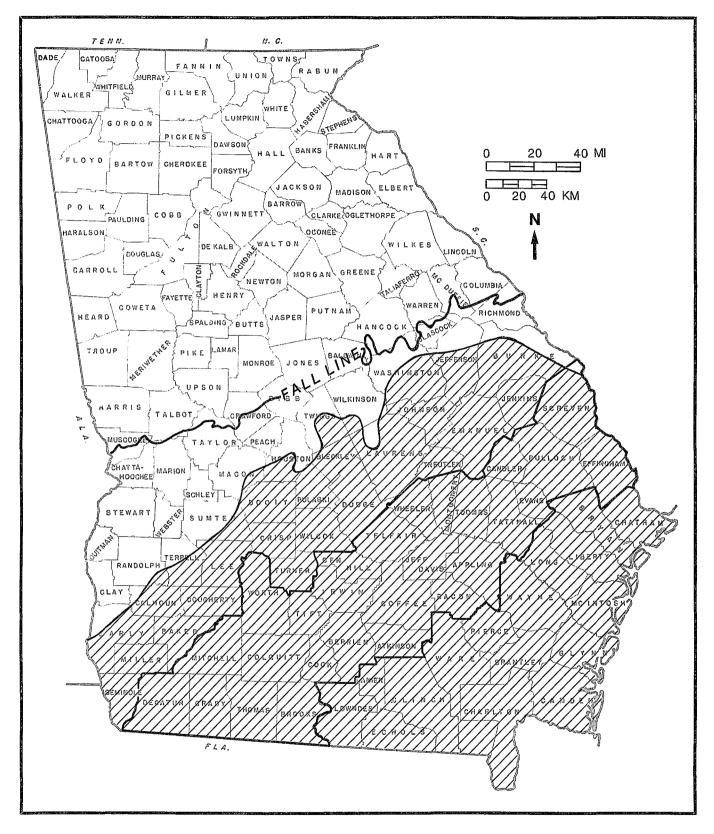


Figure 5. Geographic extent of the Floridan aquifer system. Shaded area indicates aquifer. (After Miller, 1986.)

forms a part of the confining layer.

The stratigraphic relationship between the Miocene and the Oligocene sediments in the study area is complex, and for this reason, the top and thickness of the upper confining unit of the Floridan system have not been mapped. Plate 2 shows the thickness of all sediments overlying the Floridan aquifer system, including both the surficial aquifer and the upper confining unit of the Floridan system.

The confining Miocene sediments have been removed by erosion in parts of the study area. The Pelham Escarpment, an erosional feature of the Coastal Plain, divides the Dougherty Plain in southwestern Georgia from the Tifton and Vidalia Uplands of the central Coastal Plain. West of this scarp, erosion has removed most of the Miocene sediments and all but a fringe of Oligocene sediments. The Upper Eocene Ocala Limestone, a major part of the Floridan aquifer system, is exposed at the surface, overlain only by clavey residuum. Locally, this residuum is sufficiently thick and impermeable to produce confined or semi-confined conditions in the Floridan. The upper confining unit has been breached by the Withlacoochee River and by numerous sinkholes in Brooks County, and in the Lowndes and western Echols Counties to the east. Recharge to the Floridan aquifer system takes place in this area from the river and through sinkholes and porous lakebeds (Krause, 1979).

The boundaries of the Floridan aquifer system cross both rock- and time-stratigraphic boundaries. Within the study area, the Upper Floridan aquifer is primarily Middle Eocene to Oligocene in age. Any of these units may be of low permeability locally and may be excluded from the aquifer as a result. The massive limestone of the lowermost Miocene may form a part of the aquifer in a few small areas.

Plates 3 through 5 illustrate the geology and geometry of the Floridan aquifer system in the study area. The geology and configuration of the top of the aquifer is shown in Plate 3, as determined by examination of well cuttings, cores and geophysical logs and by permeability testing of core samples. The top of the aquifer in the study area conforms most closely to the top of Oligocene sediments. Exceptions include areas such as the Dougherty Plain, where the Oligocene sediments have been removed by erosion, and the southcentral part of the Apalachicola Embayment, where the lowermost Miocene limestones may be sufficiently permeable to form a portion of the aquifer.

The regional strike of the top of the Floridan

aquifer system is southwest to northeast, but the direction of dip varies due to the presence of the Gulf Trough-Apalachicola Embayment. The top of the aquifer also varies in degree of dip, from a rate of 3.5 feet per mile southeast of the Apalachicola Embayment to 62 feet per mile on the south flank of the Gulf Trough. The subsurface relief of the top of the aquifer in the trough-embayment averages 350 feet, with a maximum of approximately 500 feet in the vicinity of southwestern Tift County.

Plate 4 shows the geology and configuration of the base of the Floridan aquifer system. This boundary is the base of the lowermost permeable limestone, as determined on the basis of well cuttings, cores, electric logs, and permeability tests. The lower confining unit varies in age and lithology, from the impermeable limestones of the upper Eocene in the Thomas-Brooks-southeastern Colquitt-southern Cook Counties area, to indurated sands of the middle Eocene southeast of the Gulf Trough.

Plate 5 shows the thickness of the Floridan aquifer system in the study area. At its thickest, near the central portion of the study area, the aquifer is 800-900 feet thick. The aquifer is thinnest in Screven and northern Effingham Counties where the Oligocene and upper Eocene limestones grade into clastic sediments. The aquifer is also thin in the Apalachicola Embayment and southwestern Gulf Trough, where impermeable limestones make up the lower portion of the Oligocene section.

The Gulf Trough-Apalachicola Embayment is an area of rapid and complex facies changes. The trough-embayment contains limestones of a deeper-water origin than those beyond the flanks of the feature (Huddlestun and others, in preparation). Thus, the flanks of the trough-embayment represent areas of rapid facies change. Additional facies changes mark the transition from the Apalachicola Embayment to the Gulf Trough, and also the northeastern termination of the Gulf Trough. The relationship of the Floridan aquifer system to the stratigraphic units in the study area is shown on Plate 1, using a series of stratigraphic columns keyed to various parts of the study area. Complete descriptions of these stratigraphic units can be found in Huddlestun and others (in preparation).

# **CLAIBORNE AQUIFER**

The Claiborne aquifer extends into the western part of the study area (Figure 6), and it underlies the Floridan system in Mitchell, northern Worth, and extreme northwestern Colquitt Counties (McFadden and Perriello, 1983). The

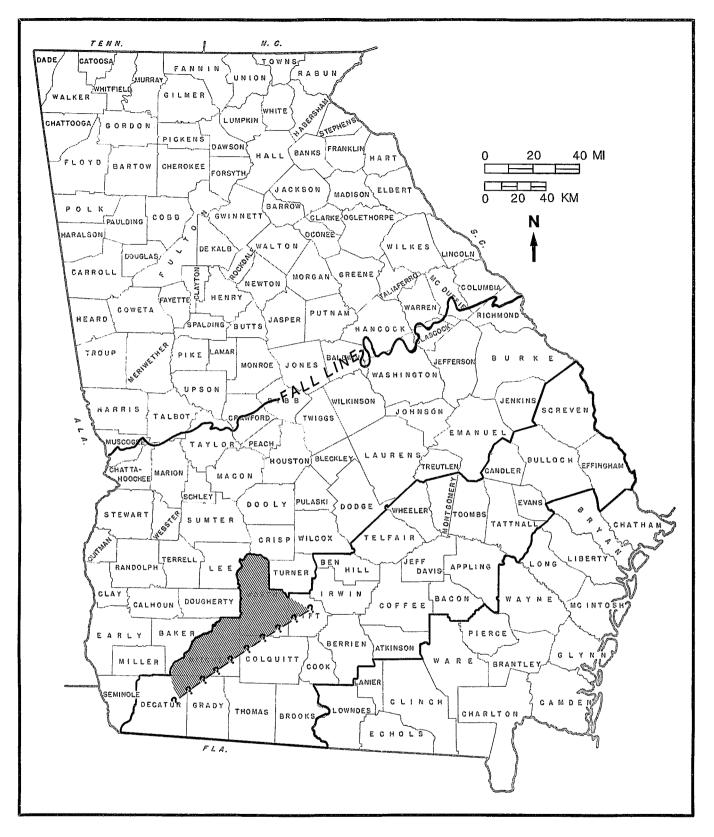


Figure 6. Approximate geographic extent of the Claiborne aquifer in the study area. Shaded area indicates aquifer. (After Arora, 1984.)

Claiborne aquifer is composed of Middle Eocene sands of the Tallahatta Formation in its updip portion, and in some areas it includes clastic sediments of the lower part of the overlying Lisbon Formation and the underlying Hatchetigbee Formation. The Claiborne is confined above by the clay-rich upper part of the Lisbon Formation. In the downdip region, where the Claiborne aquifer enters the study area, the distinctions between the Claiborne aguifer and the overlying Floridan aguifer system become less distinct due to facies changes in both aquifers. Although the Upper Eocene to Middle Eocene section is carbonate, the uppermost Claiborne sediments consist of relatively impermeable glauconitic limestones which serve to confine the Claiborne aquifer.

Recharge to the Claiborne aquifer is through its outcrop area in the northwestern part of the Coastal Plain and possibly through downward leakage from the Floridan aquifer system. Outside the study area, in the vicinity of Albany, declining head in the Claiborne aquifer may be causing such leakage (McFadden and Perriello, 1983). Potentiometric declines in the Albany area, and throughout the area occupied by the Claiborne aquifer, suggest that it is not a good candidate for extensive development in the study area.

# CLAYTON AQUIFER

The Lower Paleocene Clayton aguifer extends into the study area in western Mitchell and northern Worth Counties (Figure 7). This aquifer underlies the Claiborne aquifer and is separated from it by a confining unit which consists of the Nanafalia Formation and the clay-rich upper Clayton Formation (McFadden and Perriello, 1983). The Clayton aquifer is made up of permeable limestone of the middle unit of the Clayton Formation. It locally includes permeable sands of the upper and lower parts of the Clayton Formation. The Clayton aquifer is confined below by clay layers in the lower Clayton Formation and upper Providence Sand. Recharge is by leakage from other aquifers and by infiltration in the area of outcrop. This aquifer has a relatively small outcrop area; thus recharge to it is limited (McFadden and Perriello, 1983).

The Clayton aquifer has been extensively developed in the area northwest of the Apalachicola Embayment. Large ground-water withdrawals, combined with the limited recharge to this aquifer, have resulted in dramatic head declines in the Clayton aquifer. Although a small portion of this aquifer extends into the study area, its future development potential is low. Because this aquifer underlies the more productive Floridan aquifer system, no wells tapping the Clayton exclusively are known in the study area.

#### **CRETACEOUS AQUIFERS**

The interbedded sands and clays of the Cretaceous stratigraphic units of the Coastal Plain form a number of aquifers and intervening confining units throughout the area. Pollard and Vorhis (1980) identified seven such Cretaceous aquifers in the Coastal Plain and designated them aquifers  $A_1$  through  $A_7$ . These aquifers are rarely tapped in the study area, due to the ease of obtaining water from the shallower Floridan aquifer system.

Aquifer  $A_1$  extends into Screven County, in the northeastern portion of the study area. In 1976, 1.5 million gallons of water were pumped from this aquifer for industrial use in Screven County (Pollard and Vorhis, 1980).

The Providence aquifer of southwestern Georgia, also called Aquifer  $A_2$ , is unconformably overlain by the Clayton Formation. It is composed of the the upper sand member of the Upper Cretaceous Providence Sand. Lithology of the aquifer is variable, ranging from a sand in the updip region to a coquina in the downdip region. The aquifer underlies a portion of Mitchell County, and the northern part of Worth County. Recharge to the Providence aquifer is through its area of outcrop. Discharge is to streams and also to the Clayton aquifer, through upward leakage. The declining head in the Clayton aquifer has increased the potential for such upward leakage.

Pollard and Vorhis (1980) also identified an aquifer, which they designated  $A_3$  composed primarily of the Cretaceous Cusseta Sand. Where aquifer  $A_3$  underlies the study area, it is not separated from the Providence aquifer (aquifer  $A_2$ ) by a confining unit. Hence, Pollard and Vorhis called this aquifer  $A_2C_2A_3$ , also called the Providence-Cusseta aquifer. No wells are known in the study area which tap this aquifer exclusively.

The greatest development potential for the Cretaceous aquifers is north of the study area, in their updip regions, where they are closer to the surface and contain a greater percentage of sand. Due to the availability of water from the shallower Floridan aquifer system, the Cretaceous aquifers are rarely tapped in the study area. Northeast of the Gulf Trough, aquifer  $A_1$  is used quite extensively, and the Providence aquifer is used in the vicinity of Albany and Americus. Potential for use of the Providence aquifer also exists in northerm

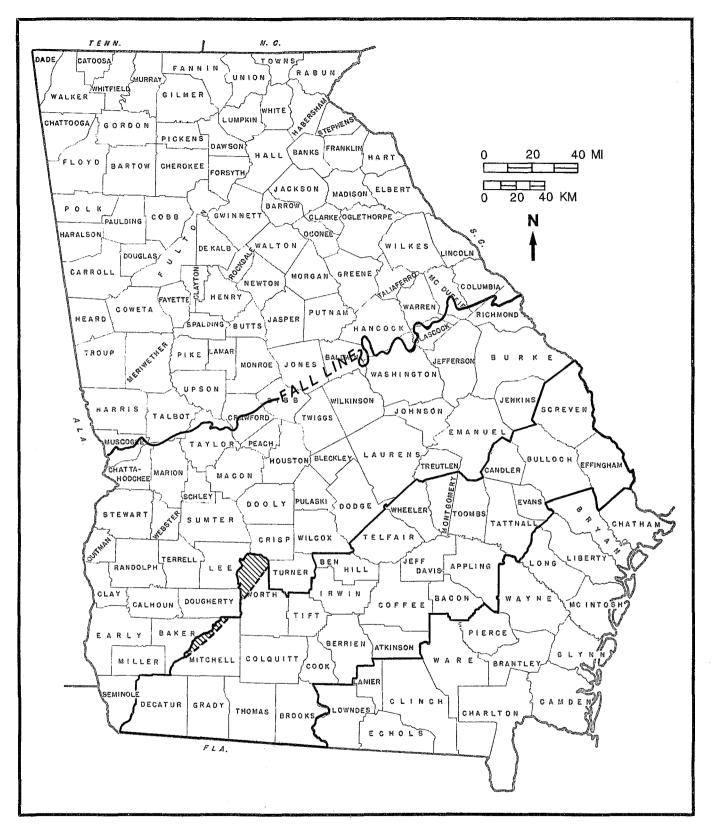


Figure 7. Approximate geographic extent of the Clayton aquifer in the study area. Shaded area indicates aquifer. (After Arora, 1984.)

Worth County. Although deeper Cretaceous aquifers cross the Gulf Trough study area, few wells are known which tap them exclusively, and development potential for these aquifers in the study area is quite low at present. The reader is referred to Pollard and Vorhis' (1980) study of the Cretaceous aquifers for a more complete treatment of their hydrology.

# POTENTIOMETRIC TRENDS AND WATER USE

#### GENERAL

The potentiometric surface of a confined aquifer is an imaginary surface connecting the altitudes to which water will rise in tightly cased wells tapping the aquifer. Water rises in the wells due to hydraulic head. A potentiometric map is a contour map of this imaginary surface, constructed from water-level measurements made in wells completed in the aquifer. The varying altitudes on a potentiometric map represent hydraulic head values. The slope of the potentiometric surface is, therefore, the hydraulic gradient. Ground water flows downgradient, from areas of high hydraulic head to areas of low hydraulic head. Under isotropic conditions, flow directions are perpendicular to the potentiomentric contours, and for this reason, potentiometric maps reveal ground-water flow patterns.

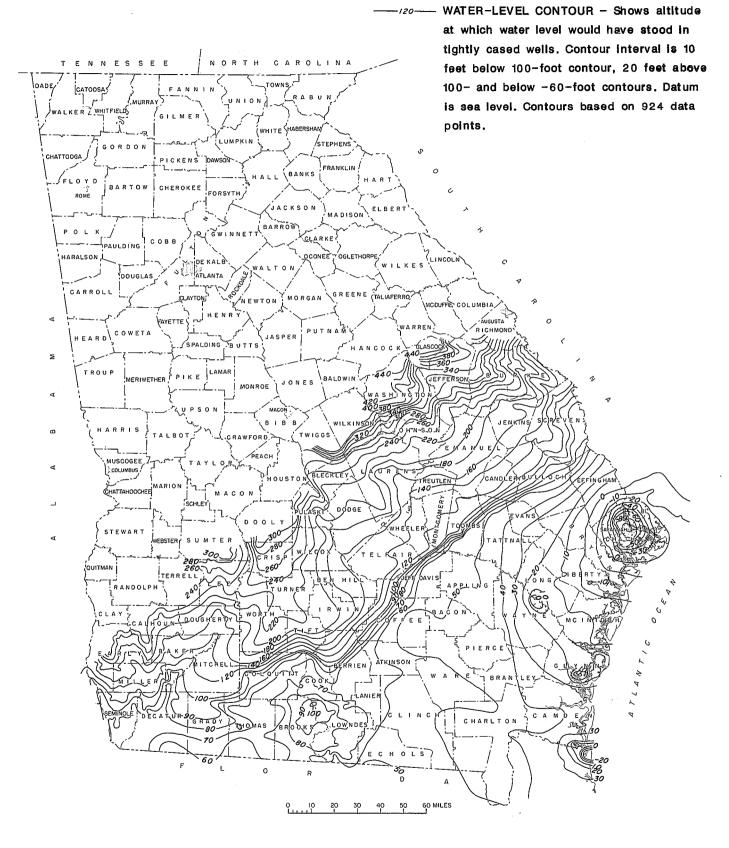
# POTENTIOMETRIC SURFACE OF THE UPPER FLORIDAN AQUIFER

Many factors influence the configuration of the potentiometric surface of a confined aquifer. Aquifer properties, recharge to the aquifer, and discharge from the aquifer interact to produce the ground-water conditions depicted by the potentiometric map. The potentiometric map of the Upper Floridan aquifer in Georgia shows highest head values at the northwestern limit of the aquifer, near its outcrop area (Figure 8). Head values generally decline southeastward, with the steepest hydraulic gradient perpendicular to the trend of the Gulf Trough. A "dome" or high area appears in the Brooks-Lowndes-Thomas-Cook Counties area. East of this high, the potentiometric surface is relatively flat, with head values declining eastward. This smooth eastward slope is broken by four significant lows in the potentiometric surface, caused by high water use at Savannah, Brunswick, St. Marys, and the Jesup-Doctortown area.

The physical properties of the aquifer, such as transmissivity and storage coefficient, can affect the steepness of the hydraulic gradient. For example, low transmissivity may produce a steep hydraulic gradient, visible on the potentiometric map as closely spaced contours. The potentiometric map of the Upper Floridan aquifer in Georgia illustrates this point (Figure 8). The highly permeable, locally cavernous limestones which make up the aquifer outside the Gulf Trough have very high transmissivity values, typically greater than 10.000 ft<sup>2</sup>/d and commonly greater than 100,000  $ft^2/d$ . The potentiomentric surface of the Floridan system in the Atkinson-southeastern Coffee-Bacon-Appling Counties area, where the Suwannee and Ocala Limestones form the bulk of the aquifer, is characterized by an extremely low hydraulic gradient. This contrasts with the northern Berriennorthwestern Coffee-northwestern Jeff Davis Counties area of the Gulf Trough, where the dense, micritic to dolomitic limestones of the trough have a much lower transmissivity, typically 10,000 ft<sup>2</sup>/d or less. This is illustrated by the potentiometric contours, which are closely spaced across the trough. The Gulf Trough cannot be detected east of central Bulloch County. This is reflected by the potentiometric contours, which begin to diverge in this area.

Recharge to an aquifer and discharge from it also affect the configuration of the potentiometric surface. Recharge areas are characterized by high hydraulic head. On the potentiometric map, high head values can be observed in the Dougherty Plain, where recharge occurs by the direct infiltration of rainfall. Another recharge area appears as a potentiometric "dome" or high area in the vicinity of Lowndes, Brooks, eastern Thomas, and southern Cook Counties, where the upper confining unit is breached by numerous sinkholes and by the Withlacoochee River, allowing recharge to enter the system rapidly. Natural discharge from an aquifer occurs where a stream is in hydraulic connection with an aquifer and the hydraulic head of the stream is lower than that of the aquifer. The Floridan aquifer in the western portion of the study area discharges to the Flint River south of Albany.

Other types of natural discharge are possible. Leakage to other aquifers can occur, but it does not show on potentiometric maps because it is diffuse. This type of discharge can occur when an adjacent aquifer has suffered severe head declines as a result of pumping. Leakage between aquifers is sometimes apparent as an overall



**EXPLANATION** 

Figure 8. Water level in the Upper Floridan aquifer, May 1985 (Clarke, et. al., 1986).

lowering of head values over time in the affected area. Large quantities of water are also discharged offshore, beyond the scope of most potentiometric mapping.

Pumpage from wells is a major type of groundwater discharge. During 1980, pumpage from the Floridan aquifer system in Georgia totaled more than 600 million gallons per day (Krause and Hayes, 1981). Sustained pumpage from an aquifer can result in water levels lower than predevelopment levels. The May 1985 potentiometric map of the Upper Floridan aquifer system (Figure 8) shows several areas where the water levels have been lowered as a result of pumpage. The cities of Savannah and Brunswick, on the Georgia Coast, are areas of such water-level declines. The concentric, hatchured contour lines centered on these cities delineate a type of feature called a cone of depression. A cone of depression can be produced around any pumping well; however, extensive, sustained pumpage is required to produce a regional cone of depression, such as those shown.

#### POTENTIOMETRIC TRENDS

The potentiometric surface of an aquifer is not static. Climatic variations cause changes in the water levels in an aquifer, through changes in precipitation and infiltration rates, evapotranspiration rate, and stream stages. All of these factors influence the amount of water available for recharge to the aquifer. These climatic changes, in turn, produce dramatic variations in water levels through pumpage. Ground-water levels in the Floridan aquifer system in Georgia are generally lowest in the late fall following the driest months of the year, when evapotranspiration rates are high and agricultural withdrawals are heavy. Water levels are generally highest in spring, following late winter and spring rains coupled with low evapotranspiration rates. These short-term fluctuations in water levels are best observed by studying hydrographs, or graphic records, of water levels in a single well or stream over time.

Long-term fluctuations also occur in the potentiometric surface of aquifers, and these changes are magnified when the aquifer is developed. Long-term fluctuations in the potentiometric surface occur when there are prolonged changes in recharge, discharge, or flow paths, such as those produced by drought or by increased pumpage from wells. These long-term changes can be observed by studying hydrographs or by constructing water-level change maps.

In northeastern Ben Hill County, in the updip portion of the aquifer, the Upper Floridan is thinly confined and close to a recharge area. Figure 9a clearly shows the seasonal variation, with waterlevel highs produced by peak recharge in the late winter and spring and lows occuring in the summer and fall. The drought years of 1981 and 1986 produced record low water levels, but water-level recovery was rapid. Little water-level decline was observed in this well during the period of record (1972-1987). A similar pattern can be observed in the record from the Mitchell County well (Figure 9b), which is also thinly confined and close to a recharge area, the Dougherty Plain. This hydrograph shows the 1981 drought to have been locally more severe than that of 1986.

The hydrograph of the city of Sylvester well, in Worth County, shows subdued seasonal peaks (Figure 10a). The Floridan system is more thickly confined in this area, which contributes to this effect. The drought years of 1981 and 1986 are clearly indicated. This hydrograph suggests a greater long-term decline in the potentiometric surface in the Sylvester area than in the lessthickly-confined areas to the north and northeast. The Toombs County well (Figure 10b), near the city of Vidalia, experienced a steady potentiometric decline for the period of record (1974-1987). with a more severe decline during the drought of 1986. The subdued peaks of the curve show that this well is located in an area where the aquifer is thickly confined.

Other types of water-level fluctuations are possible, including those caused by pumping, by atmospheric pressure changes, and by aquifer loading (Hendry and Sproul, 1966). Pumping a well causes a drop in water level in that well and produces a cone of depression in the potentiomentric surface around the well. Other wells located inside the radius of influence of the pumping well will also show declines in water levels. Atmospheric pressure changes also cause water-level fluctuations. When atmospheric pressure decreases, water levels rise, and when atmospheric pressure increases, water levels drop. Aquifer loading can also cause changes in water levels, and may be responsible for a portion of the water-level rise noted after periods of increased rainfall. The sediments overlying a confined aquifer become saturated with water and exert increased pressure on the aquifer, thus raising water levels. Changes in water levels caused by atmospheric pressure changes and aquifer loading are are minor.

Water-level change maps show the net change

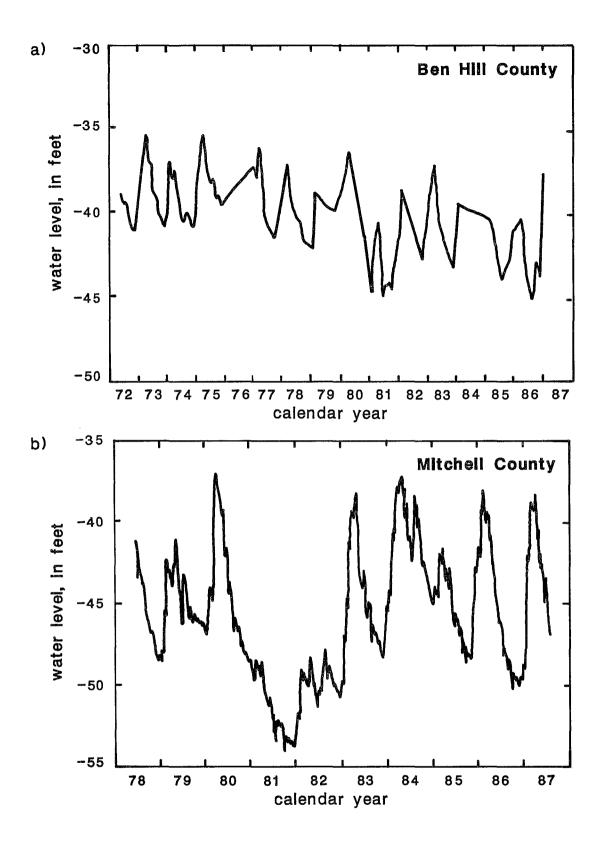


Figure 9. Water levels in Floridan aquifer wells. a). Trees Inc., northern Ben Hill County. b). Wright well, eastern Mitchell County.

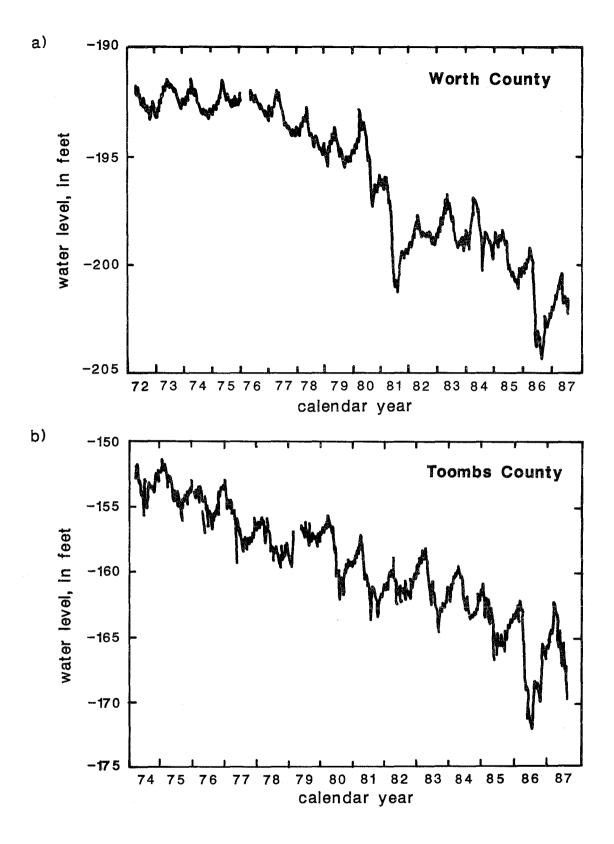


Figure 10. Water levels in Floridan aquifer wells. a). City of Sylvester, Worth County. b). City of Vidalia, Toombs County.

in water levels over large areas. Development of aquifers as water supplies produces changes in recharge and discharge relationships. Declines in water levels commonly result from large withdrawals of ground water. In the Floridan aquifer system, water levels over much of the Coastal Plain have declined (Figure 11). No decline is seen at the northwest extent of the aquifer near the outcrop area, and in the Brooks-Lowndes-Thomas-Cook Counties area, where the aquifer is recharged. The largest water-level declines appear at Savannah and in Wayne and Long Counties in the vicinity of Jesup and Doctortown. These declines are the result of large industrial withdrawals to supply the paper industries in these cities. Regional water-level declines resulting from these large withdrawals do not extend westward of the Gulf Trough, suggesting that the low transmissivity of the aquifer within the trough prevents the pumpage-produced pressure changes from extending further westward.

A comparison of the May 1980 (Krause and Hayes, 1981) and May 1985 (Bush and others, 1987) potentiometric maps of the upper permeable zone of the Floridan aquifer system (now called the upper Floridan aquifer) in Georgia shows that major water-level decline occurred in only one portion of the study area. The southwestern portion of the state, in and adjacent to the Dougherty Plain, showed a water-level decline of 10 to 30 feet. This decline was brought about by a combination of local drought conditions and resulting increased pumpage during this time.

# WATER USE

Total reported ground-water use in the study area in 1985 was approximately 179.4 million gallons per day (Mgal/d) (Turlington and others, 1987). Most of this water was withdrawn from the Floridan aquifer system. Municipalities were once the main consumers of ground water in the Coastal Plain and still rely almost exclusively on wells to provide adequate water to meet public-supply needs. Agricultural withdrawals, however, account for an increasing percentage of ground-water use and in most counties have surpassed municipal use. Locally, industrial withdrawals form a growing segment of total ground-water use. Ground water is used for thermoelectric power generation in two counties of the study area.

The largest ground-water withdrawals in the study area are for agricultural purposes, including both irrigation and livestock use. Recent decades have seen phenomenal growth in the number of acres of irrigated farmland (Table 1, after Bachtel, 1987). With the advent in the seventies of sophisticated irrigation systems supplied by water wells, ground-water withdrawals have played an increasingly large role in crop irrigation. The largest agricultural withdrawals in 1985, an average of 32.94 million gallons per day (Mgal/d), were in Decatur County (Turlington and others, 1987). Four other counties reported agricultural withdrawals in excess of 5 Mgal/d: Mitchell, with 11.29 Mgal/d; Colquitt, with 7.54 Mgal/d; Tift, with 6.58 Mgal/d; and Screven, with 5.10 Mgal/ d. Some of the withdrawals reported from Decatur and Mitchell Counties, which border the Dougherty Plain, may have been obtained from the Clayton or Claiborne aquifers. Total reported agricultural use in the study area in 1985 was 106.08 Mgal/ d. These figures are average daily-use estimates which do not take into account the highly seasonal nature of irrigation withdrawals.

The city of Thomasville is the largest municipal user of ground water in the study area, withdrawing 4.51 million gallons per day for public supply purposes (Turlington and others, 1987). Three other cities in the study area reported withdrawals in excess of 3.00 Mgal/d. They were: Adel, with 3.71; Douglas, with 3.11; and Moultrie, with 3.08 Mgal/d. Total reported ground-water withdrawal for public supply in the study area for 1985 was 45.45 Mgal/d. Self-supplied domestic and commercial withdrawals locally form a large segment of county-wide ground-water use. Estimates of ground-water use in this category include all household water users not supplied by public water systems, as well as commercial users such as restaurants, hotels, stores and other businesses. These amounts also include withdrawals by military and recreational facilities, schools, hospitals, prisons, and other institutions (Turlington and other, 1987). Total withdrawals for these and other categories are presented in Table 2.

Industrial users locally account for significant ground-water withdrawals. Colquitt and Thomas Counties contain two of the largest population centers in the study area, and industrial withdrawals are correspondingly high. Significant withdrawals for industrial use in 1985 were reported for Colquitt County, 1.30 Mgal/d and Thomas County, 1.28 Mgal/d. Both Jeff Davis and Screven Counties have established textile industries which withdraw large quantities of ground water, 1.68 Mgal/d in Jeff Davis, and 1.36 Mgal/d in Screven County. Total industrial and mining use in 1985 was 9.78 Mgal/d. Thermoelectric power generation, a separate category of water

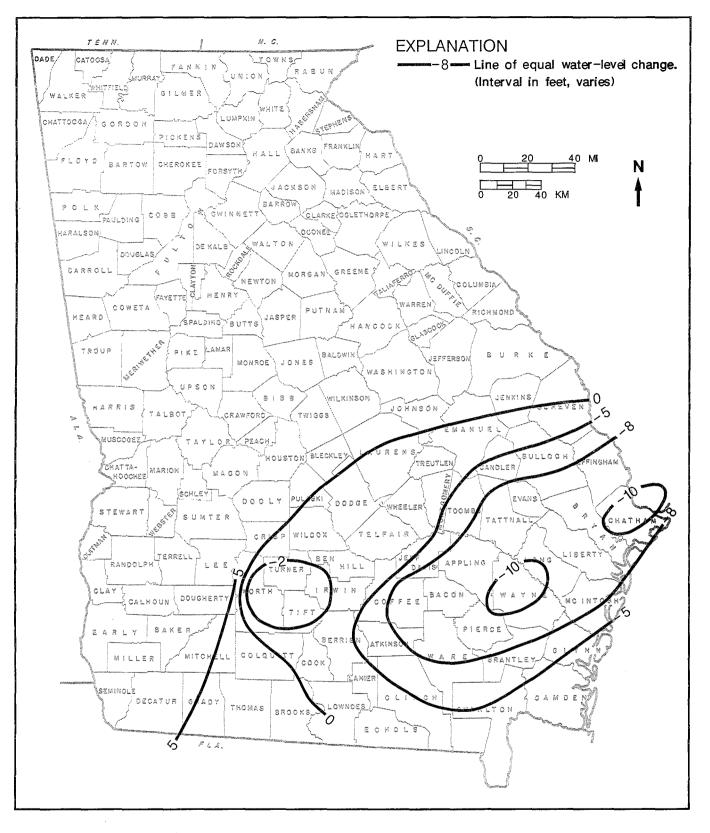


Figure 11. Water-level change, Floridan Aquifer System, 1969-78. (After Clarke et. al., 1978.)

# Table 1. Number of acres irrigated, 1974 and 1984 (after Bachtel, 1987).

	Ye	ar
County	1974	1984 °
Appling	609	3012
Atkinson	624	5365
Bacon	376	4475
Ben Hill	265	10625
Berrien	1904	11530
Brooks	1484	10056
Bulloch	559	14870
Candler	851	12010
Coffee	2430	21000
Colquitt	3623	28373
Cook	2074	8164
Decatur	9575	66872
Effingham	29	25885
Evans	564	2620
Grady	1840	12272
Irwin	1653	7034
Jeff Davis	217	19350
Mitchell	8353	54506
Montgomery	46	2341
Screven	276	14300
Tattnall	2246	7122
Telfair	406	10760
Thomas	632	7078
Tift	5262	39516
Toombs	1190	10149
Wheeler	147	2187
Worth	1363	19382

# Table 2.Water use in the study area, by county, in million gallons per day<br/>(Turlington and others, 1987).

County	Public Supply	Domestic and Commercial	Industry and Mining	Agri- cultural	Thermo electric	Total
Appling	0.89	0.75	0.15	0.75	0.22	2.76
Atkinson	0.35	0.22	0.00	1.13	0.00	1.70
Bacon	0.56	0.41	0.48	1.01	0.00	2.46
Ben Hill	2.69	0.28	0.00	2.44	0.00	5.41
Berrien	0.36	0.51	0.71	3.87	0.00	5.45
Brooks	1.56	0.63	0.00	2.11	0.00	4.30
Bulloch	1.32	1.49	0.80	3.39	0.00	7.00
Candler	0.63	0.29	0.00	2.11	0.00	3.03
Coffee	3.51	0.93	0.00	4.52	0.00	8.96
Colquitt	3.65	0.65	1.30	7.54	0.00	13.14
Cook	3.84	0.45	0.00	1.13	0.00	5.42
Decatur	2.14	1.33	0.80	32.94	0.00	37.21
Effingham	0.73	1.08	0.00	0.44	0.27	2.52
Evans	0.45	0.22	0.72	0.21	0.00	1.60
Grady	2.17	0.90	0.08	1.57	0.00	4.72
Irwin	0.68	0.35	0.01	1.10	0.00	2.14
Jeff Davis	0.72	0.53	1.68	4.06	0.00	6.99
Mitchell	2.86	0.78	0.00	11.29	0.00	14.93
Montgomery	0.33	0.32	0.00	1.07	0.00	1.72
Screven	1.32	0.81	1.36	5.10	0.00	8.59
Tattnall	1.06	1.54	0.00	1.17	0.00	3.77
Telfair	1.54	0.27	0.16	3.47	0.00	5.44
Thomas	5.19	0.99	1.28	1.55	0.00	9.01
Tift	3.26	0.32	0.25	6.58	0.00	10.41
Toombs	2.16	0.58	0.00	1.59	0.00	4.33
Wheeler	0.23	0.18	0.00	0.56	0.00	0.97
Worth	1.25	0.79	0.00	3.38	0.00	5.42
Total	45.45	17.60	9.78	106.08	0.49	179.40

use, accounts for a portion of ground-water use in two counties in the study area. Total withdrawals for power generation in 1985 were 0.49 Mgal/d; 0.22 Mgal/d were reported from Appling County and 0.27 Mgal/d from Effingham County.

#### WELL CONSTRUCTION

Wells constructed in the Floridan aquifer system follow a fairly consistent pattern. The well is typically drilled to the top of the aquifer, usually the first major limestone unit encountered, and casing is installed. Drilling is then resumed: the aquifer is penetrated, and the bottom of the hole is left open. The massive limestones of the Floridan system require no well screens. The well is developed by pumping, airlift, or surging to remove drilling fluids, and a pump is installed. A diagram of the construction of a typical Floridan aquifer system well is shown in Figure 12. Within the Gulf Trough and Apalachicola Embayment, such construction methods may not produce a satisfactory well. Because the top of the Floridan aquifer system is deeper than normal, it may be necessary to geophysically log a well, or collect and examine well cuttings carefully, in order to ensure that the aquifer is actually penetrated. The lowermost Miocene unit in some areas within the the troughembayment is a dense, massive limestone, which superficially resembles the limestone of the Floridan. The Miocene limestone is significantly less permeable than the Oligocene limestone which usually forms the top of the aquifer, but in most areas can be distinguished by the presence of sand in the Miocene limestone. For best yields, wells drilled in the vicinity of the Gulf Trough-Apalachicola Embayment should be completed in Oligocene and, where permeable, upper Eocene limestones. However, these limestones in the Gulf Trough and Apalachicola Embayment are, in general, less permeable than those outside. For this reason, it may be necessary to drill wells with a much longer open-hole interval, thus allowing flow into the borehole from a number of the most permeable zones, thereby maximizing yield. All of these factors may increase the cost of drilling wells in the vicinity of the trough-embayment.

Water quality may dictate well-construction practices in some parts of the study area. The lowermost Miocene sediments and uppermost portions of the Oligocene limestones may contain zones of naturally radioactive water which must be cased off if the well is to be used. This topic will be dealt with in greater detail in the water-quality section of this report.

# **GROUND WATER AVAILABILITY**

#### GENERAL

The amount of ground water available from an aquifer is dependent on many interrelated factors, including the volume and hydraulic properties of the aquifer and the amount and distribution of recharge and discharge. In addition, the method of well construction can influence the ease with which water can be obtained from an aquifer. The Gulf Trough-Apalachicola Embayment has been noted as an area of reduced well yields from the Floridan aquifer system. A variety of theories have been advanced to explain this.

# WELL CHARACTERISTICS AND AQUIFER PROPERTIES

In order to assess the availability of ground water from an aquifer it is necessary to attempt to quantify its hydraulic properties. Such properties include transmissivity, storage coefficient, and hydraulic conductivity. These quantities cannot be measured directly, but they can be derived using aquifer-test data and applying various formulae derived from Darcy's Law, a basic equation of ground-water flow. Well yields, which can be measured directly, are also useful for assessing ground-water availability; however, they are affected by factors other than those intrinsic to the aquifer. The locations of wells used to assess aquifer properties are displayed on Plate 6.

Specific capacity is a measure of the yield of a pumping well. It is the rate of ground-water withdrawal, expressed in gallons per minute, per unit of drawdown, expressed in feet (gpm/ft). The specific-capacity value of a well gives a rough estimate of ground-water availability, but reflects properties of the well in addition to properties of the aquifer. Factors which influence the efficiency of pumping wells, such as well diameter, degree of well development, and pumping rate affect the specific-capacity value. The length of open borehole or screen and the length of pumping time also affect specific capacity. When the specific-capacity value is divided by the length of open borehole, in feet, the result is an average yield per crosssectional area of aquifer, known as the specificcapacity index. Specific-capacity indices can be compared more directly than specific capacityvalues, but the indices do not allow for the varying efficiencies of wells of different construction. In fractured carbonate aquifers, specific capacity

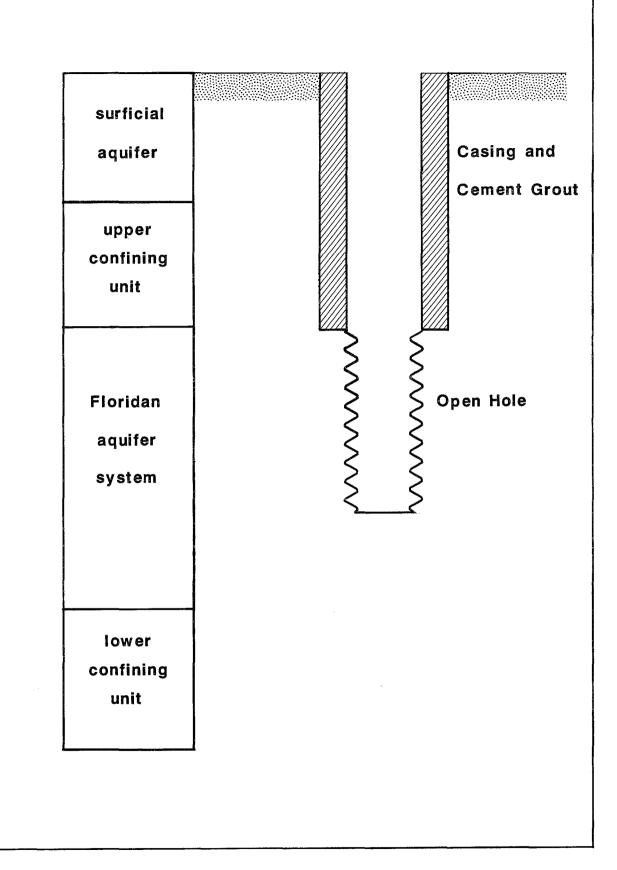


Figure 12. Typical well construction, Floridan aquifer system.

indices may be anomalously high.

Transmissivity (T) is a measure of the relative ease with which water moves through an aquifer. It is the rate at which water will move through a unit width of aquifer under a unit hydraulic gradient. Transmissivity is expressed in units of feet squared per day  $(ft^2/d)$ . Transmissivity values reflect both the permeability of the aquifer and the thickness of the aquifer. Storage coefficient is the volume of water an aquifer releases from or takes into storage per unit surface area under a unit change in head. This dimensionless number is a measure of both the expandability of water and the compressability of the aquifer. The response of an aquifer to changes in the ground-water flow system is dependent in part on the storage coefficient and transmissivity.

Hydraulic conductivity is another relative measure of the permeability of an aquifer. It is the rate at which water moves through a unit area of aquifer under a unit hydraulic gradient, and it is expressed in feet per day (ft/d). The hydraulic conductivity (K) value is commonly obtained by dividing the transmissivity value by the thickness of the aquifer. This approach assumes that the transmissivity is homogeneous. Where this is not the case, the K value obtained represents an average value.

# Specific Capacity

Although specific-capacity values are affected by the construction and development of a given well in addition to the physical properties of the aquifer, they are often useful as a gauge of the availability of ground water from an aquifer in a given area. Low specific-capacity values often indicate an area where aquifer permeability is reduced, making ground water difficult to obtain. The effects of differing well diameters and depths produce many exceptions to this general rule, however. Specific capacity values from the Floridan aguifer system in the study area are displayed on Plate 7. Examples of areas in the troughembayment where wells exhibit low specific-capacity values include: the Hazelhurst area, in Jeff Davis County: the Lyons area, in Toombs County; and the vicinity of Meigs, in northern Thomas and southern Mitchell Counties. Northern Berrien County, in the vicinity of Enigma, is also characterized by low specific-capacity values, but data in this area are sparse. These areas may be contrasted with the city of Tifton, in Tift County, north of the Gulf Trough. Wells in the Tifton area have much higher specific capacity values than many wells within the trough-embayment, but allowances must be made for the much larger diameters of the Tifton city wells compared to those commonly drilled elsewhere in the study area.

# Specific-Capacity Indices

In order to minimize the effect of varying well depths on specific-capacity values, specific-capacity indices were calculated. Like the specificcapacity values, the indices vary considerably, but generally they are lower in the the troughembayment than outside it (Plate 8). Several observations can be made using specific-capacity indices which are not possible using specificcapacity values. The southwestern half of the study area, from Coffee County southwestward, exhibited generally higher specific-capacity indices than does the northeastern half. The specificcapacity indices in this area are also lower inside the trough-embayment than outside it. For example, in the Tift and Berrien Counties area, and southwestward, 17 of 22 wells with specific-capacity indices of 0.1 gallons per minute per square foot  $(gpm/ft^2)$  or less lie in the trough-embayment. This trend continues to the northeast, as far as and including Tattnall County. In this area, 39 of 45 wells with specific-capacity indices in excess of 0.1 gpm/ft<sup>2</sup> lie outside the Gulf Trough. The influence of the trough can be seen as far northeastward as Statesboro, in central Bulloch County. Wells on the north side of Statesboro have higher specific capacity indices than those on the south side, which lie near the probable terminus of the Gulf Trough.

# Transmissivity

The range and distribution of estimated transmissivity values are shown on Plate 9. In the northeastern portion of the study area, from northern Berrien County to central Bulloch County, transmissivity values are lowest along the trend of the Gulf Trough. Low values also extend northward beyond the flank of the trough proper, into Wheeler, Montgomery, and southeastern Telfair Counties, and southward beyond the flank into Appling County. The southwestern part of the study area shows a more complex distribution of transmissivity values. Although low transmissivity values are observed within the trough-embayment, they also occur in scattered places to the north of the trough in Worth County and western Tift County. Low values are observed within the the trough-embayment as far southward

as northern Grady and Thomas Counties, whereas the southern portions of these counties exhibit some of the highest estimated transmissivity values in the study area. The Cairo East-Side Water Plant well exhibits a transmissivity value of 430,000 ft<sup>2</sup>/d, probably a result of a large void encountered during drilling (Dan Wells, pers. comm.). On the southeastern side of the trough-embayment, high transmissivity values (100,000 ft<sup>2</sup>/d or greater) can be observed in southern Thomas, southern Cook and Berrien Counties, and central Coffee County.

# Hydraulic Conductivity

The distribution and range of estimated hydraulic-conductivity values (Plate 10) in the study area is broadly similar to that of transmissivity values. The lowest values cluster along the trend of the trough-embayment. The highest values in the study area appear in the Dougherty Plain, along the northern edge of the Apalachicola Embayment and along the southern flank of the trough-embayment from central Coffee County southwestward into Berrien, Cook, and Thomas Counties. A Cairo city well within the embayment, in Grady County, has an estimated hydraulic conductivity value of 5800 ft/d.

#### RECHARGE

Recharge patterns are an important factor in ground-water availability. The Floridan aquifer system receives recharge from a variety of sources. One primary recharge area is the Dougherty Plain, where the upper Eocene Ocala Limestone crops out or is covered by a thin veneer of residuum. Topographic slopes in this area are low and infiltration rates high. Rainfall infiltrates the aquifer directly, at an estimated rate of 10 inches per year over an area of 4000 square miles (Bush, 1982). Limestones of the Floridan system also crop out northeast of the Dougherty Plain as far as Wilkinson and Laurens Counties, but recharge in this area is reduced by the smaller outcrop area and steeper topographic slope. Further to the northeast, Oligocene and Eocene rocks are primarily clastic in the outcrop area, but grade downdip into limestones. Recharge to the Floridan in this area is through the clastic Jacksonian aquifer (Vincent, 1982), which is continuous with, and stratigraphically equivalent to, a portion of the downdip carbonate Floridan aquifer system.

The upper confining unit of the Floridan is thin in the Brooks and Lowndes Counties area, and it is breached by numerous sinkholes as well as by the Withlacoochee River. Krause (1979) estimated that, on the average, the Withlacoochee River loses 112 cubic feet of water per second (ft<sup>3</sup>/ s) to the aquifer. Sinkholes along the stream will accept all the water from the river when flow rates do not exceed 40 ft<sup>3</sup>/s.

A third important source of recharge to the Floridan aquifer system is diffuse leakage of water from overlying clastic sediments. Although clay layers of very low permeability separate the Floridan from these overlying sediments, small amounts of water are able to move across the confining layers and enter the aquifer. Areas where the potentiometric surface has been lowered by pumping of the aquifer are particularly subject to leakage of this type. The amount of water which crosses the confining layer in any given area is small, but taken over the entire extent of the aquifer, the amount of recharge by leakage is significant (Bush, 1982).

# **GROUND-WATER FLOW**

The potentiometric map of the Floridan aguifer system shows the effects of the Gulf Trough on ground-water flow (Figure 8). Water entering the aquifer system northwest of the Gulf Trough flows laterally downgradient towards discharge points to the southeast. The hydraulic gradient north of the trough is fairly uniform, but it steepens abrubtly across the trough. The low-permeability limestones of the Gulf Trough exert a damming effect on ground water in the aquifer. Northeast of the Gulf Trough, in Bulloch County and northeastward, the direction of ground-water flow is southeast, under a uniform hydraulic gradient. Southeast of the Gulf Trough, ground-water flow is sluggish, despite the high transmissivity of the aquifer in this area (Bush, 1982).

Ground-water flow in the southwestern half of the study area shows a more complex pattern. Water entering the aquifer where it is unconfined and thinly confined in the Dougherty Plain area flows laterally downgradient both to the southeast and southwest. Water entering the aquifer in the recharge area near Valdosta flows downgradient in all directions, away from the potentiometric high. It is important to note that certain areas in and near the Apalachicola Embayment, such as the southern Cook and Berrien Counties area, receive ground-water flow from two directions, across the Gulf Trough from the north and from the Valdosta area in the south.

# ANALYSIS OF GROUND-WATER AVAILABILITY

The availability of ground water from the

Floridan aquifer system in the study area is determined by a complex interaction of 1) the lithology of the rocks which compose the aquifer, 2) the morphology of the Gulf Trough and Apalachicola Embayment, and 3) the recharge, discharge, and flow relationships within the trough-embayment. These factors combine to reduce the permeability of the Floridan system in this area and hence affect the availability of ground water from the aquifer.

# Lithologic Factors and Availability of Ground Water

The Gulf Trough and Apalachicola Embayment appear to have existed as bathymetric depressions from middle Eocene through early Miocene time. Because the trough and embayment were different environments, in terms of water depth and energy conditions, than the surrounding shallow shelf, stratigraphic units change in lithology as they cross the trough-embayment. The rocks which were deposited in the troughembayment are fine-grained, relatively deep-water limestones (Huddlestun and others, in preparation) Permeability tests show these limestones to be lower in average primary premeability than those found outside. Some stratigraphic units are confined to the trough-embayment and show abrupt facies changes from rocks of the same age outside the trough. For example, the Lower **Oligocene** Ochlockonee Formation and its Pridgen Limestone Member are both relatively deep-water limestones and are confined to the trough or embayment, whereas the more permeable, shallow-water Bridgeboro Limestone occupies the flanks. A similar situation occurs in the Upper Eocene; the permeable, shallow-water Ocala Limestone is present outside the troughembayment, and a dense, deeper-water limestone (undifferentiated Upper Eocene limestone) is present inside it.

Another possible cause of reduced permeability of the Floridan aquifer system in the troughembayment may be the presence of small amounts of swelling clay within the limestone. Visual and microscopic examinations commonly do not reveal the presence of any clay. However, its presence is suggested by the fact that limestones in the trough, the Ochlockonee Limestone for example, often produce core samples which are longer than the coring run. For example, a fifteen-foot coring run may yield sixteen feet of core when removed from the core barrel. Also, during permeability testing, some newly saturated samples produce hydraulic conductivity values that decrease with time. Samples that are allowed to "rest" after saturation yield values that plot linearly. This effect is interpreted to be the result of swelling of clays during saturation.

Northeast of the Gulf Trough, in portions of Bulloch and Screven Counties, the Oligocene sediments contain a higher percentage of clastic material than do those to the southwest. The Oligocene section in Bulloch County may locally be represented by a sandy limestone or even a sand, and the Upper Eocene limestones grade laterally updip into clastic rocks of the Barnwell Group. The Floridan aquifer system in this area exhibits reduced permeability as a result.

# Ground-water Flow Factors and Availability of Ground Water

All of the above factors relate, for the most part, to the primary permeability of the limestone. Secondary permeability is produced by dissolution of the limestone as ground water flows through joints, fractures, and other openings in the rock, and it is the major source of permeability in most limestone aquifers. Both the lithology of the limestones and the morphology of the Gulf Trough-Apalachicola Embayment may affect the secondary permeability of the Floridan aquifer system in the study area.

The development of secondary permeability in limestone aquifers follows a common pattern. Massive limestones, which may have little primary permeability, are prone to develop networks of joints, which then provide a path for ground-water flow. Dissolution of the limestone occurs along the joints. The degree to which dissolution occurs along a given ground-water flow path is dependent on the length of the flow path and the saturation of the water with respect to carbon dioxide. Short, shallow flow paths traversed by water relatively high in carbon dioxide concentration will undergo the most dissolution per unit volume of limestone. In this way, shallow flow zones are developed at the expense of the deeper flow zones (Rhoades and Sinacori, 1941).

Bush (1982), in his model of pre-development flow in the Tertiary (Floridan) aquifer system, showed that the greatest degree of secondary permeability was produced in the unconfined and thinly confined portions of the aquifer, where the most active flow was taking place. These areas had the greatest inflow and outflow of ground water, and hence experienced the greatest degree of dissolution.

The Floridan aquifer system within the study area conforms to the pattern of highest permeability

in the unconfined or thinly confined areas. Permeability is low in areas such as the Gulf Trough, where the aquifer is overlain by a thick overburden. This is also true for the thickly confined Wheeler and Montgomery Counties area, for the Appling and Bacon Counties area within the Southeast Georgia Embayment, and for the thickly confined portions of the Apalachicola Embayment. The Apalachicola Embayment in Colquitt County is an example of thick overburden coupled with low permeability; however, thinly confined portions of the embayment show much higher permeability. This is true in southeastern Grady County, where thinner overburden and proximity to recharge from the Valdosta area produce a more active flow system. The southern Cook and Berrien Counties area receives ground-water flow from across the Gulf Trough as well as recharge from the Valdosta area. Transmissivity of the shallow zone of the Floridan system in this area reaches  $360.000 \text{ ft}^2/$ d, one of the highest values reported from the study area.

Development of secondary permeability, and, hence, the availability of ground water in the Gulf Trough and Apalachicola Embayment area is dependant on such lithologic factors as the density of the deep-water limestones in the area, their susceptibility to fractures, and possibly, the presence of swelling clays within the limestones. The morphology of the Gulf Trough and Apalachicola Embayment exerts a profound influence on ground-water availability by determining the thickness of sediments overlying the aquifer and by its effects on regional groundwater flow patterns.

# **GROUND-WATER QUALITY**

#### GENERAL

All ground water is ultimately derived from precipitation. Precipitation contains almost no impurities; however, the soil and rocks which this water infiltrates contribute various chemical constituents to the water. The chemical species present in ground water, and their concentrations, reflect all of the chemical processes that have affected the water since it fell as precipitation. The elements present in the rocks along the flow path of the water, the solubility of the rocks, the pH of the water, and the sequence in which that water contacts the various minerals along its flow path, are some of the factors which will affect the chemical makeup of ground water (Freeze and Cherry, 1979). As water moves through the ground its chemical constituents and their concentrations may change. Ground water in a limestone aquifer typically becomes higher in dissolved solids and in pH with longer residence time.

The quality of ground water from the Floridan aquifer system in the study area is, in general, quite good. The Georgia Rules for Safe Drinking Water establish primary Maximum Contaminant Levels (MCLs) for potentially harmful substances in drinking water, and secondary MCLs for substances that affect the sight, taste, or smell of drinking water. Water from the majority of wells in the area falls below the specified MCLs. Elevated levels of sulfate, barium, and natural radioactivity are, however, associated with the Gulf Trough and Apalachicola Embayment, and reduce water quality in some areas.

Ground-water chemistry may be characterized by examining the abundance of the major cations, including calcium, magnesium, sodium, and potassium, and the major anions, including bicarbonate, sulfate, and chloride. The relative percentages of these ions in a water sample may be illustrated by using Piper diagrams (Piper, 1944). Plots of the concentration of the major ions (in milliequivalents per liter) are known as Stiff diagrams (Stiff, 1951).

# GROUND-WATER QUALITY IN THE GULF TROUGH AND APALACHICOLA EMBAYMENT

The dominant anion in ground water from the Floridan aquifer is bicarbonate (Plate 11). Most of the samples which showed greater than 15 percent sulfate anions were from wells located in the Apalachicola Embayment. Cation percentages were more variable, but calcium was the most prevalent cation. Ground-water samples taken from near recharge areas typically contained a high ratio of calcium to other cations. Most of the samples which had significant percentages of sodium or potassium were taken from wells located in the Gulf Trough-Apalachicola Embayment.

Because ground water typically increases in dissolved solids content as it progresses downgradient through the flow system, dissolvedsolids concentration is a useful indication of flow path length or residence time. Water from the Floridan aquifer system in the study area contains total dissolved solids (TDS) concentrations ranging from 26 milligrams per liter (mg/l) to 761 mg/ l; however, most values fall between 130 and 250 mg/l. High TDS values are present within the Apalachicola Embayment in Grady County and in southern Colquitt County, where the thick overburden retards ground-water flow and increases residence time. Most TDS values reported for ground water from Thomas County are high, although some fall within the typical range of the study area. Slightly elevated values are reported for water from scattered wells in Brooks and Appling County, in the thickly confined Southeast Georgia Embayment. The Georgia Rules for Safe Drinking Water establish a secondary MCL of 500 mg/l dissolved solids. Elevated levels of sulfate, barium, and natural radioactivity have been reported from the study area. The close geographic association of such water-quality anomalies with the Gulf Trough and Apalachicola Embayment suggests a possible relationship.

# SULFATE IN GROUND WATER

The secondary MCL for sulfate in drinking water has been established not to exceed 250 mg/ 1. Sulfate may produce a detectable taste at 300 to 400 mg/l, and at 500 mg/l it will produce a medicinal taste and, possibly, a laxative effect (Lehr and others, 1980).

# **Distribution of Sulfate**

Elevated levels of sulfate have been reported from wells tapping the Floridan aquifer system in the Gulf Trough-Apalachicola Embayment area. Plate 13 shows the range and distribution of sulfate levels in the study area. Sulfate concentrations exceeding 100 mg/l are restricted to the Gulf Trough-Apalachicola Embayment, with the exception of water from one USGS test well in Cook County. A number of counties southeast of the trough-embayment contain wells that produce water with sulfate concentrations of 50 to 100 mg/l. They include Appling, Atkinson, Bacon, southern Berrien, Evans, and southern Tattnall Counties.

Sulfate levels vary widely with depth. For example, water samples from the USGS test well at Adel in Cook County, varied from 256 mg/l at a depth of 227 to 243 feet, to 610 mg/l at 452 to 468 feet (Grantham and Stokes, 1976). Nearby municipal wells in Adel do not exceed 400 feet in depth, and sulfate concentrations in water from these wells are less than 100 mg/l. Water samples from the USGS test well at Cairo, in Grady County, contained concentrations of sulfate that ranged from 5.6 mg/l to as high as 1000 mg/l, depending on the depth sampled (Grantham and Stokes, 1976). The lowest concentrations were from samples obtained from sediments overlying the Floridan aquifer, whereas the highest concentrations were from the base of the Floridan aquifer.

#### Source of Sulfate

The most common source of sulfate inground water is gypsum. Within and southeast of the Apalachicola Embayment, the lowermost portions of the Floridan aquifer system contains significant amounts of interstitial gypsum. Southeast of the Apalachicola Embayment, the lower part of the Upper Eocene Ocala Limestone contains sufficient amounts of interstitial gypsum to exclude it from the aquifer.

The presence of the Gulf Trough and Apalachicola Embayment inhibits the development of secondary permeability in the lower parts of the Floridan aquifer system. Reduced permeability in turn inhibits the dissolution of gypsum and the removal of sulphate from the aquifer. Relatively high concentrations of gypsum thus remain in the aquifer matrix in its lower parts. Sluggish groundwater flow through these zones and correspondingly longer residence time contribute to the elevated levels of sulfate in ground water.

# BARIUM IN GROUND WATER

The Georgia Environmental Protection Division samples water from public-supply systems for barium content. The majority of these analyses were conducted on treated water; however, barium concentrations are not affected by most types of water treatments. The established primary MCL for barium in drinking water is 1000 micrograms per liter (ug/l). Barium concentrations in ground water from the Floridan aquifer system are generally low. Most of the water samples analyzed between January 1976, and June 1982, had concentrations of barium that were at or below the 200 ug/l detection limit.

# **Distribution of Barium**

Plate 14 shows the concentration of barium for those samples that exceeded the detection limit and also shows the total number of municipal water systems in each county whose samples fell below the detection limit for barium. The Floridan aquifer system is assumed to be the source for most public-supply systems in the study area; however, this could not be confirmed in all cases due to a lack of well construction data. Samples from specific wells known to tap the Floridan aquifer system are distinguished on the map from those taken from public-supply systems, which may use more than one well, or from wells of unknown construction.

Detectable concentrations of barium are generally restricted to wells north of the axis of the Gulf Trough-Apalachicola Embayment. Concentrations of barium in excess of the drinking water standards are found at Fitzgerald, in Ben Hill County (Plate 14). Fitzgerald municipal wells A, B, C, D, and E consistently produce water with barium concentrations in the range of 1300 to 2260 ug/l. Water samples from city wells F and G, which are shallower than wells A through E. contain concentrations at or below the detection limit. Shallow domestic wells tapping the Floridan system in the vicinity of Fitgerald also produce water with lower concentrations of barium, ranging from 250 to 350 ug/l. High barium concentrations thus appear to be confined to the lower portions of the aquifer. Water samples collected from discrete depth intervals in municipal wells C and E failed to pinpoint zones of barium concentration, possibly due to mixing of water in the borehole.

# Source of Barium

The source of barium in the Fitzgerald area is not understood. Mineral sources of barium in ground water include such common minerals as barite and such rare ones as gorceixite (Milton and others, 1958; Michel and others, 1982). Barite is one of the most common barium-containing minerals; however, its solubility is such that water would typically be saturated with respect to barium at concentrations that fall below the limits of detection. The presence of sulfate, even at relatively moderate concentrations, will cause the precipitation of barite, thus removing barium from the ground water. Sulfate levels in ground water must be relatively low in order for levels of barium to reach detection limits. This most often occurs where bacterial activity removes sulfate from the ground water (Gilkeson and others, 1983) and may be the case in the Fitzgerald area. This study found no evidence of a causal relationship between elevated barium levels and the presence of the trough-embayment.

# NATURAL RADIOACTIVITY IN GROUND WATER

Elevated activity of radioactive elements is closely associated with the Gulf Trough-Apalachicola Embayment. Several public-supply wells have yielded water that exceeds drinking water standards for natural radioactivity and have been plugged or reconstructed as a result. In other cases, water from affected and unaffected wells is combined in the municipal water system, and the mixed water then meets drinking water standards.

Radioactivity is a product of the unstable decay of a number of different naturally occurring radioactive isotopes. The Georgia Rules for Safe Drinking Water specify MCLs for several specific isotopes as well as for total particle activity. Within the study area, the only two parameters known to exceed the MCLs are gross alpha activity and Radium-226. All municipal water systems are tested for gross alpha activity, for which the MCL is 15 picocuries per liter (piC/l), excluding radon and uranium. Water samples which exceed 5 piC/ l gross alpha activity are then tested for the combined level of Radium-226 and Radium-228. The MCL for this parameter is 5 piC/l. Radium-226 and 228 are of concern from a health standpoint because they can be ingested and can accumulate in the bones. The daughter products of the nuclides are short-lived alpha-emitters, which are particularly harmful to the body (Gilkeson and others, 1983).

Laboratory results indicate that Radium-226 is the dominant alpha emitter in the study area, and that Radium-228 activity is negligible. Because of the greater availability of data on gross alpha activity, and because the majority of that activity can be attributed to Radium-226, only gross alpha activity was mapped in this study.

# **Distribution of Radioactivity**

Plate 15 shows the known values of gross alpha activity in the study area. Most of the values included are from samples collected from the distribution lines of municipal water systems. If a system uses multiple wells, the values often cannot be assigned to water from any particular well. Two types of map symbols are used to distinguish these values from those of water from specific wells. The majority of samples tested had gross alpha activities of 4 piC/l or less. Many of the samples that exceeded this level were taken from wells in the Gulf Trough or Apalachicola Embayment. The two areas that show the highest gross alpha activity are the Tift-Berrien Counties area, and the Wheeler-Montgomery Counties area. The occurrence of radioactivity in these areas indicates two separate patterns.

High gross alpha levels in ground water are associated with high gamma-ray activity. Gammaray logs of water wells can help identify zones which will produce water with high gross alpha levels. In the Wheeler-Montgomery Counties area, two distinct zones of gamma radiation can be identified on gamma-ray logs. The upper zone appears above the Floridan aquifer in the Miocene section, where it appears to be associated with voids in the limestone (John Fernstrom, EPD, personal communication). The lower zone of high gamma radiation is located at the top of the Floridan aquifer system. Several public supply wells in the area contained water which exceeded drinking water standards for radiation. The cities of Ailey, Alamo, Mount Vernon, and Tarrytown drilled new wells to replace those that yielded water with high radiation levels. The new wells were cased to greater depths in an attempt to exclude the radioactive zones. Most of these wells subsequently produced water which met standards, with one exception. The replacement well at Alamo was cased to four feet above the base of the gamma-ray anomaly. Water from the well met drinking water standards for five years before the radiation again exceeded standards. In 1987, a third well was drilled and logged, and casing was installed to a depth below the zones of radiation. This well now produces water free from significant amounts of radiation.

High radiation levels in ground water from the Tift and Berrien Counties area are restricted to wells that are in or near the Gulf Trough; however, high gross alpha activity is not found in all of the wells within the trough. Highest levels are found in the vicinity of Tifton, in Tift County, and Alapaha, in Berrien County.

The city of Tifton, on the north flank of the Gulf Trough, has removed municipal well 5 from production due to high radioactivity levels. The gamma log of this well shows large gamma anomalies at depths of 350 feet (cased), 495 feet, and 525 feet. The city replaced this well with municipal well 7, located 3400 feet to the northwest, farther from the trough. The gamma log of well 7 shows moderate gamma-ray activity at 190 feet (cased) and at 290 feet. The gross alpha activity of the water from this well is at or below background levels. Gross alpha activity of water from nearby municipal well number 4 has declined from  $7 \pm 2$  piC/l to  $4 \pm 1$  piC/l since well 5 was taken off line. The city of Alapaha, which lies in the Gulf Trough, has two production wells, both of which produce water with higher than normal amounts of radioactivity. Gamma-ray logs of these wells show high gamma-ray activity between depths of 380 and 400 feet. A test well (GGS 3555) was drilled, logged, and sampled in an attempt to develop a new well to supply water to the city of Alapaha. An inflatable packer was used to isolate and sample discrete depth intervals.

The packer was set at depths of 360, 375, and 381 feet. Tests of water samples collected from beneath the packer for each of these depths indicated gross alpha activities of  $12 \pm 2$ ,  $12 \pm 2$ , and  $10 \pm 2$  piC/l, respectively. A gamma-ray log showed no discrete zones of high radiation. A nearby domestic well, located 800 feet to the east, produces water which meets drinking water standards, but this well is significantly shallower than the city of Alapaha test well. Although at the same land elevation, the domestic well is cased to 272 feet, while the test well is cased to 358 feet.

Assuming that both wells are cased to the top of the aquifer, this means that there is a significant amount of relief on the top of the aquifer. Logs of the city of Tifton municipal wells also indicate that the top of the aquifer is irregular, and wells number 4 and 5, which produce water with higher than normal gross alpha activity, are located in areas where the top of the aquifer is low. Drillers in the Berrien County area also report that high radioactivity seems to be associated with low areas of the top of the aquifer.

# Source of Radioactivity

Radioactivity in the study area is dominated by the decay of Radium-226. Radium-226 is a part of the Uranium-238 decay series that follows, in order, Uranium-238, Thorium-234, Proactinium-234, Uranium-234, Thorium-230, and Radium-226. Radium-226 in turn decays to form Radon-222, and a succession of short-lived daughter products. The activity levels of these isotopes vary. Some, like Uranium-238, have low alpha particle activity, while others, such as Radium-226, are shorter-lived and have high activity levels.

In order to define the controls on the occurrence of Radium-226 in ground water, it is necessary to determine the activity of the other isotopes in the decay series (Gilkeson and others, 1984). These data are not available for the study area; however, certain hypotheses can be made as to the source of the radioactivity.

Uranium-bearing minerals are the ultimate source of the Radium-226 in ground water in the study area. Elevated radioactivity levels are geographically widespread, indicating that the source of the parent isotopes is also widespread. The Miocene and younger sediments in the Coastal Plain contain clastic sediments derived from the crystalline rocks of the Piedmont, which contain uranium-bearing minerals such as monazite. Portions of the Miocene sediments in Georgia are rich in radioactive phosphate minerals, which contain inclusions of Piedmont-derived quartz, microcline, and opaque minerals. Additionally, the dark phosphate pellets contain pyrite and carbonaceous organic matter (Simmons, 1968). Uranium is soluble under oxidizing conditions and precipitates under reducing conditions. Uranium was incorporated in the phosphate minerals due to the reducing conditions produced by the decay of organic matter and the presence of pyrite. Under proper conditions the uranium contained in these minerals can be leached and can enter the ground water.

Typically, ground water in recharge areas is oxidizing and has relatively high levels of uranium, which has a low activity level (Korosy, 1984). As ground water enters reducing conditions, the uranium is deposited on the aquifer matrix, lowering concentrations of uranium in ground water. The uranium then decays, producing daughter products with high activity levels, such as Radium-226. Through the alpha recoil process, the Radium-226 is thrown off the aquifer matrix, and it enters the ground water (Gilkeson and others, 1983).

Reducing conditions in an aquifer can be produced where ground-water flow is sluggish, or where reducing agents such as pyrite or organic matter are present in the aquifer. The Gulf Trough and Apalachicola Embayment provide these conditions. The thick sediments overlying the Floridan aquifer system in the Gulf Trough and parts of the Apalachicola Embayment retard the inflow of oxygen-rich water. In addition, the limestones which comprise the Floridan system in the trough and embayment are less permeable and contain more pyrite than their counterparts outside the feature. Finally, the top of the Oligocene section was exposed and eroded. The paleo-karst developed on this surface trapped fine-grained sediments, rich in organic debris.

High radioactivity levels follow the trend of the Gulf Trough and Apalachicola Embayment, appearing most often in water from the lower Miocene section and the upper portion of the Floridan aquifer system. It is probable that reducing conditions produced in the Lower Miocene sediments and the Oligocene limestones of the Floridan system caused the precipitation of uranium on the aquifer matrix and overlying sediments. The Floridan aquifer system in the Wheeler-Montgomery-Toombs Counties area, though outside the Gulf Trough, is thickly confined and its upper surface karstic and irregular. Therefore, it would also provide the reducing conditions necessary for the precipitation of uranium. Radioactive decay of the uranium would then contribute Radium-226 to the ground water.

Gilkeson and others (1984) and Michel and others (1982) demonstrated the importance of analyzing data on all isotopes in the decay series in order to develop a comprehensive model of the distribution of radioactivity in ground water. Thus, further delineation of the controls on the occurrence of Radium-226 will require more data on the distribution of the parent and daughter isotopes. However, the available information is useful in understanding the mechanism by which Radium-226 enters the ground water, and in identifying areas where high levels of natural radioactivity are likely to be encountered.

# SUMMARY

The hydrogeology of the study area is dominated by the presence of a subsurface geologic feature known as the Apalachicola Embayment and by its narrow, northeastward extension, the Gulf Trough. The Gulf Trough-Apalachicola Embayment extends, in Georgia, from the extreme southwest corner of the State northeastward to central Bulloch County. The feature is sinuous and trough-shaped, widest at the southwest and narrowing northeastward. It was produced by a marine current, the Suwannee Current, which was active in the study area from the middle Eocene through the early Oligocene. This current flowed northeastward from the Gulf of Mexico to the Atlantic, inhibiting sedimentation in the Apalachicola Embayment and Gulf Trough during the late Eocene. Rising sea level during the late Oligocene and Miocene caused the cessation of the current. Filling of the trough-embayment occurred during the Oligocene and early Miocene (Aquitanian). The Suwannee Current controlled sedimentation in the trough-embayment from late Eocene through early Miocene. The Gulf Trough and Apalachicola Embayment are characterized by dense, low-permeability, deeper-water limestones. Upper Eocene sediments in the troughembayment are uncharacteristically thin, whereas those on the north and south flanks are much thicker. Oligocene sediments thicken as they cross the trough-embayment, as do the lower Miocene sediments.

The Floridan aquifer system is the most widely used aquifer in the Coastal Plain of Georgia. It is composed of a thick sequence of permeable limestones, ranging in age from Paleocene to early Miocene. The Floridan aquifer system in its updip region is composed of a single permeable zone, whereas downdip one of several regional middle confining units divides the system into an Upper and a Lower Floridan aquifer. The lower confining unit of the system is highly variable in age and lithology. Throughout most of its extent in Georgia, the aquifer is confined above by clastic and carbonate rocks, mostly Miocene in age. Locally, the upper confining unit has been breached by sinkholes or streams, and in some areas it has been removed entirely by erosion. Thus, water in the Floridan aquifer system may be under semiconfined or unconfined conditions in these areas.

The Floridan aquifer system in the study area yields ground water for agricultural, domestic, municipal, and industrial uses. Total water use in the study area in 1985 was 179.4 Mgal/d. Dramatic increases in ground-water withdrawals for irrigation in recent years have produced water-level declines in some areas; nevertheless, the Floridan aquifer system continues to yield adequate quantities of water to support these withdrawals.

Within the Gulf Trough and parts of the Apalachicola Embayment, the availability of ground water from the Floridan aquifer system is less than in surrounding areas. The permeability of the aquifer is reduced by a combination of factors: the low primary permeability of the deeperwater limestones of the trough-embayment; the greater thickness of overburden which limits development of secondary permeability, and possibly, a lack of joints or fractures to enhance movement of ground water. Certain areas within the Apalachicola Embayment and along its south flank are exceptions to this trend, however. The contact between the Miocene and Oligocene sediments in these areas is a zone of enhanced secondary permeability, capable of supplying large quantities of water to wells.

The quality of ground water from the Floridan aquifer system is reduced in certain parts of the study area. Elevated levels of sulfate, barium, and natural radioactivity are associated with the Gulf Trough and Apalachicola Embayment. High levels of sulfate are reported from the trough-embayment and from the Colquitt-Thomas-Grady Counties area. The most probable source of sulfate in ground water from the Floridan aquifer system in and southeast of the trough-embayment is interstitial gypsum contained in the limestones of the system. The sluggish ground-water flow through the lower parts of the aquifer system has inhibited the dissolution of gypsum and the removal of sulphate from the aquifer. The long residence time of ground water in these lower parts produces high concentrations of sulphate.

Elevated levels of barium in ground water from the Floridan aquifer system are reported from the vicinity of Fitzgerald in Ben Hill County. The source of the barium is not understood. High levels of barium in ground water are usually the result of bacterial activity which lowers the concentration of sulfate in the water. This prevents the precipitation of barite and allows the concentration of barium in ground water to rise. Bacterial activity may be the cause of elevated barium concentrations in the Fitzgerald area.

High levels of natural radioactivity are also associated with the Gulf Trough and Apalachicola Embayment. The highest levels are found in the Wheeler-Montgomery Counties area, and in the Tift-Berrien Counties area, but elevated radioactivity levels are reported from water samples at other locations throughout the trough and embayment. The ultimate source of radioactivity in the ground water from this area is Uranium-238, probably derived from natural sources in or near the study area. The crystalline rocks of the Piedmont Province contain such uranium-bearing minerals as monazite, which were weathered and transported into the Coastal Plain. Also, the phosphate minerals of the Miocene sediments incorporate uranium in their crystal structure. and, hence, are another potential source. Uranium is soluble under oxidizing conditions and precipitates under reducing conditions. Oxidizing waters in recharge areas dissolve uranium from these sources and transport it until reducing conditions are encountered. Uranium is then deposited on the aquifer matrix. Reducing conditions are provided by the limestones of the trough-embayment because of their pyrite content and thick overburden. Paleo-sinkholes could also have provided reducing conditions, due to the decay of trapped organic matter. Through decay of the uranium, Radium 226 is thrown off the aguifer matrix and carried in ground water.

# RECOMMENDATIONS

The following recommendations are intended to provide suggestions for maximizing water quality and yield for wells in the study area.

1) Wells should be located as far from the axis of the Gulf Trough and Apalachicola Embayment as possible, in areas with the thinnest overburden. 2) Whenever practical, wells should be geophysically logged to locate permeable zones and facilitate design of efficient wells.

3) Water samples should be collected from wells drilled in the areas of high radioactivity (Figure 13). These samples should be analyzed for gross alpha levels.

4) Municipalities located in the area of high radioactivity should run gamma-ray logs of new wells so that radioactive zones may be cased.

5) Municipalities which already have wells producing radioactive water may wish to consider drilling small-diameter test wells when choosing sites for new wells. These wells could be drilled at less expense than large-diameter wells, and could then be enlarged if conditions were found to be favorable.

6) The Miocene sediments in the Gulf Trough and Apalachicola Embayment area should be investigated as an alternative source of groundwater supply.

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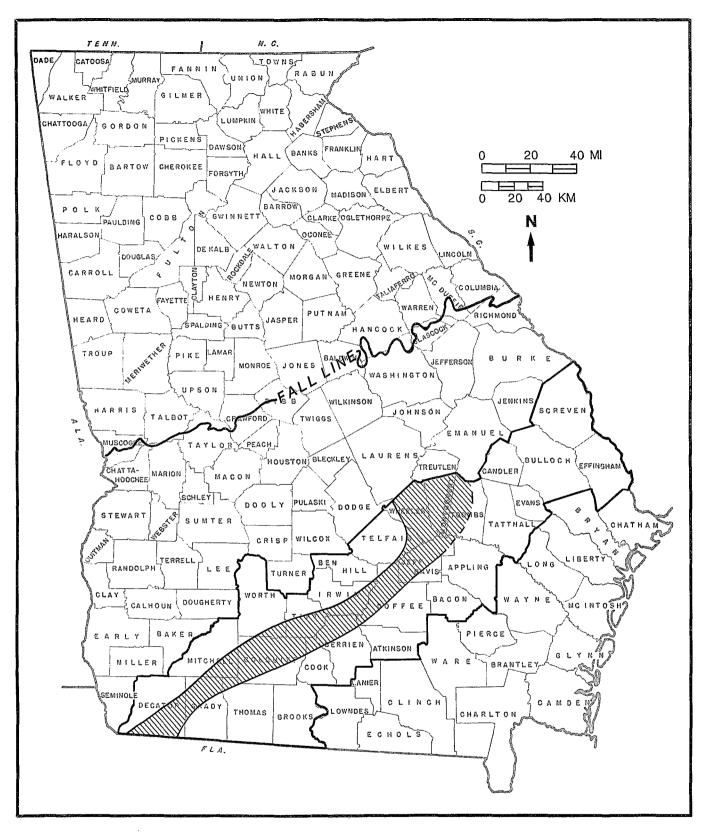


Figure 13. Areas at greatest risk for elevated levels of natural radioactivity in ground water.

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# APPENDICES

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WELL NUMBER	LAND SURFACE ELEVATION (FEET)	DEPTH TO TOP OF AQUIFER (FEET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON I SOPACH MAP
** APPI	LING				
50	204	515	b 840	В	I
148	225	520	1325	В	I
161	242e	550	b 640	В	
1059	203	b 520			
1701	144	610			
28L005	130	540			
** ATK	INSON				
107	214	260	780	В	I
410	295	274	b 425	В	I
425	199	290	b 460	В	I
918	243	270	b 445	В	I
1548	171	340	ь 380		
1549	189	270	b 300		
1557	206	290	b 360		
1714	193	300	b 330		
1715	195	270	b 335		
1716	212	310	b 350		
1717	150	350	b 390		
1848	164	340	b 420		
1855	154	360	b 370		
1877	166	360	b 400		
2122	186	350	b 430		
2164	162	360	b 410		
** BAC	ON				
58	201	450	b 625	В	I
** BEN	HILL				
154	353	256	b 739	В	I
160	355	260	b 380	В	I
355	363	243	b 295		
1738	359	260	b 410	В	I
1830	368	240	b 310		
1832	354	240	b 370	В	I
1838	248	130	b 232	В	Ι
1842	335	200	b 310	В	Ι
1858	362	260	b 382	В	I
1863	372	210	b 215		
1867	352	264	b 330		
1868	365	180	b 240		

WELL	LAND	DEPTH	DEPTH	USED	USED
NUMBER	SURFACE	TO TOP	TO BOTTOM	ON BASE	ON
	ELEVATION	OF AQUIFER	OF AQUIFER	OF AQUIFER	ISOPACH
	(FEET)	(FEET)	(FEET)	MAP	MAP
1869	378	190	b 270		
1872	334	230	b 240	В	I
1883	350	270	b 368		
1884	356	300	b 410	В	Ι
1898	335	240	b 706	В	Ι
2111	260	130	b 218		
3037	197	100	b 390	В	I
	RIEN	· _ · _			
159	250	b 317			
1368	291	380	b 550	В	Ι
1815	235	260	b 485	В	I
1843	244	270	b 298		
1856	249	270	b 290		
1860	243	260	b 285		
1875	215	320	b 350		
1881	272	a 300	b 335		
1960	210	240	b 300		
2039	307	440	b 575	В	I
2040	220	250	b 278		
2049	214	230	b 310		
2082	308		b 500		
2083	217	230	b 320		
2104	226	270	b 320		
2105	222	240	b 340		
2128	216	420	b 430		
2146	223	275	b 350		
2167	220	230	b 244		
3542	320	604	1016	В	I
3555	278	440	b 540		
** BRO0					
3	165	60	b 200	В	I
21	195	175	b 310	В	I
77	200	120	b 160		
87	245	Ь 220			
469	210	150	b 304	В	I .
723	191	210	b 240		
759	235	110	b 231	В	I
840	189	105	b 205		
846	219	175	b 296	В	I
888	150	100	b 200		
889	184	120	b 156		

WELL	LAND	DEPTH	DEPTH	USED	USED
NUMBER	SURFACE	ΤΟ ΤΟΡ	TO BOTTOM	ON BASE	ON
	ELEVATION	OF AQUIFER	OF AQUIFER	OF AQUIFER	ISOPACH
	(FEET)	(FEET)	(FEET)	MAP	MAP
892	212	190	b 240		
893	228	150	b 250		
894	127	90	b 190		
895	228	120	ь 240	В	I
896	223	100	ь 200		
897	205	160	b 250		
898	127	100	b 209	В	I
899	219	90	b 220	В	I
900	201	100	b 186		
901	225	110	b 210		
902	218	120	b 226	В	I
911	215	170	b 218		
912	155	80	b 200	В	I
1005	213	190	ь 230		
1006	183	120	ь 220		
1106	185	115	b 205		
1387	235	150	b 300	В	I
1390	165	100	ь 180		
1436	185	90	b 182		
3189	220	143	b 335	В	I
3208	160	a 61			
3209	200	a 223	627	В	I
3211	260	a 186	472	В	I .
** BUL	LOCH				
81	162	300	430	В	I
378	223	365	585	В	I
393	193	475	b 577	В	I
430	305	348	b 456	В	Ι
432	185	380	ь 460		
439	241	470	b 560		
553	155	310	b 515	В	I
571	290	383	505	В	I
576	252	351	b 450		
580	228	363	b 512	В	I
586	230	360	b 410		
666	222	330	b 670	В	Ι
929	242	286	b 360		
1044	190	334	524	В	Ι
1707	187	450	b 520		
1709	215	430	b 480		
3210	200	302	556	В	Ι
3520	198	270	605	В	I

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WELL NUMBER	LAND SURFACE ELEVATION (FEET)	TC OF	PTH TOP AQUIFER EET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON I SOPACH MAP
3522	118		450	770	В	I
** CANE	DLER					
429	193e		320	b 577	В	I
574	255		345	b 471	В	I
575	218		413	b 533	В	I
581	273		296	b 430	В	I
582	285		389	b 450		
591	215		327	Ь 450	В	I
592	249		307	b 450	В	I
636	278		329	b 371		
740	230		327	b 431	В	I
963	232		524	b 635	В	I
1702	268		440	b 530		
** COF	=EE					
434	198e		400	b 600	В	I
445	165		290	1010	В	I
446	270		495	1085	В	I
468	312		530	1250	В	I
508	265		540	1350	В	I
509	309		520	1370	В	I
510	280		440	1280	В	I
1538	257	b	400			
1825	315		620	b1120	В	I
3033	215		340	b 600	В	I
3034	200		290	b 600	В	I
3041	251		400	b 650	В	I
3127	275	а	420	1300	В	I
3541	290		567	b1026	В	I
	TTIU					
170	287		470	820	В	I
175	317		460	640	В	I
188	282		245	570	В	I
688	330	b	523		В	
767	312		415	b 555		I
785	280		210	b 267		
786	266		165	b 254	В	
848	282		350	b 485	В	I
870	238		400	b 500		
877	352		515	b 850	В	I
1018	235		145	b 155		

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WELL NUMBER	LAND SURFACE ELEVATION (FEET)	DEPTH TO TOP OF AQUIFER (FEET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON ISOPACH MAP
1242	279	240	b 270		
1243	365	290	b 300		
1246	291	440	b 495		
1248	310	430			
1256	299	450	b 545		
1260	305	440	b 560	В	I
1268	305	460	b 540		
1416	270	270	b 300		
1419	307	475			
1455	355	280	b 380		
1467	290	440	ь 500		
1614	330	480	b 530		
1617	355	460	b 620	В	I
1620	328	280	b 365		
1649	328	440	ь 540		
1910	332	b 760			
1911	235	a 130	ь 190		
1918	338	582	b 702	В	I
1922	239	250	b 267		
1943	358	176	b 240		
1952	332	622	b1017	В	I
1964	324	482	ь 522		
1965	359	b 482			
1968	318	480	670	В	I
1975	350	230	b 250		
2043	365	470	b 640	В	I
2094	338	260	b 285		
3179	350	b 705			
3195	330	470	830	В	I
3196	245		620	В	
3199	290	396			
3212	225	a 170	590	В	I
3213	270	a 195			
3214	245	149	500	В	I
3456	348	500		_	_
3535	290	396	700	В	I
3544	255	175	b 240	_	_
3545	350	316	791	В	I
14H10	357	440	885	В	I
** COC	к				
25	293	358	b 491	B ,	I
39	240	209	ь 270		

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WELL NUMBER	LAND SURFACE ELEVATION (FEET)	DEPTH TO TOP OF AQUIFER (FEET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON ISOPACH MAP
105	272	b 280			
114	235	b 220			
118	228	190	b 280		
122	239	200	b 270		
682	236	240	b 260		
684	295	260	b 500	В	I
966	241	195	444	в	I
1423	245	215	b 275		
1497	231	200	b 230		
1576	295	b 370			
1638	268	290	b 320		
1927	290	b 581			
1969	222	240	b 300		
3350	205	170	b 440	В	I
** DEC	ATUR				
10	130	82	373	В	I
49	133	a 190	390	В	I
57	135	a 115	400	В	I
168	88	a 138	530	В	I
206	270		930	В	
228	131	75	375	В	I
805	316	598	b 904	В	I
1359	299	340	b 442	В	I
3359	118	56	b 185	В	I
3360	119	50	b 145		
3434	140	85	b 160		
	INGHAM				
211	75	195	ь 400	В	I
457	102	277	b 360		
458	70	250	b 360	В	I
569	48	319	Ь 400		
1035	17	220			
1704	34	240			
2179	95 120	165	b 175	_	_
3107	120	180	b 345	В	I
3108	112	146	b 198		
3109	113	168	b 188		
3110	109	158	b 210		
3140	57	281	b 315		
3155	68	233	b 276		

WELL NUMBER	LAND SURFACE ELEVATION (FEET)	DEPTH TO TOP OF AQUIFER (FEET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON I SOPACH MAP
** EVA	NS				
635	105	368			
773	193	445	ь 700	В	I
1547	143	440			
** GRA	DY				
140	265e	368	b 495	В	I
141	235	402	b 434		
196	209	365	587	В	I
205	245	477	b 587	В	I
493	308	340	b 550	В	I
801	163	190	b 215		
883	238	460	b 482		
884	239	472	b 550		
916	233	70	b 205	В	I
962	205	471	670	в	I
1446	242	300	b 353		
** IRW	TN				
274	331	230	b 630	В	I
1551	292	570	b 620	2	•
1552	315	320	b 340		
1712	350	250	0 340		
1713	378	250	ь 300		
1847	344	250	b 310		
1847	344	250	b 310		
1865	340	154	b 352	в	I
1873	330e	270	b 350	5	•
1961	330	220	b 352	8	I
1979	328	180	b 320	В	I
2017	325	220	b 520 b 501	В	I
2114	355	210	b 330	В	I
2134	322	170	b 233	Б	1
2154			b 233 b 365	D	7
	317	255		В	I
3103	353	260	b 696	В	I
	F DAVIS			_	
157	250	557	b 840	В	I
1165	252	580		•	
1749	280	b 520			
1826	220	580			
3128	272	a 440	b1250	В	I
3384	202	425	b 760	В	I

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WELL NUMBER	LAND SURFACE ELEVATION (FEET)	DEPTH TO TOP OF AQUIFER (FEET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON I SOPACH MAP
3457	287	450	1270	В	I
** MIT(	CHELL				
89	335	305	b 337		
100	371	a 315	ь 500	В	I
109	318	370	850	В	I
218	177	90	b 310	В	I
400	318	b 316			
417	160	63	b 84		Ι
564	164e	50	340	В	1
620	265	0	b 171	В	I
1397	272		b 648	В	I
1539	153	a 50			
1459	322	240		_	
3081	340	234	b 822	В	I
** MON1	GOMERY				
190	260	370			
319	133	220	b 240		
450	221	330	b 500	В	I
514	190	430	b 547	В	I
515	170	315	b 512	В	I
600	258	283	b 645	В	I
1520	291	390			
3153	222	471	b 700	В	I
25R002	239	b 400			
	EVEN	47/	2/2	-	-
295	212	134	268	В	I
413	192	91 220	b 216	В	Ι
462 579	220	220	b 300		
578 590	165 111	177 123	b 207 143		Ŧ
979	160	125	637	B	I
1007	261	180	b 325	B B	I I
1170	41	60	b 123	B	I
1175	90	30	116	В	I
B31	70 71	a 30	61	В	I
B32	75	a 33	114	В	I
B36	49	a 37	113	B	I
B37	102	118	213	B	I
			215	~	•

522       187       505       b       678       B         572       172       510       b       950       B         583       250       634       b       675         593       190       412	I
180       182       480       b       820       B         522       187       505       b       678       B         572       172       510       b       950       B         583       250       634       b       675         593       190       412	I
572       172       510       b 950       B         583       250       634       b 675         593       190       412         662       213       391         1509       228       415       b 465         1530       210       380       b 480         1531       165       350         1545       97       590       b 710       B         1731       153       500       b 550       B         1741       130       460       1742       205       490	
583       250       634       b 675         593       190       412         662       213       391         1509       228       415       b 465         1530       210       380       b 480         1531       165       350       500       b 550       B         1731       153       500       b 550       B       1741       130       460         1742       205       490       490       100	Ι
593       190       412         662       213       391         1509       228       415       b 465         1530       210       380       b 480         1531       165       350	
662       213       391         1509       228       415       b 465         1530       210       380       b 480         1531       165       350       500         1545       97       590       b 710       B         1731       153       500       b 550       B         1741       130       460       1742       205       490	
1509       228       415       b 465         1530       210       380       b 480         1531       165       350       500         1545       97       590       b 710       B         1731       153       500       b 550       B         1741       130       460       1742       205       490	
1530       210       380       b 480         1531       165       350         1545       97       590       b 710       B         1731       153       500       b 550       B         1741       130       460         1742       205       490	
1531       165       350         1545       97       590       b 710       B         1731       153       500       b 550       B         1741       130       460         1742       205       490	
1545         97         590         b         710         B         1           1731         153         500         b         550         B           1741         130         460	
1731 153 500 b 550 B 1741 130 460 1742 205 490	
17411304601742205490	I
1742 205 490	
1743 224 520 b 630 B	I
1744 217 600	
1745 212 500	
3026 210 460 b 744 B	I
** TELFAIR	
	I
	I
1053 263 208	
** THOMAS	
	I
	I
	I
	I
603 201 b 240	
747 200 165 b 240	
748 189 58 6 80	
768 230 130 b 175	
771 272 a 210 b 295	
778 255 190 Ь 200	
	I
784 170 85 b 115	
787 230 125 b 225	
	I
808 225 115 b 180	
810 265 170 b 195	
811 268 205 b 245	
814 229 a 140 b 250 B	

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WELL NUMBER	LAND SURFACE ELEVATION (FEET)	DEPTH TO TOP OF AQUIFER (FEET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON ISOPACH MAP
817	195	45	b 250	В	I
826	261	195	b 210		
830	210	330	b 360		
854	232	165	b 270	8	I
866	180	105	b 190		
886	262	395	b 410		
914	285	195	b 220		
915	275	b 395			
924	305	500	b 530		
925	248	356	b 380		
934	198	130	b 240	В	I
995	255	140	b 170		
996	260	160	b 180	_	_
1022	191	a 110	b 240	В	I
3186 3188	327	470	b 810	B	I
3207	200 238	a 96	740 701	B	I
3215	238	130 157	701 565	B B	I
3534	330	444	892	В	I I
5554	550	****	072	D	1
** TIF	г				
82	328	256	b 501	В	I
292	355	270	b 585	В	I
419	338	170	b 350	В	Ι
1465	370	200	b 260		
1632	325	b 540			
1687	321	b 700			
1692	329	870			
1782	335	278	b 580	В	I
1903	250	580	b 670		4
1912	269	365			
1914	295	400			
1930	295	308	b 352		
1977	311	b 95	b 280	В	I
1989	324	450	b 490		
1993	392	254	b 294		
2027	330	575			
2034	600	470			
2067	300	195	b 220		
2088	390 705	185			
2095	395	200	1050		•
16J005 16J030	295 280	865 860	1050 h1046	B	I
101020	200	860	b1046	В	I

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WELL LAND DEPTH DEPTH USED NUMBER SURFACE TO TOP TO BOTTOM ON BASE ELEVATION OF AQUIFER OF AQUIFER OF AQUI (FEET) (FEET) (FEET) MAP	USED ON FER ISOPACH MAP
** TOOMBS	
95 198 448 1180 B	I
146 205 645	
640 217 460 b 560	
650 290 420 b 808 B	I
652 231 b 715 b 715	
667 194 600 b 885 B	I
1090 292 460	
1521 176 370	
1540 212 510 b 530	
1542 230 640 b 820 B	I
1546 220 370	
1700 252 390	
1732 247 640	
1740 208 680 b 740	
1753 236 480	
1754 255 b 600 b 600	
1800 188 630	
1801 240 500 b 609 B	I
1802 188 630	
1803 169 b 575	
** 10155150	
** WHEELER 92 225 254 b 288	
92 225 254 b 288 336 180 360 1100 B	I
337 141 345 b 610 B	I
340 235 295 b 340	1
1045 195 170	
3080 172 260 900 в	I
3084 161 250 1050 в	- I
23q002 205 240	-
** WORTH	
232 260 a 50 b 80	
420 355 65 b 180 B	I
456 410 280 b 300	
1231 425 190 b 460 B	I
1235 350 225 b 300	
1265 407 220 b 235	
	Ι
1405 372 240 b 405 B	1
1405 372 240 b 405 в 1644 412 210	1

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WELL NUMBER	LAND SURFACE ELEVATION (FEET)	DEPTH TO TOP OF AQUIFER (FEET)	DEPTH TO BOTTOM OF AQUIFER (FEET)	USED ON BASE OF AQUIFER MAP	USED ON ISOPACH MAP
1939 1999 2023	360 370 389	360 374 240	b 620 b 610	B B	I I
2024 2045 2066	378 340 395 378	180 90 300	b 210 b 320	В	I
2080 2093 3154	338 296 322	275 110 550	820	В	I

Notes:

a maximum depth to top of aquifer

b minimum depth to top or bottom of aquifer

e land surface elevation is estimated

B indicates that the well was used on the bottom of aquifer structure-contour map

I indicates that the well was used on the isopach map

MAP OWNER/WELL NAME NUM- BER	OTHER GGS, USGS G			LENGTH	DEPTH		DOWN		SAMPLE DATE	PLATES	DATA SOURCE
** APPLING B001 CITY OF BAXLEY	1059	27N001	12	500	764	1000		24HRS	04/28/71	H,T,S	1,4
B002 FILTERED ROSIN PROD. CO.	27N004		8	525	625	100		20MIN	/ /	н	1
B003 GEORGIA POWER #1	27P001		12	455	680	750		8HRS	/ /	н	1
B004 GEORGIA POWER #2	27P002		12	490	711	750		8HRS	/ /	н	1
BOO5 CITY OF BAXLEY	27N003		12	564	849	704		24HRS	04/18/67		2,4
BOOG ALTAMAHA MHP			6	470	600	200	4.0		08/27/80		3
B007 GA BAPTIST CHILDRENS HOME			4	578	650	300	10.0	1HR	05/15/84	•	3
BOO8 R. PEARCE	28N001		0	580	700	0	0.0		03/12/63		4
B009 TOWN OF SURRENCY			0	553	651	0	0.0		05/11/66	T,S	4
** ATKINSON											
B010 CITY OF WILLACOOCHEE #2	918	21J003	0	289	445	0	0.0		05/09/66	•••	
B011 CITY OF WILLACOOCHEE #1	21J001		0	380	408	0	0.0		05/09/46		
B012 CITY OF PEARSON	231003		0	361	471	0	0.0		12/01/59	H,T,S	4
** BACON	50	2/1 004	10	7/7	(2)	7/0	1 (	FUDO	10 /02 /50		1 /
BO13 CITY OF ALMA		26L001	10	363	626	360		5HRS	12/02/59	• •	1,4
BO14 CITY OF ALMA #3	26L004		12	501	840 705	1000 2250		12HRS		н	1
B015 DEERING MILLIKEN SER. #2			16	397	795	2250	25.0	10HRS	/ /	н	2
** BEN HILL	15/	204007	10	260	750	1000	27.0	8HRS	, ,	u	2
B016 CITY OF FITZGERALD C	154	20M003	12						/ /	н	2
BO17 CITY OF FITZGERALD D	355 1898	19M001	12 12	283	612	1016 1192		24HRS	12/03/51		2,4 1
B018 CITY OF FITZGERALD E B019 CITY OF FITZGERALD F	1090		12	250 295	663 453	1200		12HRS 8HRS		н	1
B019 CITY OF FITZGERALD G			12	318	450	1200		24HRS		н Н	2
BO21 TREES, INC.	3037	20N002	6	272	390	0	0.0	24083		T,S	1
BO21 TREES, INC. BO22 CITY OF FITZGERALD A	20M002		10	260	825	0	0.0		/ / 04/22/71		4
B022 CITT OF FITZGERALD A B023 H. COWAN	21N001		0	189	299	0	0.0		04/20/67		4
** BERRIEN	211001		Ŭ	107	277	Ũ	0.0		04/20/01	1,5	4
BO24 CITY OF ALAPAHA	1368	20K002	8	368	550 0	00000	000 0	999999	11	н	5,1
B024 CITY OF RAY CITY #2	1508	ZUKUUZ	10	208	396	750	1.5		11/30/78		3
BO26 CITY OF NASHVILLE #4	1815	20H003	16	283	485	1000		24HRS	06/18/70		
BO27 CITY OF NASHVILLE #5	1015	2011005	16	280	505	1000		24HRS	/ /	н, г, з Н	2
B028 CITY OF ENIGMA #2	19K005		6	386	620	225		24HRS	03/09/82		3,4
B029 J.C. TYSON	18J022		0	380	540	0	0.0	241183	05/09/66		4
B030 CITY OF NASHVILLE #2	19H026		0	265	450	0	0.0		08/02/61		4
BO31 CITY OF RAY CITY #1	206009		0	200	450 350	0			05/26/43		4
** BROOKS	200007		Ŭ	200	570	Ũ	0.0		0)/20/45	1,0	-
B032 C.L. WILLAFORD	900	17F007	4	158	186	0	0.0		06/20/74	тs	1
B033 J.M. TYSON #1	1005	16F009		185	230	0	0.0		06/20/74	•	1
B034 CITY OF MORVEN #3	1005	101 007	8	160	315	285			11/04/82		
B034 CITT OF MORVEN #3 B035 FAWN HIGHTS S/D			4	180	220	56		24HRS	10/22/84		
BO36 FERNWOOD MHP #1			4	99	220 126	56		24885 1HR	10/22/84		
BO36 FERNWOOD MAP #1 BO37 CITY OF QUITMAN #3	17E012		4 0	120	304	0 0	0.0	(B <b>N</b>	08/03/61		4
** BULLOCH	112012		0	120	504	U	0.0		50/05/01	1,5	-
B038 STATESBORO AIR FIELD #2	81		10	275	475	500	28.0	2	/ /	н	1
BODO STATESBOKO AIK TIELD #2	01		10	213	-15	200	20.0	•	, ,	**	•

MAP OWNER/WELL NAME NUM- BER	OTHER ID# GGS, USGS GRID	ETER	LENGTH	DEPTH	CHARGE	DRAW LENGI DOWN OF (FT) TEST	H SAMPLE DATE	PLATES	DATA SOURCE
BER	USGS GRID	(IN)	((1)	(1)	(GPM)	(FT) 1251			
B039 CITY OF STATESBORD #4	378	18	400	555	1040	92.0 ?		н	2,1
BO40 WILLOW HILL SCHOOL	430	6	386	450	36	12.5 8HRS	1 1	 Н	1
BO41 CITY OF BROOKLET #1	32T13	8	302	510	0	0.0	06/10/43		4
B042 BULLOCH CO. GROWERS ASSN.	666	6	357	670	350	9.0 ?	1 1	Н	1
B043 CITY OF STATESBORO #7		20	360	490	1400	133.0 24HRs	11	Н	1
B044 CITY OF BROOKLET #1	553	8	346	525	175	13.0 3HRS	11	н	2
B045 ITT GRINNELL #1		10	320	430	500	80.0 8HRS	11	Н	2
B046 COOPER WISS #1		8	315	420	400	40.0 24HRS	11	н	2
B047 GA. SOUTHERN COLLEGE #1		8	420	550	225	90.0 8HRS	1 1	Н	2
B048 GA. SOUTHERN COLLEGE #2		8	420	610	610	90.0 8HRS	11	Н	2
B049 CITY OF STATESBORO #2	31T010	8	320	555	305	5.0 ?	01/06/60	H,T,S	2
B050 COUNTRY CLUB HILLS S/D		6	375	480	220	15.0 24HRS	12/30/80	H,T,S	3
B051 GEORGIAN WALK WATER CO.		6	296	420	210	4.0 6HRS	1 1	Н	3
B052 LAKESIDE ESTATES S/D		8	281	355	500	10.0 ?	1 1	Н	3
B053 NEVILS WATER ASSOCIATION		8	475	600	385	4.0 9HRS	1 1	н	3
B054 CITY OF PORTAL	300002	0	395	596	0	0.0	04/11/63	T,S	4
B055 A. DORMAN	320002	0	150	516	0	0.0	06/11/43	st,s	4
** CANDLER									
B056 CITY OF METTER #2 SOUTH	29T010	10	386	616	626	14.0 24HRs	09/12/79	, н <b>,</b> т,ѕ	1,2
B057 CITY OF METTER #2 NORTH	29T011	12	321	540	1000	4.0 12HRs	11	Н	1
B058 CITY OF METTER #2	291006	0	308	520	0	0.0	08/07/61	T,S	4
B059 L. RUSHTON	290001	0	350	389	0	0.0	03/31/66	τ,s	4
** COFFEE									
B060 CITY OF AMBROSE	1825	8	442	1120	385	5.0 8HRS	/ /	н	1
BOG1 CITY OF DOUGLAS #5	23L004	16	514	684	1800	1.1 33HRS		Н	2
B062 CITY OF DOUGLAS #4	23L002	14	506	728	1250	1.8 36HRS			1,2
B063 CITY OF NICHOLLS #3		10	506	760	800	8.0 24HRs			2
BO64 PARKVIEW VILLAGE MHP	07.007	4	370	380	50	2.0 ?	/ /	Н	3
B065 CITY OF DOUGLAS #3	23L003	0	395	590	0	0.0	08/02/61	T,S	4
** COLQUITT	475 45400	7 4/	/ 25	750	40/0	74 0 0/110		– .	
B066 CITY OF MOULTRIE #3	175 15H00		425	752		31.0 24HRs		• •	1
B067 CITY OF NORMAN PARK B068 SWIFT & CO #4	3195	8	490	1220	305	28.0 24HRs		H	1,2
BOOS SWIFT & CO #4 BOOS CITY OF MOULTRIE #5	15H011 15H040	18	380	800		120.0 ?	/ /	H	1
B070 CRESTWOOD S/D	158040	18 4	422	580	2150	8.0 ?	09/01/76		3
-	15H032		324	480	40 500	3.0 24HRS			3
B071 COLQUITT COUNTY HOSPITAL	12H022	10	438	564	500	2.0 48HRS		Н	3
B072 CITY OF ELLENTON #2	14J001	8	246	410	150	20.0 48HRs		H	3
B073 D.E. SMITH B074 D.C. SMITH		0	260	350	0	0.0	04/28/69	-	4
BO74 D.C. SMITH BO75 T. WILLIAMS	15J003	0	300	380	0	0.0	04/28/69		4
B076 G. POWELL	16J019	0	386	684	0	0.0	04/28/69	•	4
B077 N.C. BRANNON	17J015	0	726	1008	0	0.0	04/29/69	-	4
BO77 N.C. BRANNON BO78 R. BAKER	17H022 17H014	0 0	215 218	350 298	0	0.0 0.0	04/29/69	•	4
B079 MT. OLIVE BAPTIST CHURCH	16H032	0	218 310		0		05/25/65		4
B080 BRIDGEPORT BRASS CO.	16H032 16H014	0	425	500 579	0 0	0.0	04/29/69		4
BOOD BRIDGET ONT BRASS CO.	1011014	U	420	717	U	0.0	05/25/65	1,5	4

MAP OWNER/WELL NAME NUM-	OTHER GGS,	ID#		CASING LENGTH					SAMPLE DATE	PLATES	DATA SOURCE
BER	USGS (	GRID	(IN)		(FT)		(FT)				
		_									,
BO81 SOUTH GEORGIA WATER CO.	16H02		0	515	700	0	0.0		10/08/69		4
BO82 N.D. GUNN	15H022		0	396	480	0	0.0		04/28/69		4
BO83 J. KIRK II	15H03		0	840 (F8	840	0	0.0		04/28/69	-	4
B084 O.C. CAUSEY	15H019		0	458 ( 05	625	0	0.0		05/12/65	•	4
B085 W.M. BROOKS	158004		0	485	930	0	0.0		05/12/65	-	4
BO86 W.H. SUMMERLAIN	15H002		0	44	740	0	0.0		05/12/65	-	4
B087 J.A. FAISON	14H01		0	630 205	810	0	0.0		04/30/69		4
BO88 R.L. MILLINGS #2	14009		0	285	403	0	0.0		04/30/69	-	4
B089 L. FUNDERBURKE	15H033		0	457	780	0	0.0		04/30/69	•	4
B090 H. TOMLINSON	158002		0	426	474	0	0.0		04/21/64	-	4
B091 E. LEWIS	15G004		0	394 772	494	0	0.0		05/11/65		4
B092 L. SMITH	15G010		0	372	431	0	0.0		04/30/69	-	4
B093 D. BELL	16G001		0	182	210	0	0.0		05/11/65	•	4
B094 K.G. CARDIN	17G014		0	155	310	0 0	0.0		10/07/69	-	
B095 C. LAWRENCE	16G001		0	215	307		0.0		04/30/69	-	4 4
B096 E. WALDEN	17600		0	202	318	0	0.0		05/11/65	-	4
B097 TYSON & DEAN DRILLING	16H018		0	294	400	0	0.0		04/29/69		
B098 G. COLE	16G022		0	205	320	0	0.0			•	4
B099 CITY OF BERLIN #1	16G017		0	200	400	0	0.0		05/11/65		4
B100 K.G. CARDIN #2	176015		0	206	315	0	0.0		10/07/69		4
B101 J.B.VAUGHN	16,009		0	531	630	0	0.0		04/28/69	-	4
B102 CITY OF NORMAN PARK	16,002		0	499	817	0	0.0		06/12/65	-	4
B103 J.B. PRICE	15,012		0	417	528	0	0.0		04/28/69		4
B104 CITY OF DOERUN #2	14J002	2	0	266	555	0	0.0		05/12/65	•	4
B105 E.T. GAY			0	256	426	0	0.0		04/19/67	1,5	4
** COOK	400	100000	10	774	70/	500	10.0	01100	, ,		<b>`</b>
B106 CITY OF ADEL #3	122	18H002	12	231	386	500	10.0		/ /		2
B107 CITY OF ADEL #1	39 (82	18H005	12	213 253	375 335	1200	20.0		04/19/67		2,4
B108 CITY OF ADEL #4	682 ( 8)	18H008	12			1200		10HRS		H	1,2
B109 CITY OF LENOX #2	684 1218	18J012	8 19	266 200	501 393	308		10HRS	/ /	H	1
B110 CITY OF ADEL #5	1218	18H033				1571		8HRS	11/28/78		1,2
B111 CITY OF CECIL	1423	18G018		214	308	53	12.8		03/17/65		1,4
B112 CITY OF ADEL #2B			12	221	359	1120	30.0		/ /		2
B113 CITY OF ADEL #6			16	229	405	1865		24HRS	11/17/65		
B114 SUNSHINE TRAILER COURT	40.004	-	4	256	300		21.0		08/15/85		
B115 CITY OF SPARKS	18H01		0	400	407	0			04/29/65		
B116 USGS ADEL TEST WELL	18H01	5	0	207	865	0	0.0		12/01/64	1,8	4
** DECATUR		0-101	40	400		40/0	50.0	201111	00.05.70		
B117 CITY OF BAINBRIDGE #3	228	9F486	12	109	464			20MIN			
B118 CITY OF BAINBRIDGE #2	804	9F519	12	122	351	1700		22HRS			1
B119 J. CAMPBELL CO.	1412	10E199		285	329	15	1.0		11	Н	1
B120 CITY OF BAINBRIDGE #5	0-000		14	230	375		47.0			н	1,2
B121 AMOCO FABRICS CO. #1	8F008		12	127	222	800	4.0		/ /	H	2
B122 AMOCO FABRICS CO. #2	9F003		12	100	240	800	4.0		/ /	н	2
B123 CITY OF BAINBRIDGE #1			20	147	445	1650	02.U	12HRS	/ /	Н	2

MAP OWNER/WELL NAME NUM-	OTHER GGS,		ETER	LENGTH	DEPTH	CHARGE	DOWN	OF	SAMPLE DATE	PLATES	DATA SOURCE
BER	USGS G	RID	(IN)	(FT)	(FT)	(GPM)	(FT)	TEST			
	85/0/		40	2/0	( 00	(07					-
B124 DECATUR COUNTY AIR PARK B125 C.W. WHITE	8F494 8F004		10	240 78	408 83	607	8.0	?	/ /	Н	2
	9F004		0 0	78 82		0	0.0		09/07/61		4
B126 H.M. WHITLEY			0		88	0	0.0		08/08/61	•	4
B127 CITY OF BAINBRIDGE #4	9F488		-	147	485	0	0.0		08/09/61	•	4
B128 A.J. NEWTON	9F002		0	83	105	0	0.0	2/1122	03/30/62	•	4
B129 RED BARN MHP			4	200	220	40	5.0	24HRS	/ /	н	3
** EFFINGHAM	244		40	400	(	(00	~~ ~				_
B130 CITY OF SPRINGFIELD #2	211	-	10	180	400	400	20.0		//	Н	2
B131 WESTWOOD HEIGHTS S/D	961	36\$004	11	303	565	900		4HRS	/ /	н	1
B132 CITY OF SAVANNAH	1035	36\$021		234	454	600	9.3		11	Н	1
B133 DAWES SILICA COMPANY	1527	34R043		320	689	2600	17.0		/ /	Н	1,2
B134 DAWES SILICA COMPANY	1704	34R044		312	520	500	6.0		/ /	Н	1
B135 CITY OF RINCON #2	365022		10	281	500	700		12HRS	/ /	Н	2
B136 FORT HOWARD PAPER CO. #1	368025		14	280	500	750		10HRS	/ /	Н	2
	368026		14	280	520	750		24HRS	11	н	2
B138 FORT HOWARD PAPER CO. #3	36s027		8	282	500	300	16.0	1HR	04/11/86	H,T,S	2
B139 LAKESIDE WATER CO. #2			8	300	500	400		3HRS	1 1	н	2
B140 SEPCO #1			10	240	500	525	6.0	12HRS	/ /	Н	2
B141 SEPCO #2			10	242	500	800	8.0	12HRS	/ /	Н	2
B142 FOXBOW NORTH S/D #2			8	320	460	600	17.0	24HRS	/ /	н	3
B143 FOXBOW NORTH S/D #1			8	317	440	500	15.0	8HRS	11/02/82	H,T,S	3
B144 LAKESIDE FARMS S/D #3			8	340	450	500	10.0	8HRS	1 1	Н	3
B145 MEADOWWOOD S/D			4	340	440	90	2.0	24HRS	12/12/83	H,T,S	3
B146 PECAN GROVE S/D			6	323	420	300	7.0	24HRS	/ /	Н	3
B147 SILVERWOOD PLANTATION			14	292	500	1001	16.4	24HRS	09/23/86	H,T,S	3
B148 TARA MHP			4	284	355	50	12.0	8HRS	01/18/84	H,T,S	3
B149 GOSHEN VILLAS			8	295	410	360	70.0	24HRS	1 1	Н	3
B150 COASTAL PUBLIC SERVICE CC	)		0	280	425	0	0.0		01/29/41	T,S	4
B151 CENTRAL OF GEORGIA RR	<b>3</b> 4R036		0	273	431	0	0.0		03/12/40	T,S	4
** EVANS											
B152 CITY OF CLAXTON	773	30R002	10	452	805	510	2.7	1HR	04/28/71	H,T,S	1
B153 CITY OF CLAXTON #2	30R001		12	401	701	780	7.0	?	11	Н	1,2
B154 CLAXTON POULTRY CO. #1			10	420	620	600	5.0	24HRS	11	н	2
B155 CLAXTON POULTRY CO. #3			10	380	600	1000	10.0	4HRS	11	н	2
B156 CITY OF DAISEY #2			8	491	705	400	6.0	24HRS	10/26/83	H,T,S	3
B157 P.H. JONES	30s002		0	440	480	0	0.0		11/14/63	T,S	4
B158 CITY OF CLAXTON	30R003		0	600	662	0	0.0		08/04/66		4
B159 G. TIPPENS	31Q001		0	460	515	0	0.0		04/01/66	-	4
** GRADY										•	
B160 CITY OF CAIRO #8			16	390	465	2500	2.0	11HRS	1 1	н	3
B161 CITY OF WHIGHAM			8	426	604	160		36HRS	10/18/77		3
B162 GRADY CO. CHILD DEV. CTR.			4	286	425	30		2HRS	/ /	н,,,,,,	1
B163 CITY OF CAIRO #1	12F030		· 0	492	671	0	0.0		10/02/62		4
B164 USGS CAIRO TEST WELL	12F036		0	560	740	Ō	0.0		06/23/64		4
· · · · · · · · · · · · · · · ·			Ŭ			Ŭ				.,-	•

MAP OWNER/WELL NAME NUM- BER	OTHER GGS, USGS GI			LENGTH	DEPTH		DOWN	OF	SAMPLE DATE	PLATES	DATA SOURCE
** IRWIN											
B165 CITY OF OCILLA #3	274	20L003	12	266	645	1000	30.0	?	08/02/61	H,T,S	1,4
B166 CITY OF OCILLA #4	3103		12	303	696	1200		12HRS	11	H	1
B167 CITY OF OCILLA #2			12	266	672	1200	20.0	12HRS	11	н	2
B168 J.W. PAULK	21L001		0	432	620	0	0.0		04/20/67	T,S	4
B169 J. MCDUFFIE	18M001		0	195	230	0	0.0		05/04/66	T,S	4
** JEFF DAVIS											
B170 CITY OF HAZELHURST #3	1165		12	600	950	1052	37.0	24HRS	11	н	3
B171 HAZELHURST MILLS #5			6	595	800	450	8.0	24HRS	11	н	2
B172 CITY OF DENTON			8	430	475	250	10.0	?	1 1	н	3
B173 LAKE OWL HEAD S/D			6	435	500	235	17.0	30HRS	03/21/86	H,T,S	3
B174 S. STOKES & C.W. CAIN #1	24M001		0	435	450	0	0.0		03/06/63	T,S	4
B175 CITY OF HAZELHURST #2	<b>25N</b> 004		0	450	648	0	0.0		01/05/60	T,S	4
** MITCHELL											
B176 CITY OF CAMILLA #3	218		12	155	341	2000	4.0	6HRS	1 1	н	2
<b>B177 GRAVEL HILL PLANTATION</b>	1062	13K001	10	116	386	732	2.0	5HRS	1 1	н	1
B178 CITY OF PELHAM #4	3081		12	240	822	856	72.0	24HRS	1 1	н	1,2
B179 BOWEN MOBILE ESTATES			4	300	465	41	5.0	1HR	1 1	н	3
B180 HINSONTON COM WATER ASSN			6	300	345	145	10.0	8HRS	1 1	н	3
B181 CITY OF SALE CITY #2			10	242	575	503	40.0	8HRS	1 1	Н	3
B182 CITY OF CAMILLA #1	12H004		0	120	396	0	0.0		03/29/63	T,S	4
B183 CITY OF CAMILLA #4			0	150	335	0	0.0		05/08/58	T,S	4
B184 L. BATEMAN	12M006		0	142	287	0	0.0		02/11/60	T,S	4
B185 CITY OF COTTON	13H006		0	300	305	0	0.0		02/10/60	T,S	4
B186 CITY OF PELHAM #1	12G001		0	190	720	0	0.0		02/10/60	T,S	4
B187 G.W. HENDLEY	11H001		0	100	110	0	0.0		05/02/67	T,S	4
B188 E. VANN, JR.	12J001		0	382	460	0	0.0		02/11/60	T,S	4
** MONTGOMERY											
B189 CITY OF UVALDA #2	3153		8	501	700	250			08/08/75		
B190 CITY OF MT VERNON #1			8	400	700	480			02/18/81		
B191 CITY OF AILEY #2			4	516	700	340			06/04/81		
B192 CITY OF ALSTON #1			8	522	700	183			08/28/72		
B193 MONIGOMERY CORR. INST. #2	2		6	450	570			24HRS	02/02/70	H,T,S	3
B194 CITY OF TARRYTOWN #2			4	474	580	165	44.0		1 1		3
B195 WILDWOOD MHP			4	415	504	45			08/31/76		
B196 T.A. BLOCKER	25s001		0	373	452	0	0.0				4
B197 CITY OF AILEY #1	25R001		0	345	403	0	0.0		08/04/61		4
B198 CITY OF MT VERNON	25R002		0	347	400	0	0.0		03/05/43		4
B199 CITY OF UVALDA #1	250002		0	430	700	0	0.0		03/06/63	Τ,S	4
** SCREVEN											
B200 J.P. KING #2	32U018		24	253	670		36.0		/ /		1
B201 INDIGO MOBILE ESTATES			4	173	220	50		2HRS	/ /	н	3
B202 CITY OF HILLTONIA	32X034		0	178	400	0	0.0		05/04/64		4
B203 P.H. JOHNSTON	31x017		0	160	249	0	0.0		09/17/63	-	4
B204 MEAD INVESTMENT CORP.	33x020		0	205	369	0	0.0		08/12/63	T,S	4

MUM-         GGS,         ETER LENGTH DEPTH CHARGE DOWN OF         DATE         SOURCE           BER         USSG GRID         (1N)         (FT) (GPM)         (FT) TEST         SOURCE           B205         GA, DEPT. OF TRANS.         34W004         0         220         434         0         0.0         03/16/70         T,S         4           B206         CITY OF SYLVANIA #2         32W015         0         150         301         0         0.0         05/21/43         T,S         4           B206         CITY OF SYLVANIA #2         32W010         0         1212         275         0         0.0         05/17/70         T,S         4           B209         H.I. CONRER & C. FARMER         31W010         0         270         280         0         0.0         09/18/63         T,S         4           B211         CITY OF MUNASAS         3026         8         555         724         305         12.3         4488         / / H         1,2           B212         GERGIA STATE PRISON #3         3026         8         555         724         305         12.3         4488         / / H         1,2           B214         GENTY MENDARIZ         3026	MAP OWNER/WELL NAME	OTHER	ID#							SAMPLE	PLATES	
B205         GA. DEPT. OF TRANS.         34W004         0         220         434         0         0.0         05/16/70         7,5         4           B206         CITY OF SYLVANIA #2         32W015         0         150         301         0         0.0         05/16/70         7,5         4           B206         CITY OF SYLVANIA #4         32W070         0         197         257         0         0.0         05/16/70         7,5         4           B209         H.I. COMBER & C. FRAMER         31W010         0         212         275         0         0.0         09/18/63         7,5         4           B211 <city of="" oliver<="" td="">         33JU019         0         270         280         0         0.0         09/18/63         7,5         4           B212         CITY OF NAMASSAS         3026         8         555         744         305         12.3         4800         1.0         09/18/63         7,5         1.4           B213         CITY OF RAMASSAS         3026         8         555         744         00         15.0         20.0         300110         3/04/61         1,7,5         1,4           B213         CITY OF RAMASSAS         3026</city>	NUM-	GGS,	חזפי							DATE		SOURCE
B206         CITY OF SYLVANIA #2         S2U015         0         150         301         0         0.0         05/21/43 T,S         4           B207         CITY OF SYLVANIA #1         32W013         0         190         490         0         0.0         05/21/43 T,S         4           B208         CITY OF SYLVANIA #1         32W013         0         197         257         0         0.0         06/17/70 T,S         4           B209         H.I. COMMER & C. FARMER         31W010         0         212         275         0         0.0         09/18/63 T,S         4           B210         CITY OF NEWINGTOM         33W009         0         270         280         0         0.0         09/18/63 T,S         4           B212         CERCRIA STATE FRISON #3         879         12         556         855         1270         24.0         12.3 HHKS         / / H         3         12.2           B214         CERCRIA STATE FRISON #1         280001         8         560         713         400         15.0         300         30.0 24HRS         / / H         2           B216         CERCRIA STATE FRISON W112         290001         500         500         100         0.00 <td>DER</td> <td>0303 0</td> <td></td> <td>(14)</td> <td>(1)</td> <td>(FI)</td> <td>(GPM)</td> <td>(FI)</td> <td>IESI</td> <td></td> <td></td> <td></td>	DER	0303 0		(14)	(1)	(FI)	(GPM)	(FI)	IESI			
B206         CITY OF SYLVANIA #2         S2U015         0         150         301         0         0.0         05/21/43 T,S         4           B207         CITY OF SYLVANIA #1         32W013         0         190         490         0         0.0         05/21/43 T,S         4           B208         CITY OF SYLVANIA #1         32W013         0         197         257         0         0.0         06/17/70 T,S         4           B209         H.I. COMMER & C. FARMER         31W010         0         212         275         0         0.0         09/18/63 T,S         4           B210         CITY OF NEWINGTOM         33W009         0         270         280         0         0.0         09/18/63 T,S         4           B212         CERCRIA STATE FRISON #3         879         12         556         855         1270         24.0         12.3 HHKS         / / H         3         12.2           B214         CERCRIA STATE FRISON #1         280001         8         560         713         400         15.0         300         30.0 24HRS         / / H         2           B216         CERCRIA STATE FRISON W112         290001         500         500         100         0.00 <td></td>												
B206         CITY OF \$YLVANIA #2         324015         0         150         301         0         0.0         0.72/1/3 T,S         4           B207         CITY OF \$YLVANIA #4         324070         0         190         490         0         0.0         0/11/17/0 T,S         4           B208         CITY OF \$YLVANIA #4         324070         0         197         257         0         0.0         0/11/17/0 T,S         4           B210         CITY OF NEWINGTON         330009         0         200         280         0         0.0         0/9/18/63 T,S         4           B211         CITY OF NEWINGTON         330009         0         270         290         0         0.0         0/9/18/63 T,S         4           B211         CITY OF NEWINGTON         330019         0         270         290         0         0.0         0/9/18/63 T,S         4           B212         GEORGIA STATE PRISON #3         879         12         556         855         1270         24.0         128.4         17.5         1.4           B214         CITY OF REIDSVILLE #1         280001         8500         710         10.0         300.1         / H         2           B216<	B205 GA. DEPT. OF TRANS.	34W004	÷	0	220	434	0	0.0		03/16/70	T,S	4
B208       CITY OF SYLVANIA #4       32U070       0       107       257       0       0.0       06/17/70 T,S       4         B209       H.I. CONNER & C. FARMER       31W010       0       212       275       0       0.0       05/16/70 T,S       4         B210       CITY OF NEXINATION       33U009       0       200       280       0       0.0       09/18/63 T,S       4         B211       CITY OF NEXINATION       33U009       0       270       290       0       0.0       09/18/63 T,S       4         B212       GEORGIA STATE PRISON #3       879       12       556       855       1270       24.0       12HRS       / / H       1,2         B213       GEORGIA STATE PRISON #1       280002       8       500       810       550       20.0       30NIN       / / H       2         B216       GEORGIA STATE PRISON #1       280001       8       500       750       6.0       24HRS       / / H       2         B216       GEORGIA FATE PRISON #1       280001       500       750       6.0       24HRS       / / H       2         B217       GA. STATE PRISON WILTC       14       510       10.0       BHRS	B206 CITY OF SYLVANIA #2	32W015	5	0	150	301	0	0.0				4
B209       H.I. CONNER & C. FARMER       314010       0       212       275       0       0.0       03/16/70       T,s       4         B210       CITY OF NEWINGTON       330009       0       200       280       0       0.0       09/18/63       T,s       4         B211       CITY OF OLIVER       330019       0       270       290       0       0.0       09/18/63       T,s       4         B212       ECRAGALS STATE PRISON #3       879       12       556       855       127       24.0       128.85       08/04/61       H,T,S       1,2,4         B214       CITY OF REISON #3       879       12       556       855       120       20.0       30MIN       /       H       1,2,4         B215       GEORGIA STATE PRISON #1       280002       8       500       1016       10.0       304/04/61       H,T,S       1,2,4         B216       CITY OF GLENNVILLE #1       280001       0       500       700       6.0       24HRS       07/17/82       H       1         B216       CITY OF GLENNVILLE #1       30P001       0       508       955       0       0.0       05/12/26       T,S       4	B207 CITY OF SYLVANIA #1	32W013	3	0	190	490	0	0.0		11/17/59	T,S	4
B210         CITY OF         NEWINGTON         33U009         0         200         280         0         0.0         09/18/63         T,S         4           B211         CITY OF NURR         33U019         0         270         290         0         0.0         09/18/63         T,S         4           B211         CITY OF NURR         33U019         0         270         290         0         0.0         09/18/63         T,S         4           B212         GEORGLA STATE PRISON #2         879         12         556         855         1270         24.0         12kms         /         H         3           B213         CITY OF REIDSVILLE #1         290001         8         500         810         15.0         ?         08/04/61         H,T,S         1,2           B216         GEORGLA STATE PRISON W1LT         280002         8         500         810         1016         10.0         BHRS         02/17/62         H,T,S         3           B219         CITY OF GLENNVILLE #2         8         520         729         300         3.0         24/HRS         /         H         2           B219         CITY OF GLENNVILLE #1         300001 <t< td=""><td></td><td>32W070</td><td>)</td><td>0</td><td>197</td><td>257</td><td>0</td><td>0.0</td><td></td><td>06/17/70</td><td>T,S</td><td>4</td></t<>		32W070	)	0	197	257	0	0.0		06/17/70	T,S	4
B211 CITY OF OLIVER       33U019       0       270       290       0       0.0       09/18/c3 T,S       4         *** TATINALL       877       12       556       855       1270       24.0       12RS       /       H       1,2         B212 GEORGIA STATE PRISON #3       879       12       556       855       1270       24.0       12RS       /       H       3         B214 CITY OF REIDSVILLE #1       29001       8       560       713       400       15.0       7       36004       15.0       7       37.4       37.4       17.5       1,2       4         B216 GEORGIA STATE PRISON #1       280002       8       500       729       300       3.0       24.1       1.4       52.2       2		31W010	)	0	212	275	0	0.0		03/16/70	T,S	4
**         TATTNALL         B212         CEN         DEF         DEF<         DEF         DEF<         DEF<         DEF<         DEF         DEF<         DEF<         DEF<         DEF<         DEF<         DEF<         DEF<         DEF<         DEF<         DEF< <thdef<< th=""> <thdef<< th=""> <thdef<< th=""></thdef<<></thdef<<></thdef<<>	B210 CITY OF NEWINGTON	330009	2	0	200	280	0	0.0		09/18/63	T,S	4
B212 GEORGIA STATE PRISON #3       879       12       556       855       1270       24.0       12HRS       /       H       1,2         B213 GEORGIA STATE PRISON #1       280001       8       555       744       305       12.3       4HRS       /       H       3         B214 CITY OF MANASSAS       3026       8       550       713       400       15.0       ?       08/04/61 H, T, S       1,4         B215 GEORGIA STATE PRISON #1       280002       8       500       810       550       20.0       30MIN       /       H       2         B216 GEORGIA STATE PRISON #2       10       460       818       700       19.0       30MIN       /       H       2         B217 GA. STATE PRISON WILT #2       8       520       729       300       3.0       24HRS       12/22/266 H, T, S       3         B220 GEORGIA FORRESTRY COMM.       28P001       0       544       714       0       0.0       05/12/66 T, S       4         *** TELFAIR       222001       14       120       640       1200       5.0       7HRS       /       H       1         B224 CITY OF MCRAE #1       220001       14       120       640		330019	)	0	270	290	0	0.0		09/18/63	T,S	4
B213 CITY OF MANASASA       3026       8       555       744       305       12.3 4HRS       /       H       3         B214 CITY OF REDSVILLE #1       29001       8       560       713       400       15.0       ?       08/06/15       H,T,S       1,4         B216 GEORGIA STATE PRISON #1       28002       8       500       810       550       20.0       30MIN       /       H       2         B217 GEORGIA STATE PRISON W11       C       14       551       940       1016       10.0       8HK       0/       H       2         B217 GIORGIA STATE PRISON W1       C       14       551       940       1016       10.0       8HK       /       H       2         B218 CITY OF GLENNVILLE #3       12       560       800       750       6.0       24HKS       1/2/2/86 H,T,S       3         B220 CITY OF GLENNVILLE #3       30P001       0       344       714       0       0.0       0.5/12/66 T,S       4         B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5       ?       /       H       1         B224 CITY OF LUMBER CITY #1       24P0001       10       366 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
B214 CITY OF REIDSVILLE #1       290001       8       560       713       400       15.0 ?       00/04/61 H,T,S       1,4         B215 GEORGIA STATE PRISON #1       280002       8       500       810       550       20.0 30MIN       03/04/36 H,T,S       1,2,4         B216 GEORGIA STATE PRISON #2       10       460       818       700       19.0 30MIN       /       H       2         B217 GA. STATE PRISON WINT C       14       551       940       1016       10.0 BHRS       02/17/2E L,T,S       2         B218 CITY OF GLENNVILLE #3       12       560       800       750       6.0 24HRS       1// H       2         B220 GEORGIA FORRESTRY COML       28P001       0       5.0 7       /       H       1         B2221 CITY OF GLENNVILLE #1       30P001       0       344       714       0       0.0       05/12/66 T,S       4         B2221 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5 ?       /       /       H       1         B224 CITY OF LUMBER CITY #1       24P006       6       350       150       1.6 0.18RS       /       H       1         B225 CITY OF LUMBER CITY #1       240001       1053											Н	
B215 GEORGIA STATE PRISON #1       280002       8       500       810       550       20.0       30MIN       03/04/36       H,T,S       1,2,4         B216 GEORGIA STATE PRISON #2       10       460       818       700       19.0       30MIN       /       H       2         B217 GA. STATE PRISON WHI C       14       551       940       1016       10.0       8HRS       02/17/82 H,T,S       2         B218 CITY OF GLENNVILLE #3       12       560       800       750       6.0       24HRS       /       H       2         B210 GEORGIA FORRESTRY COMM.       280001       0       508       955       0       0.0       04/14/67       T,S       3         B222 CITY OF GLENNVILLE #1       30P001       0       344       714       0       0.0       05/12/66       7,S       4         B222 CITY OF MCRAE #1       220001       14       120       640       1200       5.0       7,H       1       1         B223 CITY OF NCRAE #3       1053       220003       12       235       545       750       6.0       18HRS       / / H       1         B224 CITY OF NCRAE #3       1053       220003       12       235       545<												
B216 GEORGIA STATE PRISON #2       10       460       818       700       19.0       30M1N       /       H       2         B217 GA. STATE PRISON UNIT C       14       551       940       1016       10.0       80Rs       02/17/82       H,T,S       2         B218 CITY OF GLENNVILLE #2       8       520       729       300       3.0       24HRS       1/2/22/86       H,T,S       3         B220 CEORGIA FORESTRY COMM.       280001       0       508       955       0       0.0       04/14/67       T,S       4         B221 CITY OF GLENNVILLE #1       30P001       0       344       714       0       0.0       05/12/66       T,S       4         B222 CITY OF LUMBER CITY #1       240006       6       350       450       132       5.5       ?       /       H       1         B224 CITY OF LUMBER CITY       10       353       220031       12       235       545       750       6.0       18Rs       /       H       1         B224 CITY OF LUMBER CITY       10       353       22003       12       235       545       750       6.0       18Rs       /       H       1         B225 CITY OF LUMBER CITY <td></td> <td>-</td> <td></td>											-	
B217 GA. STATE PRISON UNIT C       14       551       940       1016       10.0       8HRS       02/17/82       H, T, S       2         B218 CITY OF GLENNVILLE #2       8       520       729       300       3.0       24HRS       / / H       2         B219 CITY OF GLENNVILLE #3       12       560       800       750       6.0       24HRS       12/17/82       H, T, S       3         B220 GEORGIA FORRESTRY COMM.       28P001       0       568       955       0       0.0       05/12/66       T, S       4         B222 CITY OF GLENNVILLE #1       30P001       0       344       714       0       0.0       05/12/66       T, S       4         *** TELFAIR       8222 CITY OF MCRAE #1       220001       14       120       640       1200       5.0       7HRS       / H       1         B225 CITY OF NCRAE #3       1053       22003       12       235       545       750       6.0       18HRS       / / H       1         B226 CITY OF NCRAE #3       1053       220001       10       375       868       900       35.0       1HR       / / H       2         B226 CITY OF SCOTLAND       10       266       00 <td< td=""><td></td><td>280002</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td></td<>		280002	2								-	
B218 CITY OF GLENNVILLE #2       8       520       729       300       3.0       24RS       /       H       2         B219 CITY OF GLENNVILLE #3       12       560       800       750       6.0       24HRS       12/22/86       H, T,S       3         B220 GEORGIA FORRESTRY COMM.       280001       0       508       955       0       0.0       05/12/66       T,S       4         **       TELFAIR       30001       0       344       714       0       0.0       05/12/66       T,S       4         B222 CITY OF LUMBER CITY #1       240006       6       350       450       132       5.5       ?       /       H       1         B223 CITY OF NCRAE #1       220001       14       120       640       1200       5.0       7HRS       /       H       1         B225 CITY OF LUMBER CITY       10       375       868       900       35.0       18K       /       K       1       1         B226 CITY OF SCOTLAND       10       266       00       1700       65.0       7       03/25/77       H,T,S       3         B227 CITY OF THOMASVILLE #2       5       14F012       10       180       300<												
B219 CITY OF GLENNVILLE #3       12       560       800       750       6.0       24HRS       1/2/22/86 H,T,S       3         B220 GEORGIA FORRESTRY COMM.       28P001       0       508       955       0       0.0       0/14/67 T,S       4         B221 CITY OF GLENNVILLE #1       30P001       0       3/4       714       0       0.0       0/14/67 T,S       4         B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5       ?       /       H       1         B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5       ?       /       H       1         B225 CITY OF LUMBER CITY       10       375       868       900       35.0       18K       /       H       1         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0       120HRS       08/09/83 H,T,S       3         B227 CITY OF SCOLAND       10       266       600       1700       65.0       ?       0/2/25/77 H,T,S       4         B229 J.E.       D0BSON       22N001       0       270       415       0       0.0       0/2/05/66 T,S       4												
B220 GEORGIA FORRESTRY COMM.       28P001       0       508       955       0       0.0       04/14/67       T,S       4         B221 CITY OF GLENNVILLE #1       30P001       0       344       714       0       0.0       05/12/66       T,S       4         *** TELFAIR       B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5       ?       /       H       1         B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5       ?       /       H       1         B225 CITY OF LUMBER CITY       10       375       868       900       35.0       11R       /       H       2         B226 CITY OF LUMBER CITY       10       375       868       900       35.0       11R       /       H       2         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0       120RS       08/09/83       H,T,S       3         B227 CITY OF SCOTLAND       10       266       600       1700       65.0       0       0.0       03/06/63       T,S       4         B230 TIOMASVILLE ARMY AIR BASE 19       14F012       10       180												
B221 CITY OF GLENNVILLE #1       30P001       0       344       714       0       0.0       05/12/66 T,S       4         ** TELFAIR       B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5 ?       /       /       H       1         B223 CITY OF LUMBER CITY #1       220001       14       120       640       1200       5.0 7HRS       /       H       1         B224 CITY OF NCRAE #3       1053       220003       12       235       545       750       6.0 18HRS       /       H       1         B225 CITY OF LUMBER CITY       10       375       868       900       35.0 1HR       /       H       2         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0 120HRS 08/09/83 H,T,S       3         B227 CITY OF JACKSONVILLE #2       6       2420       343       170       0.0       0.3/06/63 T,S       4         B228 N.S. WHEELER       24P008       0       400       778       0       0.0       0.5/05/66 T,S       4         B230 THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6 1HR       01/06/64 H,T,S       1,4		290001	r						24885			
*** TELFAIR         B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5 ?       /       /       H       1         B222 CITY OF LUMBER CITY #1       22Q001       14       120       640       1200       5.0 7HRS       /       H       1         B224 CITY OF NCRAE #1       22Q001       12       235       545       750       6.0 18HRS       /       H       1         B225 CITY OF LUMBER CITY       10       375       868       900       35.0 1HR       /       H       2         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0 120HRS 08/09/83 H,T,S       3         B227 CITY OF SCOTLAND       10       266       600       1700       65.0 ?       03/25/77 H,T,S       3         B229 J.E. DOBSON       220001       0       270       415       0       0.0       05/05/66 T,S       4         B230 THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6 1HR       01/06/64 H,T,S       1,4         B233 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       1/212/1											•	
B222 CITY OF LUMBER CITY #1       24P006       6       350       450       132       5.5 ?       /       /       H       1         B223 CITY OF MCRAE #1       220001       14       120       640       1200       5.0 7HRS       /       H       1         B224 CITY OF MCRAE #3       1053       220003       12       235       545       750       6.0 18HRS       /       H       1         B225 CITY OF MCRAE #3       1053       220003       12       235       545       750       6.0 18HRS       /       H       1         B226 CITY OF MCRAE #3       1053       220003       12       235       545       750       6.0 18HRS       /       H       1         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0 120HRS 08/09/83 H,T,S       3         B227 CITY OF SCOTLAND       10       266       600       1700       65.0 ?       03/26/63 T,S       4         B228 N.S. WHEELER       24P008       0       400       778       0       0.0       05/05/66 T,S       4         B230 THOMASVILLE ARMY AIR BASE       19       14F012       10       180       300       425       5.6 1HR       01/		204001	L	0	244	/14	U	0.0		05/12/66	1,5	4
B223 CITY OF MCRAE #1       22001       14       120       640       1200       5.0       7HRS       /       H       1         B224 CITY OF NCRAE #3       1053       220003       12       235       545       750       6.0       18HRS       /       H       1         B225 CITY OF LUMBER CITY       10       375       868       900       35.0       1HR       /       H       2         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0       120HRS       08/09/83       H, T, S       3         B227 CITY OF SCOTLAND       10       266       600       1700       65.0       0.0       03/06/63       T, S       4         B229       J.E. DOBSON       22N001       0       270       415       0       0.0       05/05/66       T, S       4         B230 THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6       1HR       01/06/64       H, T, S       1,4         B231 CITY OF THOMASVILLE #3       186       14E011       16       112       305       960       1.3 </td 12/02/51       H, T, S       1,4         B233 CITY OF THOMASVILLE #4		24P004	ς	6	350	450	132	55	2	, ,	u	1
B224 CITY OF NCRAE #3       1053       22003       12       235       545       750       6.0       18Rs       /       H       1         B225 CITY OF LUMBER CITY       10       375       868       900       35.0       1HR       /       H       2         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0       120HRS       08/09/83       H, T, S       3         B227 CITY OF SCOTLAND       10       266       600       1700       65.0       ?       03/25/77       H, T, S       3         B228 N.S. WHEELER       24P008       0       400       778       0       0.0       03/06/63       T, S       4         B230 THOMASVILLE ARMY AIR BASE       19       14F012       10       180       300       425       5.6       1HR       01/06/64       H, T, S       1,4         B231 CITY OF THOMASVILLE #3       186       14E011       16       118       300       425       5.6       1HR       01/06/64       H, T, S       1,4         B233 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       / / H       1,2         B23												
B225 CITY OF LUMBER CITY       10       375       868       900       35.0       1RR       /       H       2         B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0       120HRS       08/09/83       H,T,S       3         B227 CITY OF SCOTLAND       10       266       600       1700       65.0       ?       03/25/77       H,T,S       3         B228 N.S. WHEELER       24P008       0       400       778       0       0.0       03/06/63       T,S       4         B229 J.E. DOBSON       22N001       0       270       415       0       0.0       05/05/66       T,S       4         B230 THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6       1HR       01/06/64       H,T,S       1,4         B231 CITY OF THOMASVILLE #3       186       14E011       16       112       305       960       1.3       ?       12/02/51       H,T,S       1,4         B233 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51       H,T,S       1,2         B235       OF THOMASVILLE #3												
B226 CITY OF JACKSONVILLE #2       6       242       343       170       15.0       120HRS       08/09/83       H,T,S       3         B227 CITY OF SCOTLAND       10       266       600       1700       65.0       ?       03/25/77       H,T,S       3         B228 N.S. WHEELER       24P008       0       400       778       0       0.0       03/06/63       T,S       4         B229 J.E. DOBSON       22N001       0       270       415       0       0.0       05/05/66       T,S       4         ** THOMAS       B230 THOMASVILLE #A       56       14E010       16       112       305       960       1.3 </td 12/02/51       H,T,S       1,4         B231 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51       H,T,S       1,4         B233 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51       H,T,S       1,4         B233 CITY OF THOMASVILLE #4       56       14E011       16       108       550       1000       2.0       3HRS       1/2/02/51       H,T,S       1,2/4 </td <td></td> <td>1035</td> <td>224003</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		1035	224003									
B227 CITY OF SCOTLAND       10       266       600       1700       65.0 ?       03/25/77 H,T,S       3         B228 N.S. WHEELER       24P008       0       400       778       0       0.0       03/06/63 T,S       4         B229 J.E. DOBSON       22N001       0       270       415       0       0.0       05/05/66 T,S       4         **       THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6 1HR       01/06/64 H,T,S       1,4         B230 THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6 1HR       01/06/64 H,T,S       1,4         B231 CITY OF THOMASVILLE #4       56       14E010       16       112       305       960       1.3 ?       12/02/51 H,T,S       2,4         B233 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0 3HRS       12/02/51 H,T,S       1,4         B235 CITY OF THOMASVILLE #6       401       14E013       20       157       400       3200       9.0 23HRS       /       H       1,2         B235 CITY OF MEIGS       3186       10       460       1004       160       80.0 2HRS       <												
B228 N.S. WHEELER       24P008       0       400       778       0       0.0       03/06/63 T,S       4         B229 J.E. DOBSON       22N001       0       270       415       0       0.0       05/05/66 T,S       4         ** THOMAS       B230 THOMASVILLE ARMY AIR BASE       19       14F012       10       180       300       425       5.6       1HR       01/06/64 H,T,S       1,4         B231 CITY OF THOMASVILLE #4       56       14E010       16       112       305       960       1.3       ?       12/02/51 H,T,S       2,4         B232 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51 H,T,S       1,4         B233 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51 H,T,S       1,4         B233 CITY OF THOMASVILLE #3       186       14E013       20       157       400       3200       9.0       23HRS       / / H       1,2         B234 WAVERLY MINERAL PROD. #1       495       13G003       8       605       905       280       85.0 ?       01/24/64 H,T,S       1,2,4         <												
B229 J.E. DOBSON       22N001       0       270       415       0       0.0       05/05/66 T,S       4         ** THOMAS         B230 THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6       1HR       01/06/64 H,T,S       1,4         B231 CITY OF THOMASVILLE #4       56       14E010       16       112       305       960       1.3       ?       12/02/51 H,T,S       2,4         B232 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51 H,T,S       1,4         B233 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51 H,T,S       1,4         B233 CITY OF THOMASVILLE #4       401       14E013       20       157       400       3200       9.0       23HRS       / / H       1,2,2         B234 WAVERLY MINERAL PROD. #1       495       13G003       8       605       905       280       85.0       ?       01/24/64 H,T,S       1,2,4         B235 O. NESMITH       769       13F003       4       168       261       30       4.0       1HR       / /	B228 N.S. WHEELER	24P008	3	0								
** THOMAS         B230 THOMASVILLE ARMY AIR BASE 19       14F012       10       180       300       425       5.6       1HR       01/06/64       H,T,S       1,4         B231 CITY OF THOMASVILLE #4       56       14E010       16       112       305       960       1.3       ?       12/02/51       H,T,S       2,4         B232 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51       H,T,S       1,4         B233 CITY OF THOMASVILLE #4       401       14E013       20       157       400       3200       9.0       23HRS       / / H       1,2         B234 WAVERLY MINERAL PROD. #1       495       13G003       8       605       905       280       85.0       ?       01/24/64       H,T,S       1,2,4         B235 O. NESMITH       769       13F003       4       168       261       30       4.0       1HR       / / H       1         B236 CITY OF MEIGS       3186       10       460       1004       160       80.0       2HRS       / / H       3         B237 CIRCLE C MHP #3       12       6       134       240       200       2.0	B229 J.E. DOBSON	22N001	1	0	270	415	0	0.0			•	
B231 CITY OF THOMASVILLE #4       56       14E010       16       112       305       960       1.3       ?       12/02/51       H,T,S       2,4         B232 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51       H,T,S       2,4         B233 CITY OF THOMASVILLE #6       401       14E013       20       157       400       3200       9.0       23HRS       /       H       1,2         B234 WAVERLY MINERAL PROD. #1       495       13G003       8       605       905       280       85.0       ?       01/24/64       H,T,S       1,2,4         B235 O. NESMITH       769       13F003       4       168       261       30       4.0       1HR       /       H       1         B236 CITY OF MEIGS       3186       10       460       1004       160       80.0       2HRS       /       H       3         B237 CIRCLE C MHP #3       6       134       240       200       2.0       6HRS       /       H       3         B238 HIDDEN ACRES S/D       6       134       240       200       2.0       6HRS       /       H       3	** THOMAS										•	
B232 CITY OF THOMASVILLE #3       186       14E011       16       108       550       1000       2.0       3HRS       12/02/51       H,T,S       1,4         B233 CITY OF THOMASVILLE #6       401       14E013       20       157       400       3200       9.0       23HRS       / / H       1,2         B234 WAVERLY MINERAL PROD. #1       495       13G003       8       605       905       280       85.0       ?       01/24/64       H,T,S       1,2,4         B235 O. NESMITH       769       13F003       4       168       261       30       4.0       1HR       / / H       1         B236 CITY OF MEIGS       3186       10       460       1004       160       80.0       2HRS       / / H       3         B237 CIRCLE C MHP #3       4       228       288       45       5.0       18HRS       10/15/84       H,T,S       3         B239 LAKE LILLIQUIN S/D       6       134       240       200       2.0       6HRS       / / H       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       09/19/83       H,T,S       3         B242 SUGARWOOD ESTATES #2       6	B230 THOMASVILLE ARMY AIR BASE	19	14F012	10	180	300	425	5.6	1HR	01/06/64	H,T,S	1,4
B233 CITY OF THOMASVILLE #6       401       14E013       20       157       400       3200       9.0       23HRS       /       H       1,2         B234 WAVERLY MINERAL PROD. #1       495       13G003       8       605       905       280       85.0 ?       01/24/64       H,T,S       1,2,4         B235 O. NESMITH       769       13F003       4       168       261       30       4.0       1HR       /       H       1         B236 CITY OF MEIGS       3186       10       460       1004       160       80.0       2HRS       /       H       3         B237 CIRCLE C MHP #3       4       228       288       45       5.0       18HRS       10/15/84       H,T,S       3         B238 HIDDEN ACRES S/D       6       134       240       200       2.0       6HRS       /       H       3         B239 LAKE LILLIQUIN S/D       10       196       294       500       1.0       12HRS       12/18/84       H,T,S       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       01/16/84       H,T,S       3         B242 SUGARWOOD ESTATES #2       6       181 </td <td></td> <td>56</td> <td>14E010</td> <td>16</td> <td>112</td> <td>305</td> <td>960</td> <td>1.3</td> <td>?</td> <td>12/02/51</td> <td>H,T,S</td> <td>2,4</td>		56	14E010	16	112	305	960	1.3	?	12/02/51	H,T,S	2,4
B234 WAVERLY MINERAL PROD. #1       495       13G003       8       605       905       280       85.0 ?       01/24/64       H,T,S       1,2,4         B235 O. NESMITH       769       13F003       4       168       261       30       4.0 1HR       / / H       1         B236 CITY OF MEIGS       3186       10       460       1004       160       80.0 2HRS       / / H       3         B237 CIRCLE C MHP #3       4       228       288       45       5.0 18HRS       10/15/84       H,T,S       3         B238 HIDDEN ACRES S/D       6       134       240       200       2.0 6HRS       / / H       3         B239 LAKE LILLIQUIN S/D       10       196       294       500       1.0 12HRS       12/18/84       H,T,S       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0 24HRS       01/16/84       H,T,S       3         B242 SUGARWOOD ESTATES #2       6       181       340       175       16.0 24HRS       09/19/83       H,T,S       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CI		186	14E011	16	108	550	1000	2.0	3HRS	12/02/51	H,T,S	1,4
B235 O. NESMITH       769       13F003       4       168       261       30       4.0       1HR       /       H       1         B236 CITY OF MEIGS       3186       10       460       1004       160       80.0       2HRS       /       H       3         B237 CIRCLE C MHP #3       4       228       288       45       5.0       18HRS       10/15/84       H,T,S       3         B238 HIDDEN ACRES S/D       6       134       240       200       2.0       6HRS       /       H       3         B239 LAKE LILLIQUIN S/D       10       196       294       500       1.0       12HRS       12/18/84       H,T,S       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       01/16/84       H,T,S       3         B241 RIVERWOOD ESTATES #2       6       181       340       175       16.0       24HRS       09/19/83       H,T,S       3         B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0.0       0		401	14E013	20	157	400	3200	9.0	23HRS	1 1	Н	1,2
B236 CITY OF MEIGS       3186       10       460       1004       160       80.0       2HRS       /       H       3         B237 CIRCLE C MHP #3       4       228       288       45       5.0       18HRS       10/15/84       H,T,S       3         B238 HIDDEN ACRES S/D       6       134       240       200       2.0       6HRS       /       H       3         B239 LAKE LILLIQUIN S/D       10       196       294       500       1.0       12HRS       12/18/84       H,T,S       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       01/16/84       H,T,S       3         B241 RIVERWOOD ESTATES #2       6       181       340       175       16.0       24HRS       09/19/83       H,T,S       3         B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64				8	605	905	280	85.0	?	01/24/64	H,T,S	1,2,4
B237 CIRCLE C MHP #3       4       228       288       45       5.0       18HRS       10/15/84       H,T,S       3         B238 HIDDEN ACRES S/D       6       134       240       200       2.0       6HRS       /       H       3         B239 LAKE LILLIQUIN S/D       10       196       294       500       1.0       12HRS       12/18/84       H,T,S       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       01/16/84       H,T,S       3         B241 RIVERWOOD ESTATES #2       6       181       340       175       16.0       24HRS       09/19/83       H,T,S       3         B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64       T,S       4         B245 D.O. MIMMS       15E002       0       155       210       0       0.0       01/07/64       T			13F003	4		261	30	4.0	1HR	1 1	Н	1
B238 HIDDEN ACRES S/D       6       134       240       200       2.0       6HRS       /       H       3         B239 LAKE LILLIQUIN S/D       10       196       294       500       1.0       12HRS       12/18/84       H,T,S       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       01/16/84       H,T,S       3         B241 RIVERWOOD ESTATES #2       6       181       340       175       16.0       24HRS       09/19/83       H,T,S       3         B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64       T,S       4         B245 D.O. MIMMS       15E002       0       155       210       0       0.0       01/07/64       T,S       4		3186						80.0	2HRS	/ /	H	3
B239 LAKE LILLIQUIN S/D       10       196       294       500       1.0       12HRS       12/18/84       H,T,S       3         B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       01/16/84       H,T,S       3         B241 RIVERWOOD ESTATES #2       6       181       340       175       16.0       24HRS       09/19/83       H,T,S       3         B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64       T,S       4         B245 D.O. MIMMS       15E002       0       155       210       0       0.0       01/07/64       T,S       4										10/15/84	H,T,S	3
B240 LAKE RIVERSIDE S/D       6       226       360       150       15.0       24HRS       01/16/84       H,T,S       3         B241 RIVERWOOD ESTATES #2       6       181       340       175       16.0       24HRS       09/19/83       H,T,S       3         B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64       T,S       4         B245 D.O. MIMMS       15E002       0       155       210       0       0.0       01/07/64       T,S       4												
B241 RIVERWOOD ESTATES #2       6       181       340       175       16.0       24HRS       09/19/83       H, T, S       3         B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T, S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64       T, S       4         B245 D.O. MIMMS       15E002       0       155       210       0       0.0       01/07/64       T, S       4												
B242 SUGARWOOD ESTATES MHP       4       261       300       50       5.0       18HRS       /       H       3         B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64       T,S       4         B245 D.O. MIMMS       15E002       0       155       210       0       0.0       01/07/64       T,S       4												
B243 CITY OF THOMASVILLE #5       14E012       0       230       400       0       0.0       08/01/61       T,S       4         B244 CITY OF COOLIDGE       15G011       0       237       383       0       0.0       01/06/64       T,S       4         B245 D.O. MIMMS       15E002       0       155       210       0       0.0       01/07/64       T,S       4											• •	
B244 CITY OF COOLIDGE         15G011         0         237         383         0         0.0         01/06/64         T,S         4           B245 D.O. MIMMS         15E002         0         155         210         0         0.0         01/07/64         T,S         4		4/-045							18HRS			
B245 D.O. MIMMS 15E002 0 155 210 0 0.0 01/07/64 T,S 4											,	
		152003	,	U	120	200	U	0.0		01/07/64	1,5	4

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### APPENDIX B: WELLS USED IN HYDRAULIC PARAMETER AND INORGANIC CHEMISTRY PLATES (CONTINUED)

MAP OWNER/WELL NAME NUM- BER	OTHER ID# GGS, USGS GRID	ETER	LENGTH	DEPTH		DOWN	OF	SAMPLE DATE	PLATES	DATA SOURCE
BER	USGS GRID	(IN)	(1)	(FI)	(GPM)	(())	1251			
B247 CITY OF PAVO ** TIFT	16F004	0	104	305	0	0.0		01/06/64	T,S	4
B248 CITY OF TIFTON #6	3125	24	280	652	2360	5.0	12HRS	11	н	1
B249 CITY OF TIFTON #2	17K062	12	275	501	1000	5.5	30M I N	04/28/58	H,T,S	1,4
B250 CITY OF TIFTON #5		20	360	610	1500	13.4	7HRS	/ /	н	1
B251 ABAC #1		10	263	500	700	47.0	?	12/22/78	H,T,S	3
B252 ABAC #2		10	260	514	800	10.0	10HRS	/ /	Н	2
B253 CITY OF TIFTON #4		20	398	612	1500	63.0		/ /	н	2
B254 WENDELL HOBBS S/D #1		4	147	220	70	5.0		01/04/79	H,T,S	3
B255 NORTHGATE LAKE S/D #2		0	253	340	50	20.0		/ /	Н	3
B256 PEBBLE BROOK MEADOWS #1		6	201	400	150	5.0	?	03/20/78		3
B257 PINE HILL MHP		4	407	600	20		24HRS	10/19/82	H,T,S	3
B258 SPRING HILL PROPERTIES		6	192	320		10.0		/ /	Н	3
B259 CITY OF TIFTON #7		14	350	750	2335		24HRS	11/24/86	H,T,S	3
B260 TOWN & COUNTRY MHP		6	190	300	20		24HRS	/ /	н	3
B261 WHISPERING PINES ESTATES		4	400	480	150	20.0	24HRS	/ /	H	3
B262 CITY OF TIFTON	18K001	0	390	610	0	0.0		06/19/70	T,S	4
** TOOMBS										
B263 VIDALIA AIR FIELD	85	10	470	864	235	8.0		11	Н	1
B264 CITY OF VIDALIA #1	650	16	430	808		18.0		11	Н	1,2
B265 CITY OF VIDALIA	26R003	16	442	800	1200		24HRS	1 1	H	1
B266 CITY OF VIDALIA #2	26R001	8	720	1000	200		6HRS	08/04/61		1,4
B267 CITY OF LYONS #1		17	500	698		33.0		08/15/80		2
B268 CITY OF LYONS #2		19	487	764		41.0		06/06/68	• •	2
B269 CITY OF VIDALIA #3		16	442	761		28.0		08/22/73		2
B270 MCNATT FALLS S/D #1	200001	4	475	605		35.0	?	/ /	H T O	3
B271 T.C. TALLEY	28R001	0	511	714	0	0.0		04/14/67		4
B272 TOOMBS CO. BD. OF ED. ** WHEELER	270001	0	654	885	0	0.0		03/12/63	1,5	4
B273 LITTLE OCMULGEE ST. PK.	1045	10	165	266	500	20.0	24HRS	1 1	н	1
B274 CITY OF ALAMO #2	23R001	0	352	600	800	75.0	24HRS	11	н	1
B275 LITTLE OCMULGEE ST. PK.	220004	10	194	248	500	18.3	12HRS	1 1	Н	1
B276 F. JOYCE	24P001	0	400	610	0	0.0		05/06/66	T,S	4
B277 T.B. CLARK	22R001	0	220	253	0	0.0		03/07/63	T,S	4
B278 CITY OF GLENWOOD	24R001	0	300	380	0	0.0		01/05/60	τ,s	4
** WORTH										
B279 C.E. BUCK FARM #1	420 14L007	6	73	180	146	7.0	8HR S	1 1	н	1
B280 CITY OF SYLVESTER #3	15L021	18	146	536	1018	131.0	6HRS	02/05/72	H,T,S	1
B281 CITY OF WARWICK #2		10	200	350	1100	5.0	36HRS	06/15/82	H,T,S	3
B282 WORTHY MANOR S/D		10	60	185	465	14.0	8HRS	04/07/72	H,T,S	3
B283 L.L. LEVERETTE	14M002	0	206	240	0	0.0		05/10/65	•	4
B284 G.W. STROM	14M001	0	160	215	0	0.0		05/10/65	T,S	4
B285 W.J. PATE	14L002	0	260	430	0	0.0		05/10/65	T,S	4
B286 CITY OF SUMNER	16L001	0	160	410	0	0.0		05/10/65	T,S	4
B287 H.APPERSON	14K003	0	195	370	0	0.0		05/10/65	T,S	4

### APPENDIX B: WELLS USED IN HYDRAULIC PARAMETER AND INORGANIC CHEMISTRY PLATES (CONTINUED)

MAP OWNER/WELL NAME	OTHER ID#	DIAM-	CASING	TOTAL	DIS-	DRAW	LENGTH	SAMPLE	PLATES	DATA
NUM-	GGS,	ETER	LENGTH	DEPTH	CHARGE	DOWN	OF	DATE		SOURCE
BER	USGS GRID	(IN)	(FT)	(FT)	(GPM)	(FT)	TEST			
B288 I.J. WHITE	15K003	0	206	240	0	0.0		05/10/65	те	4
BLOO I.J. WHITE	12K002	U	200	240	0	0.0		05/10/05	1,5	4
B289 F. BROWN	14K005	0	240	280	0	0.0		05/04/66	T,S	4
B290 CITY OF WARWICK	14N001	0	160	325	0	0.0		04/20/67	T,S	4

PLATES CODES:

- H Hydraulic Parameters, Plates 7-10
- T Total Dissolved Solids, Plate 12
- S Sulfates, Plate 13

DATA SOURCE CODES:

- 1 Georgia Geologic Survey files
- 2 Water Resources Management Branch files
- 3 Ground-Water Program files
- 4 Grantham and Stokes (1976)
- 5 Sever (1969)

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## APPENDIX C: WELLS USED IN BARIUM AND GROSS ALPHA PLATES

	MAP SUPPLY NAME NUM.		L OTHER 1. ID #	BARIUM SAMPLE DATE	BARIUM CONC. (ug/l)	SAMPLE	GROSS ALPHA ACT. (piC/l)	RA226 ACTIV- ITY (piC/l)	RA228 ACTIV- ITY (piC/l)
,	** APPLING								
	COO1 ALTAMAHA MHP		B006	-		04/21/83	<2		
	COO2 BASS S/D EAST			05/12/82					
	COO3 CITY OF BAXLEY			05/12/82		05/12/82	2+2		
	COO4 COOPER TRAVEL TRAILER PK			11/15/78			0.0		
	COO5 GA BAPTIST CHILDRENS HOM	E	B007			07/26/83	2+2		
	COOG THE VILLAGE MHP			07/21/78		/ /	-2		
	COO7 TOWN OF SURRENCY			08/20/81	<200.	09/08/81	<2		
	** ATKINSON			0/ 107 192	~200	04/07/82	<4		
	COOS CITY OF PEARSON			• •		04/07/82		4.4	<1.0
	COO9 CITY OF WILLACOOCHEE ** BACON			04/07/82	×200.	04/07/02	4, 2	<b>-</b>	\$1.0
	CO10 BACON APPERAL			06/12/80	<200.	11			
	CO11 CITY OF ALMA			03/31/82		05/10/84	2+-2		
	CO12 HIGHLAND PARK S/D			09/17/81	<200.	1 1			
(	CO13 LEE MHP			09/17/81	<200.	11			
,	** BEN HILL								
(	CO14 CITY OF FITZGERALD a	A	B022	1 1	1300.	1 1			
(	CO15 CITY OF FITZGERALD a	в		/ /	2300.	1 1			
(	CO16 CITY OF FITZGERALD a	C	B016	/ /	2000.	1 1			
(	C017 CITY OF FITZGERALD a	D	в017	/ /	1600.	/ /			
(	CO18 CITY OF FITZGERALD a	Е	B018	/ /	2100.	1 1			
(	CO19 CITY OF FITZGERALD	o F	B019	/ /	200.	/ /			
(	CO20 CITY OF FITZGERALD E	G	B020	/ /	100.	/ /			
(	CO21 CITY OF FITZGERALD			/ /		12/31/80	3+-2	1.2	
	CO22 FOWLER (domestic) c	:		/ /	250.	/ /			
	CO23 GLADDEN (domestic) c	:		/ /	350.	/ /			
	CO24 GAINES (domestic) c	:		/ /	300.				
	CO25 MERRITT (domestic) c	:		/ /	350.				
	CO26 NETTLES (domestic) c			/ /	350.				
	CO27 MCDUFFIE (domestic) c			//	300.	11			
		:		//	250.				
	CO29 GRANTHAM (domestic) c			/ /		/ /			
		:				1 1			
	CO31 ANDERSON (domestic) c ** BERRIEN			/ /	250.	/ /			
	CO32 CITY OF ALAPAHA			08/28/79	230	1 1			
	CO32 CITY OF ALAPAHA	1		/ /	200.	/ / 08/02/83	7+-2	69	<1.0
	CO34 CITY OF ALAPAHA	2		1 1		08/02/83			<1.0
	CO35 CITY OF ALAPAHA	т1		/ /		06/10/77			<1.0
	CO36 BENNETTS MHP	2			<200	/ /			
	CO37 CITY OF ENIGMA	1				02/19/79	6+-2	6.2	0.2
	CO38 CITY OF ENIGMA	2	B028	/ /		12/27/83			
	CO39 CITY OF NASHVILLE	-				05/29/84			
	CO40 SOUTHWOOD MHP					/ /	-		
	CO41 CITY OF RAY CITY					02/19/79	5+-2	1.2	
							-		

	DATE (ug/l	) DATE	ALPHA ACT. (piC/l)	ACTIV- ITY (piC/l)
CO42 CITY OF RAY CITY 1 BO31 CO43 WALKER TRAILER PARK 0 ** BROOKS	/ / )7/24/79 <200	02/02/84 • / /	<3	
CO44 CITY OF BARWICK 0	07/29/81 <200	. / /		
CO45 CITY OF QUITMAN 1	1/20/79 <200	. 02/24/82	<3	
CO46 JA MAR S/D 1	12/18/78 <200	. / /		
CO47 CITY OF MORVEN 0	08/03/81 <200	. / /		
CO48 SHADY ACRES S/D 0	08/04/81 <200	. / /		
CO49 TROUPVILLE MOBILE ESTATES 0	08/03/81 <200	. / /		
** BULLOCH				
	02/08/82 <200			
	05/21/80 <200			
	03/24/82 <200		<3	
	12/10/81 <200			
	2/08/82 <200		<4	
	01/05/78 <200			
	10/19/78 <200	• •		
	12/09/81 <200			
	06/22/78 <200			
	12/09/81 <200			
	)8/26/81 <200 )7/15/70 <200			
	)3/15/79 <200			
-	12/10/81 <200 06/15/82 <200			
	09/13/82 <200 09/17/81 <200			
	)8/27/81 <200			
	01/19/82 <200		<4	
	01/19/82 <200 01/19/82 <200			
· · · ·	01/19/82 <200			
•	01/03/79 <200			
	10/20/81 <200			
	10/19/78 <200			
	06/15/82 <200			
	10/05/78 <200			
	06/15/82 <200			
	3/23/82 <200			
	08/26/81 <200			
	09/17/81 <200			
		. 05/12/82	<4	
CO79 NEWTON'S MH VILLAGE 0	02/08/82 <200	. / /		
CO80 REGISTER WATER ASSN. 0	09/16/81 <200	. / /		
CO81 RIDGEVIEW APARTMENTS 0	8/26/81 <200	. / /		
CO82 TANKERSLEY S/D 0	06/15/82 <200	. / /		
CO83 BARN MHP O	08/26/81 <200	. / /		
CO84 THOMAS TRAILER PARK 0	2/07/79 <200	. / /		
CO85 WESTCHESTER S/D 0	07/27/78 <200	. / /		

MAP SUPPLY NAME NUM.			BARIUM SAMPLE DATE	BARIUM CONC. (ug/l)	RAD. SAMPLE DATE	GROSS ALPHA ACT. (pīC/l)	RA226 ACTIV- ITY (piC/l)	RA228 ACTIV- ITY (pīC/l)
CO86 WINDFIELD S/D			06/15/82	<200				
CO87 WOODLAND MOBIL	E ESTATES		04/16/79					
CO88 YOUNGBLOOD MHF			12/10/81					
CO89 ZETTEROWER MHF			12/09/81		11			
** CANDLER			12,07,01	·200.	, ,			
CO90 CITY OF METTER	2		03/22/78	<200.	03/22/78	3+-2		
CO91 CITY OF PULASK			08/27/81					
** COFFEE								
CO92 BITTAKER TRAIL	.ER PARK		02/16/82	<200.	/ /			
CO93 CITY OF AMBROS	ε	в060	12/20/77	280.	05/10/84	<3		
CO94 CITY OF BROXTO	N		03/30/82	<200.	03/30/82	7+-2	5.4	<1.0
CO95 CITY OF DOUGLA	s		02/16/82	<200.	02/15/82	2+-2		
CO96 CITY OF NICHOL	LS		03/30/82	<200.	01/01/00			
CO97 CITY OF NICHOL	.LS 2		1 1		12/07/83	3+-2	2.4	
CO98 EVANS TRAILER	PARK 2		11/18/81	<200.	1 1			
CO99 GENERAL COFFEE	STATE PK.		04/10/79	<200.	/ /			
C100 HARPER'S MHP			09/27/78	<200.	/ /			
C101 HEAD S/D			09/29/78	<200.	/ /			
C102 HILLSIDE TRAIL	.ER PARK		03/30/82	<200.	/ /			
C103 LITTLE ACRES 1	AILER PARK		04/09/79	<200.	/ /			
C104 NORTH SIDE MHF			03/07/78		/ /			
C105 PARKVIEW MOBIL		B064	10/08/81		07/22/82	4+-3	2.6	
C106 SOUTHERN WATER			01/04/82		/ /			
C107 TOWN & COUNTRY	' TRAILER PK		09/14/78	<200.	/ /			
** COLQUITT			00 /07 /04					
C108 BEAR CREEK S/D			08/03/81		/ /	0.0		
C109 CITY OF BERLIN		0074	05/26/78					
C110 COLQUITT CO. M	IEM. HUSP.		07/21/78					
C111 CRESTWOOD S/D C112 CITY OF DOERUN	1	B070	01/01/00 08/03/81		12/27/81			
C113 CITY OF ELLENT	-		07/23/81					
C114 CITY OF FUNSTO			05/26/78					
C115 HARTSFIELD COM			02/04/82				4.9	<1.0
C116 CITY OF MOULTR			12/22/81				4.7	
C117 CITY OF NORMAN			07/23/81					
C118 CLUBVIEW S/D			08/03/81			-		
C119 COUNTRY CIRCLE	S/D		07/06/79					
C120 DEMOTT S/D	, -		09/14/81		1 1			
C121 GREEN ACRES ES	TATES		01/22/79		1 1			
C122 INDIAN LAKES S			09/14/81	<200.	1 1			
C123 PINEY GROVE S			10/24/79		1 1			
C124 RIVERSIDE MANU			08/22/78		1 1			
C125 RIVERWOOD SD			10/27/81		1 1			
C126 RUFUS MHP			11/14/78	<200.	1 1			
C127 SANDS MHP			05/02/79	<200.	1 1			
C128 SHADY GROVE S	′D		10/27/81	<200.	1 1			

MAP SUPPLY NAME NUM.			BARIUM SAMPLE DATE	BARIUM CONC. (ug/l)	SAMPLE	GROSS ALPHA ACT. (pic/l)	RA226 ACTIV- ITY (piC/l)	RA228 ACTIV- ITY (pīC/l)
C129 SPENCEFIELD AIRPORT			01/21/82	<200.	/ /			
C130 SPENCETON S/D 1			08/20/81	<200.	11			
C131 SPENCETON S/D 2			08/20/81	<200.	11			
C132 TALOKAS CIRCLE S/D			08/20/81	<200.	11			
C133 YANCEY TRAILER RENTALS			03/16/79	<200.	11			
** COOK								
C134 CITY OF ADEL			02/19/81	<200.	03/03/83	<2		
C135 CITY OF CECIL			02/19/81	<200.	09/13/82	<4		
C136 CITY OF LENOX			04/14/81	<200.	02/01/83	<2		
C137 CITY OF SPARKS			08/18/81	<200.	09/08/83	<4		
C138 GIDDENS TRAILER PARK			08/18/81	<200.	1 1			
C139 TILLMANS TRAILER PARK			06/28/79	<200.	1 1			
** DECATUR								
C140 CITY OF ATTAPULGUS	1		/ /		08/09/83	8+-2	4.6	<1.0
C141 CITY OF ATTAPULGUS	2		1 1		06/07/84	14+-2	11.2	<1.0
C142 CITY OF ATTAPULGUS			02/10/81	250.	1 1			
C143 CITY OF BAINBRIDGE			05/14/80	<200.	10/19/82	<3		
C144 CITY OF CLIMAX			04/15/82	<200.	04/17/84	<1		
C145 DECATUR CO. CORR. INST.			12/05/78	<200.	11			
C146 DECATUR CO. IND. PARK			05/21/79	<200.	1 1			
C147 DOLLAR COMMUNITY APTS.			06/21/79	<200.	/ /			
C148 ENGELHARDS M&C			06/21/79	<200.	/ /			
C149 FLINTWOOD S/D			04/03/79					
C150 JAMES TRAILER PARK			02/22/79		/ /			
C151 MEADOWBROOK S/D			11/19/79		/ /			
C152 REDBARN NHP		B129	•		08/19/82	<3		
C153 ROBINWOOD ESTATES			08/14/80		/ /			
C154 SANDY ACRES MHP			08/05/81		/ /	_		
C155 TOWN OF BRINSON ** FFFINGHAM			09/10/81	<200.	09/20/83	<2		
			07 (40 (00					
C156 BLOOMINGDALE S/D			03/18/82	<200.	/ /	_		
C157 CITY OF GUYTON			01/13/82			<3		
C158 CITY OF RINCON					09/20/78	1+-2		
C159 CITY OF SPRINGFIELD C160 GLEN LEE TRAILER PARK					01/04/83	<3		
C160 GLEN LEE TRAILER PARK		n1/0	01/13/82		/ /	.2		
C162 HAGIN WATER WORKS		B149	03/11/82		03/19/82	<2		
C163 LAKE CHERIE MHP			04/19/79					
C164 LAKESIDE FARMS S/D			10/16/79 05/06/82					
C165 MELDRIM LAKES								
C166 REDGATE MHP			09/18/78					
C167 WESTWOOD HEIGHTS S/D			04/20/82					
** EVANS			U) UL	·200.	, ,			
C168 CITY OF BELLVILLE			04/15/82	<200	04/15/82	<3		
C169 CITY OF CLAXTON			05/05/82		05/05/82	<2		
C170 CITY OF DAISY			04/15/82		03/23/84	<2		
· · · · · · · · · · · · · · · · · · ·			., ., 0/02	-L00.	55, 25, 04			

MAP SUPPLY NAME NUM.			BARIUM SAMPLE DATE	CONC.	RAD. SAMPLE DATE	ALPHA ACT.	RA226 ACTIV- ITY (piC/l)	ITY
C171 CITY OF HAGAN C172 EVANS MEMORIAL HOSPITAL ** GRADY			05/05/82 04/15/82		05/05/82 / /	<2		
C173 CITY OF CAIRO			09/14/78	<200.	10/26/81	3+-2	2.3	
C174 CITY OF WHIGHAM		B161	06/28/82	200.	04/10/84	2+-2		
C175 DOLLAR MHP			12/03/80	270.	01/31/83	<2		
C176 GAY'S MHP			11/14/78	<200.	11			
C177 MAXWELL COMMUNITY			02/14/79	<200.	1 1			
C178 PINE TERRACE ESTATES			08/25/81	<200.	1 1			
C179 RENO WATER SYSTEM					04/10/84	1+-1		
C180 SOUTHERN TERRACE MHP			09/24/81	<200.	11			
C181 WALDEN TRAILER PARK #1 ** IRWIN			04/09/81	<200.	1 1			
C182 CITY OF MYSTIC			01/11/82	<200.	01/31/84	<2		
C183 CITY OF OCILLA			09/11/80	<200.	12/07/82	<2		
C184 FOREST ESTATE S/D			10/30/78	485.	11			
C185 IRWINVILLE WATER WORKS CO			01/11/82	<200.	11			
C186 KITCHENS MHP			02/06/79	310.	1 1			
C187 SIZLAND TRAILER PARK ** JEFF DAVIS			08/27/79	340.	/ /			
C188 B & B TRAILER PARK			02/08/82	<200.	1 1			
C189 CITY OF DENTON		в172	04/12/78	<200.	08/30/82	<4		
C190 CITY OF HAZELHURST			04/06/78	300.	02/09/83	4+-2	3.9	<1.0
C191 EDGEWOOD TRAILER PARK			11/19/81	223.	1 1			
C192 DENDERSON TRAILER PARK ** MITCHELL			02/08/82	<200.	/ /			
C193 BOWEN MOBILE ESTATES		в179	04/24/79	<200.	11/30/82	<3		
C194 CITY OF BACONTON			02/25/82	<200.	07/27/83	<3		
C195 CITY OF CAMILLA			11/19/79	<200.	09/28/82	<3		
C196 CITY OF PELHAM			12/16/80	<200.	11/16/82	<4		
C197 CITY OF SALE CITY					09/28/82			
C198 HINSONTON WATER ASSN.		в180	06/22/82	285.	06/12/84	2+-2		
C199 SHADY GROVE TRAILER PARK			03/29/82	<200.	1 1			
C200 WACO COMMUNITY ** MONTGOMERY			10/23/80	<200.	/ /			
C201 ALLMONDS TRAILER PARK			01/18/79	<200.	1 1			
C202 CHARLOTTE WATER ASSN.			04/02/82	220.	1 1			
C203 CITY OF AILEY		B191	02/02/82	<200.	01/04/78	21+-3	20.7	0.2
C204 CITY OF AILEY (MODIFIED)		в191	11		09/22/82	<3		
C205 CITY OF ALSTON		в192	02/24/82	<200.	02/24/82	<3		
C206 CITY OF MOUNT VERNON	1	в190	05/24/78				25.5	0.5
C207 CITY OF MOUNT VERNON	2		09/15/81	<200.	08/05/82	<3		
C208 CITY OF TARRYTOWN	1		03/21/78	400.	03/21/78	30+-5	51.0	1.2
C209 CITY OF TARRYTOWN	2	в194	01/06/82	410.	03/15/82	2+~2		
C210 CITY OF UVALDA					04/02/82			
C211 MONTGOMERY CO CORR INST			05/10/82	<200.	10/25/83	<3		

MAP SUPPLY NAME NUM.				CONC.	RAD. SAMPLE DATE	ACT.	ACTIV-	ITY
C212 WILDWOOD MHP ** SCREVEN		B195	/ /		08/05/82	5+-2	4.8	<1.0
C213 BRINSONS TRAILER PARK			12/20/78	~200	, ,			
C214 CITY OF HILTONIA					09/30/82	<4		
C215 CITY OF NEWINGTON					08/25/81			
C216 CITY OF OLIVER					08/25/81			
C217 CITY OF SYLVANIA					11/18/82			
C218 GREEN ACRES MHP			12/21/78		1 1	_		
C219 INDIAN BRANCH TRAILER PK.			12/20/78		11			
C220 INDIGO MOBILE ESTATES		B201	12/21/78	<200.	07/27/83	<2		
C221 PO-ROBIN MHP			12/21/78	<200.	11			
** TATTNALL								
C222 BEARDS CREEK TRAILER PARK			01/06/82	<200.	11			
C223 CITY OF COBBTOWN			01/06/82	<200.	01/06/82	<3		
C224 CITY OF COLLINS			09/18/78	<200.	05/17/82	<4		
C225 CITY OF GLENNVILLE			11/09/77	<200.	09/14/82	<2		
C226 CITY OF MANASSAS		B213	01/06/82					
C227 CITY OF REIDSVILLE		•			09/14/83			
C228 GEORGIA STATE PRISON			06/16/82	<200.	06/16/82	<2		
** TELFAIR								
C229 CITY OF HELENA					01/26/84			
C230 CITY OF JACKSONVILLE	2	n n n n n n		<200.	01/12/84			
C231 CITY OF JACKSONVILLE	2	B226	/ /	770	04/26/83		4.5	<1.0
C232 CITY OF LUMBER CITY C233 CITY OF LUMBER CITY	1	0000	12/01/81		12/02/81			
C234 CITY OF MCRAE	1	DCCC	01/01/00 01/08/82		12/01/83 03/08/84			
C235 CITY OF MILAN					08/26/82			
C236 CITY OF SCOTLAND					08/23/83			
** THOMAS			12/00/01	243.	00/20/00	<b>`</b>		
C237 CINDY LANE S/D			02/12/81	<200.	11			
C238 CIRCLE C MOBILE ESTATES					04/19/84	3+-1		
C239 CITY OF BOSTON					01/25/83	<2		
C240 CITY OF COOLIDGE			07/18/79		11/09/82			
C241 CITY OF MEIGS			12/18/80		03/08/79			
C242 CITY OF OCHLOCKNEE			06/23/82	<200.	06/05/84	<3		
C243 CITY OF PAVO			07/18/79	<200.	08/30/82	<3		
C244 CITY OF THOMASVILLE			03/25/82		09/29/83			
C245 CRABAPPLE HILLS			02/12/81	<200.	11			
C246 CRESTWOOD MHP 1			09/09/81	<200.	11			
C247 CRESTWOODMHP 2			09/09/81	<200.	11			
C248 FOREST PARK MHP			01/18/79	<200.	1 1			
C249 FOXCROFT S/D			01/18/79	<200.	1 1			
C250 LITTLE ACRES ESTATES			09/17/81	<200.	/ /			
C251 OAKLAND S/D			03/23/82	<200.	/ /			
C252 PEBBLE HILL PLANTATION			05/10/79		1 1			
C253 PINE LAKE ESTATES MHP			09/17/81	<200.	/ /			

	IAP SUPPLY NAME UM.			SAMPLE	CONC.	RAD. SAMPLE DATE	ALPHA ACT.		ACTIV- ITY
С	254 ROSE CITY ESTATES 255 SHADY REST MHP 256 SUGARWOOD ESTATES MHP		B242	12/23/80 03/23/82 05/02/82	<200.	11	2+-1		
С	257 SUNNY BELLE ACRES WA ASSN			04/02/81	<200.	11			
С	258 THOMAS CO. CORR. INST.			09/23/80	<200.	11			
С	259 TINY ACRES MHP			03/09/82	<200.	11			
С	260 TOWN & COUNTRY ESTATES			10/09/80	<200.	1 1			
С	261 TWIN ACRES S/D			11/19/81	<200.	/ /			
	* TIFT								
	262 ABRAHAM BALDWIN AG. COL.			12/16/80		09/02/82	3+-2	2.3	
-	263 BAILEYS TRAILER PARK			02/15/79					
	264 BAR W MHP			06/23/81					
	265 BOWEN-WRIGHT S/D			10/16/78					
-	266 CHURCH OF GOD CAMPGROUND			09/29/81			-7		
	267 CITY OF OMEGA					05/22/84	<0		
	268 CITY OF TIFTON 269 CITY OF TIFTON	4	в253	03/09/82		/ / 02/10/83	7+-2	4.8	<1.0
	270 CITY OF TIFTON	5		1 1		02/10/83			
	271 CITY OF TIFTON		B259			11/26/86			
	272 CITY OF TYTY	•	0200	• •		10/07/82			
	273 COUNTRY HAVEN TRAILER PK.			02/02/82		11			
	274 FERRY LAKE TRAILER PARK			08/24/81		11			
С	275 FOREST LAKE ESTATES			02/15/79					
C	276 GREEN ACRES MHP			04/16/79		11			
C	277 HIDE A WAY TRAILER PARK			09/26/79	<200.	1.1			
С	278 HOBBS S/D			11/21/78	<200.	1 1			
C	279 KEENS TRAILER PARK 1			01/08/81	<200.	11			
C	280 OAK RIDGE TRAILER PARK			09/10/80		1 1			
C	281 PEBBLE BROOK MEADOWS S/D					06/21/82	<3		
C	282 PINE HILL MHP		B257	06/28/82	215.	03/29/84	20+-2	25.9	<1.0
	283 PITTS TRAILER PARK			12/08/80		/ /			
	284 SEABROOK TRAILER PARK			02/15/79		11			
	285 SELPH TRAILER PARK			06/01/82		//			
	286 SPRING HILL PROPERTIES		в258	10/13/81					
	287 TIFT AREA MHP		в260	06/28/79 06/28/82		/ / 05/31/84	<2		
	288 TOWN & COUNTRY ESTATES 289 VEAZEY TRAILER PARK		6200	05/06/82		/ /	~2		
	290 WILSONS MHP			10/16/78		/ /			
	291 WHISPERING PINES MHP		B261	06/14/82		02/21/84	11+-2	8.6	<1.0
	292 YANCEY TRAILER PARK		5201	02/09/82		/ /	11. 2	0.0	
	* TOOMBS			02,0,,02	2001	, ,			
	293 CATO'S TRAILER PARK			11/04/81	<200.	1 1			
	294 CENTER HILL MHP			02/08/82		1 1			
	295 CITY OF LYONS					12/08/82	2+-2		
c	296 CITY OF SANTA CLAUS					02/08/82	<4		
C	297 CITY OF VIDALIA			02/09/82	<200.	02/08/82	<4		

MAP SUPPLY NAME NUM.			BARIUM SAMPLE DATE		SAMPLE	GROSS ALPHA ACT. (piC/l)	RA226 ACTIV- ITY (piC/l)	ITY
C298 M & T WATER WORKS C299 MCNATT FALLS S/D		B270		200.	03/01/82	4+-2	3.3	<1.0
C300 PETROSS WATER SYSTEM C301 SHADY ACRES TRAILER PARK ** WHEELER			11/04/81 11/02/78					
C302 CITY OF ALAMO	1		11/07/79	500.	01/24/78	188+-	196	0.4
C303 CITY OF ALAMO	2	в274	10/21/81	<200.	04/24/80	11+-2	4.8	<1.0
C304 CITY OF ALAMO	3		11		09/01/87	<2		
C305 CITY OF GLENWOOD		в278	11/08/77	285.	12/15/81	3+-2	2.1	
** WORTH								
C306 CITY OF POULAN			04/21/82	250.	05/01/84	3+-2		
C307 CITY OF SUMNER			06/15/81	215.	12/09/82	2+-2		
C308 CITY OF SYLVESTER			06/10/81	<200.	11/18/82	2+-2		
C309 CITY OF WARWICK		B281	05/25/82	<200.	04/24/84	<3		
C310 CONGER MHP			06/10/81	<200.	11			
C311 ISABELLA WATER SYSTEM			05/13/82	200.	/ /			
C312 NETHER MHP			04/20/81	210.	11			
C313 PINE NEEDLE LANE TR. PK.			04/22/82	<200.	1 1			
C314 PLEASANT HILLS MHP			02/09/81	<200.	1 1			
C315 SOWEGA YOUTH HOME			05/14/79	<200.	1 1			
C316 WORTHY MANOR S/D		B282	08/12/81	<200.	08/11/83	<2		
Notes:								

a Barium concentration data from memorandum of 9/17/74 on file at the Georgia Geologic Survey, no sample date given

b Barium concentration data from memorandum of 9/2/80 on file at the Georgia Geologic Survey, no sample date given

c Barium concentration data from file notes dated 7/31/78 on file at the Georgia Geologic Survey, no sample date given

### APPENDIX D: PERMEABILITY TEST RESULTS

SAMPLE NUMBER	SAMPLE DEPTH (FEET)	VERTICAL HYDRAULIC CONDUCTIVITY (FT/D)
** GGS 3199		
137	276	0.048
139	305	0.056
138	330	0.027
140	360	DNS
120	385	0.081
121	403- 410	2.2
122	434- 436	25.
123	462- 468	12.
124	488	0.034
125	518	0.098
126	545	0.52
127	569	0.58
128	596	0.44
129	622	0.17
130	647	0.23
131	671	0.017
132	695	0.066
133	725	0.0022
134	748	0.0026
135	770	0.022
136	787	0.0083
** GGS 3213		
106	226	47.
107	244- 261	13.
108	271- 275	6.8
109	293- 297	0.31
110	367- 390	0.097
111	439- 443	3.2
112	466	48.
113	501	9.8
114	527	0.53
115	547	0.024
116	575	0.27
117	597	0.17
118	629	0.00083
119	651	0.033
96	674	0.0011
97	725	0.092
98	748	4.2 5.3
99 100	776 800	0.023
100	000	0.025

.

SAMPLE NUMBER	SAMPLE DEPTH	VERTICAL
NUMBER	(FEET)	HYDRAULIC
	(PEET)	CONDUCTIVITY (FT/D)
		(11/0)
101	826	0.032
102	853	0.0099
103	887	0.020
104	899- 903	0.062
105	198	0.13
** GGS 3535		
91	797	0.0055
90	822- 838	0.0034
89	848	0.0050
88	873	0.0068
87	899	0.0086
86	925	0.00048
85	948- 951	0.0020
84	977- 980	0.0091
83	1005	0.00057
82	1023-1028	0.0042
81	1057	0.0056
80	1081	0.0044
79	1106	0.00084
78	1128	0.0016
77	1150	0.0032
76	1173-1177	0.00044
** GGS 3541		
75	422	0.067
74	443	1.0
73	464	DNS
72	491	DNS
71	520- 521	DNS
70	545	0.00037
69	575	0.0011
68	592- 600	0.00049
67	625- 633	0.75
66	643- 661	0.18
65	673- 675	0.036
64	698- 701	0.011
63	718- 720	0.018
62	744- 748	0.048
61	769	0.0076
60 50	794	0.022
59	817-818	0.00044
58	845- 849	0.0099
57	875	0.078

## APPENDIX D: PERMEABILITY TEST RESULTS (CONTINUED)

SAMPLE	SAMPLE	VERTICAL
NUMBER	DEPTH	HYDRAULIC
	(FEET)	CONDUCTIVITY
		(FT/D)
56	901	0.0094
55	924	DNS
54	957	0.047
53A	979	0.25
52	1002	0.0029
51	1024	0.078
50	1051	0.16
** GGS 3542		
94	609	0.26
93	642	1.6
92	651- 662	2.1
2	722	11.
3	729	99.
4	744	23.
5	749	1.8
6	761	0.020
7	764	0.0038
8	786	0.21
9	796	0.030
10	806	0.0066
11	810	0.88
12	824	0.71
13	850	2.1
14	874	0.030
15	901	0.018
16	936	0.040
17	952	0.016
18	974	0.44
19	1008	3.7
20	1033	0.0088
21	1058-1062	0.0063
22	1086	DNS
23	1107-1121	0.018
24	1145-1146	0.029
25	1170	0.027
26	1225-1238	0.0037
27	1246-1255	0.0028
28	1265-1267	0.0041
** 000 75//		
** GGS 3544	150- 154	0.0024
29 30	170- 171	D N S
		0.0071
31	192	0.0071

### APPENDIX D: PERMEABILITY TEST RESULTS (CONTINUED)

NUMBER         DEPTH (FEET)         HYDRAULIC CONDUCTIVITY (FT/D)           32         204- 215         4.6           *** GGS 3545         33         312- 317         D N S           34         337- 339         D N S         35           36         423         0.17           37         456         0.20           38         483         1.5           39         506         0.0098           40         525- 536         0.013           41         546- 560         0.019           42         583         0.016           43         610- 619         0.0050           44         642         0.021           45         667         0.0042           46         704         0.046           47         729         0.00080	SAMPLE	SAMPLE	VERTICAL
32     204- 215     4.6       *** GGS 3545     33     312- 317     D N S       34     337- 339     D N S       35     363     3.9       36     423     0.17       37     456     0.20       38     483     1.5       39     506     0.0098       40     525- 536     0.013       41     546- 560     0.019       42     583     0.016       43     610- 619     0.0050       44     642     0.021       45     667     0.0042       46     704     0.046       47     729     0.00080	NUMBER	DEPTH	HYDRAULIC
32       204- 215       4.6         *** GGS 3545       33       312- 317       D N S         34       337- 339       D N S         35       363       3.9         36       423       0.17         37       456       0.20         38       483       1.5         39       506       0.0098         40       525- 536       0.013         41       546- 560       0.019         42       583       0.016         43       610- 619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080		(FEET)	CONDUCTIVITY
** GGS 354533 $312$ - $317$ D N S34 $337$ - $339$ D N S35 $363$ $3.9$ 36 $423$ $0.17$ 37 $456$ $0.20$ 38 $483$ $1.5$ 39 $506$ $0.0098$ 40 $525$ - $536$ $0.013$ 41 $546$ - $560$ $0.019$ 42 $583$ $0.016$ 43 $610$ - $619$ $0.0050$ 44 $642$ $0.021$ 45 $667$ $0.0042$ 46 $704$ $0.0060$			(FT/D)
** GGS 354533 $312$ - $317$ D N S34 $337$ - $339$ D N S35 $363$ $3.9$ 36 $423$ $0.17$ 37 $456$ $0.20$ 38 $483$ $1.5$ 39 $506$ $0.0098$ 40 $525$ - $536$ $0.013$ 41 $546$ - $560$ $0.019$ 42 $583$ $0.016$ 43 $610$ - $619$ $0.0050$ 44 $642$ $0.021$ 45 $667$ $0.0042$ 46 $704$ $0.0060$			
** GGS 354533 $312$ - $317$ D N S34 $337$ - $339$ D N S35 $363$ $3.9$ 36 $423$ $0.17$ 37 $456$ $0.20$ 38 $483$ $1.5$ 39 $506$ $0.0098$ 40 $525$ - $536$ $0.013$ 41 $546$ - $560$ $0.019$ 42 $583$ $0.016$ 43 $610$ - $619$ $0.0050$ 44 $642$ $0.021$ 45 $667$ $0.0042$ 46 $704$ $0.0060$			
33       312- 317       D N S         34       337- 339       D N S         35       363       3.9         36       423       0.17         37       456       0.20         38       483       1.5         39       506       0.0098         40       525- 536       0.013         41       546- 560       0.019         42       583       0.016         43       610- 619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080	32	204- 215	4.6
33       312- 317       D N S         34       337- 339       D N S         35       363       3.9         36       423       0.17         37       456       0.20         38       483       1.5         39       506       0.0098         40       525- 536       0.013         41       546- 560       0.019         42       583       0.016         43       610- 619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080	** 000 7E/E		
34       337-339       D N S         35       363       3.9         36       423       0.17         37       456       0.20         38       483       1.5         39       506       0.0098         40       525-536       0.013         41       546-560       0.019         42       583       0.016         43       610-619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080		740 747	
35       363       3.9         36       423       0.17         37       456       0.20         38       483       1.5         39       506       0.0098         40       525-       536       0.013         41       546-       560       0.019         42       583       0.016         43       610-       619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080			
36       423       0.17         37       456       0.20         38       483       1.5         39       506       0.0098         40       525-536       0.013         41       546-560       0.019         42       583       0.016         43       610-619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080			
37       456       0.20         38       483       1.5         39       506       0.0098         40       525-536       0.013         41       546-560       0.019         42       583       0.016         43       610-619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080			
38       483       1.5         39       506       0.0098         40       525-       536       0.013         41       546-       560       0.019         42       583       0.016         43       610-       619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080	36	423	0.17
39         506         0.0098           40         525-         536         0.013           41         546-         560         0.019           42         583         0.016           43         610-         619         0.0050           44         642         0.021           45         667         0.0042           46         704         0.0060	37	456	0.20
40       525-536       0.013         41       546-560       0.019         42       583       0.016         43       610-619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.0060         47       729       0.00080	38	483	1.5
41       546-       560       0.019         42       583       0.016         43       610-       619       0.0050         44       642       0.021         45       667       0.0042         46       704       0.046         47       729       0.00080	39	506	0.0098
42         583         0.016           43         610-         619         0.0050           44         642         0.021           45         667         0.0042           46         704         0.046           47         729         0.00080	40	525- 536	0.013
43610-6190.0050446420.021456670.0042467040.046477290.00080	41	546- 560	0.019
44         642         0.021           45         667         0.0042           46         704         0.046           47         729         0.00080	42	583	0.016
45         667         0.0042           46         704         0.046           47         729         0.0080	43	610- 619	0.0050
46         704         0.046           47         729         0.00080	44	642	0.021
47 729 0.00080	45	667	0.0042
	46	704	0.046
<b>/8 755- 750 0.000</b>	47	729	0.00080
	48	755- 759	0.099
49 783 0.023	49	783	0.023
i			

Notes:

13

D N S denotes samples that did not saturate

Sample depth is listed as a range where core recovery was poor

## See separate envelope for Plates 1 - 15

For convenience in selecting our reports from your bookshelves, they will be color-keyed across the spine by subject as follows:

Red	Valley and Ridge mapping and structural geology
Dk. Purple	Piedmont and Blue Ridge mapping and structural geology
Maroon	Coastal Plain mapping and stratigraphy
Lt. Green	Paleontology
Lt. Blue	Coastal Zone studies
Dk. Green	Geochemical and geophysical studies
Dk. Blue	Hydrology
Olive	Economic geology
	Mining directory
Yellow	Environmental studies
	Engineering studies
Dk. Orange	Bibliographies and lists of publications
Brown	Petroleum and natural gas
Black	Field trip guidebooks
Dk. Brown	Collections of papers

Colors have been selected at random, and will be augmented as new subjects are published.

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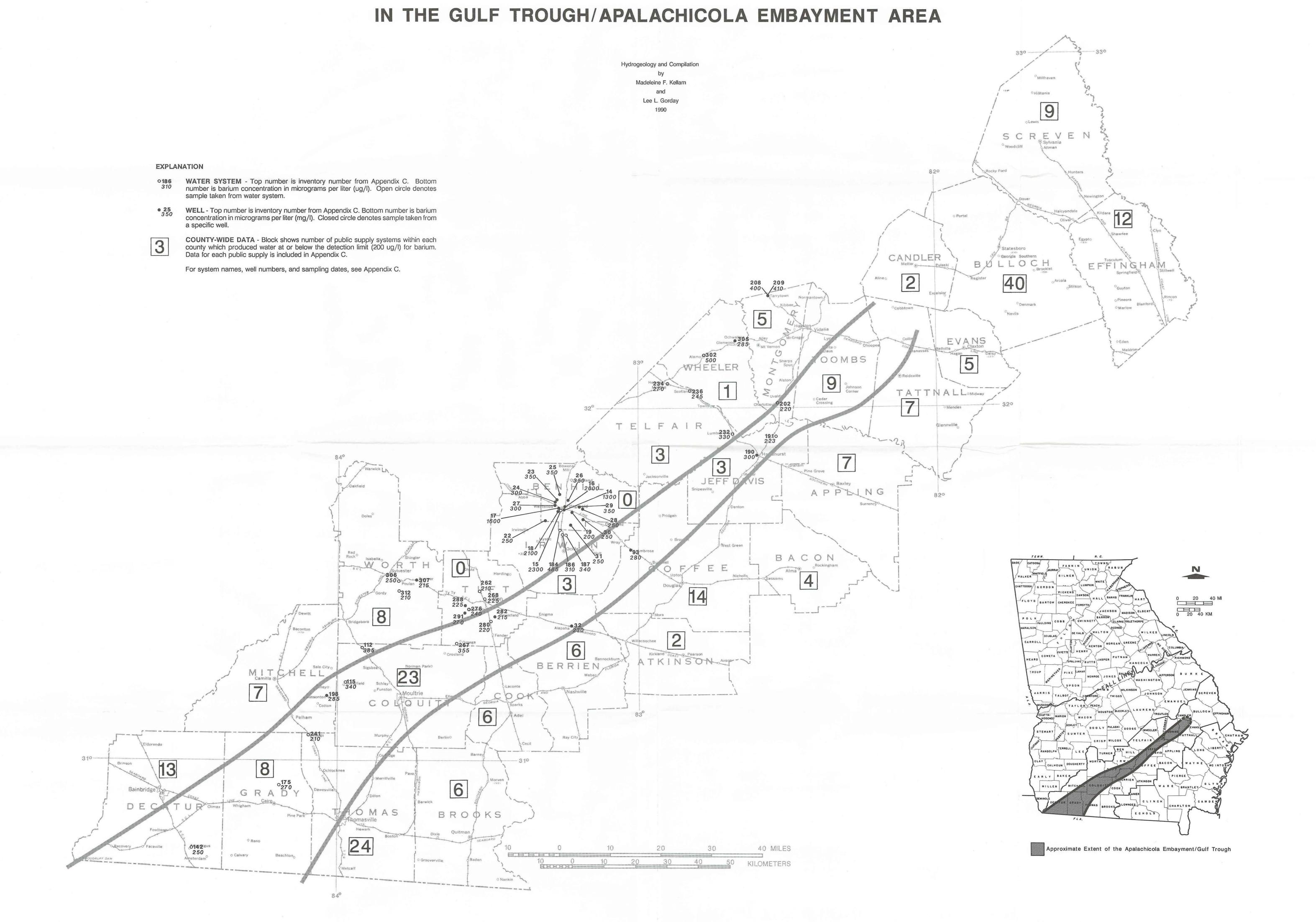
Editor: Patricia A. Allgood

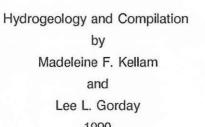
Cartographer: Don Shellenberger.

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# DISTRIBUTION OF BARIUM IN GROUND WATER FROM THE FLORIDAN AQUIFER SYSTEM IN THE GULF TROUGH/APALACHICOLA EMBAYMENT AREA

5	<b>WATER SYSTEM</b> - Top number is invento number is barium concentration in microgram sample taken from water system.
0	WELL - Top number is inventory number from concentration in micrograms per liter (mg/l). ( a specific well.
	COUNTY-WIDE DATA - Block shows number

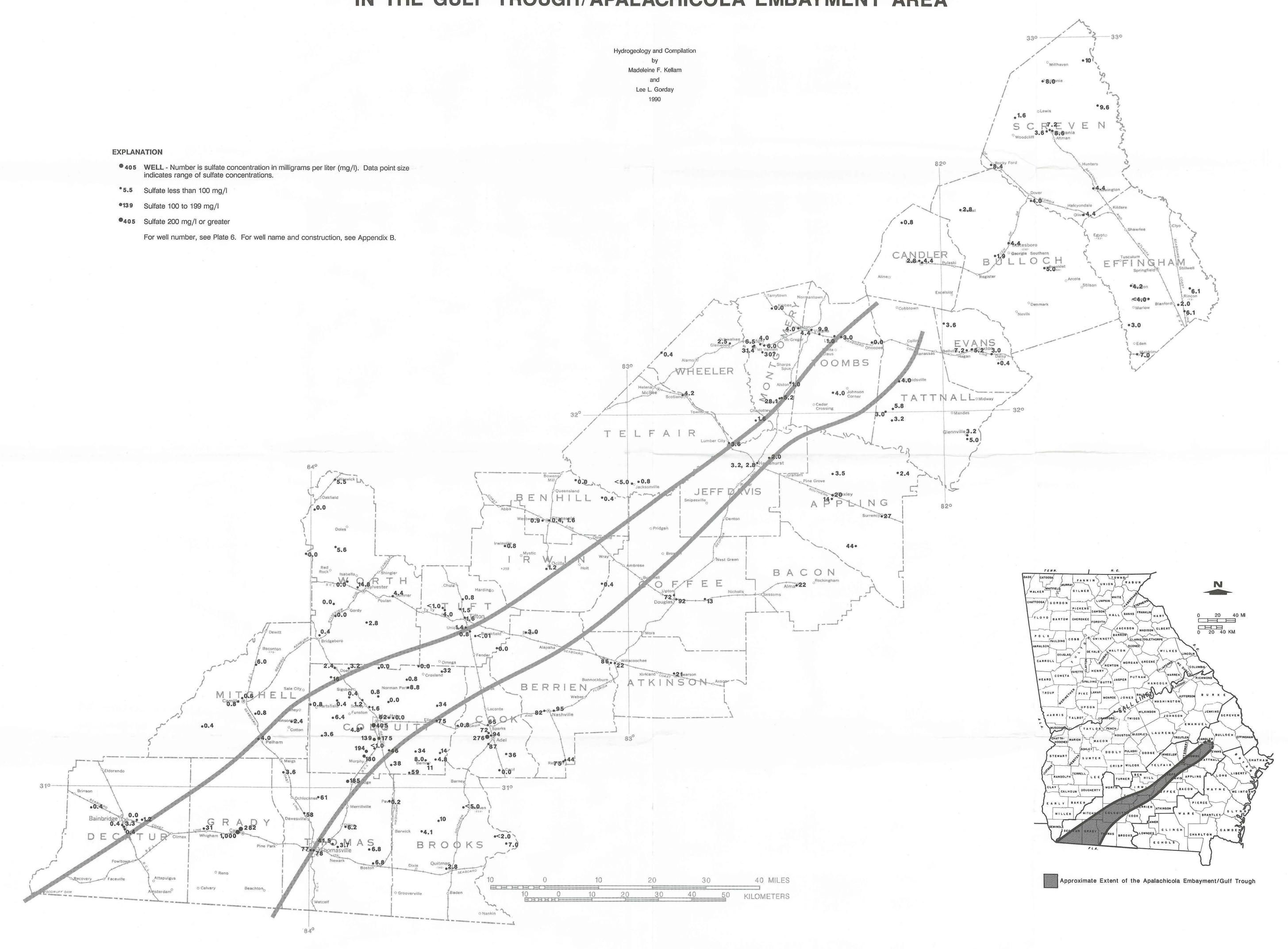




**BULLETIN 94** PLATE 14

# DISTRIBUTION OF SULFATE IN GROUND WATER FROM THE FLORIDAN AQUIFER SYSTEM IN THE GULF TROUGH/APALACHICOLA EMBAYMENT AREA

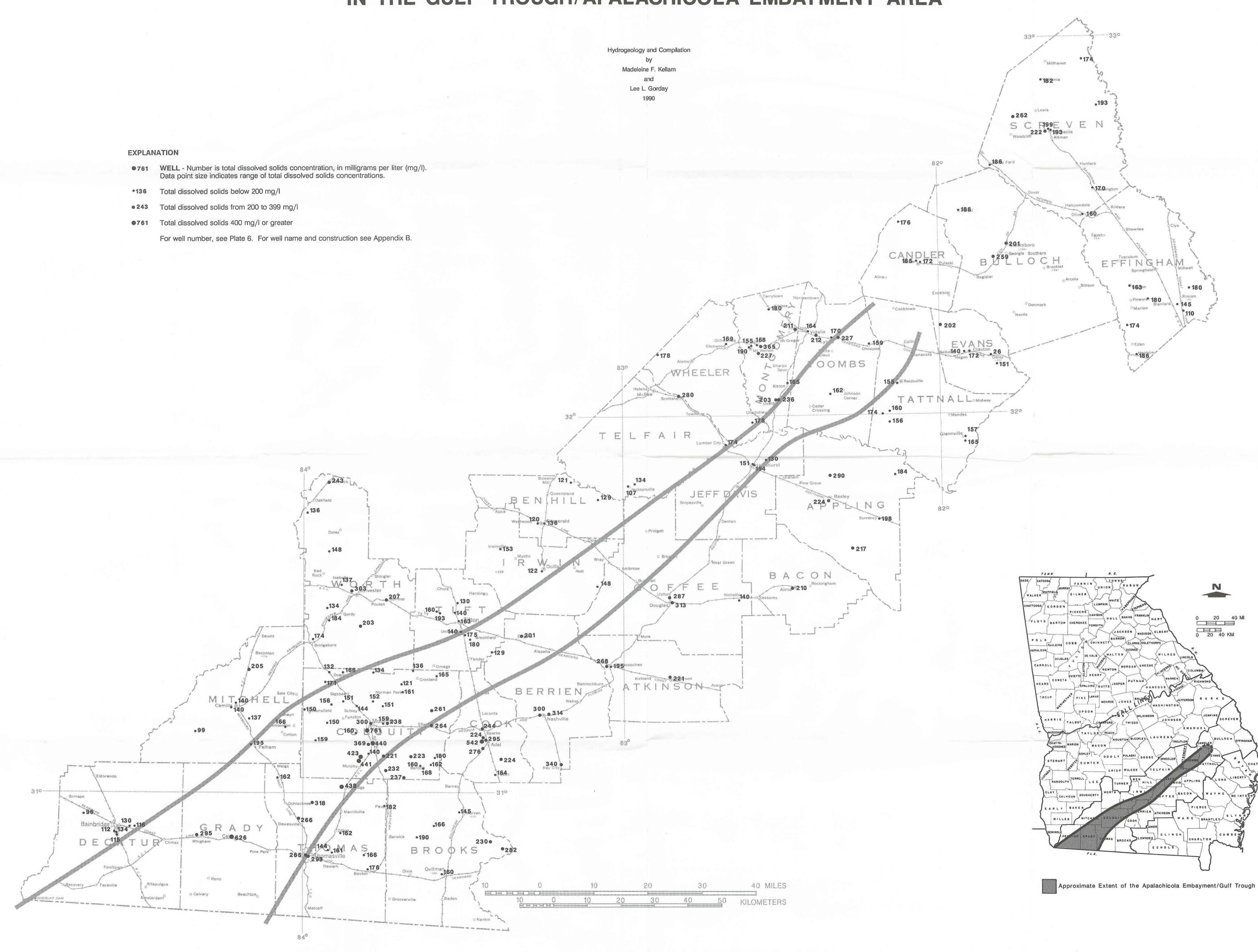
•405	WELL - Number is sulfate concentration in milligrams per liter (mg/l). indicates range of sulfate concentrations.	Data point size	
°5.5	Sulfate less than 100 mg/l		
•13 9	Sulfate 100 to 199 mg/l		
●405	Sulfate 200 mg/l or greater		



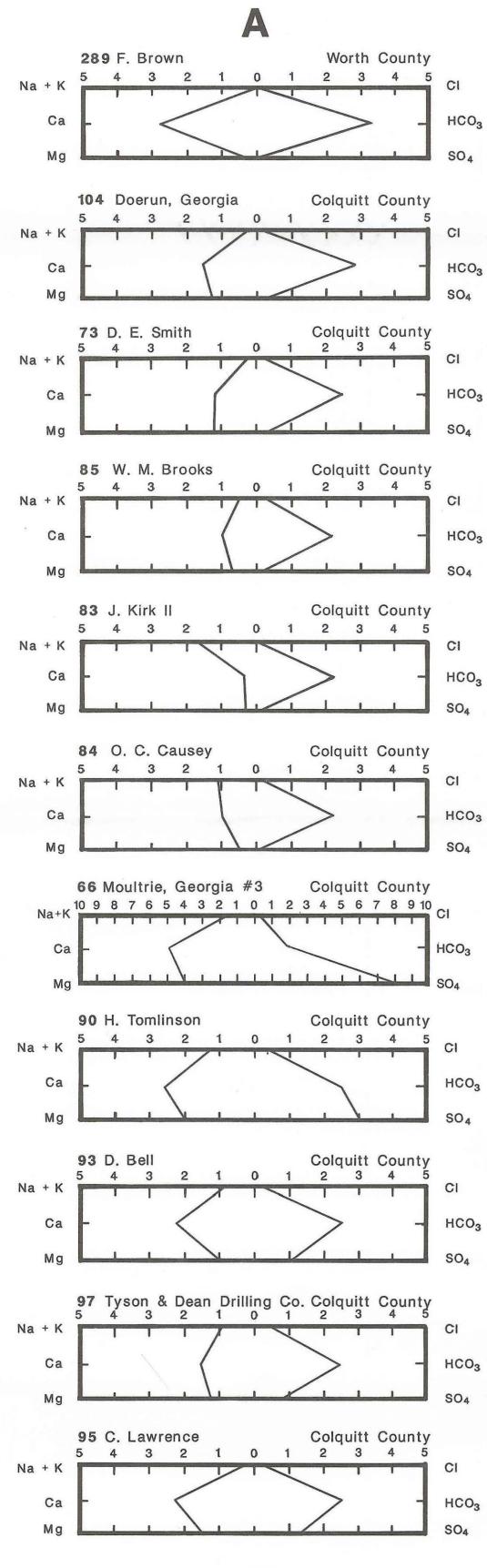
# TOTAL DISSOLVED SOLIDS IN GROUND WATER FROM THE FLORIDAN AQUIFER SYSTEM

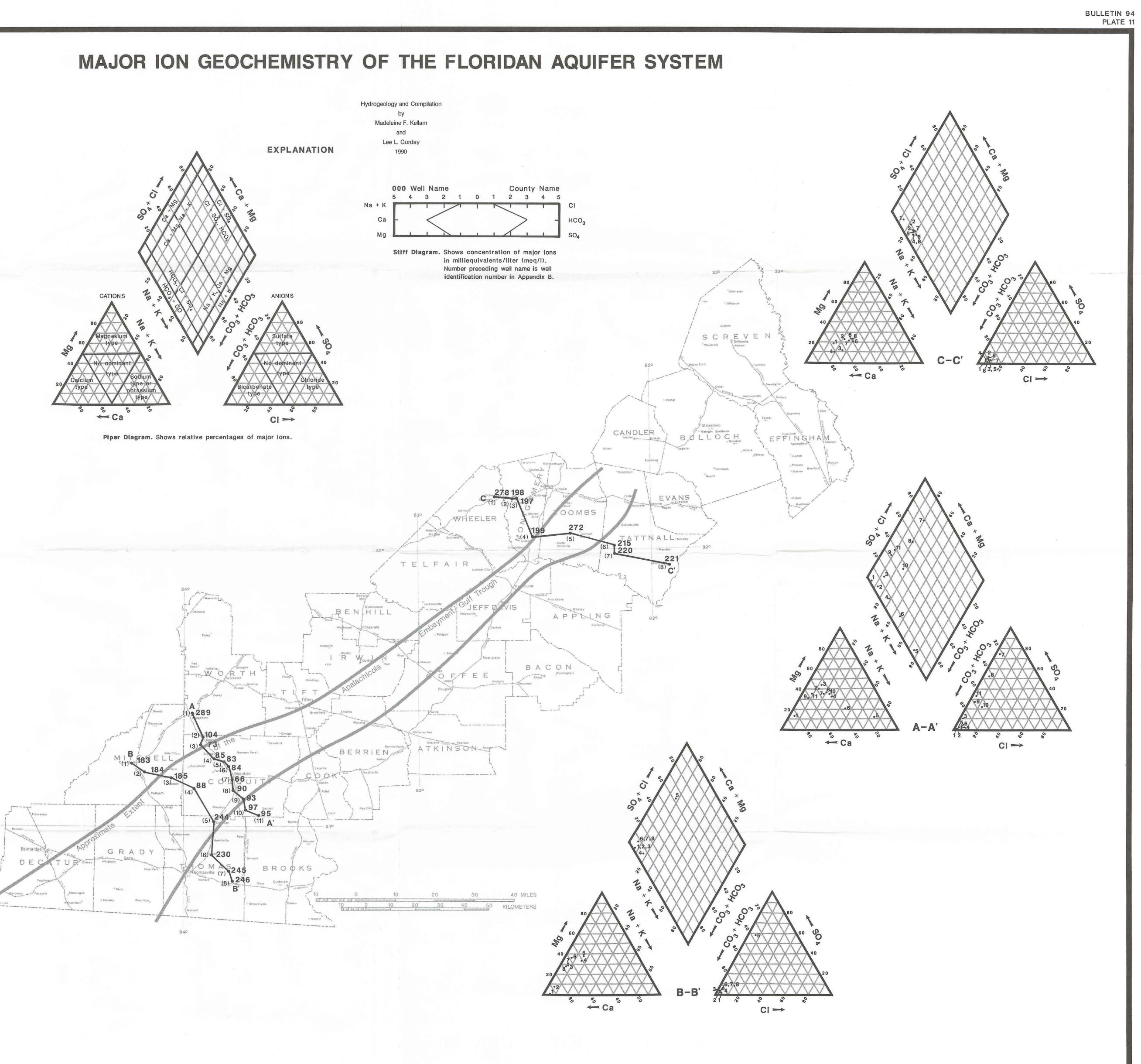
# IN THE GULF TROUGH/APALACHICOLA EMBAYMENT AREA

●761	WELL - Number is total dissolved solids concentration, in milligrams per liter (mg/l). Data point size indicates range of total dissolved solids concentrations.
•136	Total dissolved solids below 200 mg/l
●243	Total dissolved solids from 200 to 399 mg/l



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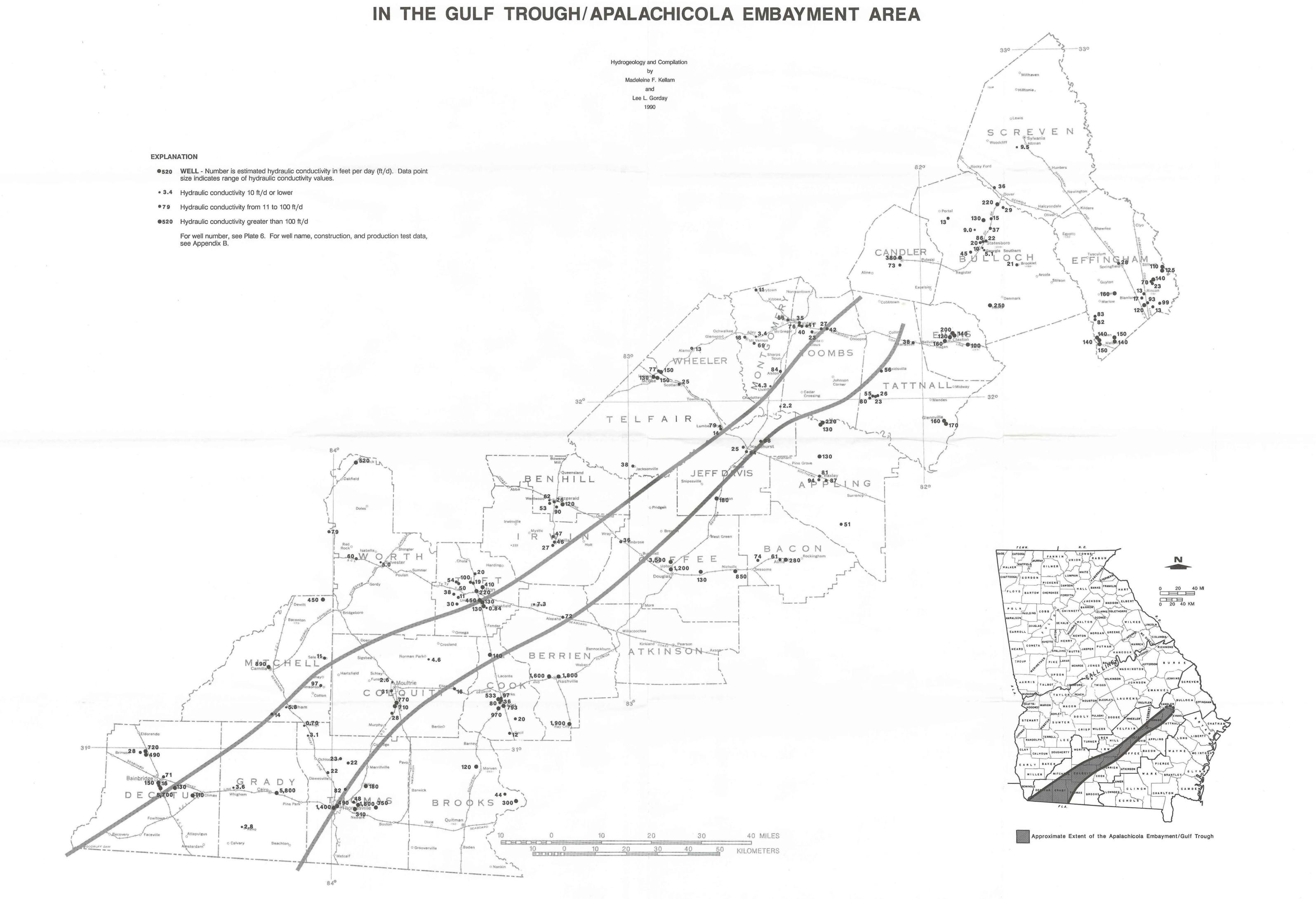






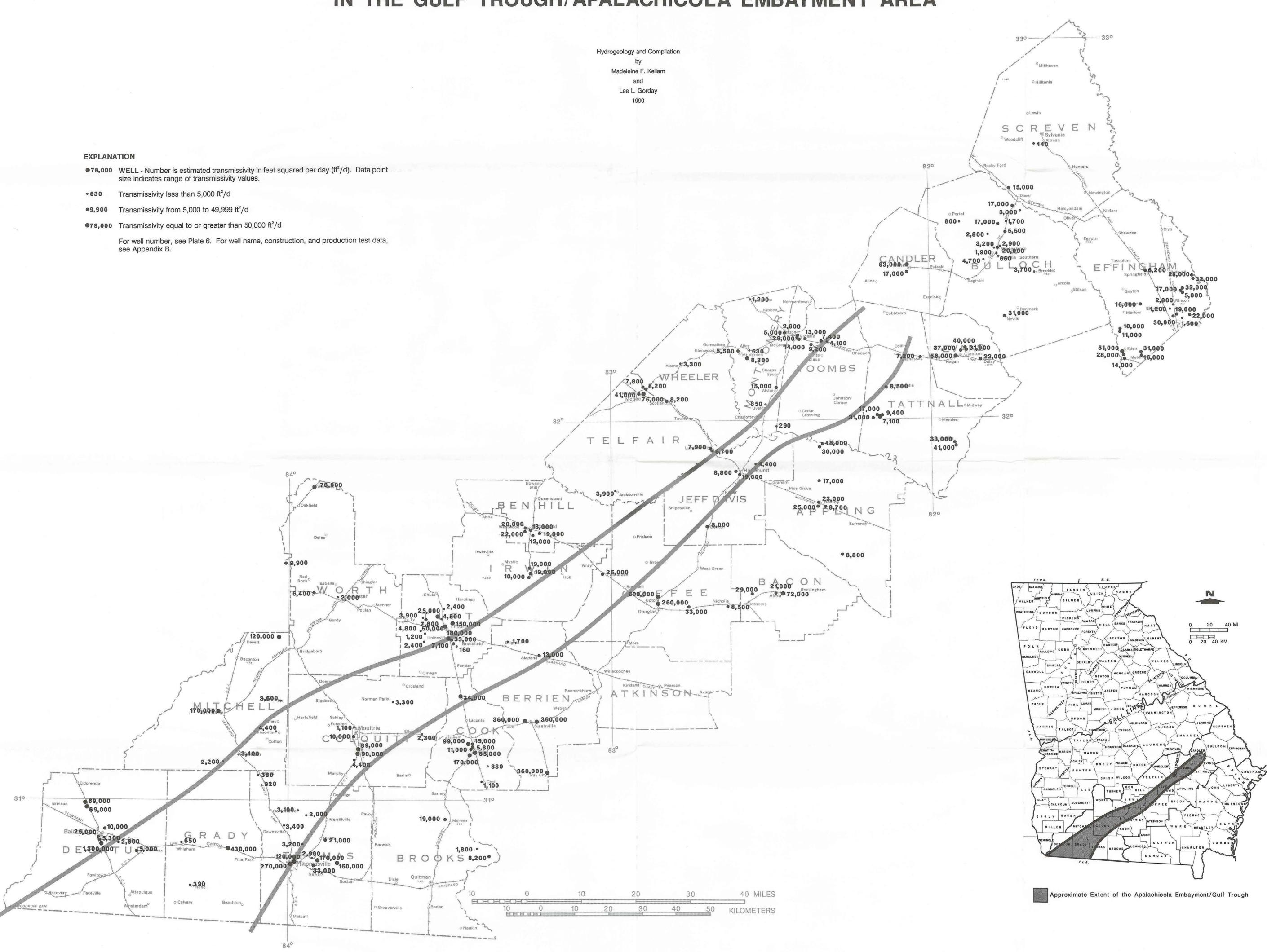
# ESTIMATED HYDRAULIC CONDUCTIVITY VALUES FOR WELLS TAPPING THE FLORIDAN AQUIFER SYSTEM

•520	WELL - Number is estimated hydraulic conductivity in feet per day (ft/d). Data point size indicates range of hydraulic conductivity values.
• 3.4	Hydraulic conductivity 10 ft/d or lower
•79	Hydraulic conductivity from 11 to 100 ft/d
0 - 0 0	Under the second with the exceptor these 100 ft/d

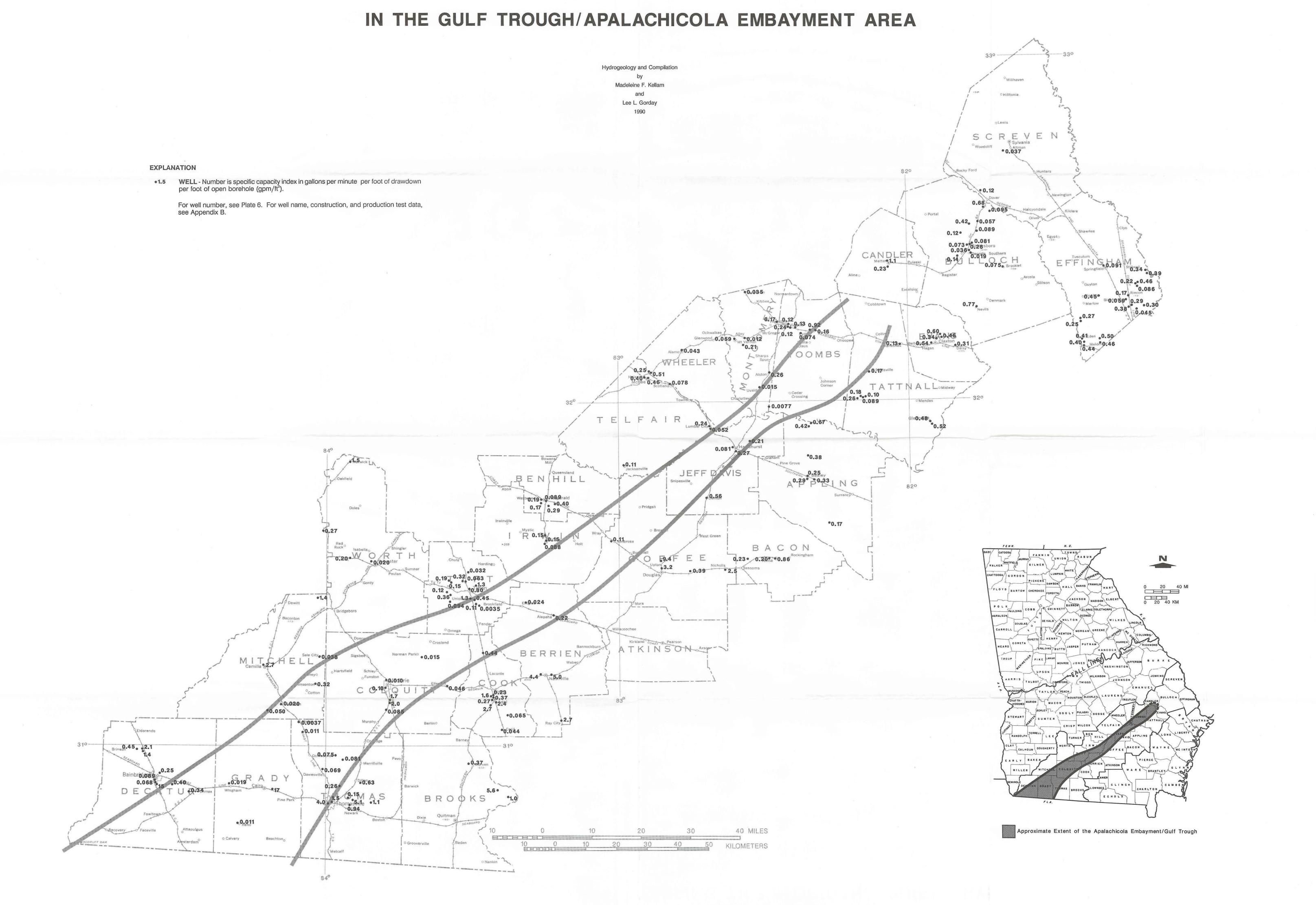


# ESTIMATED TRANSMISSIVITY VALUES FOR WELLS TAPPING THE FLORIDAN AQUIFER SYSTEM IN THE GULF TROUGH/APALACHICOLA EMBAYMENT AREA

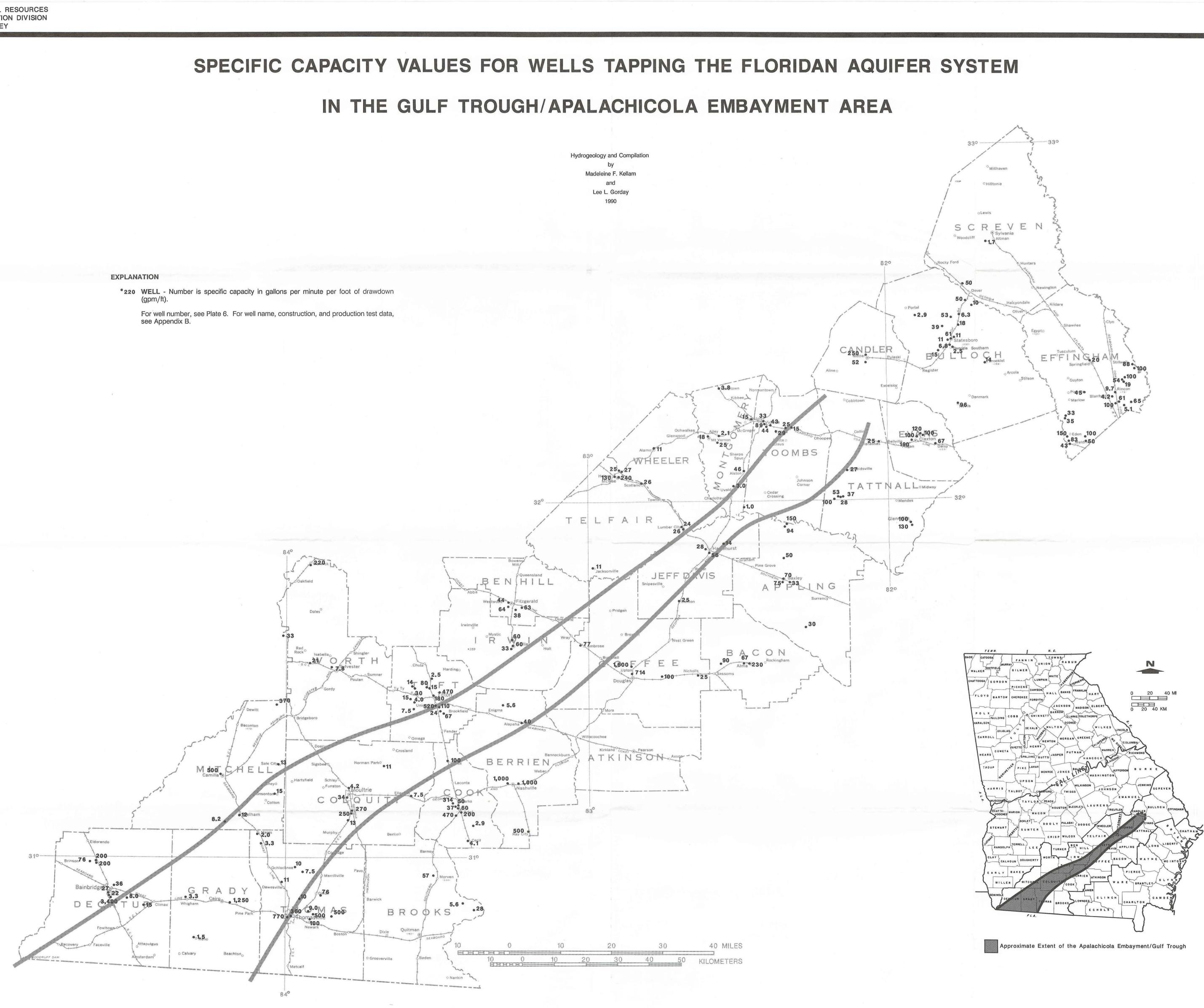
	●78,000	WELL - Number is estimated transmissivity in feet squared per day (ft²/d). Data point size indicates range of transmissivity values.	
	•630	Transmissivity less than 5,000 ft²/d	
<ul> <li>•9,900 Transmissivity from 5,000 to 49,999 ft²/d</li> <li>•78,000 Transmissivity equal to or greater than 50,000 ft²/d</li> </ul>		Transmissivity from 5,000 to 49,999 ft <sup>2</sup> /d	
		Transmissivity equal to or greater than 50,000 ft²/d	
		For well number, see Plate 6. For well name, construction, and production test data,	



# SPECIFIC CAPACITY INDICES FOR WELLS TAPPING THE FLORIDAN AQUIFER SYSTEM

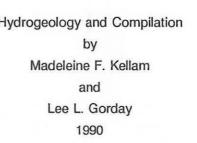


(gpm/ft).



## LOCATIONS OF WELLS USED IN MAPPING AQUIFER PROPERTIES AND WATER QUALITY







≥404

≥105

≥226 Ebomasville ≥205 ≥130 ≥644 Dixie ≥110 Boston ≥110 ≥106 ≥1 Dixie

≥14 5

3220 M A1440

≥192

≥121

≥120

O Grooverville

# THICKNESS OF THE FLORIDAN AQUIFER SYSTEM IN THE GULF TROUGH/APALACHICOLA EMBAYMENT AREA

	EXPLA	ANATION	
	300	<ul> <li>LINE OF EQUAL THICKNESS - Shows thickness, in feet, of the Floridan aquifer system. Contour interval is 100 feet. Dashed where approximately located.</li> </ul>	
	°291	1 WELL - Number is thickness, in feet, of the Floridan aquifer system.	
	<sub>●</sub> ≥115	5 WELL - Number is minimum thickness, in feet, of the Floridan aquifer system. The thickness is known to be at least this value. These data generally represent wells for which either the top or the bottom of the aquifer is uncertain. These points will dictate the location of contours of lower value, but may not influence contours of higher value.	
		840	
		Trookfield 1	
		Doles <sup>o</sup>	
		Doles 1	
		Red Rock <sup>o</sup> Isabella Shingler	Z
		ZITS We>270 R T H	120
		≥165 Pouran	/
		1 STER & Gordy	1
			L
		Baconton Astrauenta Bridgeboro 185 ≥20	solf
		≥17.10	
		475° ≥170	
		Sale City 2 2160 forman Barl	1/03
		291 ○ Hartsfield 445 OHA	1≥
		•Cotton •480	325
	-2000	≥253	
	J- 7	Idorendo	•42 B
			50
310	8rinson 291	°≥200 °571	

199

e00.

•≥135n<sub>o</sub>

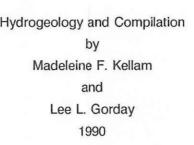
222

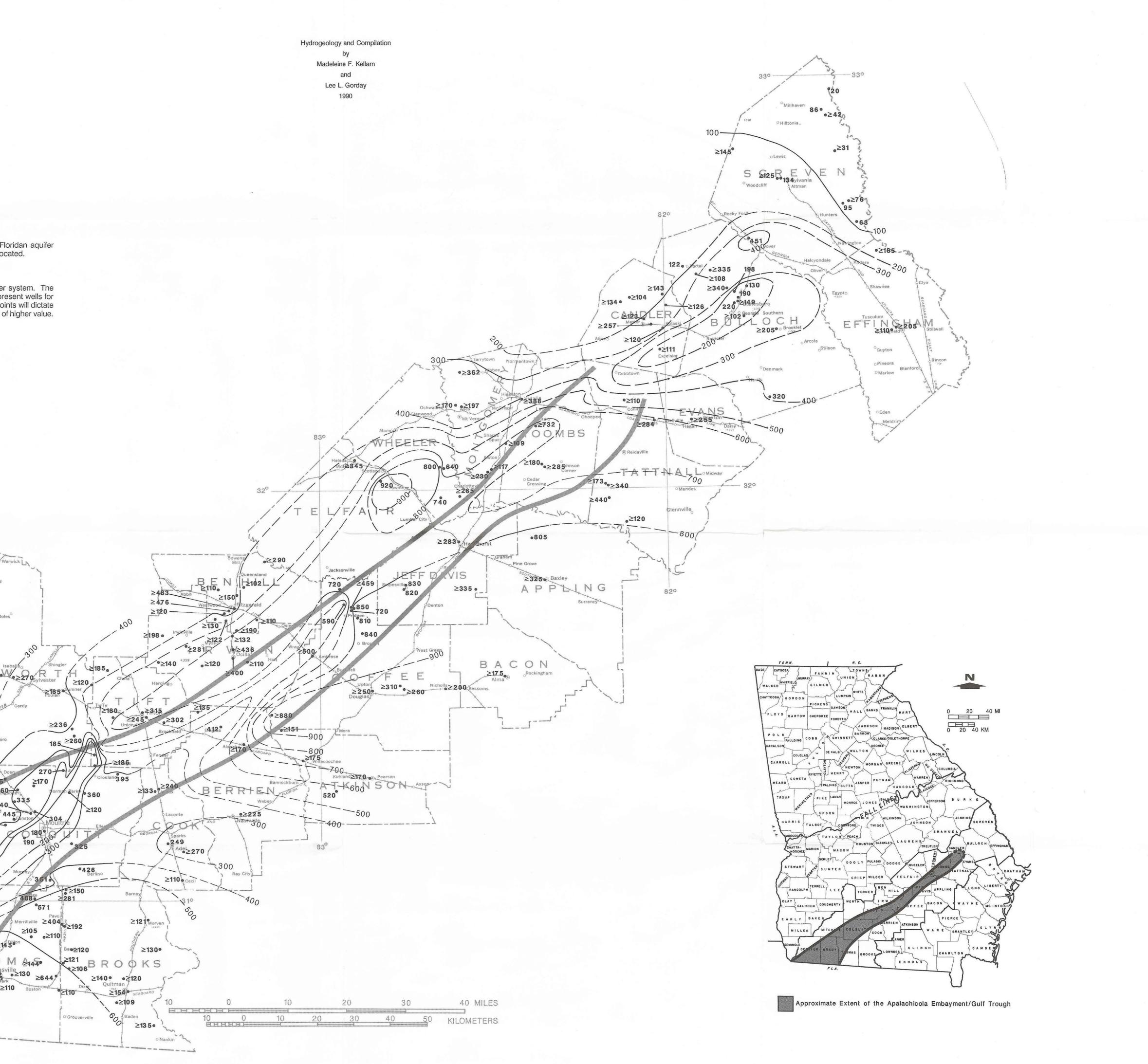
Calvary

≥129

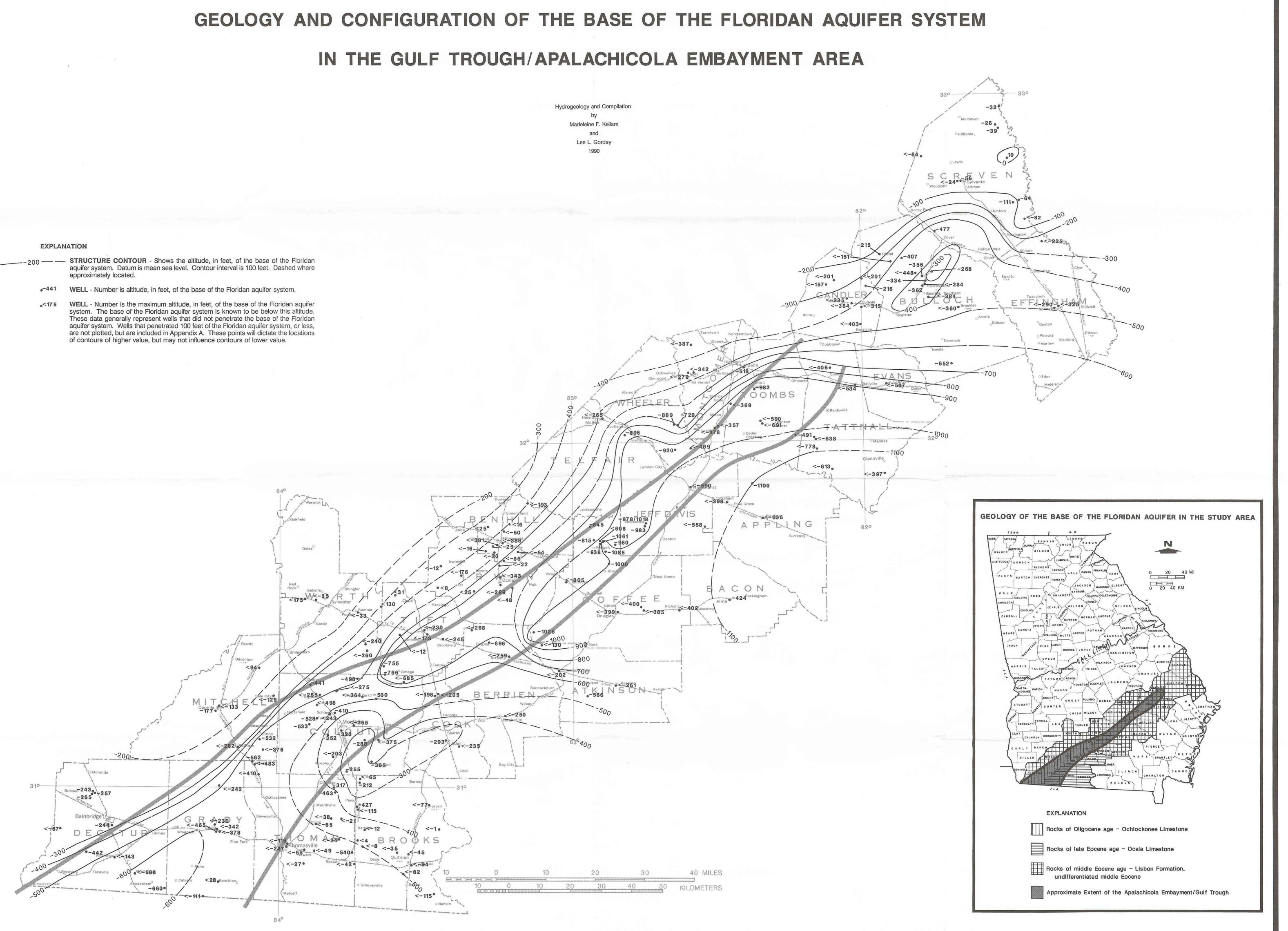
300-

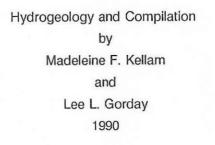
400

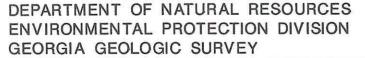




## DEPARTMENT OF NATURAL RESOURCES ENVIRONMENTAL PROTECTION DIVISION GEORGIA GEOLOGIC SURVEY

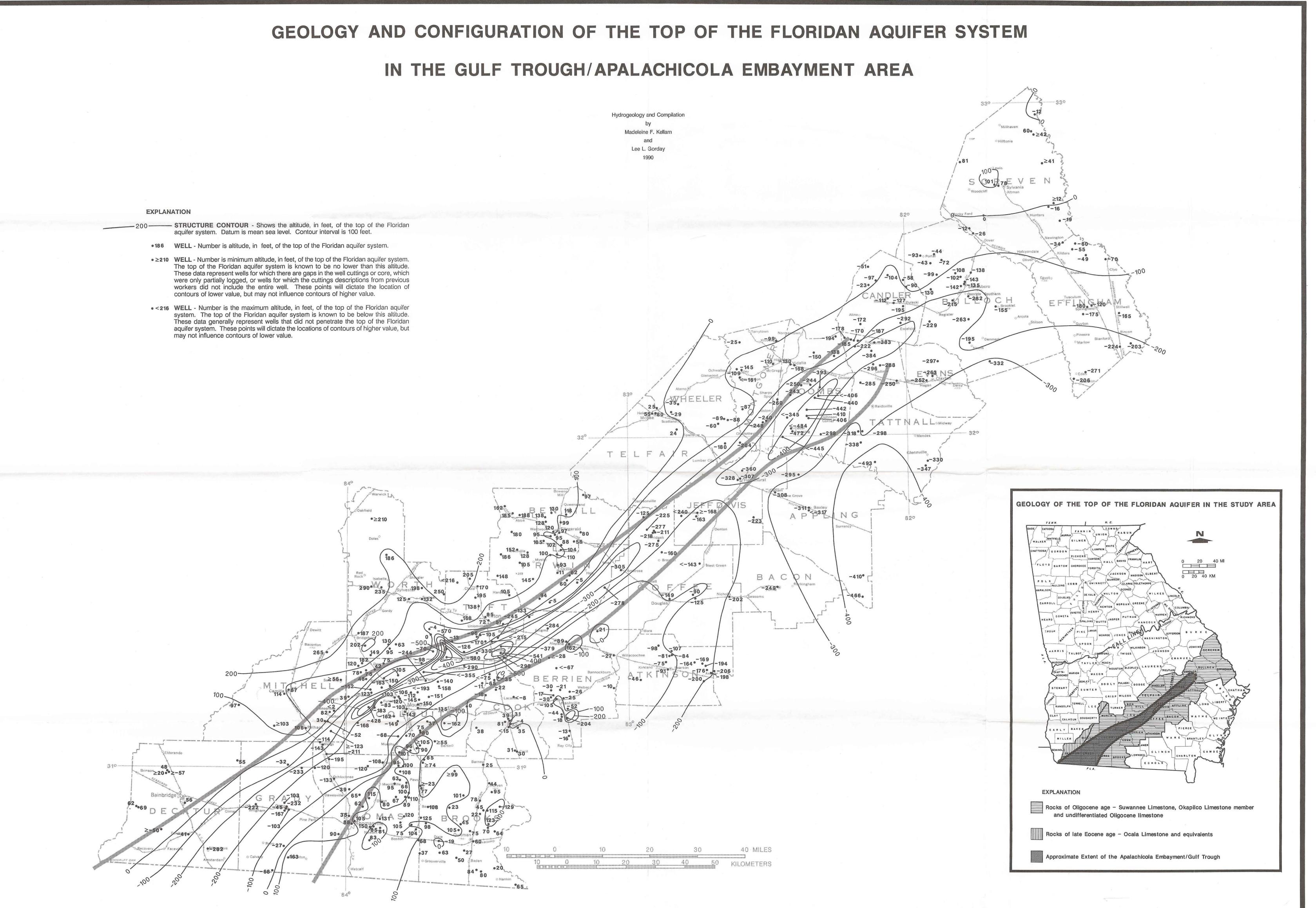






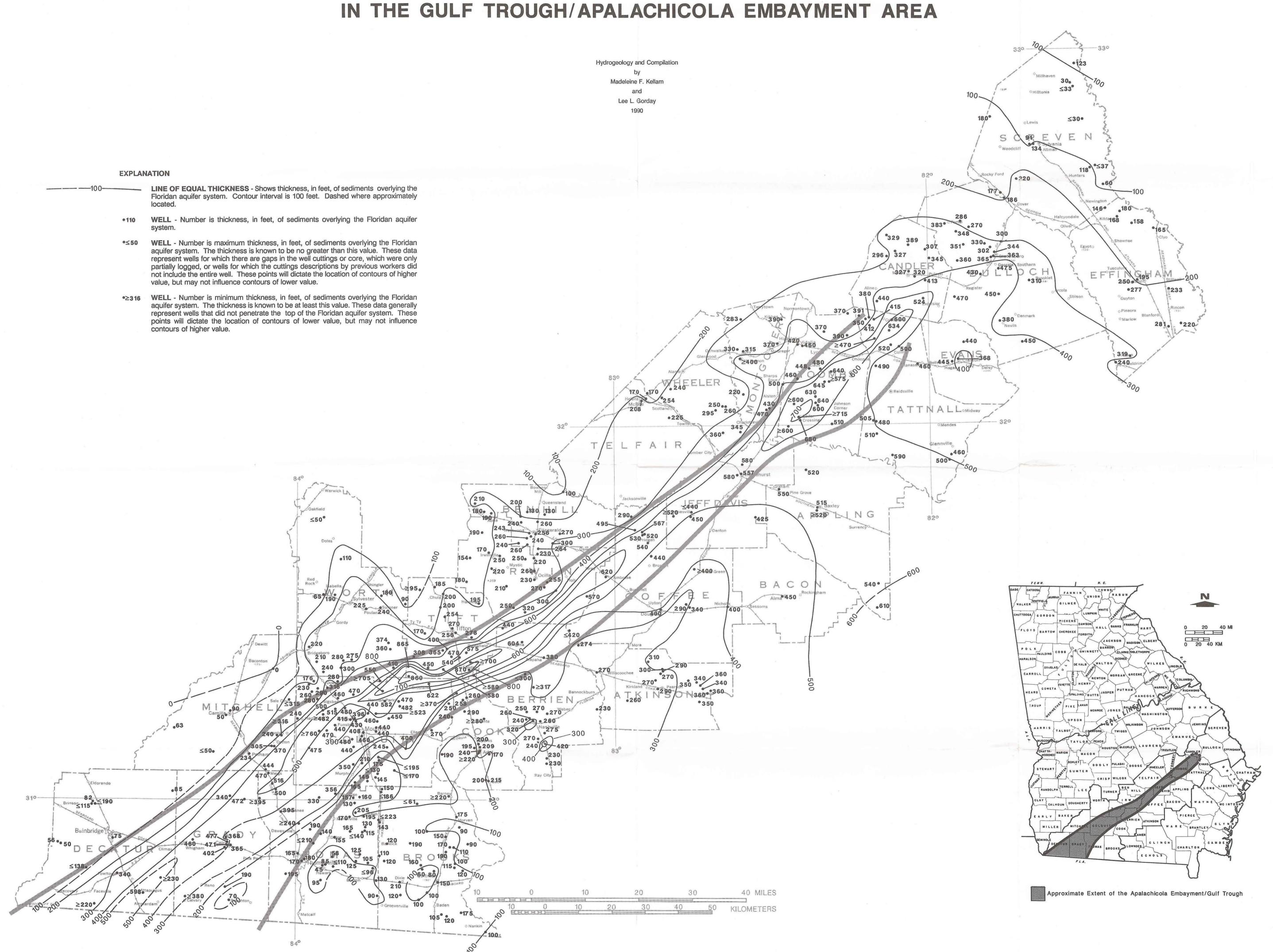
**BULLETIN 94** 

PLATE 3



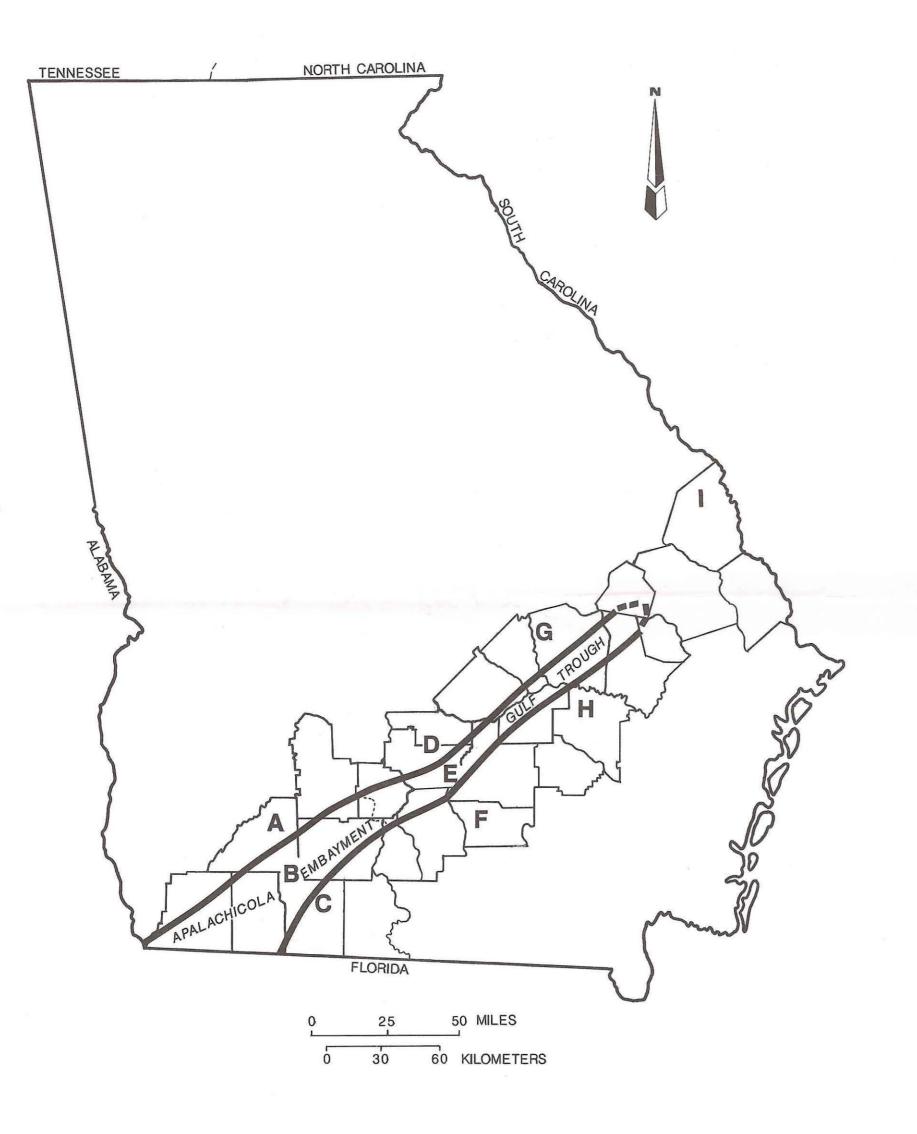
# THICKNESS OF SEDIMENTS OVERLYING THE FLORIDAN AQUIFER SYSTEM

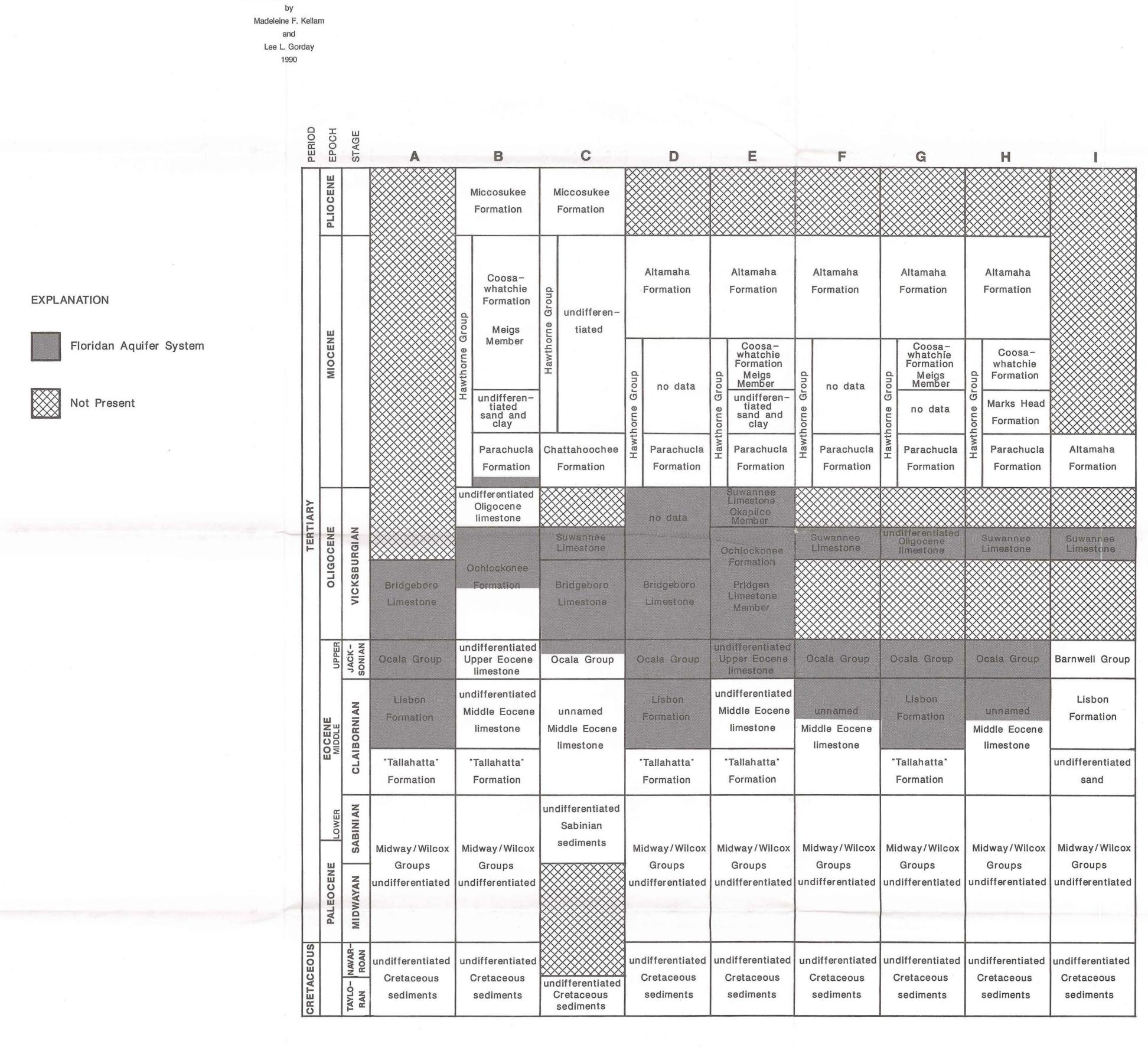
100		<b>LINE OF EQUAL THICKNESS</b> - Shows thickness, in feet, of sediments overlying the Floridan aquifer system. Contour interval is 100 feet. Dashed where approximately located.
	°110	WELL - Number is thickness, in feet, of sediments overlying the Floridan aquifer system.
	•≤50	<b>WELL</b> - Number is maximum thickness, in feet, of sediments overlying the Floridan aquifer system. The thickness is known to be no greater than this value. These data represent wells for which there are gaps in the well cuttings or core, which were only partially logged, or wells for which the cuttings descriptions by previous workers did not include the entire well. These points will dictate the location of contours of higher value, but may not influence contours of lower value.
	•≥316	<b>WELL</b> - Number is minimum thickness, in feet, of sediments overlying the Floridan aquifer system. The thickness is known to be at least this value. These data generally represent wells that did not penetrate the top of the Floridan aquifer system. These points will dictate the location of contours of lower value, but may not influence contours of higher value.



# STRATIGRAPHIC UNITS IN THE GULF TROUGH/APALACHICOLA EMBAYMENT AREA AND THEIR RELATIONSHIP TO THE FLORIDAN AQUIFER SYSTEM

Hydrogeology and Compilation





# DISTRIBUTION OF GROSS ALPHA ACTIVITY IN GROUND WATER FROM THE FLORIDAN AQUIFER SYSTEM IN THE GULF TROUGH/APALACHICOLA EMBAYMENT AREA

