

**Project Report No. 11**  
**South Georgia Minerals Program**

**Georgia**  
**State Division of Conservation**  
**Department of Mines, Mining and Geology**

**A. S. Furcron, Director**

**Phosphorite**

**By**

**Mineral Engineering Branch, Engineering Experiment Station**  
**Georgia Institute of Technology, and**  
**Georgia Department of Mines, Mining, and Geology**

**April 1969**



**This program is being carried out under contract as**  
**Project A-880 of the Georgia Institute of Technology,**  
**Atlanta, Georgia**



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## INTRODUCTION

This Project Report constitutes the eleventh in a series that have been issued since this program was initiated July 1, 1965. Three more are in preparation for issuance by July of this year (1969). To repeat from previous reports, all information from the program is published and released as progress reports as soon as feasible. An exception was Project Report No. 7, which was a contribution of the U. S. Geological Survey.

Emphasis in reports 2,3,4,5,9,10, and this report is on phosphorite. This concludes for the present, the reports wherein primary emphasis has been on phosphorite. Due to several factors, primary emphasis has shifted to other mineral commodities.

Previous reports have given all data and tests from a given hole and have reported several commodities. In this Project Report, in order to clear up the phosphorite exploration results, we are publishing only phosphorite data. In addition, phosphorite data is included from some holes where primary testing was for clays. Thus, this report, as well as the next three will be on a commodity basis. Many of the same holes will be used as different commodities were found at different horizons. Commodities for which data will be published are sand, clay, and heavy minerals. The clay report will include the fuller's earths.

Lithologic logs for the sand report will have more petrographic descriptions than included herein. Electric and gamma-ray logs may be republished.

There is a repeat of the explanation and use of the "Figures of Merit" used in this and other reports. As this report deals only with phosphorite the "Figures of Merit" should assist in evaluating the phosphorites of

potential economic use.

As an appendix there is a chart summing where information may be found in each of the eleven reports todate.

It will be noted that beneficiation data presented in this publication is all from computer printouts.

#### PLANS

Current and near future drilling is directed toward clays and other commodities of Southwest Georgia. Emphasis will be on kaolins, high alumina clays, fuller's earths, and limestones.

During the next biennial beginning in July 1969, some work is planned north of the Fall Line with a diamond drill. Other studies include the use of a new sensing device developed at Georgia Tech for heavy mineral and radiometric studies. All tests todate indicate that finding and delineating near surface heavy mineral bodies is greatly facilitated with the Tech developed instrumentation system.

## OBJECTIVE AND SCOPE

The objective of the South Georgia Mineral Program is to determine the existence, preliminary quality-quantity data, and approximate location of mineral deposits having economic feasibility potential for establishing new, or expanded, mineral industries in Georgia.

This report contains data on phosphorite from cores and wash samples from drilling in Berrien, Brooks, Bulloch, Chatham, Clinch, Colquitt, Crawford, Houston, Lowndes, Pulaski, Twiggs, and Wilkinson Counties. This concludes, for the time, data from holes where drilling was primarily for phosphorite, although data from a few holes where other commodities were of primary interest are included.

SUMMARYGeneral

Phosphorite deposits of potential economic development have been found in Eastern Chatham County and in areas northward from the Florida border between Thomas and Clinch Counties.

The Chatham County deposit has received intensive attention by industry in expectation of commercial utilization.

The Chatham County deposits thin out northward and westward. Southward it is believed that the deposit is too deep for economic recovery using present mining methods. The deposit also appears to be seaward from Chatham County. The Chatham County phosphorite is similar in composition and grade to the North Carolina deposit.

The South Georgia deposits, similar to those in Florida, appear to have their greatest potential along northward extensions of the Barwick Arch and the Ocala Uplift. The Barwick Arch appears to be truncated on the north by the extension of a structural feature described as the Gulf Trough. Whether this is synclinal, graben, or both has not been determined. On the east the Barwick Arch is bounded by the Georgia Embayment. The Gulf Trough also truncates the Ocala Uplift.

Specific For This Report:

Only Lowndes County hole number 12 revealed a matrix that would encourage further investigation of the immediate area. Clinch hole number 3 revealed multiple matrices, but for this hole they were sub-marginal. When deeper mining methods are relatively more economic some of the Berrien County areas should be re-evaluated.

## ECONOMIC FACTORS AND FIGURES OF MERIT

Different companies employ different break-levels and assign various degrees of importance to the several factors pertaining to the economic evaluation of a phosphorite deposit.

In fairness to landowners and others who might not be skilled in the calculations and application of such factors to engineering and economic evaluation, it was decided to indicate a range of levels as reported in the literature, select a mid-point level and present the calculated results for the holes-of-interest, that is, from the cores which showed promise of industrial utilization. (BPL in matrix = 9.0% and higher)

These factors, expressed as numbers, vary widely and can be confusing to the lay public. A "Figure of Merit" concept was devised whereby the calculated factor would be expressed as a ratio, to the break-point level, in such a way that figures of 1.0 or more would represent economic desirability, or if less than 1.0, economic undesirability. For clarification, typical results for a factor having a maximum economic level and for a factor having a minimum economic level are:

1. Overburden. Current strip mining practice places a maximum of 75 to 100 feet on the overburden which can be removed economically, depending upon the quantity and quality of the deposit beneath the overburden. The midpoint of this range was taken as 88 feet. When expressed in terms of "Economic Factors," Berrien County No. Be-6, for the matrix level of 91-121 feet would be "overburden = 91 feet." When expressed as a "Figure of Merit," this would appear as (88/91 : 0.97).

2. Current practice dictates that a matrix bed should be a minimum of 3 feet for mining. For the same hole (Be-6) the matrix encountered had a thickness of 30 feet, and this would be reported as an "Economic Factor." When expressed as a "Figure of Merit", it would be  $30/3 = 10.0$  which indicates economic desirability for this factor.

Note that the ratios for maximums and minimums are inverted, being

$\frac{\text{Practice}}{\text{Actual}}$  for maximum levels of interest

and

$\frac{\text{Actual}}{\text{Practice}}$  for minimum levels of interest

Economic Factors presented herein, the ranges of each as obtained from industry and publication, and the level of each employed to calculate a "Figure of Merit" are:

| <u>Factor</u>   | <u>Unit</u>   | <u>Range</u> | <u>Level-Used</u> |
|---|---------------|--------------|-------------------|
| Overburden Thickness  | ft.           | 75-100 max.  | 88                |
| Matrix Thickness  | ft            | 3 min.       | 3                 |
| Matrix BPL  | %             | 10 min.      | 10                |
| Flotation Concentrate BPL   | %             | 66 min.      | 66                |
| Rock for Electric Furnace, BPL  | %             | 52 min.      | 52                |
| Products, BPL   | tons/acre-ft. | 400 min.     | 400               |
| Overburden/Matrix   | Ratio         | 1-3 max.     | 2                 |
| Overburden/Products BPL   | cu. yd./ton   | 15-20 max.   | 17.5              |
| Matrix/Products BPL   | cu. yd./ton   | 5-7 max.     | 6                 |
| Fe <sub>2</sub> O <sub>3</sub> + Al <sub>2</sub> O <sub>3</sub> in Products | %             | 4-5 max.     | 4.5               |
| SiO <sub>2</sub> /CaO (For Electric Furnace)                                | Ratio         | 0.8-1.0 min. | 0.9               |
| Products Recovery*  | %             | 58-68 min.   | 63                |

\* Total BPL recoverable from "pebbles" and flotation concentrates divided by total BPL in matrix.



Certain assumptions, and average values and factors, were made to expedite calculations:

|                       |                    |
|-----------------------|--------------------|
| Density of overburden | = 90 lb./cu. ft.   |
| Feet thickness x 1613 | = cu. yd./acre     |
| Cubic yards x 1.215   | = Tons (2,000 lb.) |
| Feet thickness x 1960 | = Tons/acre        |

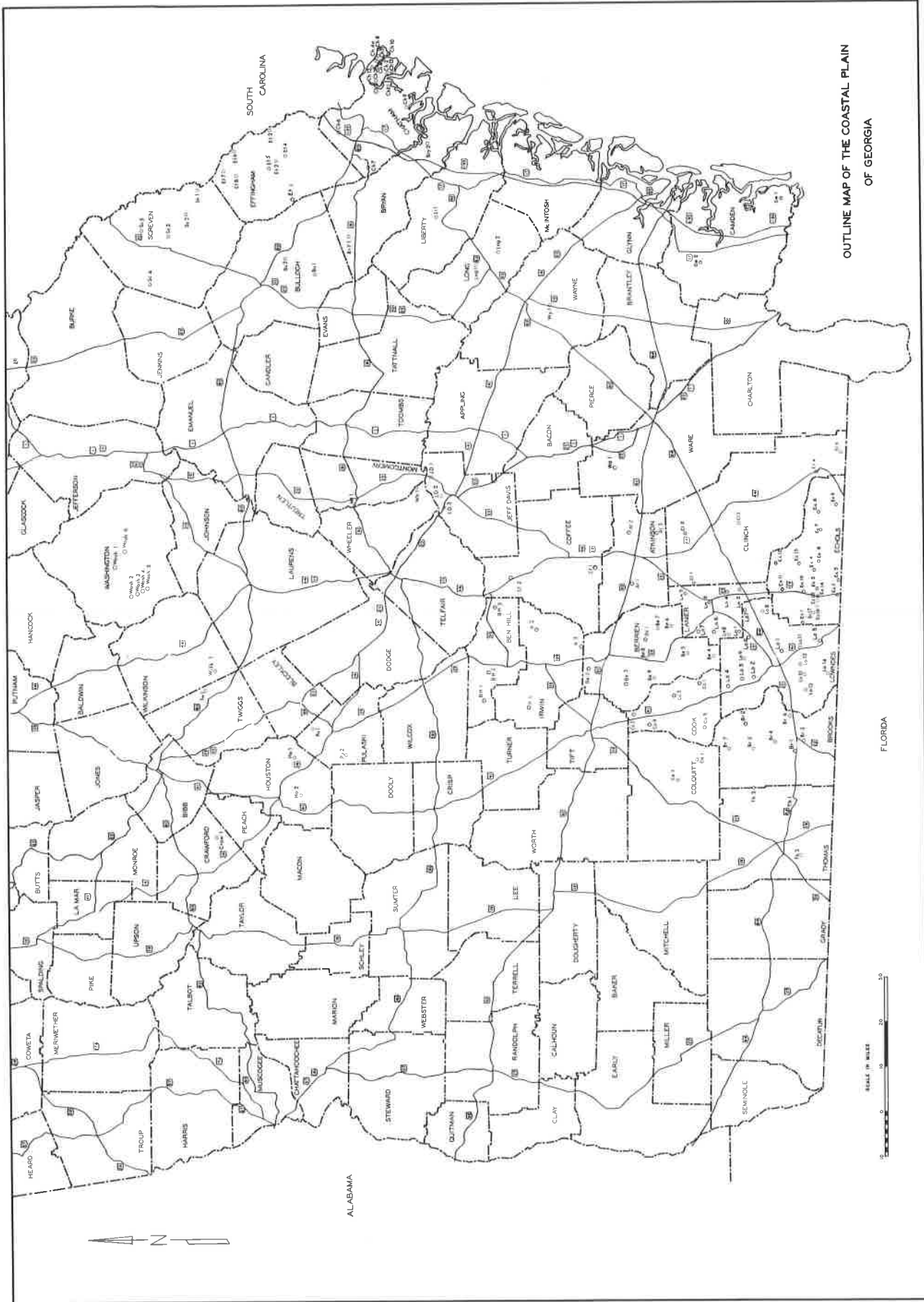
PROCEDURE

In general project procedures were the same as the previous report. Exceptions are noted below:

1. For the first time results of beneficiation with "Figures of Merit" were reproduced directly from computer printouts.
2. Figure 2 clarifies and replaces part of the flow chart of core processing as presented in previous reports.
3. X-ray diffraction of phosphorites was not done.

In addition, the BPL content of the matrix had to be at least 9 percent and of the flotation feed at least 7 percent to continue with beneficiation procedures.

Drilling was with both a Failing 1250 and a Failing 250 rig. The inside diameter of the drilling pipe of the larger rig (the 1250) permitted the gamma-ray probe to be lowered through it whereas the smaller rig's pipe did not. Hence, when the hole was caving gamma-ray logs were still obtainable with the large rig.

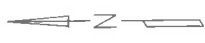


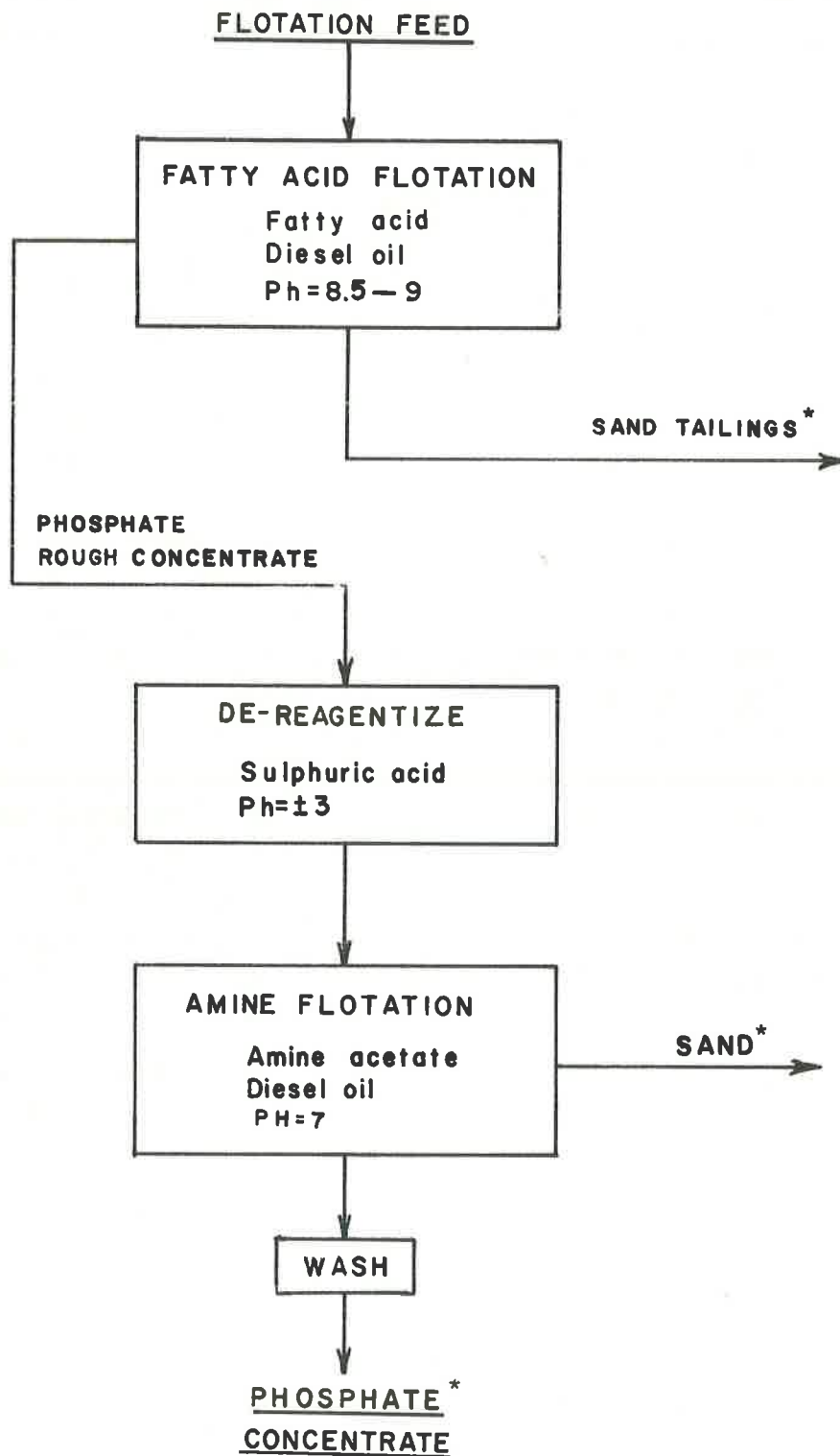
OUTLINE MAP OF THE COASTAL PLAIN OF GEORGIA

FLORIDA

ALABAMA

SOUTH CAROLINA





\* CHEMICAL ANALYSIS

Figure 2. Flow Chart of Core Processing

## LEGEND




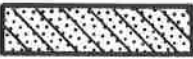
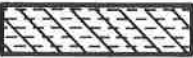



|   |                       |
|---|-----------------------|
|    | SAND                  |
|    | CLAY                  |
|    | SANDY CLAY            |
|    | CALCAREOUS SAND       |
|   | CALCAREOUS CLAY       |
|  | CALCAREOUS SANDY CLAY |
|  | LIMESTONE             |
|  | CARBONACEOUS MATERIAL |

Figure 3. Legend for Lithologic Logs.



BERRIEN COUNTY

BERRIEN COUNTY  
SUMMARY OF RESULTS

Six holes were cored in Berrien County, in addition to the three original holes. Of these only one, Be-6, had sufficient phosphorite to warrant beneficiation testing. Two factors would be against development at present. One is the 91 feet of overburden and the other is that only 10 percent of total weight is recoverable as phosphorite. The grade of this 10 percent is quite good however.

Electric logs were not run on Be-5 and Be-6 holes due to cave-in of hole walls. Gamma-ray logs were run inside the drill pipe.



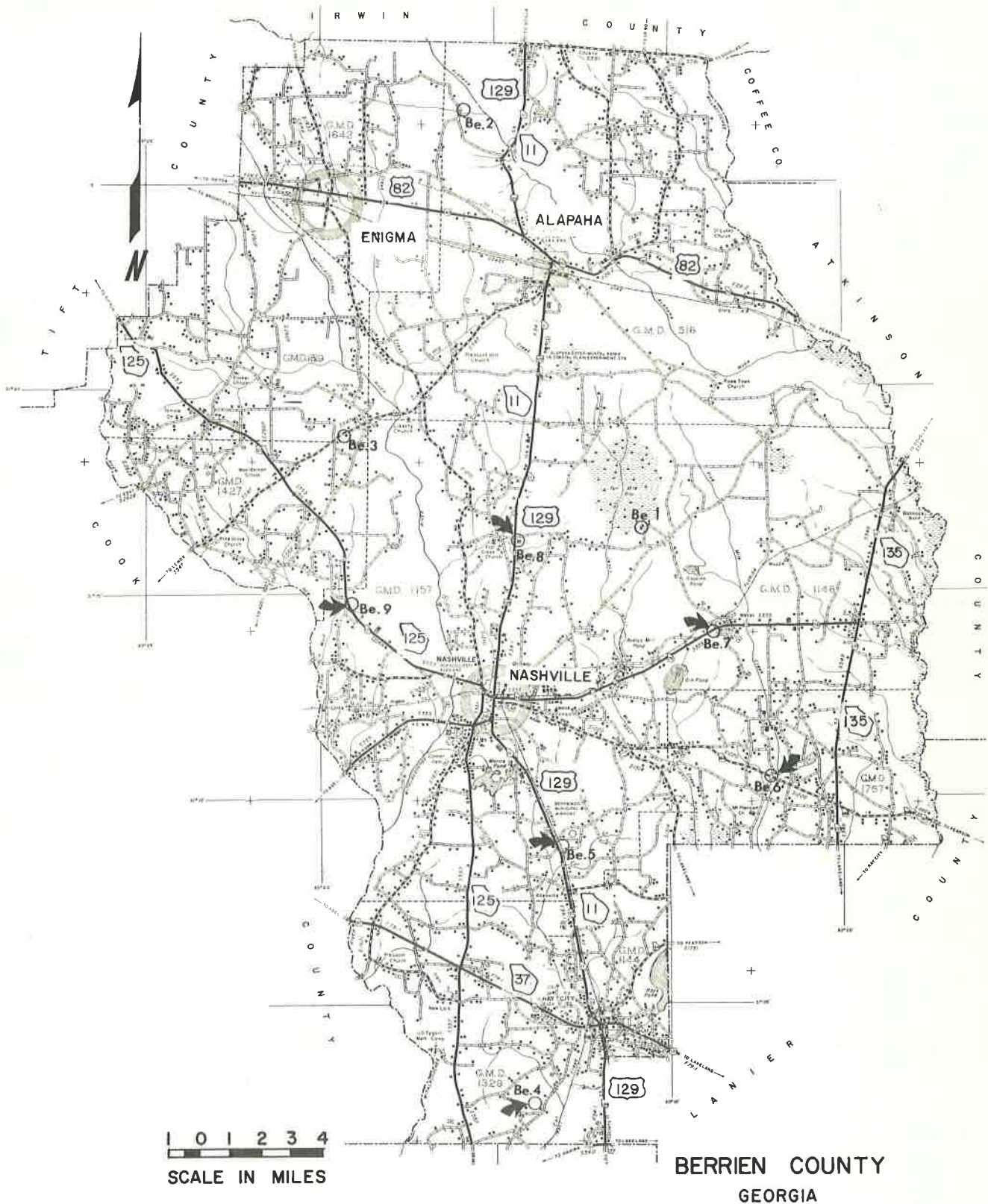


Figure BE-1. Location of Holes - Berrien County

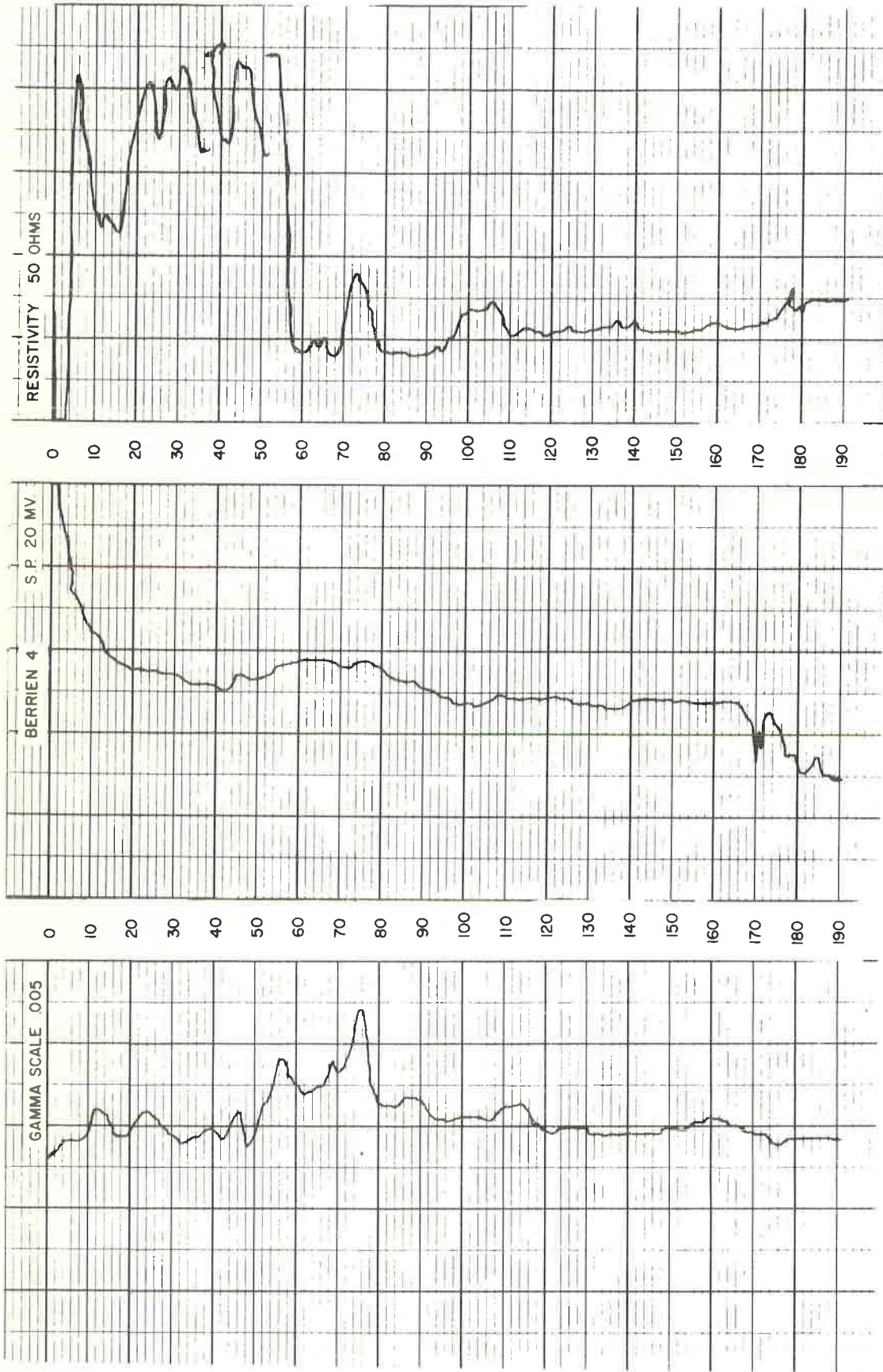


Figure BE-2. Electric and Gamma-Ray Logs - Berrien County  
Hole Be-4

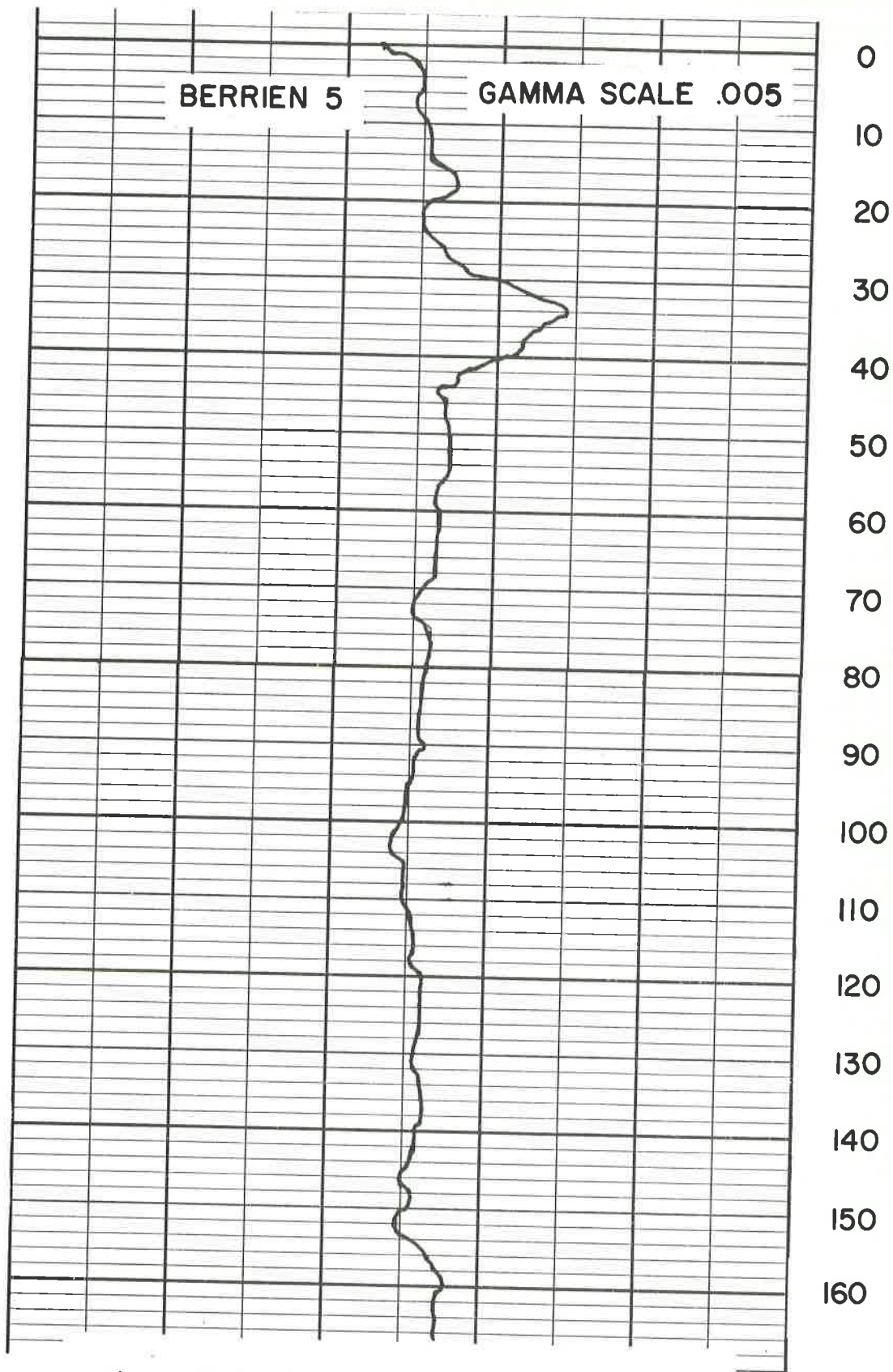


Figure BE-2. Gamma-Ray Logs - Berrien County  
Hole Be-5

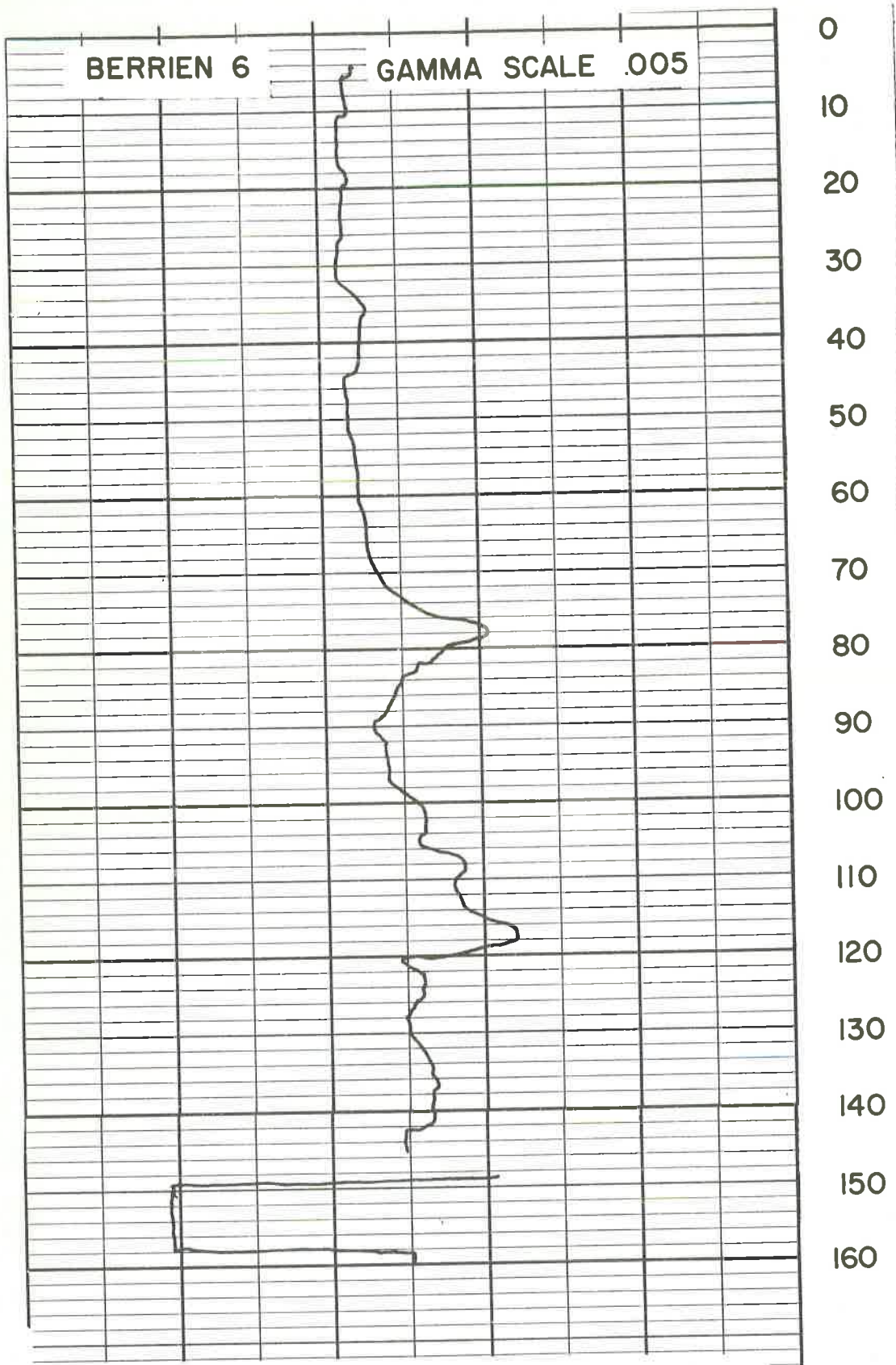


Figure BE-2. Gamma-Ray Logs - Berrien County  
Hole Be-6

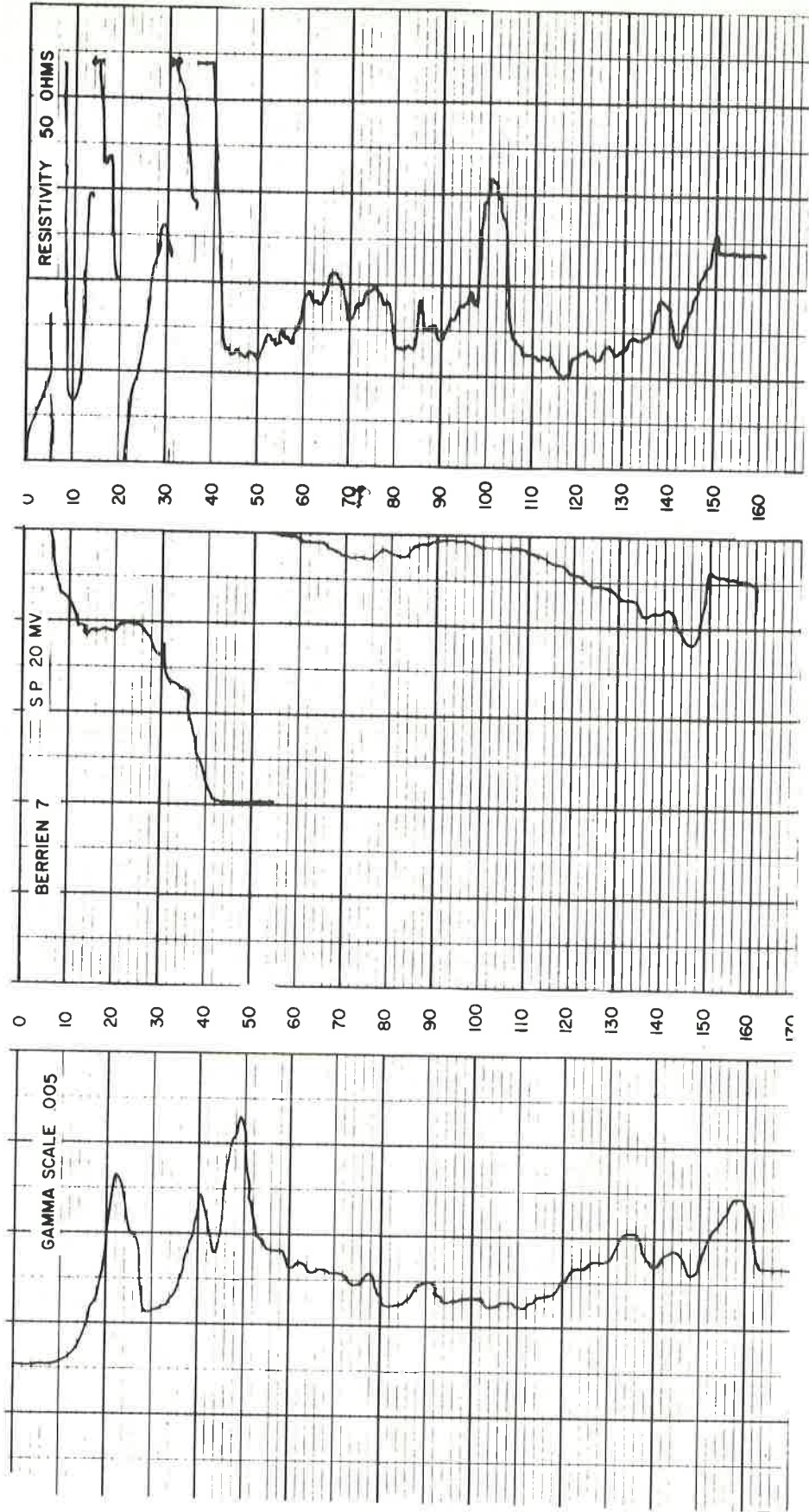


Figure BE-2. Electric and Gamma-Ray Logs - Berrien County Hole Re-7

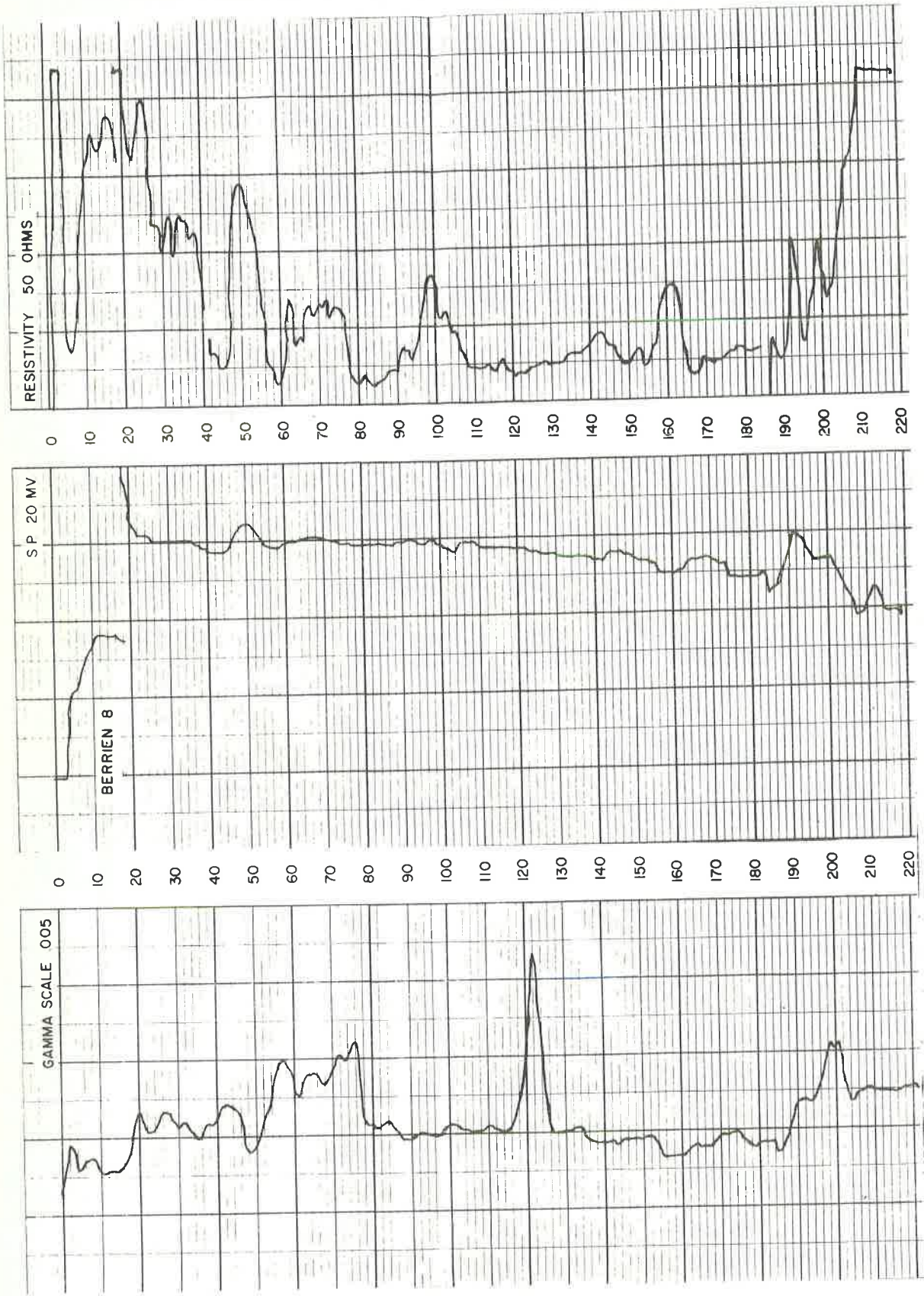


Figure PE-2. Electric and Gamma-Ray Logs - Berrien County  
Hole Be-8

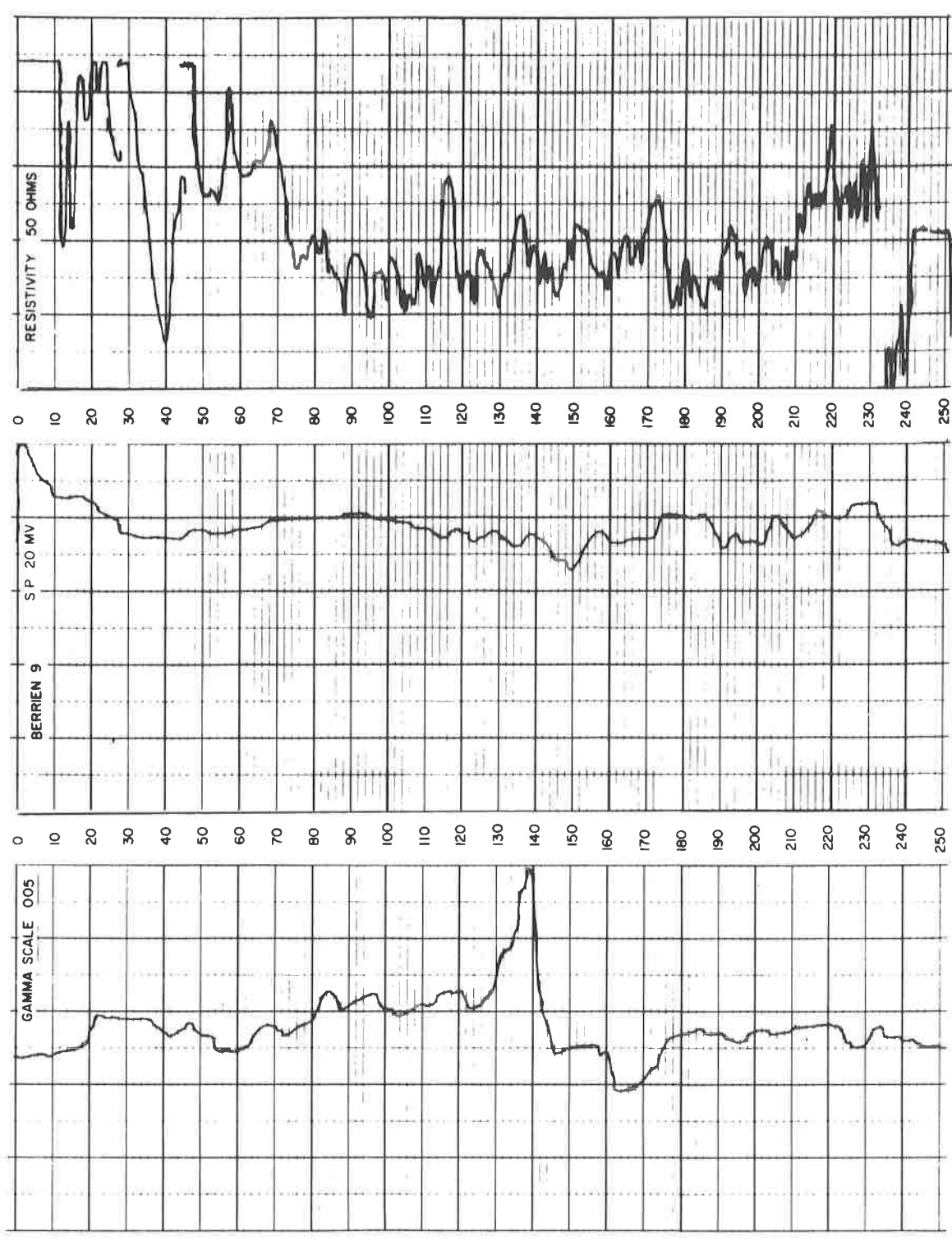


Figure BE-2. Electric and Gamma-Ray Logs - Berrien County Hole Pe-9

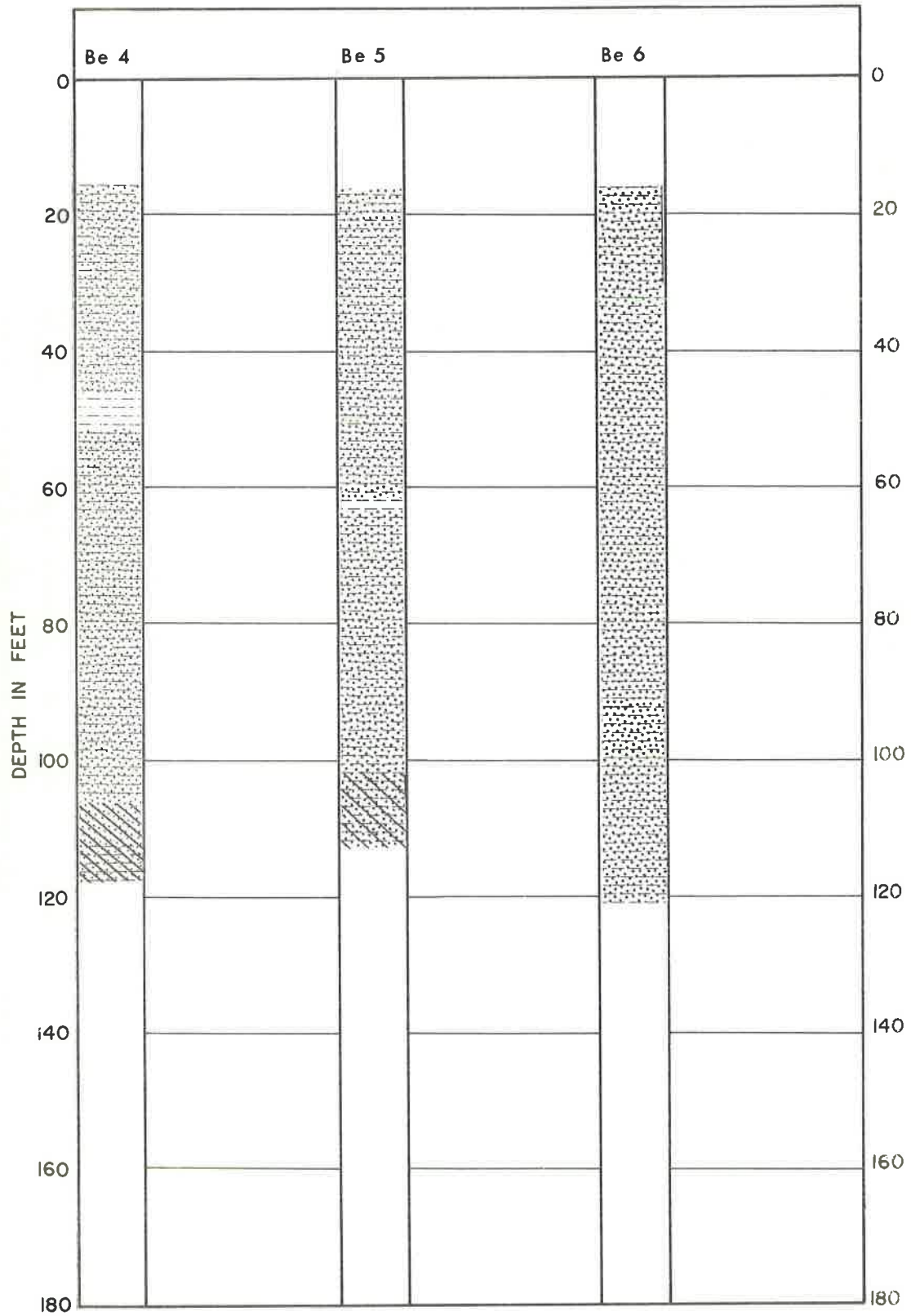


Figure Be-3. Lithologic Logs - Berrien County



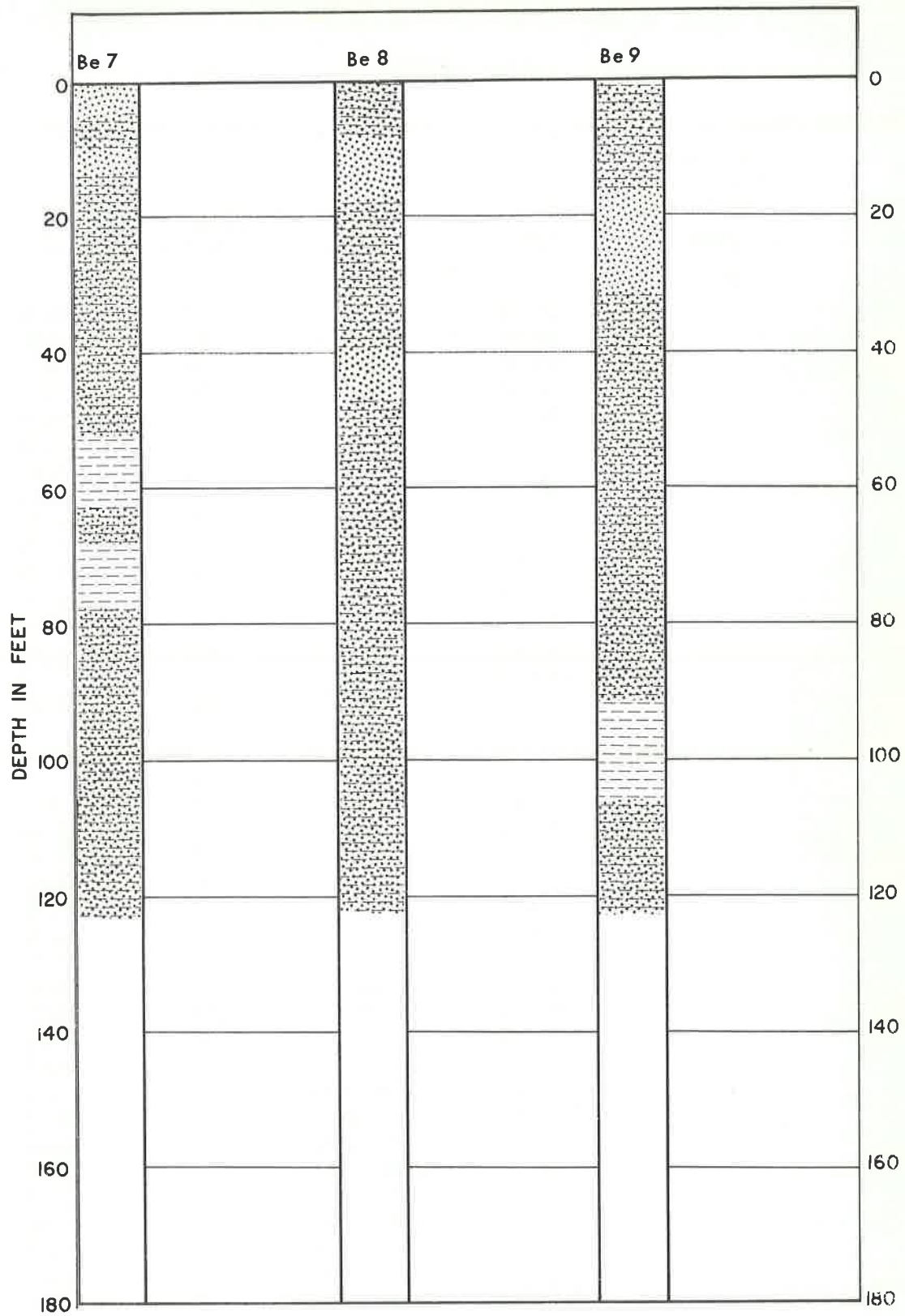


Figure Be-3. Lithologic Logs - Berrien County (Cont.)

TABLE BE-I  
BPL DETERMINATION ON CORES  
Berrien County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Be-4        | 207   | 0-16           | -             | -   | -        |
|             |   | 16-22          | 5             | 83  | 0.30     |
|             |   | 22-29          | 4             | 57  | 1.89     |
|             |   | 29-31          | 1             | 50  | 0        |
|             |   | 31-36          | 5             | 100 | 0        |
|             |   | 36-46          | 5             | 50  | 0.17     |
|             |   | 46-51          | 5             | 100 | 0.81     |
|             |   | 51-56          | 5             | 100 | 0.64     |
|             |   | 56-61          | 5             | 100 | 0.20     |
|             |   | 61-72          | 5             | 44  | 6.10     |
|             |   | 72-77          | 5             | 100 | 6.81     |
|             |   | 77-82          | 5             | 100 | 7.89     |
|             |   | 82-87          | 5             | 100 | 5.56     |
|             |   | 87-91          | 4             | 100 | 4.69     |
|             |   | 91-106         | 12            | 80  | 4.62     |
|             |   | 106-112        | 4             | 67  | 0.67     |
| 112-117     | 5   | 100            | 0.71          |     |          |
| Be-5        | 220   | 0-16           | -             | -   | -        |
|             |   | 16-31          | 10            | 67  | 0        |
|             |   | 31-46          | 8             | 53  | 5.26     |
|             |   | 46-61          | 11            | 73  | 5.90     |
|             |   | 61-63          | 1             | 50  | 8.80     |
|             |   | 63-68          | 5             | 100 | 6.54     |
|             |   | 68-73          | 5             | 100 | 6.31     |
|             |   | 73-76          | 3             | 100 | 8.09     |
|             |   | 76-91          | 11            | 73  | 2.43     |
|             |   | 91-102         | 9             | 82  | 2.70     |
|             |   | 102-112        | 3             | 30  | 1.62     |
|             |   | 112-122        | 8             | 80  | 2.66     |
|             |   | 122-125        | Wash Sample   | -   | 1.96     |
|             |   | 125-130        | Wash Sample   | -   | 2.53     |
|             |   | 130-135        | Wash Sample   | -   | 2.29     |
|             |   | 135-140        | Wash Sample   | -   | 3.20     |
|             |   | 140-145        | Wash Sample   | -   | 2.66     |
|             |   | 145-150        | Wash Sample   | -   | 2.87     |
|             |   | 150-155        | Wash Sample   | -   | 1.96     |
| 155-160     | Wash Sample                                 | -              | 1.75          |     |          |
| 160-165     | Wash Sample                                 | -              | -             |     |          |

(Continued)

TABLE BE-I (Continued)  
 BPL DETERMINATION ON CORES  
 BERRIEN COUNTY

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Be-5        | 220   | 165-170        | Wash Sample   | -   | 1.32     |
|             |   | 170-175        | Wash Sample   | -   | 1.08     |
| Be-6        | 201   | 0-5            | Wash Sample   | -   | 0        |
|             |   | 5-10           | Wash Sample   | -   | 0        |
|             |   | 10-15          | Wash Sample   | -   | 0        |
|             |   | 16-21          | 5             | 100 | 0        |
|             |   | 21-26          | 5             | 100 | 0        |
|             |   | 26-31          | 5             | 100 | 0        |
|             |   | 31-36          | 5             | 100 | 0        |
|             |   | 36-41          | 5             | 100 | 0        |
|             |   | 41-46          | 5             | 100 | 0        |
|             |   | 46-51          | 5             | 100 | 0        |
|             |   | 51-56          | 5             | 100 | 0        |
|             |   | 56-61          | 5             | 100 | 0        |
|             |   | 61-66          | 5             | 100 | 0        |
|             |   | 66-76          | 10            | 100 | .30      |
|             |   | 76-91          | 15            | 100 | 1.08     |
|             |   | 91-106         | 15            | 100 | 9.07     |
|             |   | 106-121        | 15            | 100 | 12.38    |
|             |   | 121-125        | Wash Sample   | -   | 8.94     |
|             |   | 125-130        | Wash Sample   | -   | 6.91     |
|             |   | 130-135        | Wash Sample   | -   | 8.60     |
|             |   | 135-140        | Wash Sample   | -   | 4.72     |
| 140-145     | Wash Sample                                 | -              | 5.06          |     |          |
| 145-150     | Wash Sample                                 | -              | 5.06          |     |          |
| 150-155     | Wash Sample                                 | -              | 6.20          |     |          |
| 155-160     | Wash Sample                                 | -              | -             |     |          |
| 160-165     | Wash Sample                                 | -              | 4.89          |     |          |
| Be-7        | 193   | 0-5            | 2             | 40  | 0        |
|             |   | 5-8            | 2             | 67  | 0        |
|             |   | 8-10           | 2             | 100 | 0        |
|             |   | 10-13          | 1             | 33  | 0        |
|             |   | 13-16          | 3             | 100 | 0        |
|             |   | 16-19          | 3             | 100 | 0        |
|             |   | 19-32          | 7             | 54  | 0        |
|             |   | 32-47          | 8             | 53  | 0        |
|             |   | 47-52          | 5             | 100 | 0        |
|             |   | 52-62          | 4             | 40  | 0        |
|             |   | 62-77          | 15            | 100 | .44      |
| 77-92       | 15  | 100            | 3.32          |     |          |

(Continued)

TABLE BE-I (Continued)  
 BPL DETERMINATION ON CORES  
 Berrien County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |      |
|-------------|---|----------------|---------------|-----|----------|------|
|             |   |                | Feet          | %   |          |      |
| Be-7        | 193   | 92-107         | 12            | 80  | 5.90     |      |
|             |   | 107-122        | 13            | 87  | 2.53     |      |
|             |   | 122-125        | Wash Sample   | -   | -        | 2.19 |
|             |   | 125-130        | Wash Sample   | -   | -        | 1.51 |
|             |   | 130-135        | Wash Sample   | -   | -        | 2.90 |
|             |   | 135-140        | Wash Sample   | -   | -        | 2.16 |
|             |   | 140-145        | Wash Sample   | -   | -        | 1.08 |
|             |   | 145-150        | Wash Sample   | -   | -        | 1.15 |
|             |   | 150-155        | Wash Sample   | -   | -        | 1.48 |
|             |   | 155-160        | Wash Sample   | -   | -        | 1.52 |
|             |   | 160-165        | Wash Sample   | -   | -        | 1.38 |
|             |   | 165-170        | Wash Sample   | -   | -        | 1.75 |
|             |   | 170-175        | Wash Sample   | -   | -        | 1.38 |
|             |   | 175-180        | Wash Sample   | -   | -        | 1.58 |
|             |   | 180-185        | Wash Sample   | -   | -        | 1.42 |
|             |   | Be-8           | 245           | 0-3 | 2        | 67   |
| 3-6         | 3   |                |               | 100 | 0        |      |
| 6-9         | 2   |                |               | 67  | 0        |      |
| 9-12        | 3   |                |               | 100 | 0        |      |
| 12-18       | 6   |                |               | 100 | 0        |      |
| 18-32       | 6   |                |               | 43  | 0        |      |
| 32-40       | 8   |                |               | 100 | 0        |      |
| 40-47       | 2   |                |               | 29  | 0        |      |
| 47-62       | 5   |                |               | 33  | 0        |      |
| 62-77       | 6   |                |               | 40  | .67      |      |
| 77-92       | 15  |                |               | 100 | 6.07     |      |
| 92-98       | 4   |                |               | 67  | 1.01     |      |
| 98-112      | 6   |                |               | 43  | 1.35     |      |
| 112-122     | 10  |                |               | 100 | 3.03     |      |
| 122-125     | Wash Sample                                 |                |               | -   | -        | 1.01 |
| 125-130     | Wash Sample                                 |                |               | -   | -        | 2.70 |
| 130-135     | Wash Sample                                 |                |               | -   | -        | 3.37 |
| 135-140     | Wash Sample                                 |                |               | -   | -        | 4.05 |
| 140-145     | Wash Sample                                 |                |               | -   | -        | 2.70 |
| 145-150     | Wash Sample                                 |                |               | -   | -        | 4.38 |
| 150-155     | Wash Sample                                 |                |               | -   | -        | 3.71 |
| 155-160     | Wash Sample                                 |                |               | -   | -        | 2.02 |
| 160-165     | Wash Sample                                 |                |               | -   | -        | 1.01 |
| 165-170     | Wash Sample                                 |                |               | -   | -        | 1.72 |
| 170-175     | Wash Sample                                 |                |               | -   | -        | 1.01 |
| 175-180     | Wash Sample                                 |                |               | -   | -        | 1.01 |
| 180-185     | Wash Sample                                 |                |               | -   | -        | 1.35 |

(Continued)

TABLE BE-I (Continued)

## BPL DETERMINATION ON CORES

Berrien County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Be-8        | 245   | 185-190        | Wash Sample   | -   | 0        |
|             |   | 190-195        | Wash Sample   | -   | 2.70     |
|             |   | 195-200        | Wash Sample   | -   | .67      |
|             |   | 200-205        | Wash Sample   | -   | .67      |
|             |   | 205-210        | Wash Sample   | -   | 1.01     |
|             |   | 210-215        | Wash Sample   | -   | 1.69     |
| Be-9        | 220   | 0-3            | 2             | 67  | 0        |
|             |   | 3-6            | 3             | 100 | 0        |
|             |   | 6-9            | 2             | 67  | 0        |
|             |   | 9-12           | 3             | 100 | 0        |
|             |   | 12-16          | 4             | 100 | 0        |
|             |   | 16-31          | 1             | 7   | 0        |
|             |   | 31-36          | 5             | 100 | 0        |
|             |   | 36-46          | 5             | 50  | 0        |
|             |   | 46-61          | 15            | 100 | 0        |
|             |   | 61-76          | 15            | 100 | 0        |
|             |   | 76-91          | 15            | 100 | 0        |
|             |   | 91-106         | 15            | 100 | 0        |
|             |   | 106-121        | 15            | 100 | 0        |
|             |   | 121-125        | Wash Sample   | -   | 0        |
|             |   | 125-130        | Wash Sample   | -   | 0        |
|             |   | 130-135        | Wash Sample   | -   | 0        |
|             |   | 135-140        | Wash Sample   | -   | 0        |
|             |   | 140-145        | Wash Sample   | -   | 1.82     |
|             |   | 145-150        | Wash Sample   | -   | 2.22     |
|             |   | 150-155        | Wash Sample   | -   | 2.33     |
|             |   | 155-160        | Wash Sample   | -   | 1.04     |
|             |   | 160-165        | Wash Sample   | -   | 0.71     |
|             |   | 165-170        | Wash Sample   | -   | 2.36     |
|             |   | 170-175        | Wash Sample   | -   | 2.12     |
|             |   | 175-180        | Wash Sample   | -   | 1.85     |
|             |   | 180-185        | Wash Sample   | -   | 0.88     |
|             |   | 185-190        | Wash Sample   | -   | 2.19     |
| 190-195     | Wash Sample                                 | -              | 4.28          |     |          |
| 195-200     | Wash Sample                                 | -              | 3.94          |     |          |
| 200-205     | Wash Sample                                 | -              | 1.58          |     |          |
| 205-210     | Wash Sample                                 | -              | 1.75          |     |          |
| 210-215     | Wash Sample                                 | -              | 2.02          |     |          |

(Continued)

TABLE BE-I (Continued)  
 BPL DETERMINATION ON CORES  
 Berrien County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |   | BPL<br>% |
|-------------|---|----------------|---------------|---|----------|
|             |   |                | Feet          | % |          |
| Be-9        | 220   | 215-220        | Wash Sample   | - | 2.36     |
|             |   | 220-225        | Wash Sample   | - | 2.26     |
|             |   | 225-230        | Wash Sample   | - | 2.83     |
|             |   | 230-235        | Wash Sample   | - | 2.63     |
|             |   | 235-240        | Wash Sample   | - | 1.18     |
|             |   | 240-245        | Wash Sample   | - | 3.17     |
|             |   | 245-250        | Wash Sample   | - | 1.62     |
|             |   | 250-255        | Wash Sample   | - | 1.79     |
|             |   | 255-260        | Wash Sample   | - | 2.93     |
|             |   | 260-265        | Wash Sample   | - | 3.84     |
|             |   | 265-270        | Wash Sample   | - | 3.88     |
|             |   | 270-275        | Wash Sample   | - | 7.01     |
|             |   | 275-280        | Wash Sample   | - | 8.70     |
|             |   | 280-285        | Wash Sample   | - | 8.16     |
|             |   | 285-290        | Wash Sample   | - | 6.64     |
| 290-295     | Wash Sample                                 | -              | 6.24          |   |          |

TABLE BE-II  
 MATRIX BENEFICIATION RESULTS  
 BERRIEN COUNTY

| HOLE NO.             | BE-06 | MATRIX INTERVAL = 91-121 | BERRIEN COUNTY |       |       |       |               |        |         |               |       |               |                 |  |  |  |  |
|----------------------|-------|--------------------------|----------------|-------|-------|-------|---------------|--------|---------|---------------|-------|---------------|-----------------|--|--|--|--|
|                      |       |                          | FEED           | +4    | 4X8   | 8X16  | F F<br>16X150 | (16X35 | 35X150) | SLIME<br>-150 | (CONC | F.A.<br>TAILS | AMINE<br>FLOAT) |  |  |  |  |
|                      |       |                          | 30             |       |       |       |               |        |         |               |       |               |                 |  |  |  |  |
| TOTAL MATRIX FOOTAGE |       |                          | 74.70          |       |       |       |               |        |         |               |       |               |                 |  |  |  |  |
| DRY DENSITY LB/CU FT |       |                          | 100.0          |       |       |       |               |        |         |               |       |               |                 |  |  |  |  |
| PERCENT DRY WEIGHT   |       |                          | 11.97          | .61   | 1.11  | 2.22  | 50.78         | 6.40   | 44.38   | 45.27         | 10.85 | 83.92         | 5.23            |  |  |  |  |
| PERCENT SPL          |       |                          | 79.57          | 51.43 | 63.23 | 54.46 | 12.31         | 22.26  | 9.44    | 7.71          | 75.54 | .84           | 7.08            |  |  |  |  |
| PERCENT ACID INSOL   |       |                          | 3.56           | 17.57 | 16.26 | 29.71 | 85.75         | 72.41  | 88.52   | 77.48         | 8.42  | 97.97         | 91.30           |  |  |  |  |
| PERCENT IRON OXIDE   |       |                          | 4.87           | 14.08 | 3.91  | 2.94  | .47           | .69    | .49     | 6.91          | .78   | .18           | 1.64            |  |  |  |  |
| PERCENT ALUM OXIDE   |       |                          | 7.00           | 2.14  | 1.94  | 2.46  | 1.29          | 1.12   | 1.31    | 9.11          | 1.37  | .94           | 3.21            |  |  |  |  |
| PERCENT CALC OXIDE   |       |                          |                | 31.48 | 37.78 | 32.88 | 5.60          | 12.94  | 4.90    | 6.21          | 50.40 | .70           | 7.34            |  |  |  |  |

TABLE BE-III  
ECONOMIC FACTORS - FIGURES OF MERIT

|                                     |                     | WELL NO. BE-06      |                |
|-------------------------------------|---------------------|---------------------|----------------|
|                                     |                     | INDIVIDUAL MATRICES |                |
| MATRIX NO.                          | DEPTH INTERVAL, FT. | 1<br>91-121         |                |
| ECONOMIC FACTORS *<br>UNIT (M=1000) |                     |                     |                |
| * OVERBURDEN                        |                     | FT.<br>MT/AC        | 91.00<br>178.4 |
| * MATRIX                            |                     | FT.<br>MT/AC        | 30.00<br>48.8  |
| * BPL IN MATRIX                     |                     | PERCENT<br>MT/AC    | 11.97<br>5.8   |
| * OVERBURDEN/MATRIX                 |                     | RATIO               | 3.03           |
| WASH-SCREEN PRODUCTS                |                     |                     |                |
| +16 MESH                            |                     | MT/AC               | 1.9            |
| -16+150 MESH                        |                     | MT/AC               | 24.8           |
| -150 MESH (LOSS)                    |                     | MT/AC               | 22.1           |
| * FLOTATION CONCENTRATE PRODUCT     |                     | MT/AC               | 2.7            |
| * TOTAL USEFUL PRODUCTS**           |                     | MT/AC               | 4.6            |
| BPL RECOVERY                        |                     |                     |                |
| +16 MESH                            |                     | MT/AC               | 1.1            |
| -16+150 (FLOT. CONC.)               |                     | PERCENT BPL         | 75.5           |
| -16+150 (FLOT. CONC.)               |                     | MT/AC               | 2.0            |
| * TOTAL                             |                     | MT/AC               | 3.1            |
| * RECOVERED FROM MATRIX             |                     | PERCENT             | 53.38          |
| * OVERBURDEN / PRODUCT              |                     | CU YD/T             | 38.3           |
| * MATRIX / PRODUCTS                 |                     | CU YD/T             | 10.49          |
| * 1+A IN FLOT. CONC.                |                     | PERCENT             | 2.15           |
| FIGURES OF MERIT                    |                     |                     |                |
| OVERBURDEN                          | UNIT                | ECON. LEVEL         |                |
| MATRIX                              | FT                  | 88 MAX              | .97            |
| MATRIX BPL                          | PERCENT             | 3 MIN               | 10.00          |
| BPL IN FLOT. CONC. (1)              | PERCENT             | 10 MIN              | 1.20           |
| BPL IN FLOT. CONC. (2)              | PERCENT             | 66 MIN              | 1.14           |
| OVERBURDEN/MATRIX                   | RATIO               | 2 MAX               | 1.45           |
| OVERBURDEN/PRODUCTS                 | CU YD/T             | 17.5 MAX            | .66            |
| 1+A IN FLOT. CONC.                  | PERCENT             | 5 MAX               | .46            |
| PRODUCTS RECOVERY                   | T/AC-FT             | 400 MIN             | 2.33           |
| BPL (+150) RECOVERY                 | PERCENT             | 63 MIN              | .38            |
| MATRIX/PRODUCTS                     | CU YD/T             | 6 MAX               | .85            |
|                                     |                     |                     | .57            |

(1) FOR NET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
NOTES: OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY



BROOKS COUNTY

BROOKS COUNTY  
SUMMARY OF RESULTS

Brooks County holes 3 through 7 are reported herein. None of the holes contained sufficient phosphorite to warrant beneficiation tests.

Electric and gamma-ray logs were not run on holes Br-3, Br-5, and Br-7 because of a priority use of the logging equipment on the other drilling rig.

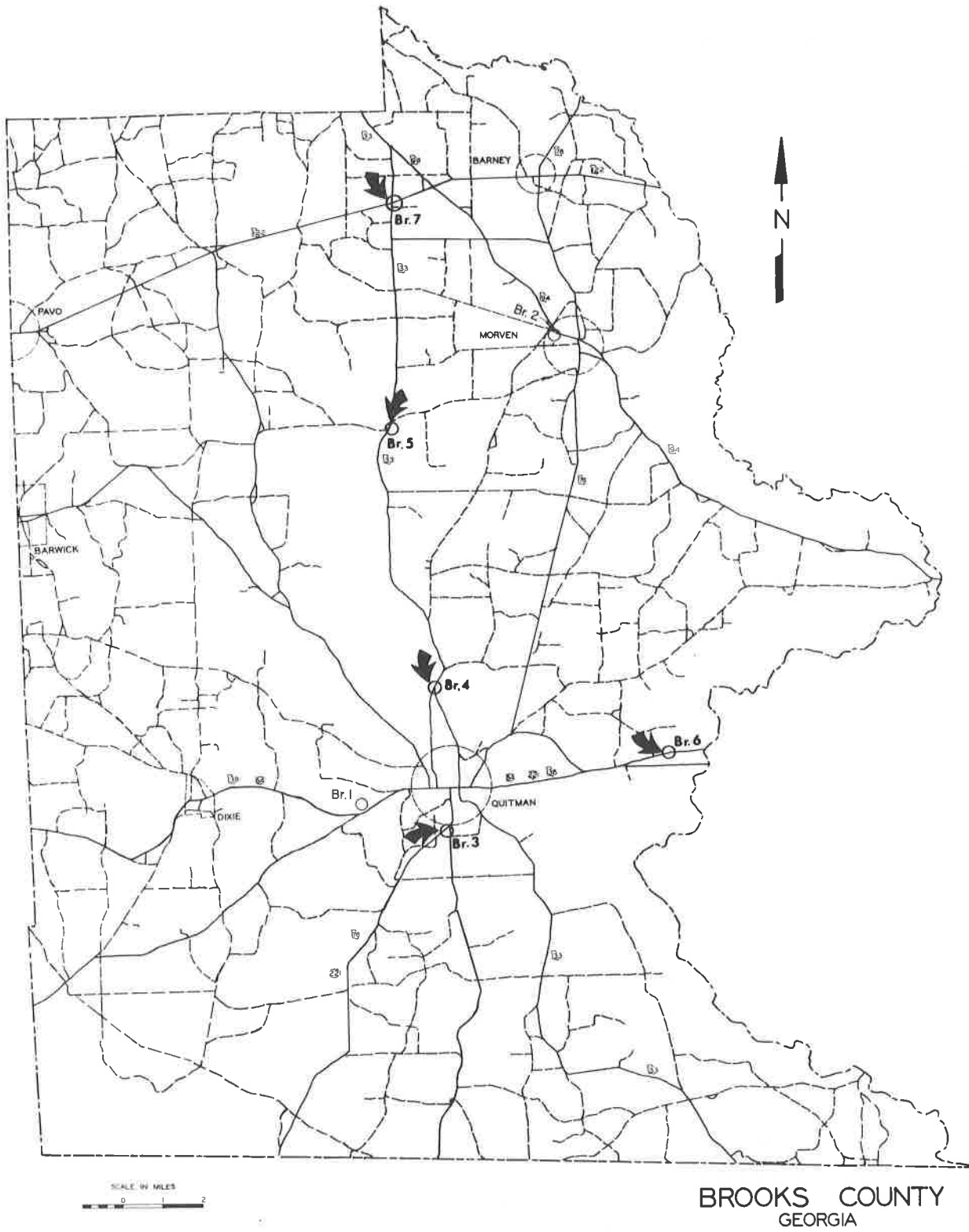


Figure BR-1. Location of Holes - Brooks County

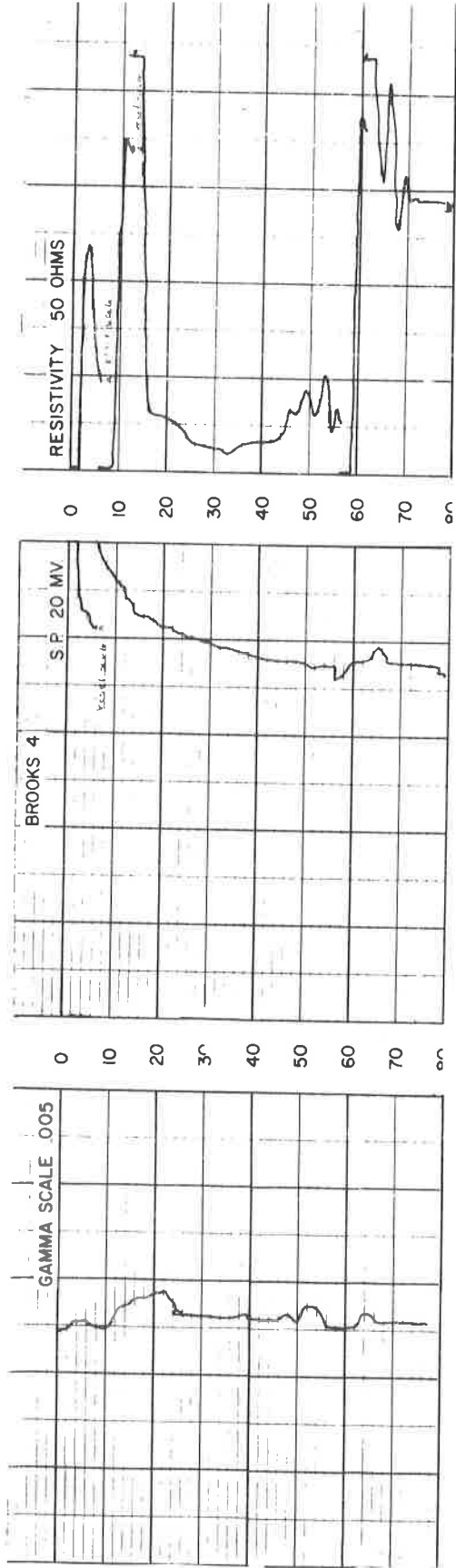


Figure BR-2. Electric and Gamma-Ray Logs - Brooks County  
Hole Br-4

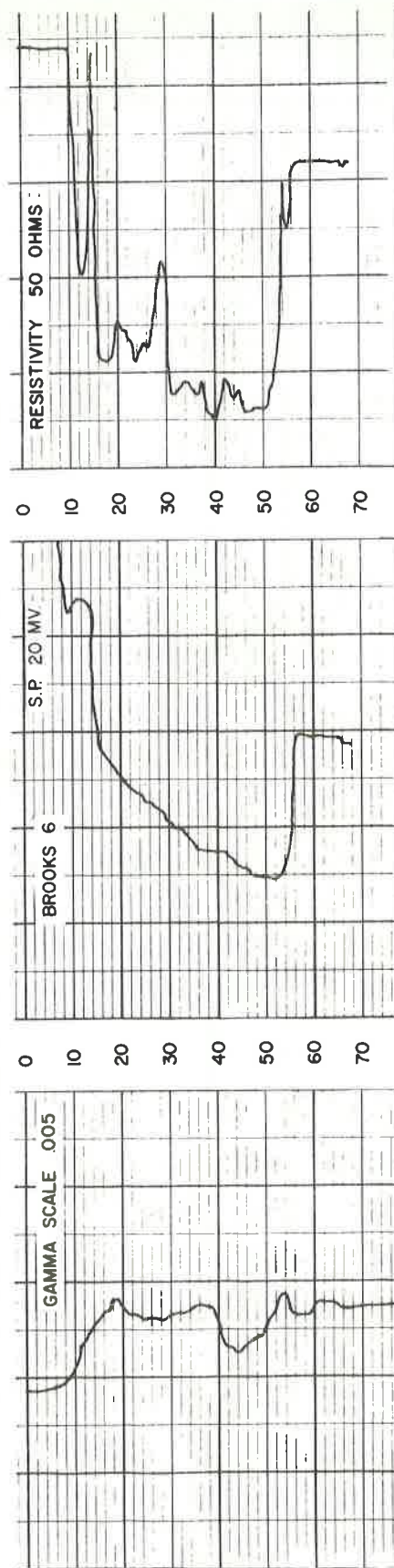


Figure BR-2. Electric and Gamma-Ray Logs - Brooks County  
Hole Br-6

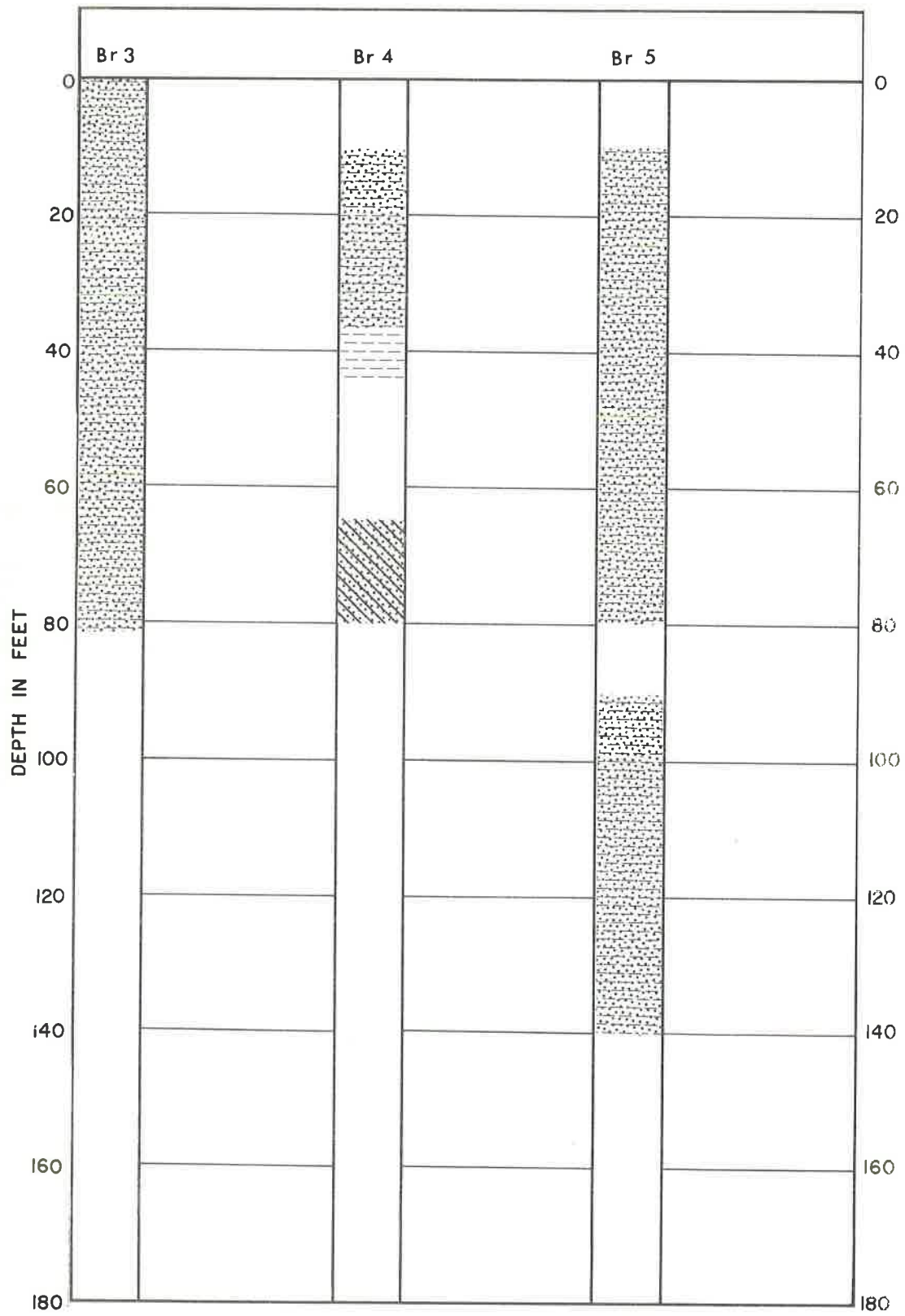


Figure Br-3. Lithologic Logs - Brooks County

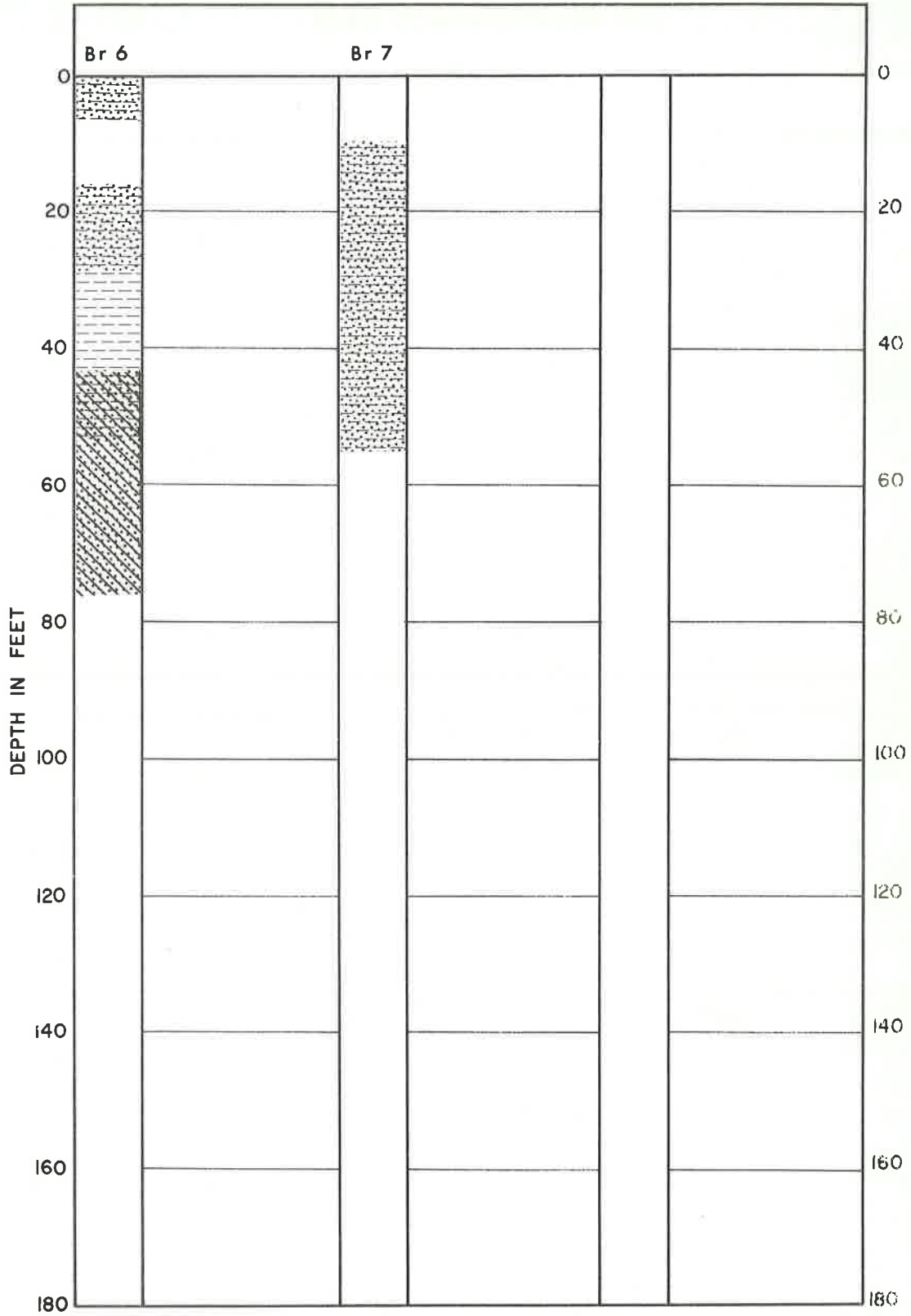


Figure Br-3. Lithologic Logs - Brooks County (Cont.)

TABLE BR-I  
BPL DETERMINATION ON CORES

## Brooks County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Br-3        | 205   | 0-3            | 2             | 67  | 0        |
|             |   | 3-6            | 2             | 67  | 0        |
|             |   | 6-9            | 2             | 67  | 0        |
|             |   | 9-12           | 2             | 67  | 0        |
|             |   | 12-22          | 3             | 30  | 0        |
|             |   | 22-30          | 2             | 25  | 0        |
|             |   | 30-40          | 3             | 30  | 1.35     |
|             |   | 40-45          | 4             | 80  | 0.40     |
|             |   | 45-50          | 4             | 80  | 0.67     |
|             |   | 50-55          | 5             | 100 | 0.57     |
|             |   | 55-60          | 4             | 80  | 4.18     |
|             |   | 60-65          | 5             | 100 | 3.00     |
|             |   | 65-70          | 3             | 60  | 3.07     |
|             |   | 70-80          | 7             | 70  | 4.25     |
| 80-90       | 10  | 100            | 9.51          |     |          |
| Br-4        | 139   | 0-10           | -             | -   | -        |
|             |   | 10-20          | 7             | 70  | 0        |
|             |   | 20-30          | 3             | 30  | 0        |
|             |   | 30-35          | 5             | 100 | 1.75     |
|             |   | 35-37          | 2             | 100 | 3.30     |
|             |   | 37-45          | 8             | 100 | 1.01     |
|             |   | 46-65          | -             | -   | -        |
|             |   | 65-75          | 6             | 60  | 0        |
|             |   | 75-80          | 2             | 40  | 0        |
| Br-5        | 202   | 0-10           | -             | -   | -        |
|             |   | 10-20          | 5             | 50  | 0        |
|             |   | 20-25          | 5             | 100 | 0        |
|             |   | 25-30          | 4             | 80  | 0        |
|             |   | 30-35          | 5             | 100 | 5.06     |
|             |   | 35-39          | 4             | 100 | 6.81     |
|             |   | 39-40          | 1             | 100 | 1.18     |
|             |   | 40-45          | 4             | 80  | 1.79     |
|             |   | 45-50          | 5             | 100 | 1.96     |
|             |   | 50-55          | 5             | 100 | 0        |
|             |   | 55-60          | 3             | 60  | 0        |
| 60-65       | 5   | 100            | 1.08          |     |          |

(Continued)



TABLE BR-I (Continued)  
 BPL DETERMINATION ON CORES  
 Brooks County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Br-5        | 202   | 65-70          | 5             | 100 | 1.69     |
|             |   | 70-80          | 4             | 40  | 2.33     |
|             |   | 80-90          | -             | -   | -        |
|             |   | 90-95          | 5             | 100 | 5.46     |
|             |   | 95-100         | 5             | 100 | 4.38     |
|             |   | 100-110        | 4             | 40  | 8.06     |
|             |   | 110-120        | 6             | 60  | 4.38     |
|             |   | 120-130        | 8             | 80  | 6.98     |
|             |   | 130-140        | 1             | 10  | 9.68     |
| Br-6        | 129   | 0-3            | 2             | 67  | 0        |
|             |   | 3-6            | 2             | 67  | 0        |
|             |   | 6-15           | -             | -   | -        |
|             |   | 15-28          | 12            | 92  | 1.38     |
|             |   | 28-31          | 3             | 100 | 2.19     |
|             |   | 31-43          | 10            | 83  | 1.69     |
|             |   | 43-46          | 1             | 33  | 0.74     |
|             |   | 46-53          | 4             | 57  | 0.94     |
|             |   | 53-66          | 2             | 15  | 0        |
|             |   | 66-76          | 5             | 50  | 0        |
| Br-7        | 230   | 0-10           | -             | -   | -        |
|             |   | 10-20          | 10            | 100 | 0        |
|             |   | 20-30          | 10            | 100 | 3.37     |
|             |   | 30-40          | 10            | 100 | 4.89     |
|             |   | 40-45          | 5             | 100 | 5.87     |
|             |   | 45-55          | 4             | 40  | 2.12     |
|             |   | 58             | W.S.          | -   | -        |



BULLOCH COUNTY

## BULLOCH COUNTY

## SUMMARY OF RESULTS

The two Bulloch County holes were chosen to test economic possibilities of relatively near surface phosphorite as reported in GGS wells numbers 432 and 553. Neither had sufficient phosphorite for beneficiation testing.

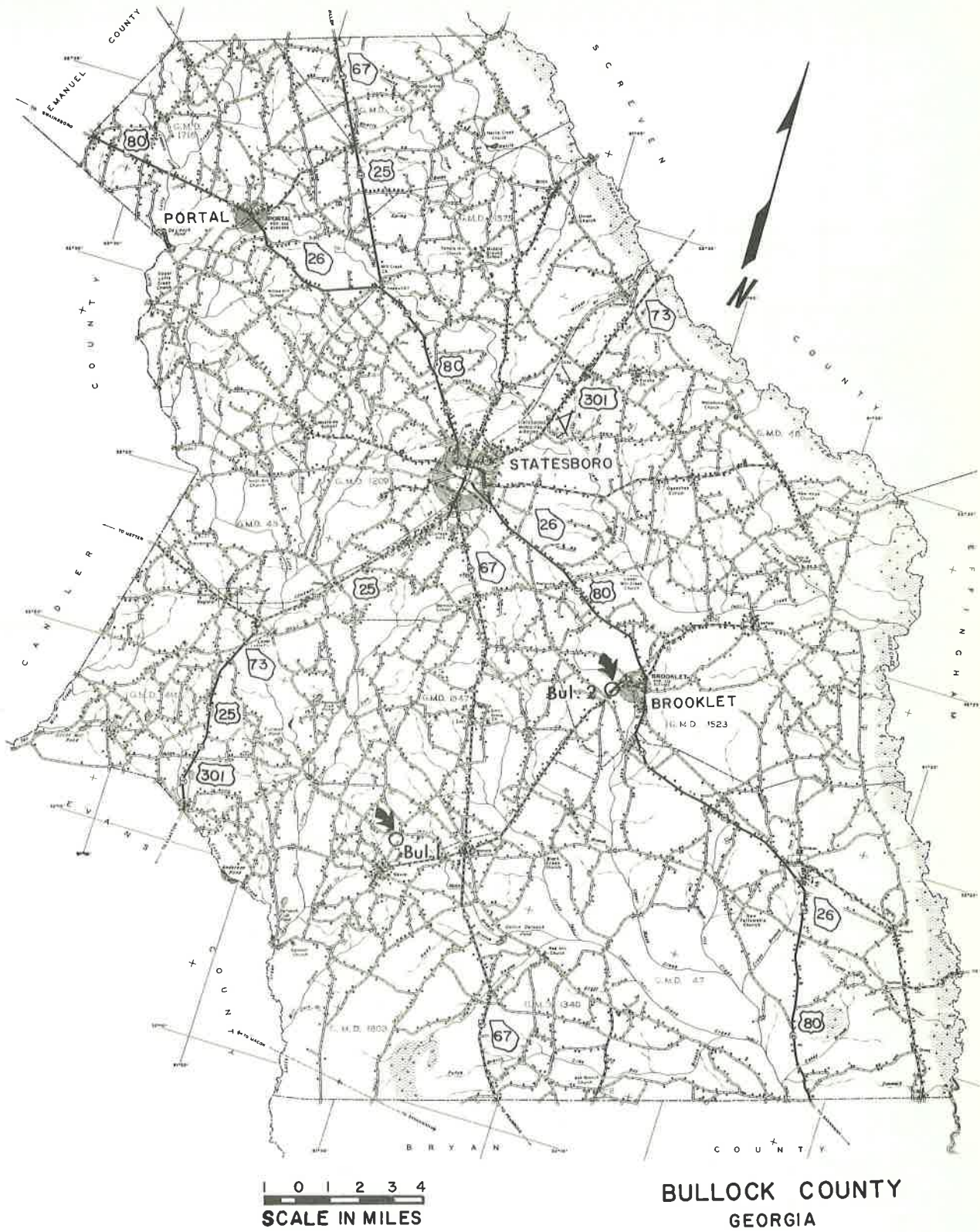


Figure BUL-1. Location of Holes - Bulloch County

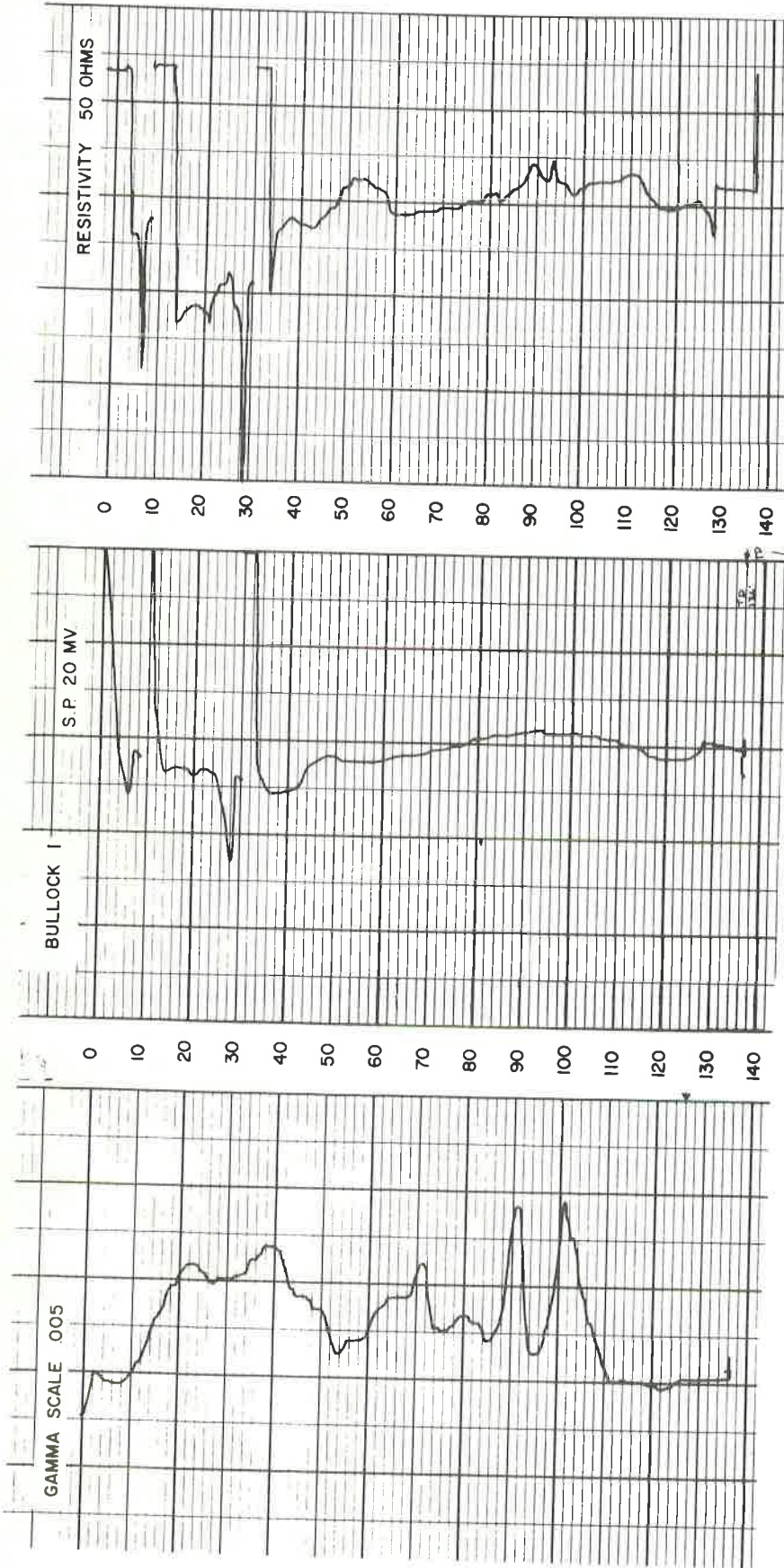


Figure BUL-2. Electric and Gamma-Ray Logs - Bulloch County Hole Bul-1

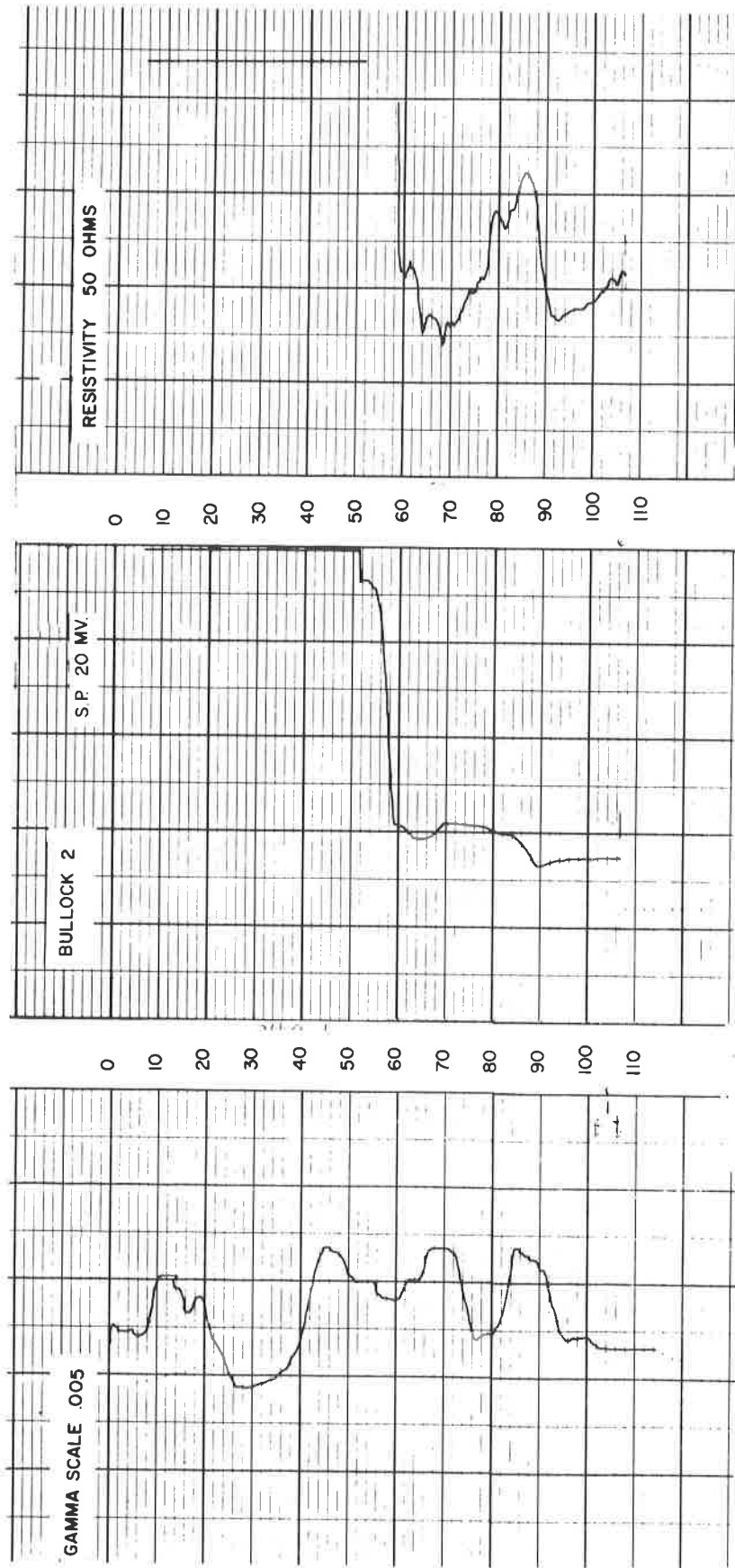


Figure BUL-2. Electric and Gamma-Ray Logs - Bulloch County Hole Bul-2

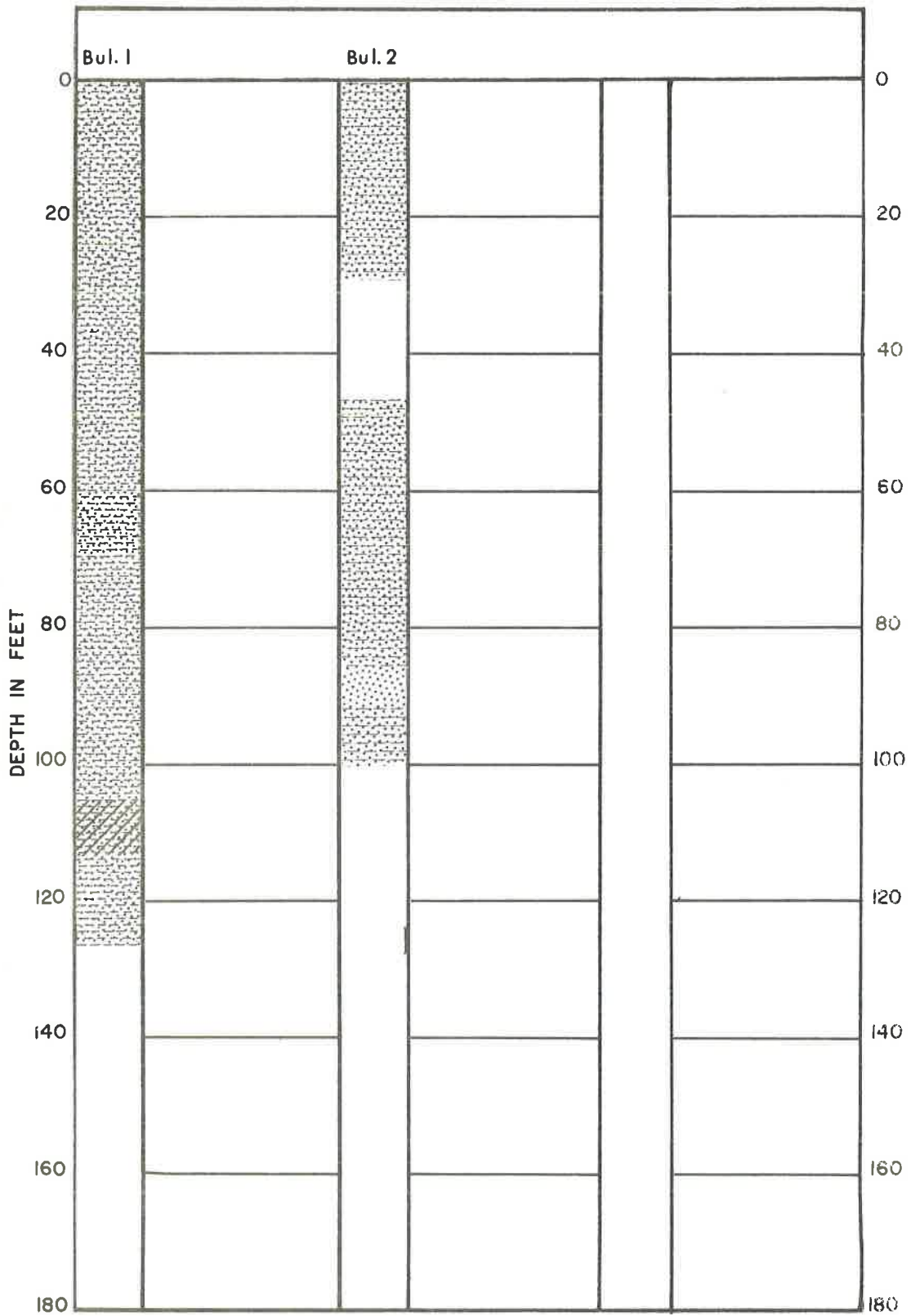


Figure BUL-3. Lithologic Logs - Bulloch County



TABLE BUL-I  
BPL DETERMINATION ON CORES  
Bulloch County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Bul-1       | 185   | 0-3            | 3             | 100 | 0        |
|             |   | 3-9            | 6             | 100 | 0        |
|             |   | 9-12           | 1             | 33  | 0        |
|             |   | 12-15          | 3             | 100 | 0        |
|             |   | 15-17          | 2             | 100 | 0        |
|             |   | 17-30          | 13            | 77  | 0        |
|             |   | 30-41          | 7             | 64  | 0        |
|             |   | 41-45          | 4             | 100 | 0        |
|             |   | 45-60          | 15            | 100 | 0        |
|             |   | 60-75          | 15            | 100 | 0        |
|             |   | 75-90          | 6             | 40  | 0        |
|             |   | 90-104         | 14            | 100 | 0        |
|             |   | 104-112        | 8             | 100 | 2.70     |
| 112-125     | 13  | 100            | 2.36          |     |          |
| Bul-2       | 165   | 0-16           | 12            | 75  | 0        |
|             |   | 16-29          | 11            | 85  | 0        |
|             |   | 46-61          | 15            | 100 | 0        |
|             |   | 61-75          | 9             | 64  | 0        |
|             |   | 75-85          | 10            | 100 | 0        |
|             |   | 85-90          | 5             | 100 | 0        |
|             |   | 90-100         | 10            | 100 | 0        |



CHATHAM COUNTY

CHATHAM COUNTY  
SUMMARY OF RESULTS

Chatham County holes 4A, 10, 11, 12, and 13 were drilled to give additional information for the State of Georgia in its consideration of a lease application by the Kerr-McGee Corporation for off-shore lands. These holes confirmed the existence of a phosphorite ore body that averages 65-67 percent BPL on beneficiation. The ore is similar in character to the North Carolina phosphorites that are being mined by the Texas-Gulf Corporation.

The depth of the holes permitted determination of the thickness of the aquiclude over one of the principal aquifers of the region. Due to cave-in of holes Ch-4A and Ch-11, electric logs were not run on these holes. Gamma-ray logs were run from inside the drill pipe. The electrical log was not run on Ch-10 because of the close proximity of a local power line and consequent electrical disturbances, but the gamma-ray was run.

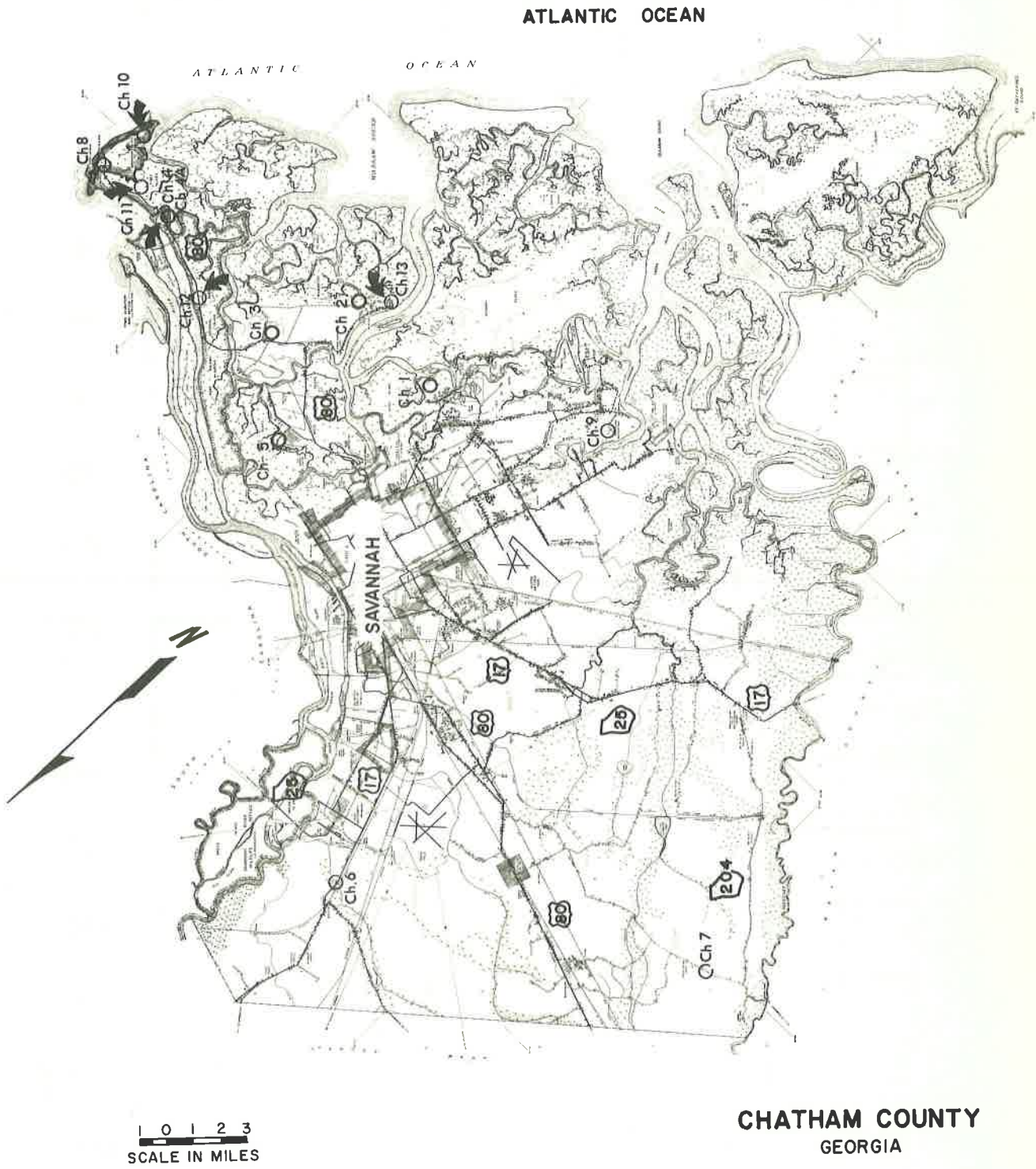


Figure CH-1. Location of Holes - Chatham County

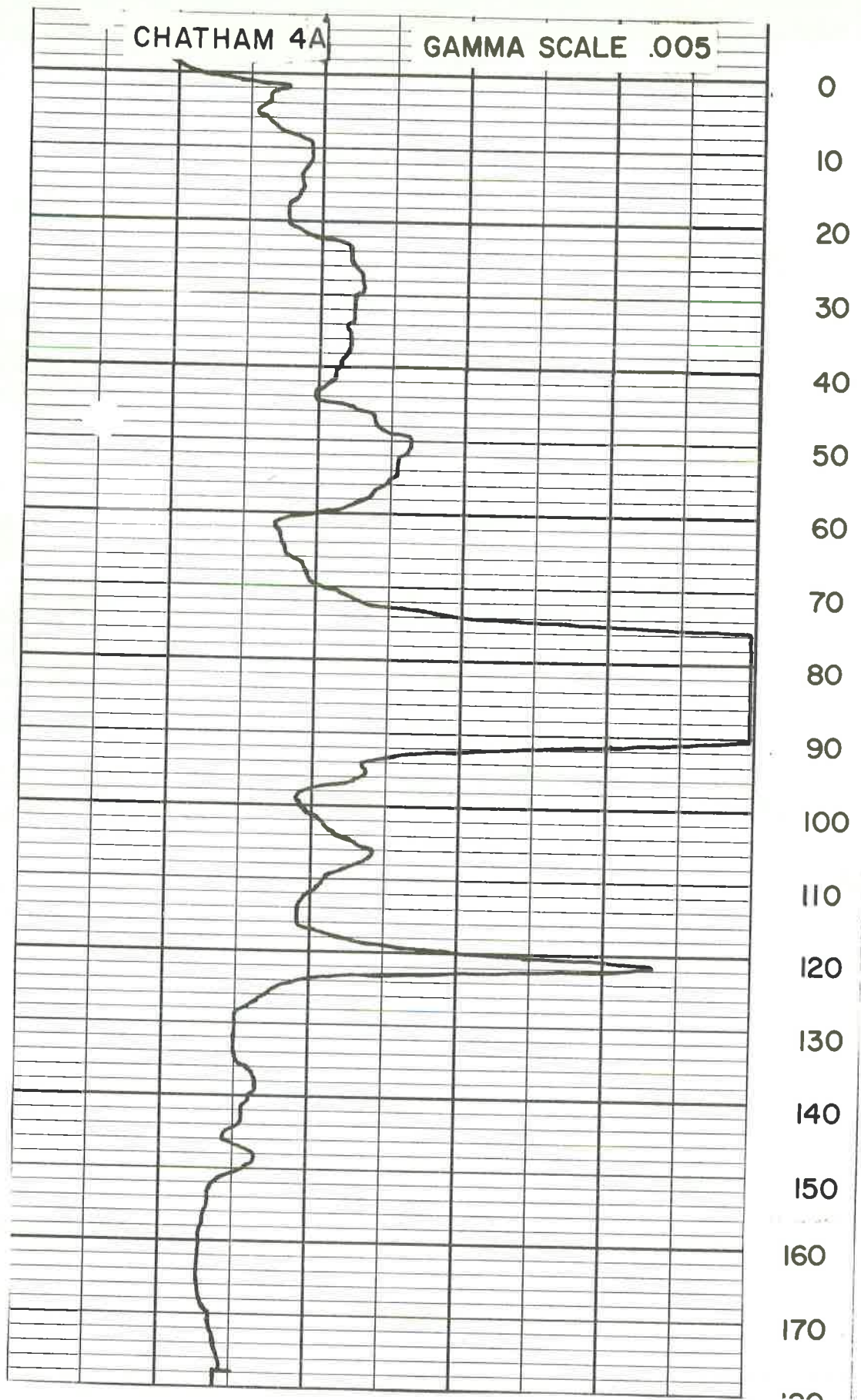


Figure CH-2. Gamma-Ray Logs - Chatham County  
Hole Ch-4A

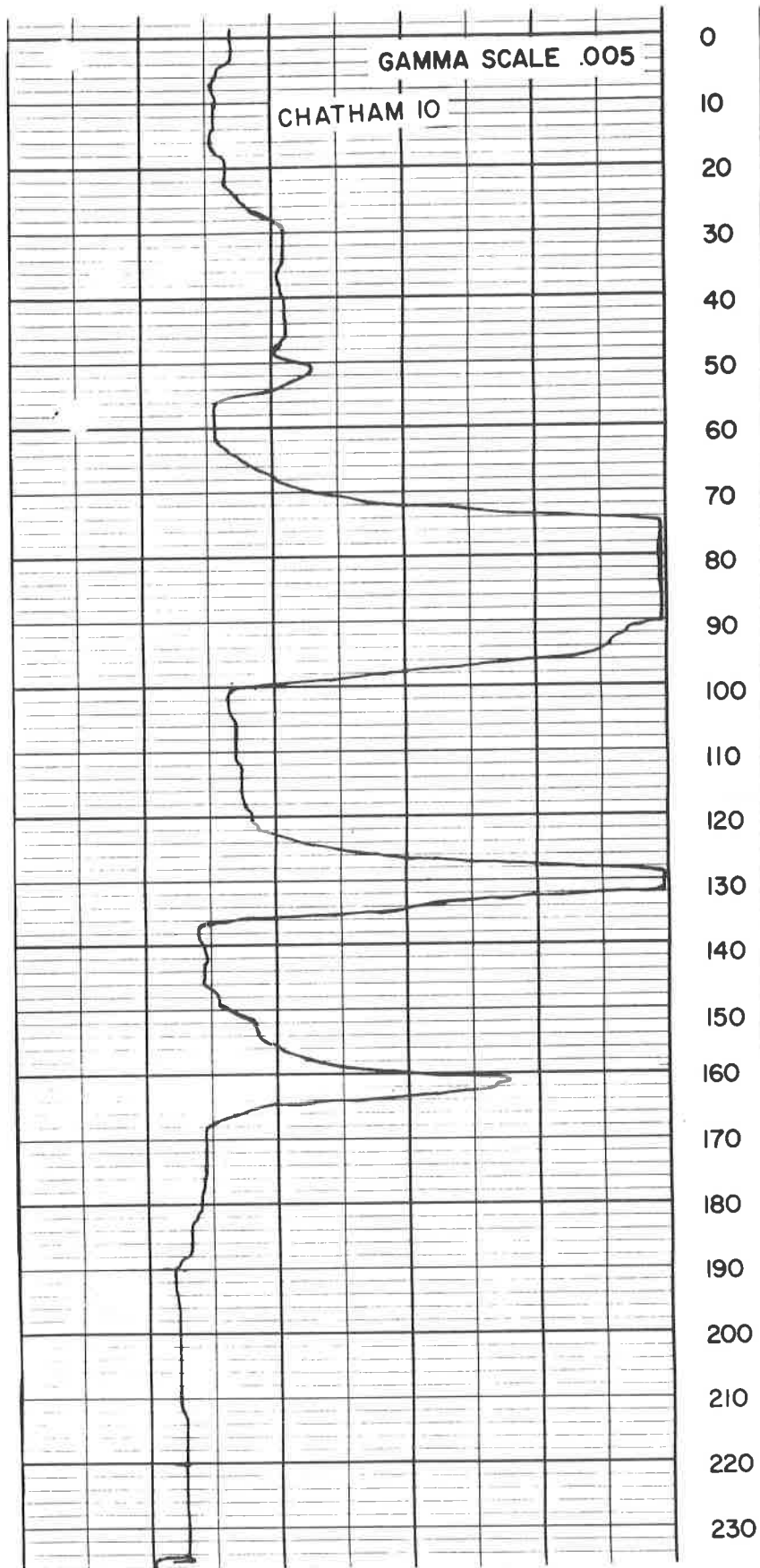


Figure CH-2. Gamma-Ray Logs - Chatham County  
Hole Ch-10

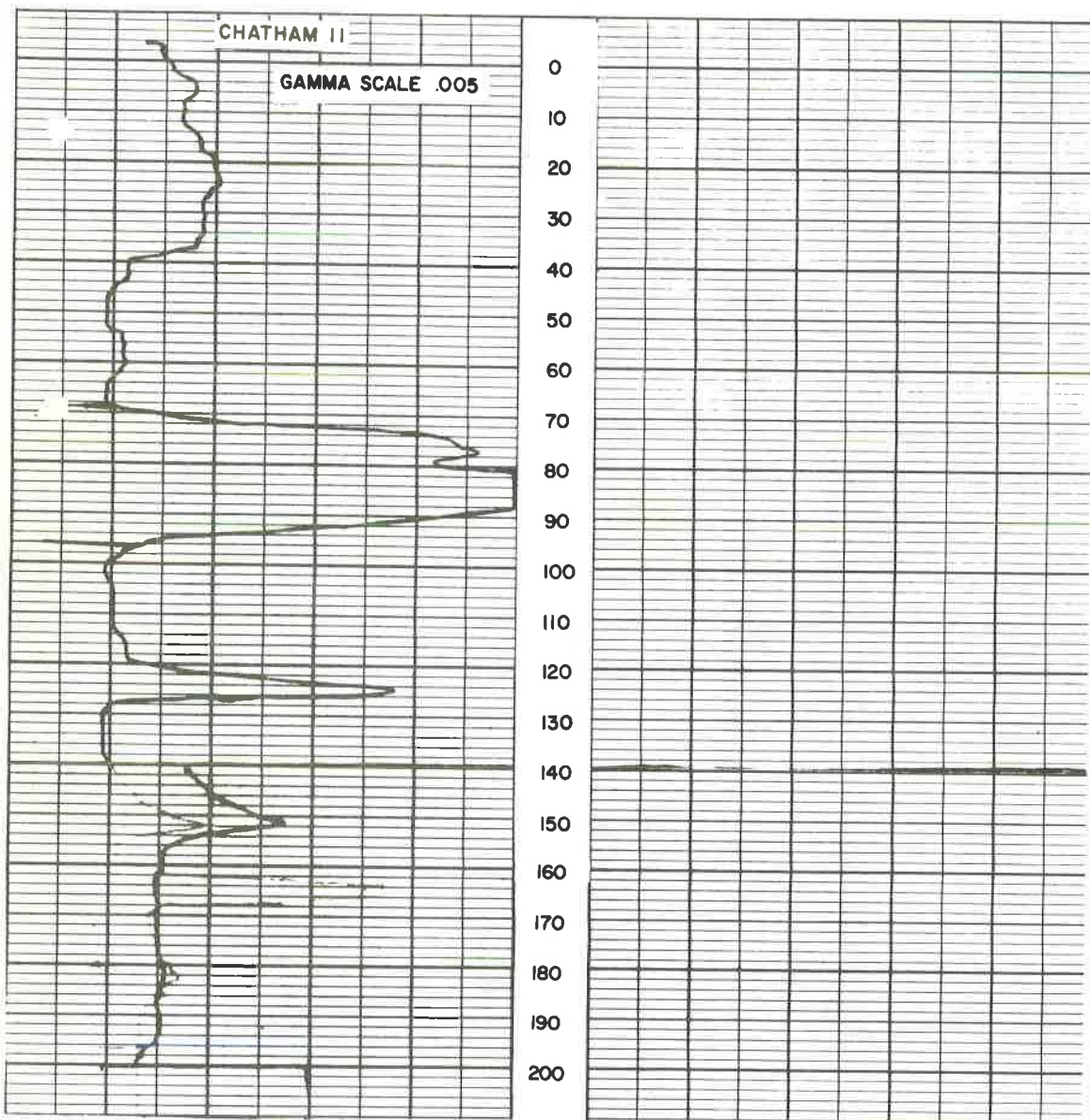


Figure CH-2. Gamma-Ray Logs - Chatham County  
Hole Ch-11



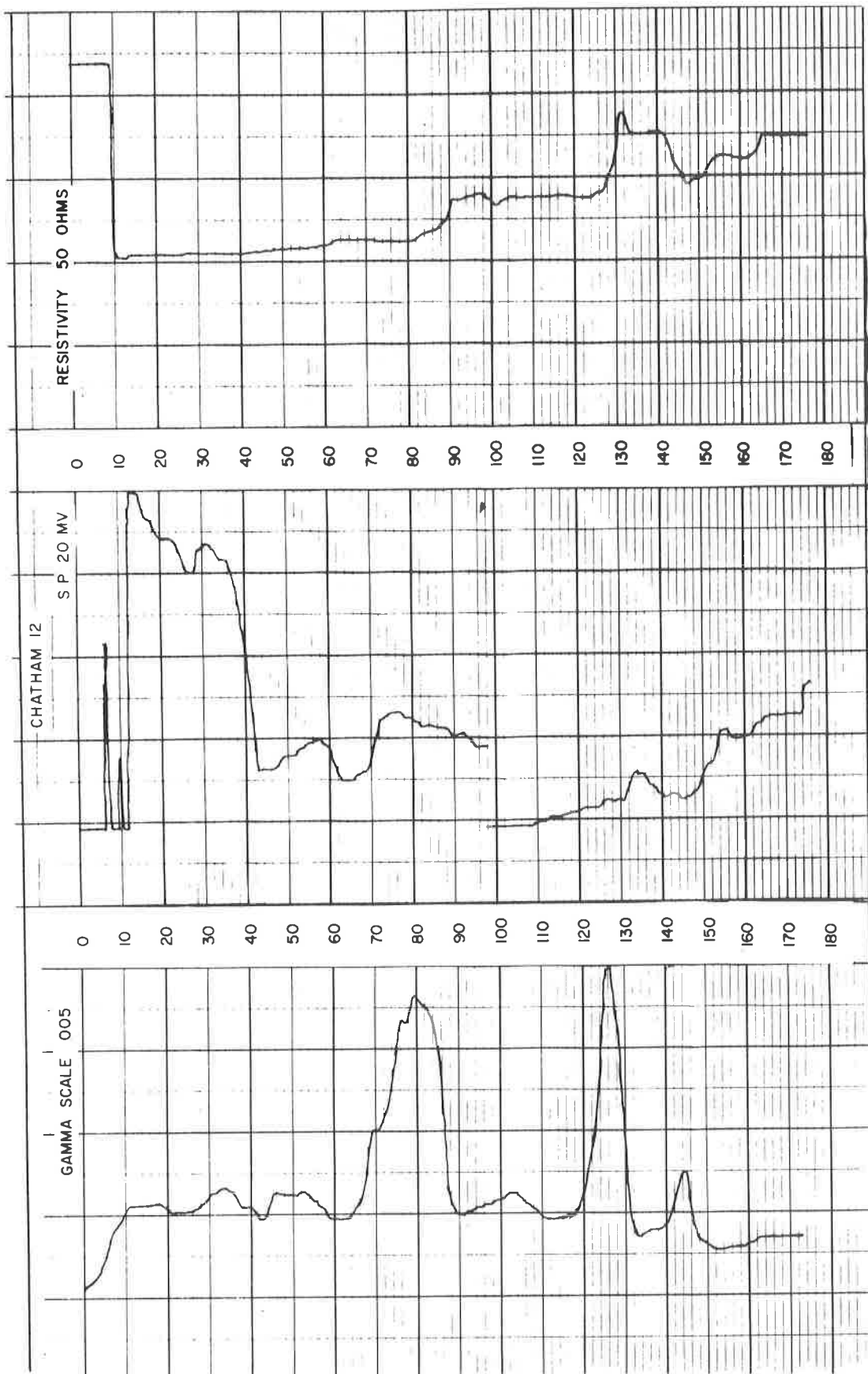


Figure CH-2. Electric and Gamma-Ray Logs - Chatham County Hole Ch-12

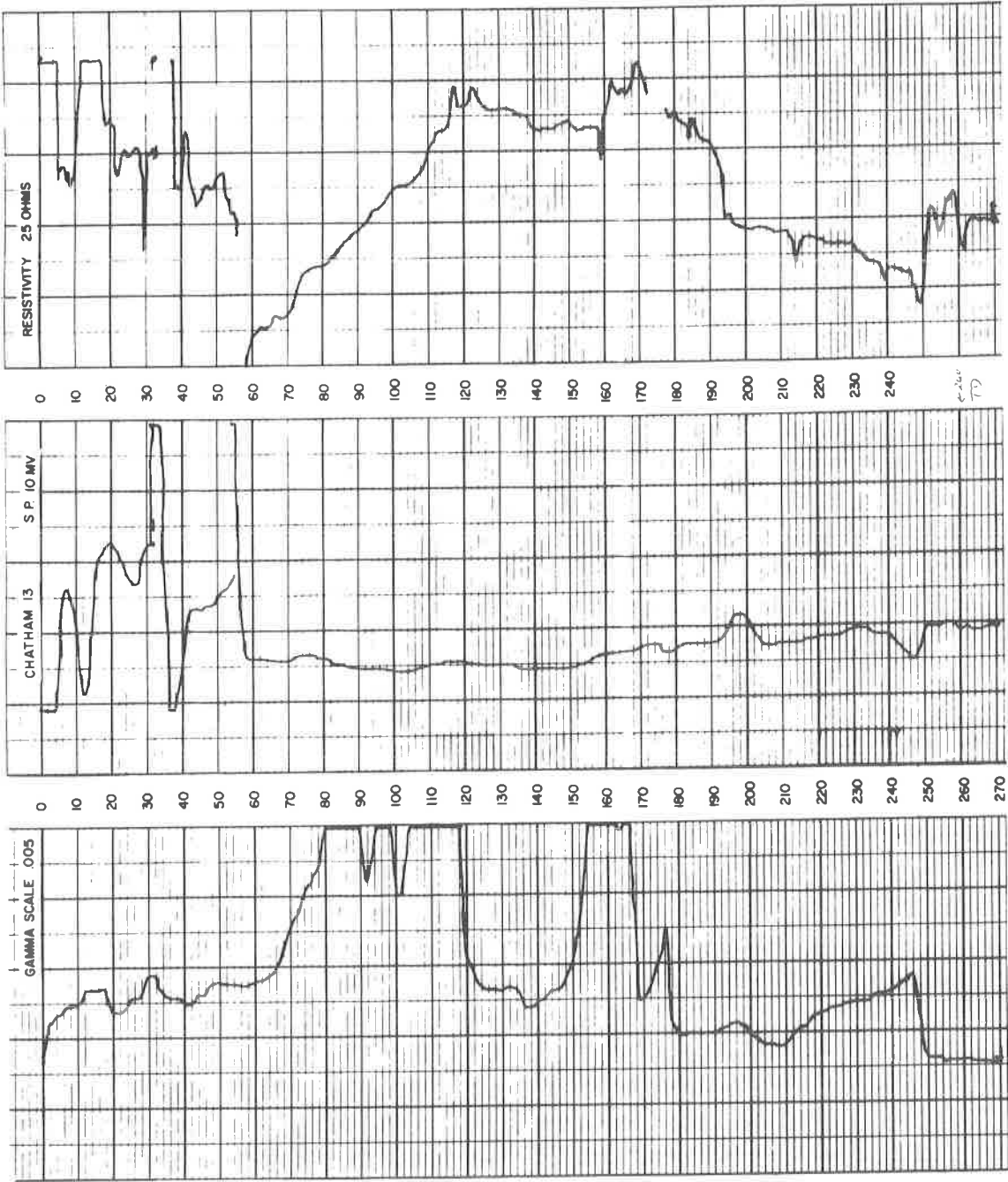


Figure CH-2. Electric and Gamma-Ray Logs - Chatham County Hole Ch-13

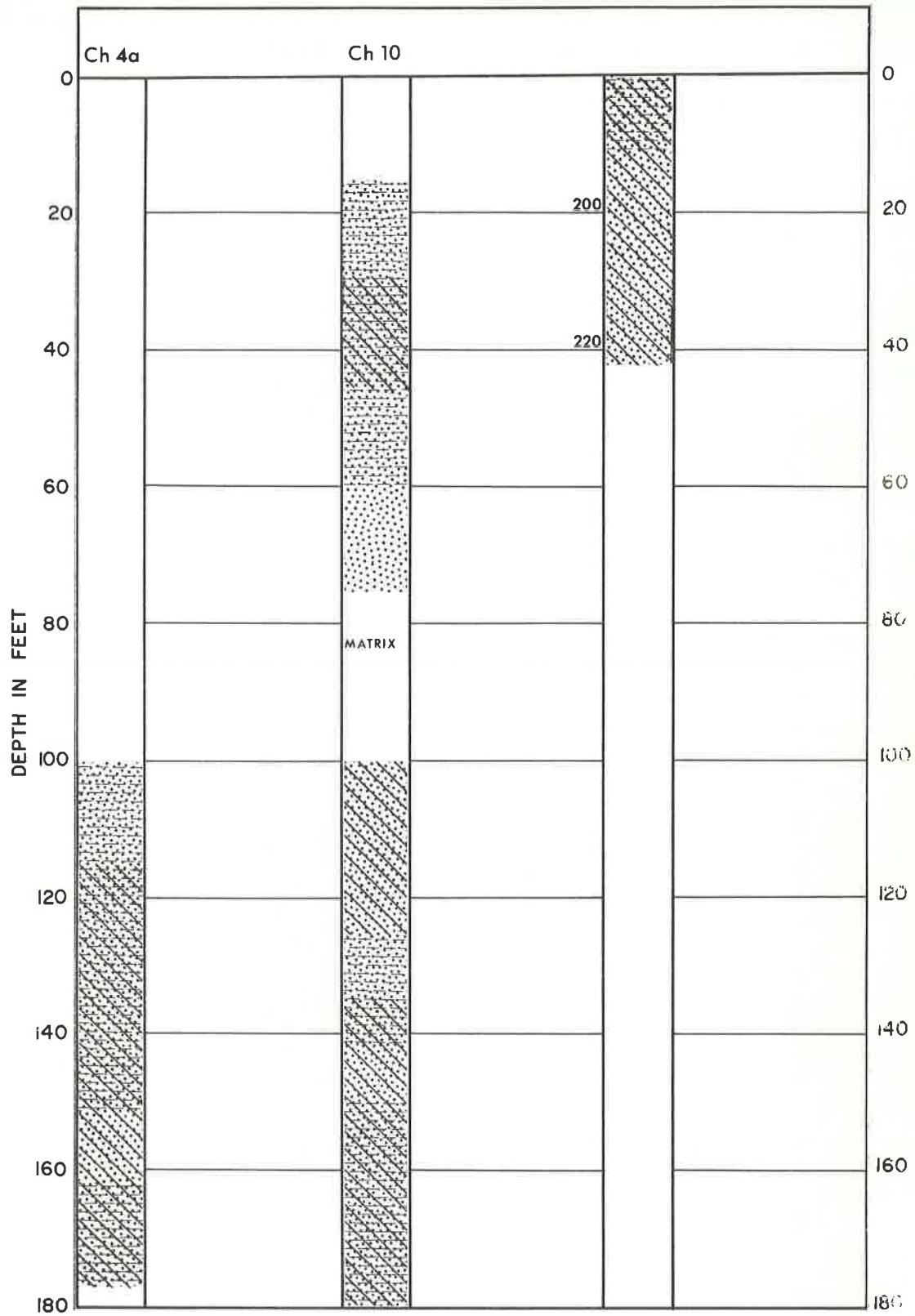


Figure Ch-3. Lithologic Logs - Chatham County

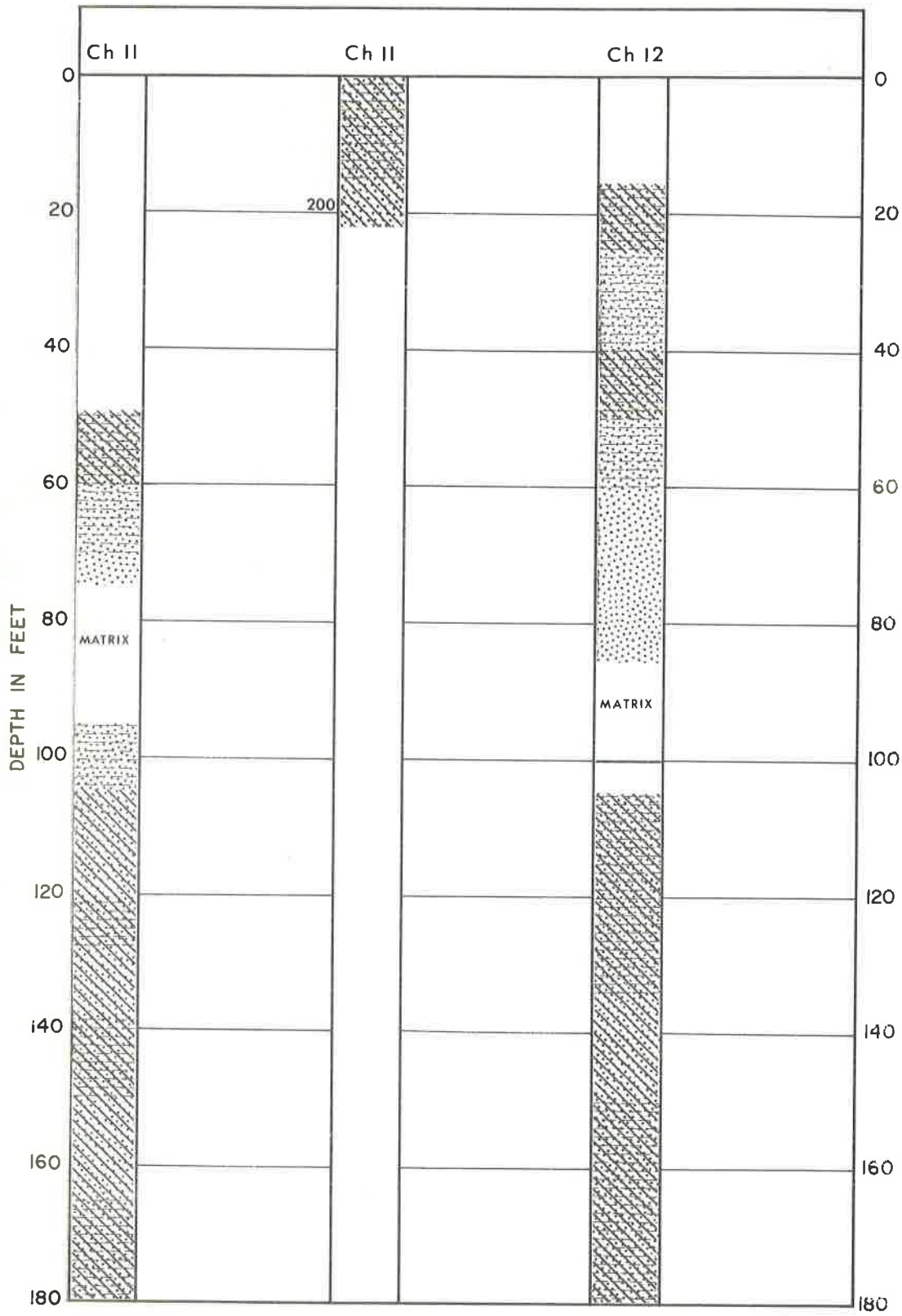


Figure Ch-3. Lithologic Logs - Chatham County (Cont.)

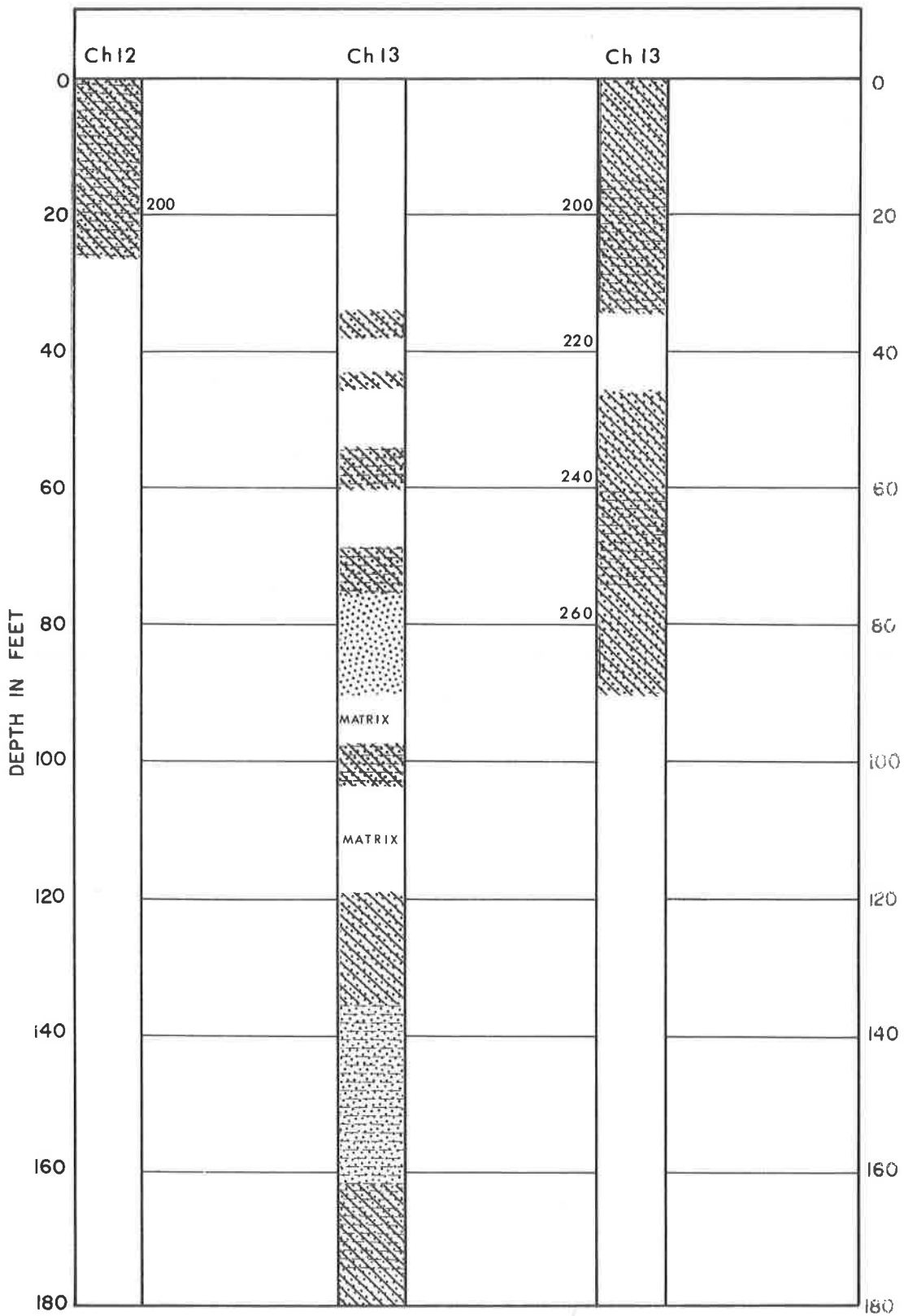


Figure Ch-3. Lithologic Logs - Chatham County (Cont.)

TABLE CH-I  
BPL DETERMINATION ON CORES  
Chatham County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Ch-4A       | 5   | 0-5            | Wash Sample   | -   | 0        |
|             |   | 5-10           | Wash Sample   | -   | 0        |
|             |   | 10-15          | Wash Sample   | -   | 0        |
|             |   | 15-20          | Wash Sample   | -   | 0        |
|             |   | 20-25          | Wash Sample   | -   | 0        |
|             |   | 25-30          | Wash Sample   | -   | 0        |
|             |   | 30-35          | Wash Sample   | -   | 0        |
|             |   | 35-40          | Wash Sample   | -   | 0        |
|             |   | 40-45          | Wash Sample   | -   | 0        |
|             |   | 45-50          | Wash Sample   | -   | 0        |
|             |   | 50-55          | Wash Sample   | -   | 0        |
|             |   | 55-60          | Wash Sample   | -   | 0        |
|             |   | 60-65          | Wash Sample   | -   | 0        |
|             |   | 65-70          | Wash Sample   | -   | 0        |
|             |   | 70-75          | Wash Sample   | -   | 0        |
|             |   | 75-80          | Wash Sample   | -   | 2.36     |
|             |   | 80-85          | Wash Sample   | -   | 20.90    |
|             |   | 85-90          | Wash Sample   | -   | 27.15    |
|             |   | 90-95          | Wash Sample   | -   | 11.47    |
|             |   | 95-100         | Wash Sample   | -   | 10.29    |
|             |   | 100-115        | 11            | 73  | 4.05     |
|             |   | 115-125        | 2             | 20  | 1.69     |
|             |   | 125-150        | 1             | 4   | 1.18     |
|             |   | 150-161        | 6             | 54  | 0        |
|             |   | 161-176        | 10            | 67  | 0        |
| Ch-10       | 7   | 0-15           | -             | -   | -        |
|             |   | 15-30          | 1             | 7   | 0        |
|             |   | 30-45          | 1             | 7   | 0        |
|             |   | 45-59          | 13            | 93  | 0        |
|             |   | 59-60          | 1             | 100 | 0        |
|             |   | 60-75          | 4             | 34  | 3.46     |
|             |   | 75-89          | 14            | 100 | 32.30    |
|             |   | 89-100         | 11            | 100 | 13.15    |
|             |   | 100-120        | -             | -   | -        |
|             |   | 120-125        | 3             | 60  | 2.19     |
|             |   | 125-135        | 2             | 20  | 2.53     |
|             |   | 135-142        | 3             | 43  | 0.67     |
|             |   | 142-150        | 3             | 38  | 1.69     |

(Continued)

TABLE CH-I (Continued)  
 BPL DETERMINATION ON CORES  
 Chatham County

| Hole No. | Surface Elevation (Sea Level) Feet | Depth, Feet | Core Recovery |     | BPL   |
|----------|------------------------------------|-------------|---------------|-----|-------|
|          |                                    |             | Feet          | %   | %     |
| Ch-10    |                                    | 150-165     | 3             | 20  | 0.84  |
|          |                                    | 165-180     | -             | -   | -     |
|          |                                    | 180-191     | 6             | 55  | 1.32  |
|          |                                    | 191-195     | 4             | 100 | 0     |
|          |                                    | 195-207     | 4             | 33  | 0     |
|          |                                    | 207-222     | 5             | 33  | 0     |
| Ch-11    | 5                                  | 0-5         | Wash Sample   | -   | 0.34  |
|          |                                    | 5-10        | Wash Sample   | -   | 0     |
|          |                                    | 10-15       | Wash Sample   | -   | 0     |
|          |                                    | 15-20       | Wash Sample   | -   | 0     |
|          |                                    | 20-25       | Wash Sample   | -   | 0     |
|          |                                    | 25-30       | Wash Sample   | -   | 0     |
|          |                                    | 30-35       | Wash Sample   | -   | 0     |
|          |                                    | 35-40       | Wash Sample   | -   | 0     |
|          |                                    | 40-45       | Wash Sample   | -   | 0     |
|          |                                    | 45-50       | Wash Sample   | -   | 0     |
|          |                                    | 50-60       | 2             | 20  | 0     |
|          |                                    | 60-70       | 6             | 60  | 0     |
|          |                                    | 70-75       | 2             | 40  | 0     |
|          |                                    | 75-85       | 10            | 100 | 23.10 |
|          |                                    | 85-95       | 10            | 100 | 30.35 |
|          |                                    | 95-105      | 7             | 70  | 1.69  |
|          |                                    | 105-115     | 2             | 20  | 3.71  |
|          |                                    | 115-121     | 6             | 100 | 3.54  |
|          |                                    | 121-128     | 7             | 100 | 7.25  |
|          |                                    | 128-138     | 1             | 10  | 1.10  |
|          |                                    | 138-150     | 2             | 17  | 1.01  |
| 150-165  | 3                                  | 20          | 0.67          |     |       |
| 165-180  | 10                                 | 67          | 0             |     |       |
| 180-195  | 14                                 | 93          | 0             |     |       |
| 195-202  | 7                                  | 100         | 0             |     |       |
| Ch-12    | 5                                  | 0-5         | Wash Sample   | -   | 0     |
|          |                                    | 5-10        | Wash Sample   | -   | 0     |
|          |                                    | 10-15       | -             | -   | -     |
|          |                                    | 15-25       | 8             | 80  | 0     |

(Continued)

TABLE CH-I (Continued)

## BPL DETERMINATION ON CORES

## Chatham County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |      | BPL<br>% |
|-------------|---|----------------|---------------|------|----------|
|             |   |                | Feet          | %    |          |
| Ch-12       |   | 25-40          | 8             | 53   | 0        |
|             |   | 40-50          | 10            | 100  | 0        |
|             |   | 50-60          | 6             | 60   | 0        |
|             |   | 60-70          | 1             | 10   | 0        |
|             |   | 70-85          | 6             | 40   | 9.78     |
|             |   | 85-100         | 3             | 20   | 28.33    |
|             |   | 100-105        | -             | -    | -        |
|             |   | 105-120        | 4             | 27   | 3.03     |
|             |   | 120-135        | 3             | 20   | 2.70     |
|             |   | 135-150        | 9             | 60   | 0        |
|             |   | 150-165        | 3             | 20   | 0        |
|             |   | 165-180        | 7             | 47   | 0        |
|             |   | 180-195        | 5             | 33   | 0        |
|             |   | 195-203        | 3             | 38   | 0        |
|             |   | 203-206        | 2             | 67   | 0        |
|             |   | Ch-13          | 5             | 0-34 | -        |
| 34-38       | 4   |                |               | 100  | 0        |
| 38-43       | -   |                |               | -    | -        |
| 43-45       | 2   |                |               | 100  | 0        |
| 45-54       | -   |                |               | -    | -        |
| 54-60       | 6   |                |               | 100  | 0        |
| 60-68       | -   |                |               | -    | -        |
| 68-75       | 7   |                |               | 100  | 0        |
| 75-90       | 11  |                |               | 73   | 5.90     |
| 90-105      | 14  |                |               | 93   | 10.45    |
| 105-119     | 14  |                |               | 100  | 30.35    |
| 119-120     | -   |                |               | -    | -        |
| 120-135     | 2   |                |               | 13   | 5.73     |
| 135-146     | 11  |                |               | 100  | 2.87     |
| 146-150     | 4   |                |               | 100  | 2.19     |
| 150-162     | 12  |                |               | 100  | 2.02     |
| 162-165     | 3   |                |               | 100  | 2.70     |
| 165-175     | 10  |                |               | 100  | 3.03     |
| 175-180     | 1   | 20             | 1.01          |      |          |
| 180-195     | 2   | 13             | 1.35          |      |          |
| 195-210     | 1   | 7              | 0.51          |      |          |
| 210-214     | 3   | 75             | 0.67          |      |          |
| 214-225     | -   | -              | -             |      |          |

(Continued)



TABLE CH-I (Continued)

## BPL DETERMINATION ON CORES

Chatham County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |    | BPL<br>% |
|-------------|---|----------------|---------------|----|----------|
|             |   |                | Feet          | %  |          |
| Ch-13       |   | 225-240        | 7             | 47 | 0.67     |
|             |   | 240-255        | 7             | 47 | 0.34     |
|             |   | 255-270        | 10            | 67 | 0.34     |



TABLE CH-II (CONT.)

MATRIX BENEFICIATION RESULTS  
CHATHAM COUNTY

HOLE NO. CH-11 MATRIX INTERVAL = 75-95

|                      | <u>FLEED</u> | <u>+4</u> | <u>4X8</u> | <u>8X16</u> | <u>F F</u>    | <u>(16X35</u> | <u>35X150)</u> | <u>SLIME</u> | <u>(CONC</u> | <u>F.A.</u>  | <u>AMTNE</u>  |
|----------------------|--------------|-----------|------------|-------------|---------------|---------------|----------------|--------------|--------------|--------------|---------------|
|                      | <u>20</u>    |           |            |             | <u>16X150</u> | <u>(16X35</u> | <u>35X150)</u> | <u>-150</u>  |              | <u>TAILS</u> | <u>FLOAT)</u> |
| TOTAL MATRIX FOOTAGE | 76.92        |           |            | 1.48        | 68.62         | 6.38          | 62.24          | 29.08        | 47.06        | 40.48        | 12.46         |
| DRY DENSITY LB/CU FT | 100.0        |           | .60        | 44.51       | 34.23         | 23.44         | 36.25          | 7.26         | 66.26        | 3.87         | 10.75         |
| PERCENT DRY WEIGHT   | 26.64        | 46.03     | 46.87      | 34.22       | 49.67         | 66.53         | 47.17          | 49.77        | 2.76         | 94.02        | 74.88         |
| PERCENT SPL          | 49.30        | 27.01     | 29.56      | .59         | .31           | .19           | .31            | 1.59         | .41          | .08          | .48           |
| PERCENT ACID INSOL   | .69          | .71       | .66        |             |               |               |                |              |              |              |               |
| PERCENT IRON OXIDE   | 2.04         | 1.23      | 2.12       | 1.64        | 1.59          | 1.35          | 1.81           | 5.19         | .70          | 1.82         | .32           |
| PERCENT ALUM OXIDE   | 23.09        | 35.68     | 33.93      | 34.28       | 26.58         | 17.49         | 26.58          | 13.97        | 48.97        | 3.22         | 14.53         |

TABLE CH-II (CONT.)

MATRIX BENEFICIATION RESULTS

CHATHAM COUNTY

| HOLE NO. CH-12       | MATRIX INTERVAL = 82-100 |       |       |       |               |         |        |               |        |               |                 |
|----------------------|--------------------------|-------|-------|-------|---------------|---------|--------|---------------|--------|---------------|-----------------|
|                      | FEED                     | +4    | 4X8   | 8X16  | F P<br>16X150 | (16X35) | 35X150 | SLIME<br>-150 | (CONC) | F.A.<br>TAILS | AMINE<br>FLOAT) |
| TOTAL MATRIX FOOTAGE | 18                       |       |       |       |               |         |        |               |        |               |                 |
| DRY DENSITY LB/CU FT | 90.56                    | 14.79 | 1.24  | 3.16  | 61.00         | 6.95    | 54.05  | 19.81         | 33.10  | 37.65         | 29.25           |
| PERCENT DRY WEIGHT   | 100.0                    | 3.54  | 48.56 | 47.89 | 34.73         | 27.99   | 33.89  | 41.47         | 66.43  | 9.80          | 26.80           |
| PERCENT PPL          | 32.04                    | 42.51 | 26.27 | 28.21 | 48.89         | 59.62   | 50.87  | 54.99         | 3.15   | 85.55         | 59.79           |
| PERCENT ACID INSOL   | 48.22                    | .49   | .86   | .83   | .56           | .27     | .34    | 1.77          | .53    | .17           | .17             |
| PERCENT IRON OXIDE   | .68                      |       |       |       |               |         |        |               |        |               |                 |
| PERCENT ALUM OXIDE   | 2.57                     | 1.94  | 1.62  | 1.37  | 1.04          | 1.23    | 1.66   | 6.16          | .70    | 1.79          | 2.22            |
| PERCENT CALC OXIDE   | 23.44                    | 19.59 | 33.93 | 32.88 | 22.74         | 19.59   | 23.79  | 26.31         | 48.27  | 7.84          | 24.79           |

NOTE: A LARGE AMOUNT OF GREENISH-YELLOW CLAY FLOATED WITH THE PHOSPHORITE IN THE ROUGH FLOTATION (FATTY ACID STEP). THE ROUGH CONCENTRATE WAS WASHED THROUGH A 200 MESH SIEVE BEFORE DE-REGENERATION TO AVOID FLOCCULATION OF CLAYS AND CONSEQUENT CARRY-OVER INTO THE AMINE FLOAT.



TABLE CH-II (CONT.)

## MATRIX BENEFICIATION RESULTS

CHATHAM COUNTY

| TOTAL MATRIX FOOTAGE<br>CUY DENSITY LB/CU FT | HOLE NO. CH-13 |       | MATRIX INTERVAL = 103-119 |       |        |       |        |               |       |               |                 |  |
|--|----------------|-------|---------------------------|-------|--------|-------|--------|---------------|-------|---------------|-----------------|--|
|  | FEED<br>16     | 44    | 4X8                       | 8X16  | 16X150 | 16X35 | 35X150 | SLIME<br>-150 | (CONC | F.A.<br>TAILS | AMINE<br>FLOAT) |  |
| 59.99  | .06            | .39   | 2.15                      | 62.12 | 8.83   | 53.29 | 35.28  | 48.77         | 33.89 | 17.34         |                 |  |
| 100.0  | 62.89          | 61.21 | 49.91                     | 38.27 | 26.81  | 41.82 | 17.68  | 65.92         | 2.19  | 34.78         |                 |  |
| 31.36  | 5.75           | 9.33  | 26.44                     | 44.43 | 61.78  | 38.52 | 55.82  | 2.41          | 96.38 | 52.28         |                 |  |
| 47.90  | .30            | .66   | .55                       | .41   | .26    | .42   | 2.50   | .41           | .08   | .36           |                 |  |
| 1.15   | .62            | 1.62  | 1.56                      | 1.71  | 1.45   | 1.61  | 8.52   | .45           | 1.80  | 3.63          |                 |  |
| 4.11   | 46.17          | 42.67 | 31.58                     | 24.84 | 17.49  | 29.56 | 12.29  | 44.77         | 1.96  | 43.61         |                 |  |
| 20.54  |                |       |                           |       |        |       |        |               |       |               |                 |  |

NOTE: CLAY CHIPS PRESENT IN FLOTATION FEED MADE ROUGHER FLOTATION VERY DIFFICULT. THE FLOTATION FEED HAD TO BE SCRUBBED, AND WASHED THROUGH A 200 MESH SCREEN PRIOR TO FLOTATION. FLOTATION WAS SUCCESSFUL AFTER THIS CLEANING TREATMENT.

TABLE CH-III.

## ECONOMIC FACTORS - FIGURES OF MERIT

WELL NO. H-10

## INDIVIDUAL MATRICES

1  
75-100MATRIX NO.  
DEPTH INTERVAL, FT.ECONOMIC FACTORS \*  
UNIT (M=1000)

|  |                      |                |
|--|----------------------|----------------|
| * OVERBURDEN   | FT.<br>MT/AC         | 75.00<br>147.0 |
| * MATRIX   | FT.<br>MT/AC         | 25.00<br>46.5  |
| * BPL IN MATRIX  | PERCENT<br>MT/AC     | 23.10<br>10.7  |
| * OVERBURDEN/MATRIX  | RATIO                | 3.00           |
| WASH-SCREEN PRODUCTS                                       |                      |                |
| +16 MESH   | MT/AC                | 2.7            |
| -16+150 MESH   | MT/AC                | 33.5           |
| -150 MESH (LUSS)   | MT/AC                | 10.4           |
| * FLOTATION CONCENTRATE PRODUCT<br>TOTAL USEFUL PRODUCTS** | MT/AC<br>MT/AC       | 9.2<br>11.8    |
| BPL RECOVERY   |                      |                |
| +16 MESH   | MT/AC                | .6             |
| * -16+150 (FLOT. CONC.)                                    | PERCENT BPL<br>MT/AC | 65.9<br>6.0    |
| * -16+150 (FLOT. CONC.)                                    | MT/AC                | 6.7            |
| * TOTAL  | PERCENT              | 62.16          |
| * RECOVERED FROM MATRIX                                    |                      |                |
| * OVERBURDEN / PRODUCT                                     | CU YD/T              | 10.8           |
| * MATRIX / PRODUCTS  | CU YD/T              | 3.41           |
| * I+A IN FLOT. CONC.                                       | PERCENT              | .86            |

## FIGURES OF MERIT

UNIT  
ECON. LEVEL

|                        |         |          |      |
|------------------------|---------|----------|------|
| OVERBURDEN             | FT      | 88 MAX   | 1.17 |
| MATRIX BPL             | FT      | 3 MIN    | 8.33 |
| BPL IN FLOT. CONC. (1) | PERCENT | 10 MIN   | 2.31 |
| BPL IN FLOT. CONC. (2) | PERCENT | 66 MIN   | 1.00 |
| OVERBURDEN/MATRIX      | PERCENT | 66 MIN   | 1.27 |
| OVERBURDEN/PRODUCTS    | RATIO   | 2 MAX    | .67  |
| I+A IN FLOT. CONC.     | CU YD/T | 17.5 MAX | 1.62 |
| PRODUCTS RECOVERY      | PERCENT | 5 MAX    | 5.81 |
| BPL (+150) RECOVERY    | T/AC-FT | 400 MIN  | 1.18 |
| MATRIX/PRODUCTS        | PERCENT | 63 MIN   | .99  |
|                        | CU YD/T | 6 MAX    | 1.76 |

(1) FOR WET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
 NOTES: OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

TABLE CH-III (CONT.)

ECONOMIC FACTORS - FIGURES OF MERIT

WELL NO. CH-11

INDIVIDUAL MATRICES

| MATRIX NO.<br>DEPTH INTERVAL, FT. | UNIT (M=1000)    | 75- 95         |
|-----------------------------------|------------------|----------------|
| ECONOMIC FACTORS *                |                  |                |
| * OVERBURDEN                      | FT.<br>MT/AC     | 75.00<br>147.0 |
| * MATRIX                          | FT.<br>MT/AC     | 20.00<br>33.5  |
| * BPL IN MATRIX                   | PERCENT<br>MT/AC | 26.64<br>8.9   |
| * OVERBURDEN/MATRIX               | RATIO            | 3.75           |
| WASH-SCREEN PRODUCTS              |                  |                |
| +10 MESH                          | MT/AC            | .8             |
| -10+150 MESH                      | MT/AC            | 23.0           |
| -150 MESH (LOSS)                  | MT/AC            | 9.7            |
| FLUTATION CONCENTRATE PRODUCT     |                  |                |
| TOTAL USEFUL PRODUCTS**           | MT/AC            | 10.8           |
|                                   | MT/AC            | 11.6           |
| BPL RECOVERY                      |                  |                |
| +10 MESH                          | MT/AC            | .3             |
| -10+150 (FLOT. CONC.)             | PERCENT BPL      | 66.3           |
| -16+150 (FLOT. CONC.)             | MT/AC            | 7.2            |
| TOTAL                             | MT/AC            | 7.5            |
| * RECOVERED FROM MATRIX           | PERCENT          | 84.23          |
| * OVERBURDEN / PRODUCT            | CU YD/T          | 12.2           |
| * MATRIX / PRODUCTS               | CU YD/T          | 2.78           |
| * 1+1 IN FLOT. CONC.              | PERCENT          | 1.11           |

FIGURES OF MERIT

| UNIT                  | ECON. LEVEL |
|-----------------------|-------------|
| OVERBURDEN            | 88 MAX      |
| MATRIX                | 3 MIN       |
| MATRIX BPL            | 10 MIN      |
| BPL IN FLOT. CONC.(1) | 66 MIN      |
| BPL IN FLOT. CONC.(2) | 66 MIN      |
| OVERBURDEN/MATRIX     | 2 MAX       |
| OVERBURDEN/PRODUCTS   | 17.5 MAX    |
| 1+1 IN FLOT. CONC.    | 5 MAX       |
| PRODUCTS RECOVERY     | 400 MIN     |
| BPL (+150) RECOVERY   | 63 MIN      |
| MATRIX/PRODUCTS       | 6 MAX       |
|                       | 2.16        |

(1) FOR NET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
 NOTES: OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY



TABLE CH-III (CONT.)

ECONOMIC FACTORS - FIGURES OF MERIT  
WELL NO. CH-12

| INDIVIDUAL MATRICES               |                                |
|-----------------------------------|--------------------------------|
| MATRIX NO.<br>DEPTH INTERVAL, FT. | UNIT (N=1000)                  |
| 1<br>82-100                       |                                |
| ECONOMIC FACTORS *                |                                |
| * OVERBURDEN                      | FT.<br>MT/AC 82.00<br>160.7    |
| * MATRIX                          | FT.<br>MT/AC 18.00<br>35.5     |
| * BPL IN MATRIX                   | PERCENT<br>MT/AC 32.04<br>11.4 |
| * OVERBURDEN/MATRIX               | RATIO 4.56                     |
| WASH-SCREEN PRODUCTS              |                                |
| +10 MESH                          | MT/AC 6.8                      |
| -16+150 MESH                      | MT/AC 21.7                     |
| -150 MESH (LOSS)                  | MT/AC 7.0                      |
| * FLOTATION CONCENTRATE PRODUCT   |                                |
| TOTAL USEFUL PRODUCTS**           | MT/AC 7.2<br>14.0              |
| BPL RECOVERY                      |                                |
| +16 MESH                          | MT/AC .9                       |
| -16+150 (FLOT. CONC.)             | PERCENT BPL 66.4               |
| -16+150 (FLOT. CONC.)             | MT/AC 4.8                      |
| TOTAL                             | MT/AC 5.7                      |
| RECOVERED FROM MATRIX             | PERCENT 50.10                  |
| * OVERBURDEN / PRODUCT            |                                |
| * MATRIX / PRODUCTS               | CU YD/T 9.4                    |
| * I+A IN FLOT. CONC.              | CU YD/T 2.08<br>PERCENT 1.23   |
| FIGURES OF MERIT                  |                                |
| OVERBURDEN                        | UNIT ECON. LEVEL               |
| MATRIX                            | FT 88 MAX 1.07                 |
| BPL                               | FT 3 MIN 6.00                  |
| BPL IN FLOT. CONC.(1)             | PERCENT 10 MIN 3.20            |
| BPL IN FLOT. CONC.(2)             | PERCENT 66 MIN 1.01            |
| OVERBURDEN/MATRIX                 | PERCENT 66 MIN 1.28            |
| OVERBURDEN/PRODUCTS               | RATIO 2 MAX .44                |
| I+A IN FLOT. CONC.                | CU YD/T 17.5 MAX 1.86          |
| PRODUCTS RECOVERY                 | PERCENT 5 MAX 4.07             |
| BPL (+150) RECOVERY               | T/AC-FT 400 MIN 1.94           |
| MATRIX/PRODUCTS                   | PERCENT 63 MIN .80             |
|                                   | CU YD/T 6 MAX 2.89             |

(1) FOR NET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
NOTES: OVERBURDEN HEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

TABLE CH-III (CONT.)

## ECONOMIC FACTORS - FIGURES OF MERIT

| MATRIX NO.<br>DEPT INTERVAL, FT. | INDIVIDUAL MATRICES |                | WELL NO. CH-13 |
|----------------------------------|---------------------|----------------|----------------|
|                                  | 1<br>90- 97         | 2<br>103-119   |                |
| ECONOMIC FACTORS *               |                     |                |                |
| * OVERBURDEN                     | FT.<br>MT/AC        | 90.00<br>176.4 | 6.00<br>11.8   |
| * MATRIX                         | FT.<br>MT/AC        | 7.00<br>12.6   | 16.00<br>20.7  |
| * BPL IN MATRIX                  | PERCENT<br>MT/AC    | 9.44<br>1.2    | 31.36<br>6.5   |
| * OVERBURDEN/MATRIX              | RATIO               | 12.86          | .38            |
| WASH-SCREEN PRODUCTS             |                     |                |                |
| +10 MESH                         | MT/AC               | 1.0            | .5             |
| -16+150 MESH                     | MT/AC               | 9.2            | 12.9           |
| -150 MESH (LOSS)                 | MT/AC               | 2.3            | 7.3            |
| * FLOTATION CONCENTRATE PRODUCT  |                     |                |                |
| TOTAL USEFUL PRODUCTS**          | MT/AC               | 1.4            | 6.3            |
|                                  | MT/AC               | 2.4            | 6.8            |
| LPL RECOVERY                     |                     |                |                |
| +10 MESH                         | MT/AC               | .1             | .3             |
| * -10+150 (FLOT. CONC.)          | PERCENT BPL         | 67.5           | 65.9           |
| * -10+150 (FLOT. CONC.)          | MT/AC               | 1.0            | 4.1            |
| * TOTAL                          | MT/AC               | 1.0            | 4.4            |
| * RECOVERED FROM MATRIX          | PERCENT             | 86.33          | 67.99          |
| * OVERBURDEN / PRODUCT           | CU YD/T             | 65.2           | 2.2            |
| * MATRIX / PRODUCTS              | CU YD/T             | 4.65           | 3.79           |
| * 1+A IN FLOT. CONC.             | PERCENT             | 1.42           | .86            |
| FIGURES OF MERIT                 |                     |                |                |
| OVERBURDEN                       | UNIT                | ECON. LEVEL    |                |
| MATRIX                           | FT                  | .98            | 14.67          |
| MATRIX BPL                       | FT                  | 2.33           | 5.33           |
| BPL IN FLOT. CONC. (1)           | PERCENT             | .94            | 3.14           |
| BPL IN FLOT. CONC. (2)           | PERCENT             | 1.02           | 1.00           |
| OVERBURDEN/MATRIX                | PERCENT             | 1.30           | 1.27           |
| OVERBURDEN/PRODUCTS              | RATIO               | .16            | 5.33           |
| 1+A IN FLOT. CONC.               | CU YD/T             | .27            | 8.12           |
| PRODUCTS RECOVERY                | PERCENT             | 3.52           | 5.81           |
| UPL (+150) RECOVERY              | T/AC-FT             | .87            | 1.06           |
| MATRIX/PRODUCTS                  | PERCENT             | 1.37           | 1.08           |
|                                  | CU YD/T             | 1.29           | 1.58           |

(1) FOR NET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
 NOTES: OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

TABLE CH-III (CONV.)

ECONOMIC FACTORS - FIGURES OF MERIT

|                                 | COMBINED MATRICES |                | WELL NO. CH-13 |          |
|---------------------------------|-------------------|----------------|----------------|----------|
|                                 | MATRICES          | MATRICES       | MATRICES       | MATRICES |
| ECONOMIC FACTORS *              | UNIT (M=1000)     |                |                |          |
| * OVERBURDEN                    | FT.<br>MT/AC      | 90.00<br>176.4 | 96.00<br>188.2 |          |
| * MATRIX                        | FT.<br>MT/AC      | 7.00<br>12.6   | 23.00<br>35.3  |          |
| * BPL IN MATRIX                 | PERCENT<br>MT/AC  | 9.44<br>1.2    | 23.07<br>7.7   |          |
| * OVERBURDEN/MATRIX             | RATIO             | 12.86          | 4.17           |          |
| WASH-SCREEN PRODUCTS            | MT/AC             | 1.0            | 1.6            |          |
| +10 MESH                        | MT/AC             | 9.2            | 22.1           |          |
| -10+150 MESH                    | MT/AC             | 2.3            | 9.6            |          |
| -150 MESH (LOSS)                |                   |                |                |          |
| * FLOTATION CONCENTRATE PRODUCT | MT/AC             | 1.4            | 6.3            |          |
| TOTAL USEFUL PRODUCTS**         | MT/AC             | 2.4            | 9.2            |          |
| BPL RECOVERY                    | MT/AC             | .1             | .4             |          |
| +10 MESH                        | PERCENT BPL       | *****          | *****          |          |
| -10+150 (FLOT. CONC.)           | MT/AC             | 1.0            | 5.1            |          |
| -10+150 (FLOT. CONC.)           | MT/AC             | 1.0            | 5.4            |          |
| TOTAL                           | PERCENT           | 86.33          | 70.82          |          |
| * RECOVERED FROM MATRIX         | CU YD/T           | 65.2           | 22.7           |          |
| * OVERBURDEN / PRODUCT          | CU YD/T           | 4.65           | 4.02           |          |
| * MATRIX / PRODUCTS             | PERCENT           | 1.42           | 1.03           |          |
| * I+A IN FLOT. CONC.            |                   |                |                |          |

FIGURES OF MERIT

|                       | UNIT    | ECON. LEVEL |
|-----------------------|---------|-------------|
| OVERBURDEN            | FT      | .98         |
| MATRIX                | FT      | 2.33        |
| MATRIX BPL            | PERCENT | .94         |
| BPL IN FLOT. CONC.(1) | PERCENT | 1.02        |
| BPL IN FLOT. CONC.(2) | PERCENT | 1.30        |
| OVERBURDEN/MATRIX     | RATIO   | .16         |
| OVERBURDEN/PRODUCTS   | CU YD/T | 8.43        |
| I+A IN FLOT. CONC.    | PERCENT | 3.52        |
| PRODUCTS RECOVERY     | T/AC-FT | .87         |
| BPL (+150) RECOVERY   | PERCENT | 1.37        |
| MATRIX/PRODUCTS       | CU YD/T | 1.29        |

(1) FOR NET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
 NOTES: OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY



CLINCH COUNTY

CLINCH COUNTY  
SUMMARY OF RESULTS

Two new holes in Southeast Clinch County, numbers 4 and 5, are reported herein.

C1-4 had four matrix areas that were beneficiated. At best the matrices may be considered marginal to sub-marginal for economic exploitation.

C1-5 had one matrix which was relatively deep and thin. It is sub-marginal.

Electric logs were not run at C1-4 because of cave-in of the hole walls. The gamma-ray log was run inside the drill pipe.

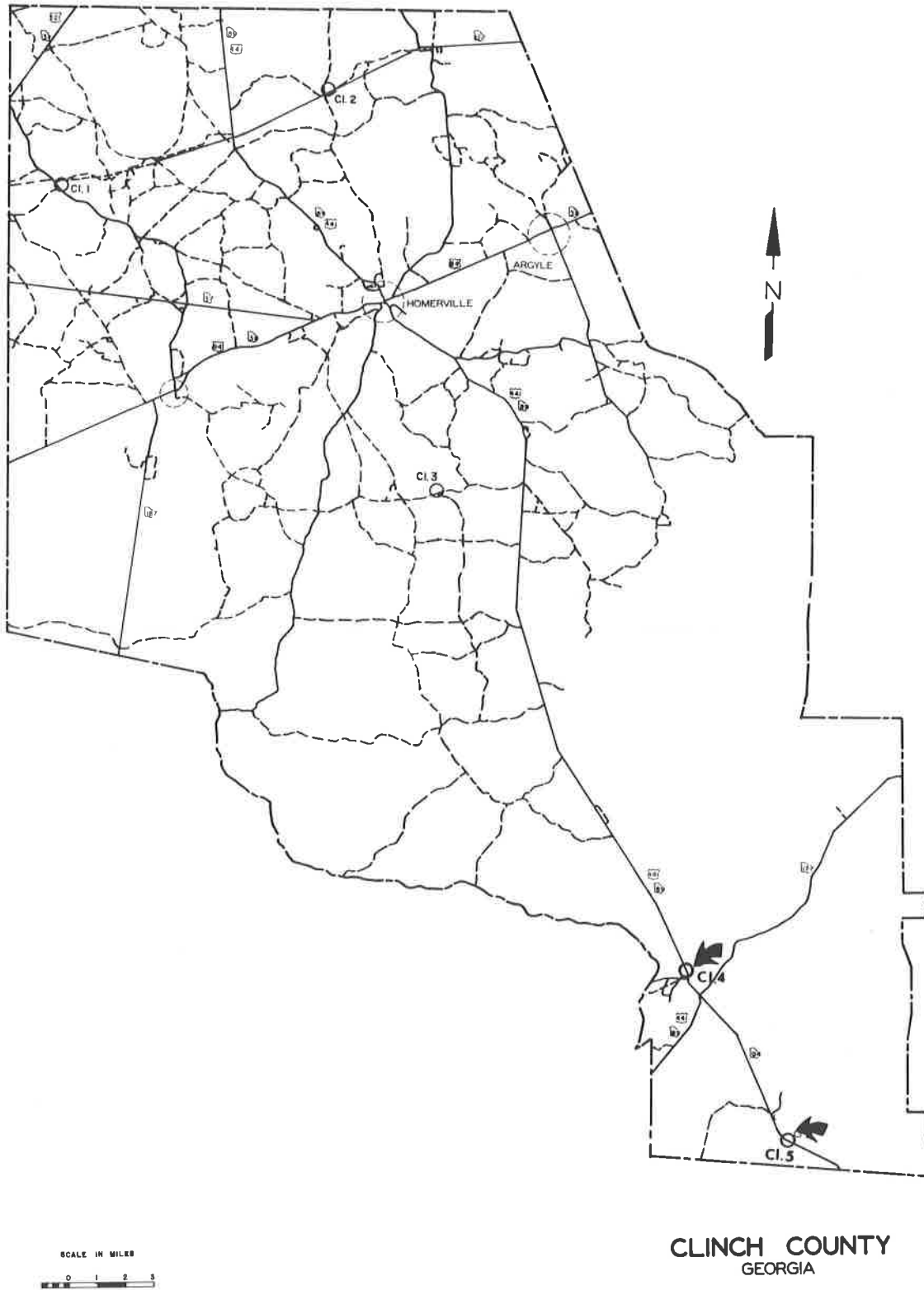


Figure CL-1. Location of Holes - Clinch County

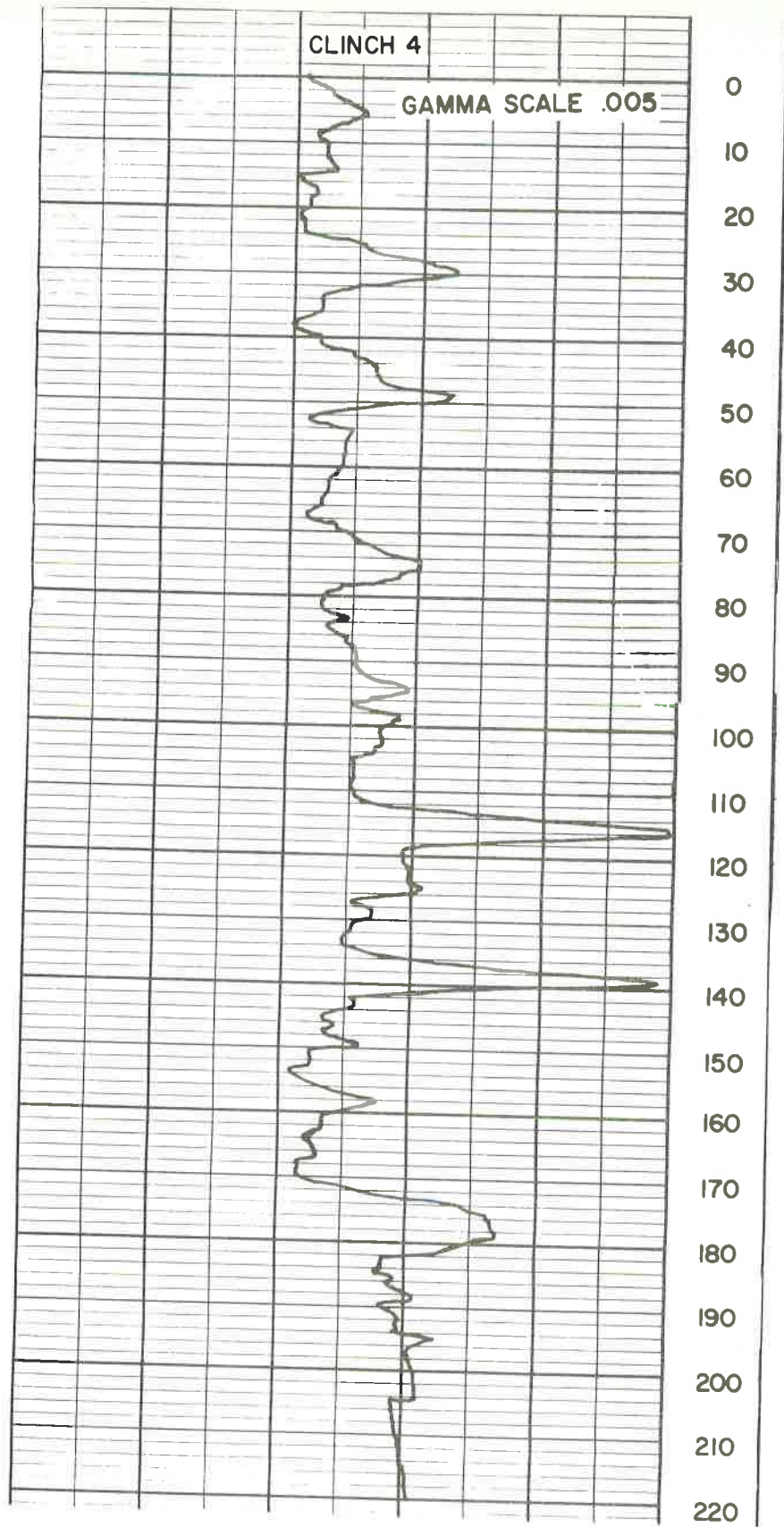


Figure CL-2. Gamma-Ray Logs - Clinch County Hole CL-4



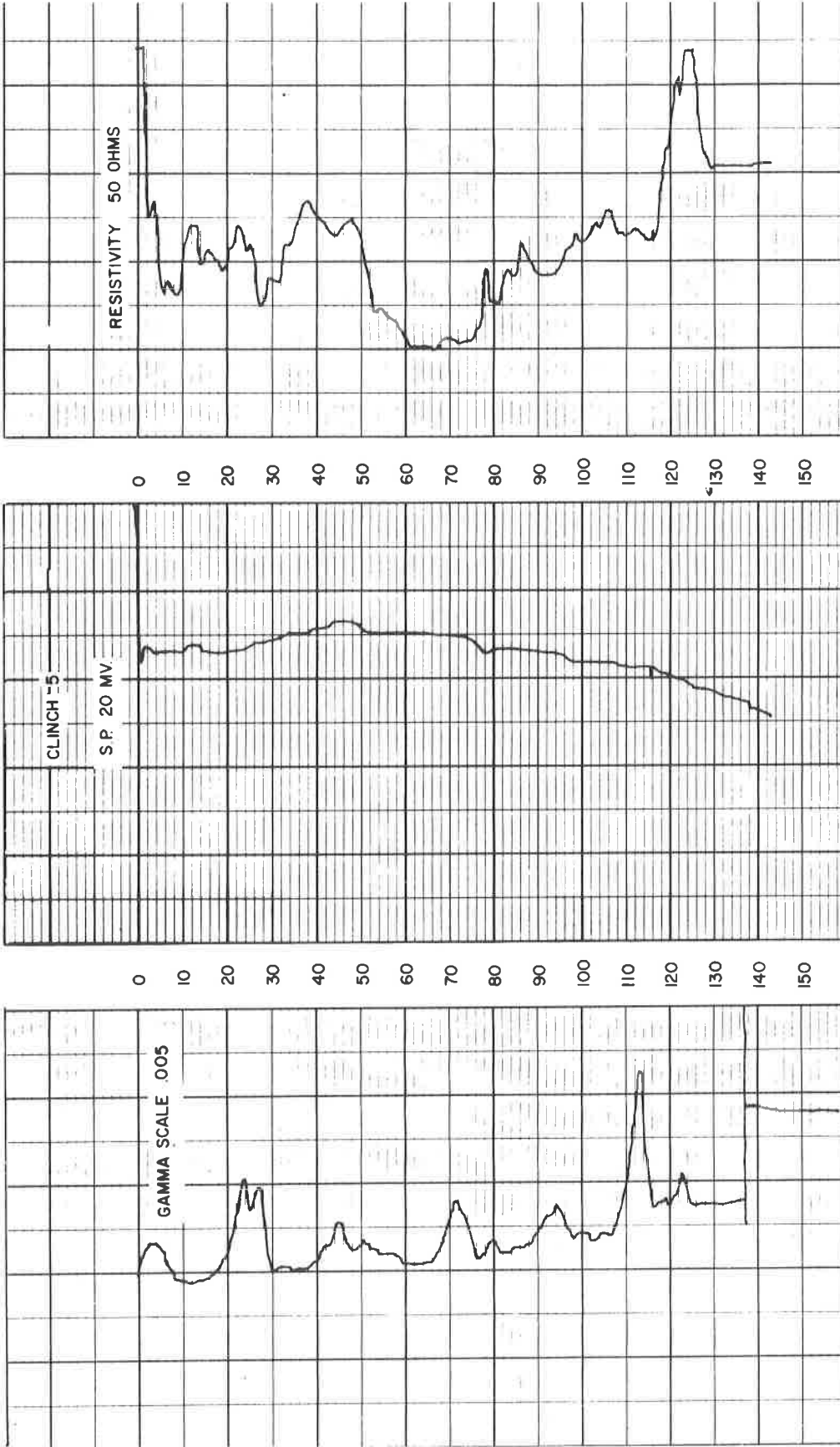


Figure CL-2. Electric and Gamma-Ray Logs - Clinch County  
Hole CI-5

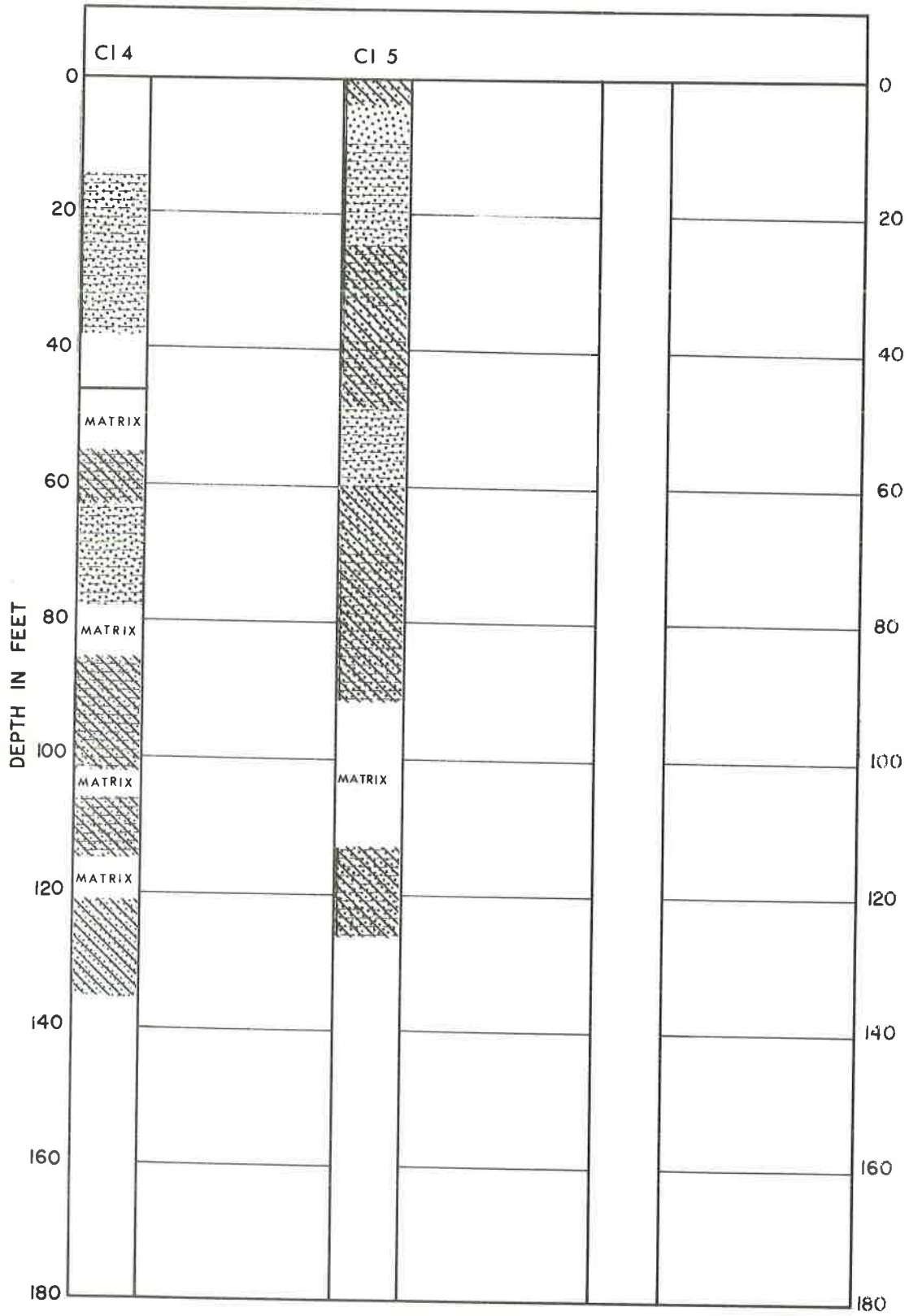


Figure Cl-3. Lithologic Logs - Clinch County

TABLE CL-I  
 BPL DETERMINATION ON CORES  
 Clinch County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| CL-4        | 119   | 0-8            | 8             | 100 | 0        |
|             |   | 8-11           | 3             | 100 | 0        |
|             |   | 11-18          | 5             | 71  | 0        |
|             |   | 18-23          | 5             | 100 | 0        |
|             |   | 23-27          | 4             | 100 | 0        |
|             |   | 27-30          | 1             | 33  | 0        |
|             |   | 30-38          | 4             | 50  | 6.71     |
|             |   | 38-46          | -             | -   | -        |
|             |   | 46-55          | 3             | 33  | 9.04     |
|             |   | 55-63          | 8             | 100 | 3.81     |
|             |   | 63-71          | 8             | 100 | 2.22     |
|             |   | 71-78          | 7             | 100 | 2.22     |
|             |   | 78-85          | 7             | 100 | 13.08    |
|             |   | 85-92          | 7             | 100 | 6.15     |
|             |   | 92-102         | 10            | 100 | 5.19     |
|             |   | 102-106        | 3             | 75  | 10.15    |
|             |   | 106-115        | 6             | 67  | 7.72     |
|             |   | 115-121        | 6             | 100 | 10.59    |
|             |   | 121-126        | 3             | 60  | 2.73     |
|             |   | 126-135        | 1             | 11  | 6.98     |
|             |   | 135-140        | Wash Sample   | -   | 8.56     |
|             |   | 140-145        | Wash Sample   | -   | 6.20     |
|             |   | 145-150        | Wash Sample   | -   | 11.30    |
|             |   | 150-155        | Wash Sample   | -   | 6.00     |
|             |   | 155-160        | Wash Sample   | -   | 4.48     |
|             |   | 160-165        | Wash Sample   | -   | 4.15     |
|             |   | 165-170        | Wash Sample   | -   | 6.00     |
|             |   | 170-175        | Wash Sample   | -   | 5.40     |
|             |   | 175-180        | Wash Sample   | -   | 3.24     |
|             |   | 180-185        | Wash Sample   | -   | 2.63     |
|             |   | 185-190        | Wash Sample   | -   | 3.91     |
|             |   | 190-195        | Wash Sample   | -   | 3.78     |
| 195-200     | Wash Sample                                 | -              | 3.44          |     |          |
| 200-205     | Wash Sample                                 | -              | 3.68          |     |          |
| 205-210     | Wash Sample                                 | -              | 4.08          |     |          |
| 210-215     | Wash Sample                                 | -              | 6.14          |     |          |
| 215-220     | Wash Sample                                 | -              | 8.33          |     |          |
| 220-225     | Wash Sample                                 | -              | 4.45          |     |          |
| CL-5        | 121   | 0-3            | 2             | 67  | 0        |
|             |   | 3-6            | 3             | 100 | 0        |
|             |   | 6-9            | 3             | 100 | 0        |

(Continued)

TABLE CL-I (Continued)  
 BPL DETERMINATION ON CORES  
 Clinch County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |      | BPL<br>% |       |
|-------------|---|----------------|---------------|------|----------|-------|
|             |   |                | Feet          | %    |          |       |
| Cl-5        | 121   | 9-13           | 2             | 50   | 0.34     |       |
|             |   | 13-18          | 4             | 80   | 0        |       |
|             |   | 18-25          | 7             | 100  | 0.44     |       |
|             |   | 25-33          | 4             | 50   | 1.79     |       |
|             |   | 33-38          | 5             | 100  | 1.58     |       |
|             |   | 38-48          | 9             | 90   | 1.01     |       |
|             |   | 48-60          | 11            | 92   | 5.90     |       |
|             |   | 60-68          | 2             | 25   | 5.83     |       |
|             |   | 68-78          | 7             | 70   | 10.55    |       |
|             |   | 78-91          | 13            | 100  | 7.22     |       |
|             |   | 91-98          | 5             | 71   | 14.36    |       |
|             |   | 98-113         | 5             | 33   | 17.54    |       |
|             |   | 113-126        | 8             | 62   | 8.23     |       |
|             |   | 126-130        | Wash Sample   | -    | -        | 12.71 |
|             |   | 130-135        | Wash Sample   | -    | -        | 13.59 |
|             |   | 135-140        | Wash Sample   | -    | -        | 14.26 |
|             |   | 140-145        | Wash Sample   | -    | -        | 13.46 |
| 145-150     | Wash Sample                                 | -              | -             | 7.01 |          |       |
| 150-155     | Wash Sample                                 | -              | -             | 8.50 |          |       |
| 155-160     | Wash Sample                                 | -              | -             | 3.88 |          |       |

TABLE CL-II  
 MATRIX BENEFICIATION RESULTS  
 CLINCH COUNTY

| HOLE NO. CL-04       | MATRIX INTERVAL = 46-55 | FEED  | +4  | 4XB   | 8X16  | F F    |                   | SLIME<br>-150 | (CONC) | F.A.<br>TAILS | AMINE<br>FLOAT) |
|----------------------|-------------------------|-------|-----|-------|-------|--------|-------------------|---------------|--------|---------------|-----------------|
|                      |                         |       |     |       |       | 16X150 | (16X35<br>35X150) |               |        |               |                 |
| TOTAL MATRIX FOOTAGE |                         | 92.24 |     |       |       |        |                   |               |        |               |                 |
| DRY DENSITY LB/CC FT |                         | 100.0 |     |       |       |        |                   |               |        |               |                 |
| PERCENT DRY WEIGHT   |                         | 9.31  | .00 | 36.08 | 1.08  | 74.08  | 4.13              | 69.95         | 10.18  | 69.78         | 20.03           |
| PERCENT BPL          |                         | 83.29 | .00 | 42.30 | 23.44 | 9.78   | 11.80             | 8.09          | 53.62  | 4.89          | 1.18            |
| PERCENT ACID INSOL   |                         | 1.02  | .00 | 2.86  | 53.87 | 85.87  | 76.19             | 90.74         | 22.28  | 92.26         | 97.91           |
| PERCENT IRON OXIDE   |                         | 4.13  | .00 | 3.59  | 1.93  | .64    | 1.01              | .46           | 2.57   | .34           | .40             |
| PERCENT ALUM OXIDE   |                         | 5.25  | .00 | 20.99 | 2.47  | 2.88   | 1.71              | 2.34          | 2.00   | 2.61          | 1.91            |
| PERCENT CALC OXIDE   |                         |       |     |       | 14.34 | 4.55   | 9.09              | 4.20          | 34.98  | 2.10          | .91             |

TABLE CL-II (CONT.)  
 MATRIX BENEFICIATION RESULTS  
 CLINCH COUNTY

| HOLE NO. CL-04       | MATRIX INTERVAL = 78-85 | CLINCH COUNTY |       |       |       |       |        |        |         |       |       |        |
|----------------------|-------------------------|---------------|-------|-------|-------|-------|--------|--------|---------|-------|-------|--------|
|                      |                         | FEEL          | +4    | 4X8   | 8X16  | F F   | 16X150 | (16X35 | 35X150) | SLIME | (CONC | F.A.   |
| TOTAL MATRIX FOOTAGE | 7                       |               |       |       |       |       |        |        | -150    |       | TAILS | FLOAT) |
| LB/CU FT             | 95.01                   |               |       |       |       |       |        |        |         |       |       |        |
| PERCENT DRY WEIGHT   | 100.0                   |               |       |       |       |       |        |        |         |       |       |        |
| PERCENT LPL          | 11.16                   | 3.42          | 3.29  | 4.58  | 47.57 | 9.24  | 38.14  | 41.34  | 20.55   | 74.06 | 5.39  |        |
| PERCENT ACID INSOL   | 49.95                   | 8.60          | 8.60  | 15.34 | 14.84 | 26.30 | 12.14  | 6.89   | 56.82   | 6.07  | 5.06  |        |
| PERCENT IRON OXIDE   | 1.43                    | 10.12         | 17.50 | 19.08 | 70.66 | 41.52 | 76.59  | 34.06  | 5.91    | 88.03 | 89.57 |        |
| PERCENT ALUM OXIDE   | 3.73                    | .69           | 1.08  | 1.50  | .92   | 1.72  | .81    | 2.10   | 2.36    | .53   | 1.43  |        |
| PERCENT CALC OXIDE   | 15.39                   | 1.89          | 2.37  | 2.37  | 3.09  | 1.70  | 3.25   | 4.87   | 1.39    | 3.08  | 7.56  |        |
|                      |                         | 28.33         | 26.24 | 26.24 | 12.59 | 13.64 | 10.14  | 15.46  | 33.93   | 4.20  | 4.20  |        |

TABLE CL-II (CONT.)

MATRIX BENEFICIATION RESULTS

CLINCH COUNTY

HOLE NO. CL-04 MATRIX INTERVAL = 102-106

|                      | <u>FEED</u> | <u>+4</u> | <u>4X8</u> | <u>8X16</u> | <u>F F</u><br><u>16X150</u> | <u>(16X35</u> | <u>35X150)</u> | <u>SLIME</u><br><u>-150</u> | <u>(CONC</u> | <u>F.A.</u><br><u>TAILS</u> | <u>AMINE</u><br><u>FLOAT)</u> |
|----------------------|-------------|-----------|------------|-------------|-----------------------------|---------------|----------------|-----------------------------|--------------|-----------------------------|-------------------------------|
| TOTAL MATRIX FOOTAGE | 176.73      |           |            |             |                             |               |                |                             |              |                             |                               |
| DRY DENSITY LB/CU FT | 100.0       | 1.32      | 1.53       | 2.21        | 31.52                       | 4.35          | 77.17          | 13.42                       | 9.87         | 83.20                       | 6.93                          |
| PERCENT DRY WEIGHT   | 9.58        | 3.54      | 5.23       | 10.12       | 8.09                        | 11.80         | 8.09           | 19.63                       | 62.05        | 1.85                        | 9.44                          |
| PERCENT RPL          | 71.55       | 31.98     | 36.19      | 32.24       | 76.32                       | 61.73         | 87.28          | 56.96                       | 5.52         | 95.39                       | 83.40                         |
| PERCENT ACID INSOL   | .44         | .38       | .51        | .78         | .28                         | .60           | .28            | 1.35                        | 1.86         | .11                         | .57                           |
| PERCENT IRON OXIDE   | 2.25        | 1.89      | 2.05       | 1.76        | 1.76                        | 1.16          | 1.32           | 5.36                        | 1.27         | 1.25                        | 3.92                          |
| PERCENT ALUM OXIDE   | 11.89       | 27.28     | 25.18      | 28.33       | 8.74                        | 19.59         | 8.04           | 25.29                       | 43.37        | .59                         | 6.72                          |





TABLE CI-II (CONT.)

MATRIX BENEFICIATION RESULTS  
CLINCH COUNTY

HOLE NO. CI-05 MATRIX INTERVAL = 91-113

|                      | FEED   | +4    | 4X8   | 8X16  | F F<br>16X150 | 16X35 | 35X150 | SLIME<br>-150 | (CONC.) | F.A.<br>TAILS | AMINE<br>E(LOAI) |
|----------------------|--------|-------|-------|-------|---------------|-------|--------|---------------|---------|---------------|------------------|
| TOTAL MATRIX FOOTAGE | 115.04 |       |       |       | 50.00         | 13.96 | 36.04  | 43.25         | 33.23   | 59.13         | 7.64             |
| DRY DENSITY LB/CU FT | 100.0  | 3.06  | 1.50  | 2.19  | 19.22         | 27.99 | 16.52  | 8.76          | 57.66   | 2.87          | 8.60             |
| PERCENT DRY WEIGHT   | 15.49  | 10.45 | 11.47 | 15.83 | 21.58         | 49.60 | 72.52  | 25.43         | 23.43   | 80.77         | 83.03            |
| PERCENT PPL          | 44.20  | 20.89 | 17.95 | 15.83 | 63.89         | 49.60 | 72.52  | 25.43         | 23.43   | 80.77         | 83.03            |
| PERCENT ACID INSOL   | .94    | .51   | .57   | .87   | .74           | .99   | .72    | 1.22          | 2.22    | .14           | .66              |
| PERCENT IRON OXIDE   | 2.69   | 1.47  | 1.38  | 1.38  | 1.80          | 1.07  | 1.88   | 3.92          | 1.55    | 1.56          | 3.61             |
| PERCENT ALUM OXIDE   | 22.74  | 27.63 | 25.18 | 37.43 | 19.24         | 27.63 | 19.24  | 25.61         | 39.18   | 1.05          | 13.99            |

TABLE CL-III

ECONOMIC FACTORS - FIGURES OF MERIT

| MATRIX NO.<br>DEPTH INTERVAL, FT. | INDIVIDUAL MATRICES |               |               |              | WELL NO. CL-04 |         |
|-----------------------------------|---------------------|---------------|---------------|--------------|----------------|---------|
|                                   | ECONOMIC FACTORS *  |               |               |              | UNITS (M=1000) |         |
|                                   | 1                   | 2             | 3             | 4            | 115-121        | 115-121 |
| * OVERBURDEN                      | FT.<br>MT/AC        | 23.00<br>45.1 | 17.00<br>33.3 | 9.00<br>17.6 |                |         |
| * MATRIX                          | FT.<br>MT/AC        | 9.00<br>18.1  | 7.00<br>14.2  | 4.00<br>15.4 | 6.00<br>15.0   |         |
| * BPL IN MATRIX                   | PERCENT<br>MT/AC    | 9.31<br>1.7   | 11.16<br>1.6  | 9.58<br>1.5  | 8.97<br>1.3    |         |
| * OVERBURDEN/MATRIX               | RATIO               | 5.11          | 3.29          | 4.25         | 1.50           |         |
| WASH-SCREEN PRODUCTS              |                     |               |               |              |                |         |
| +10 MESH                          | MT/AC               | .2            | 1.6           | .8           | 1.2            |         |
| -16+150 MESH                      | MT/AC               | 13.4          | 6.7           | 12.6         | 10.2           |         |
| -150 MESH (LOSS)                  | MT/AC               | 4.5           | 5.9           | 2.1          | 3.6            |         |
| * FLOTATION CONCENTRATE PRODUCT   | MT/AC               | 1.4           | 1.4           | 1.2          | 1.2            |         |
| TOTAL USEFUL PRODUCTS**           | MT/AC               | 1.6           | 3.0           | 2.0          | 2.5            |         |
| BPL RECOVERY                      |                     |               |               |              |                |         |
| +10 MESH                          | MT/AC               | .1            | .2            | .1           | .3             |         |
| -16+150 (FLOT. CONC.)             | PERCENT BPL         | 53.6          | 56.8          | 62.0         | 45.5           |         |
| -16+150 (FLOT. CONC.)             | MT/AC               | .7            | .8            | .8           | .6             |         |
| * TOTAL                           | MT/AC               | .8            | 1.0           | .8           | .8             |         |
| * RECOVERED FROM MATRIX           | PERCENT             | 46.58         | 61.03         | 55.76        | 60.22          |         |
| * OVERBURDEN / PRODUCT            | CU YD/T             | 45.9          | 12.0          | 6.9          | 4.6            |         |
| * MATRIX / PRODUCTS               | CU YD/T             | 9.19          | 3.78          | 3.20         | 3.94           |         |
| * 1+A IN FLOT. CONC.              | PERCENT             | 4.57          | 3.75          | 3.13         | 4.47           |         |
| FIGURES OF MERIT                  | UNIT                | ECON. LEVEL   |               |              |                |         |
| OVERBURDEN                        | FT                  | 1.91          | 3.63          | 5.18         | 9.78           |         |
| MATRIX                            | FT                  | 3.00          | 2.33          | 1.33         | 2.00           |         |
| BPL IN FLOT. CONC.(1)             | PERCENT             | .93           | 1.12          | .96          | .90            |         |
| BPL IN FLOT. CONC.(2)             | PERCENT             | 1.03          | 1.09          | 1.19         | .88            |         |
| OVERBURDEN/MATRIX                 | RATIO               | .39           | .61           | .47          | .33            |         |
| OVERBURDEN/PRODUCTS               | CU YD/T             | .38           | 1.46          | 2.53         | 3.79           |         |
| 1+A IN FLOT. CONC.                | PERCENT             | 1.09          | 1.33          | 1.60         | 1.12           |         |
| PRODUCTS RECOVERY                 | T/AC-FT             | .44           | 1.07          | 1.26         | 1.02           |         |
| BPL (+150) RECOVERY               | PERCENT             | .74           | .97           | .89          | .96            |         |
| MATRIX/PRODUCTS                   | CU YD/T             | .65           | 1.59          | 1.88         | 1.52           |         |

(1) FOR WET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
 NOTES: OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

TABLE CL-III (CONT.)

## ECONOMIC FACTORS - FIGURES OF MERIT

| ECONOMIC FACTORS *              | COMBINED MATRICES |                |                |                |          | WELL NO. CL-04 |
|---------------------------------|-------------------|----------------|----------------|----------------|----------|----------------|
|                                 | MATRICES          | MATRICES       | MATRICES       | MATRICES       | MATRICES |                |
|                                 | 1-1               | 1-2            | 1-3            | 1-4            |          |                |
| UNIT (M=1000)                   |                   |                |                |                |          |                |
| * OVERBURDEN                    | 46.00<br>90.2     | 69.00<br>135.2 | 66.00<br>168.6 | 95.00<br>186.2 |          |                |
| FT.<br>MT/AC                    |                   |                |                |                |          |                |
| * MATRIX                        | 9.00<br>18.1      | 16.00<br>32.3  | 20.00<br>47.7  | 26.00<br>62.7  |          |                |
| FT.<br>MT/AC                    |                   |                |                |                |          |                |
| * BPL IN MATRIX                 | 9.31<br>1.7       | 10.12<br>3.3   | 9.95<br>4.7    | 9.71<br>6.1    |          |                |
| PERCENT<br>MT/AC                |                   |                |                |                |          |                |
| * OVERBURDEN/MATRIX             | 5.11              | 4.31           | 4.30           | 3.65           |          |                |
| RATIO                           |                   |                |                |                |          |                |
| WASH-SCREEN PRODUCTS            |                   |                |                |                |          |                |
| +16 MESH                        | .2                | 1.8            | 2.6            | 3.8            |          |                |
| -16+150 MESH                    | 13.4              | 20.1           | 32.7           | 42.9           |          |                |
| -150 MESH (LOSS)                | 4.5               | 10.3           | 12.4           | 16.0           |          |                |
| MT/AC<br>MT/AC<br>MT/AC         |                   |                |                |                |          |                |
| * FLOTATION CONCENTRATE PRODUCT | 1.4               | 1.4            | 1.2            | 1.2            |          |                |
| TOTAL USEFUL PRODUCTS**         | 1.6               | 4.6            | 6.6            | 9.0            |          |                |
| MT/AC<br>MT/AC                  |                   |                |                |                |          |                |
| BPL RECOVERY                    |                   |                |                |                |          |                |
| +16 MESH                        | .1                | .2             | .3             | .5             |          |                |
| -16+150 (FLOT. CONC.)           | *****             | *****          | *****          | *****          |          |                |
| -16+150 (FLOT. CONC.)           | .7                | 1.5            | 2.3            | 2.8            |          |                |
| TOTAL                           | .8                | 1.8            | 2.6            | 3.4            |          |                |
| * RECOVERED FROM MATRIX         | 46.58             | 53.59          | 54.27          | 55.58          |          |                |
| PERCENT                         |                   |                |                |                |          |                |
| * OVERBURDEN / PRODUCT          | 45.9              | 23.6           | 17.3           | 13.8           |          |                |
| * MATRIX / PRODUCTS             | 9.19              | 5.65           | 4.90           | 4.64           |          |                |
| * I+A IN FLOT. CONC.            | 4.57              | 4.21           | 3.99           | 4.10           |          |                |
| CU YD/T<br>CU YD/T<br>PERCENT   |                   |                |                |                |          |                |
| FIGURES OF MERIT                |                   |                |                |                |          |                |
| UNIT                            |                   |                |                |                |          |                |
| ECON. LEVEL                     |                   |                |                |                |          |                |
| OVERBURDEN                      | 1.91              | 1.28           | 1.02           | .93            |          |                |
| MATRIX                          | 3.00              | 5.33           | 6.67           | 8.67           |          |                |
| BPL IN FLOT. CONC.(1)           | .93               | 1.01           | .99            | .97            |          |                |
| BPL IN FLOT. CONC.(2)           | .81               | .84            | .87            | .83            |          |                |
| OVERBURDEN/MATRIX               | 1.03              | 1.06           | 1.10           | 1.05           |          |                |
| RATIO                           | .39               | .46            | .47            | .55            |          |                |
| CU YD/T                         | 4.36              | 1.90           | 3.10           | 3.57           |          |                |
| PERCENT                         | 1.09              | 1.19           | 1.25           | 1.22           |          |                |
| I+A IN FLOT. CONC.              | .44               | .71            | .82            | .87            |          |                |
| PRODUCTS RECOVERY               | .74               | .85            | .86            | .88            |          |                |
| BPL (+150) RECOVERY             | .65               | 1.06           | 1.22           | 1.29           |          |                |
| MATRIX/PRODUCTS                 |                   |                |                |                |          |                |

(1) FOR WET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC. NOTES. OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

TABLE CL-III (CONT.)

ECONOMIC FACTORS - FIGURES OF MERIT

|                                 |               | INDIVIDUAL MATRICES |      |
|---------------------------------|---------------|---------------------|------|
|                                 |               | WELL NO. CL-05      |      |
|                                 |               | 1                   |      |
|                                 |               | 91-113              |      |
|                                 |               | JUNIT (#=1000)      |      |
| MATRIX NO.                      |               | 91.00               |      |
| DEPTH INTERVAL, FT.             |               | 178.4               |      |
| ECONOMIC FACTORS *              |               |                     |      |
| * OVERBURDEN                    | FT. MT/AC     | 22.00               |      |
|                                 |               | 55.1                |      |
| * MATRIX                        | PERCENT MT/AC | 15.49               |      |
|                                 |               | 8.5                 |      |
| * BPL IN MATRIX                 | RATIO         | 4.14                |      |
| * OVERBURDEN/MATRIX             |               |                     |      |
| WASH-SCREEN PRODUCTS            |               |                     |      |
| +10 MESH                        | MT/AC         | 3.7                 |      |
| -10+150 MESH                    | MT/AC         | 27.6                |      |
| -150 MESH (LOSS)                | MT/AC         | 23.8                |      |
| * FLUTATION CONCENTRATE PRODUCT |               |                     |      |
| TOTAL USEFUL PRODUCTS**         | MT/AC         | 9.2                 |      |
|                                 | MT/AC         | 12.9                |      |
| BPL RECOVERY                    |               |                     |      |
| +16 MESH                        | MT/AC         | 5                   |      |
| -16+150 (FLOT. CONC.)           | PERCENT BPL   | 57.7                |      |
| -16+150 (FLOT. CONC.)           | MT/AC         | 5.3                 |      |
| TOTAL                           | MT/AC         | 5.8                 |      |
| RECOVERED FROM MATRIX           | PERCENT       | 67.74               |      |
| * OVERBURDEN / PRODUCT          | CU YD/T       | 8.9                 |      |
| * MATRIX / PRODUCTS             | CU YD/T       | 2.76                |      |
| * I+A IN FLOT. CONC.            | PERCENT       | 3.77                |      |
| FIGURES OF MERIT                |               |                     |      |
| OVERBURDEN                      | UNIT          | ECON. LEVEL         |      |
| MATRIX                          | FT            | 88 MAX              | .97  |
| MATRIX BPL                      | PERCENT       | 3 MIN               | 7.33 |
| BPL IN FLOT. CONC. (1)          | PERCENT       | 10 MIN              | 1.55 |
| BPL IN FLOT. CONC. (2)          | PERCENT       | 66 MIN              | .87  |
| OVERBURDEN/MATRIX               | RATIO         | 66 MIN              | 1.11 |
| OVERBURDEN/PRODUCTS             | CU YD/T       | 2 MAX               | .48  |
| I+A IN FLOT. CONC.              | PERCENT       | 17.5 MAX            | 1.96 |
| PRODUCTS RECOVERY               | T/AC-FT       | 5 MAX               | 1.33 |
| BPL (+150) RECOVERY             | PERCENT       | 400 MIN             | 1.46 |
| MATRIX/PRODUCTS                 | CU YD/T       | 63 MIN              | 1.08 |
|                                 |               | 6 MAX               | 2.18 |

(1) FOR NET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC. NOTES. OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

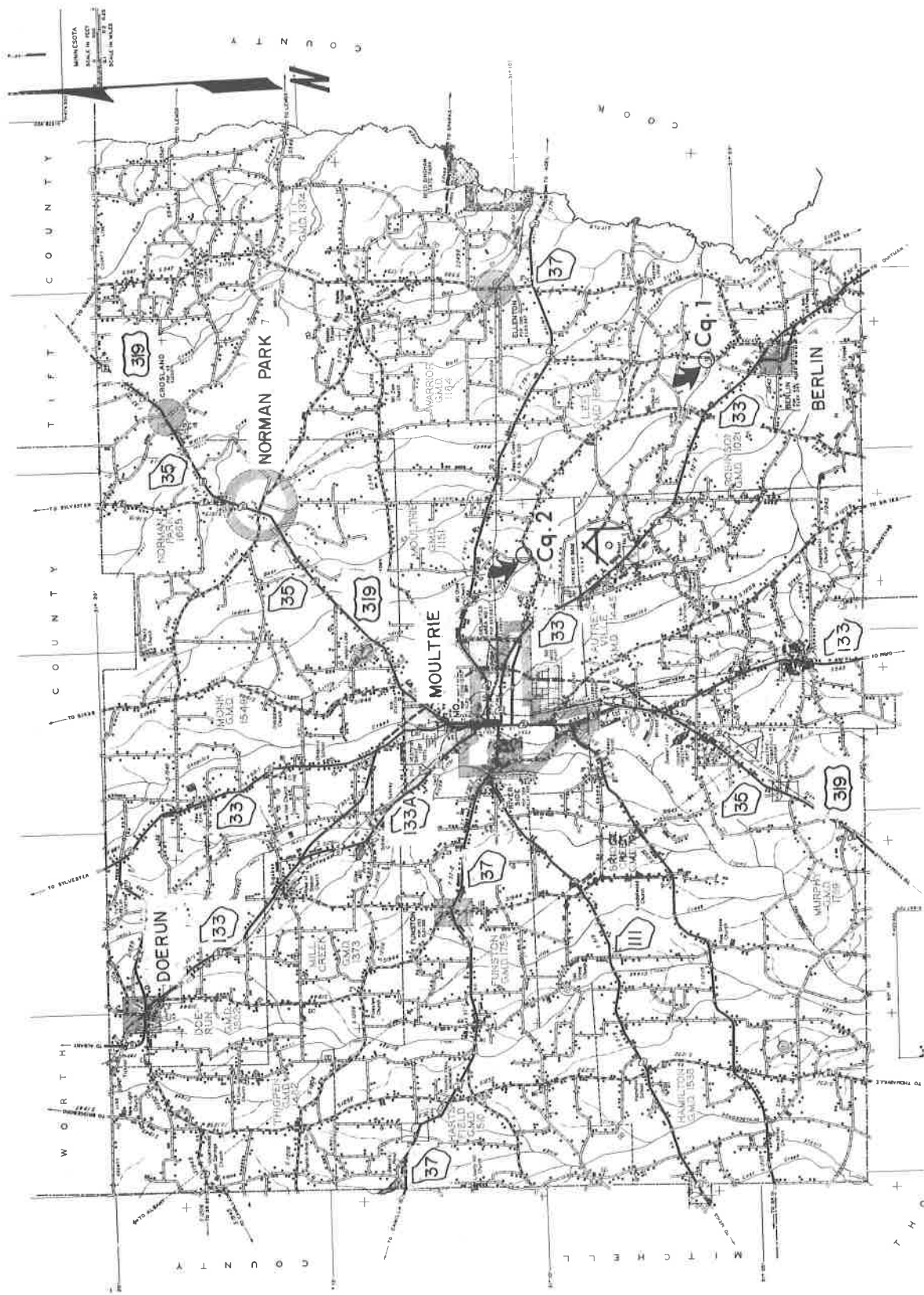
COLQUITT COUNTY

COLQUITT COUNTY  
SUMMARY OF RESULTS

The holes in Colquitt County were drilled primarily for fuller's earth, but phosphorite was checked.

Phosphorite content was insufficient for beneficiation.

No logs were run on these holes because of a priority use of the logging equipment in another part of the state in conjunction with the other drilling rig.



**COLQUITT COUNTY**  
**GEORGIA**

0 1 2 3 4  
**SCALE IN MILES**

Figure CQ-1. Location of Holes - Colquitt County

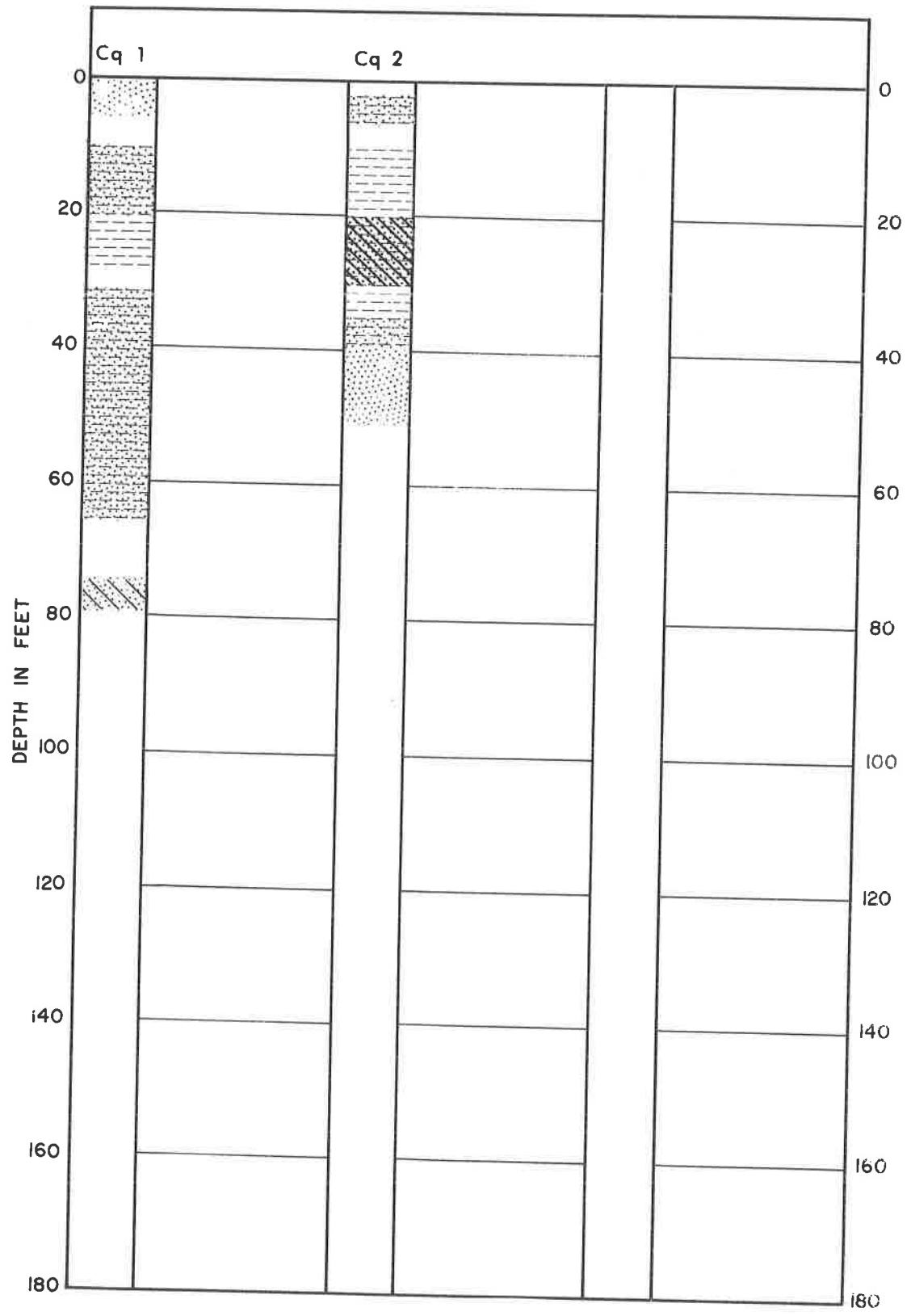


Figure Cq-3. Lithologic Logs - Colquitt County



TABLE CQ-1  
 BPL DETERMINATION ON CORES  
 Colquitt County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Cq-1        | 224   | 0-5            | 2             | 40  | 0        |
|             |   | 5-10           | 0             | 0   | -        |
|             |   | 10-20          | 10            | 100 | 0        |
|             |   | 20-28          | 8             | 100 | 0        |
|             |   | 28-30          | 2             | 100 | -        |
|             |   | 30-40          | 9             | 90  | .34      |
|             |   | 40-50          | 8             | 80  | 1.35     |
|             |   | 50-57          | 7             | 100 | 5.40     |
|             |   | 57-65          | 8             | 100 | 6.74     |
|             |   | 65-75          | 0             | 0   | -        |
|             |   | 75-80          | 2             | 40  | 1.01     |
| Cq-2        | 260   | 0-2            | -             | -   | -        |
|             |   | 2-6            | 4             | 100 | 0        |
|             |   | 6-10           | -             | -   | -        |
|             |   | 10-20          | 4             | 40  | 4.72     |
|             |   | 20-30          | 10            | 100 | 3.20     |
|             |   | 30-35          | 5             | 100 | 6.10     |
|             |   | 35-40          | 5             | 100 | 3.14     |
|             |   | 40-50          | 1             | 10  | 2.70     |



CRAWFORD COUNTY

## CRAWFORD COUNTY

## SUMMARY OF RESULTS

The one hole drilled in Crawford County was to check the extent of a kaolin lense noted in surface geology. This will be reported in later clay commodity study.

Since phosphorite is reported on occasions from older formations of the Coastal Plain, a systematic check was made of samples. No phosphorite was found. Cave-in of the hole prevented the obtaining of electric logs. The gamma-ray log was run inside the drill pipe.

# CRAWFORD COUNTY GEORGIA

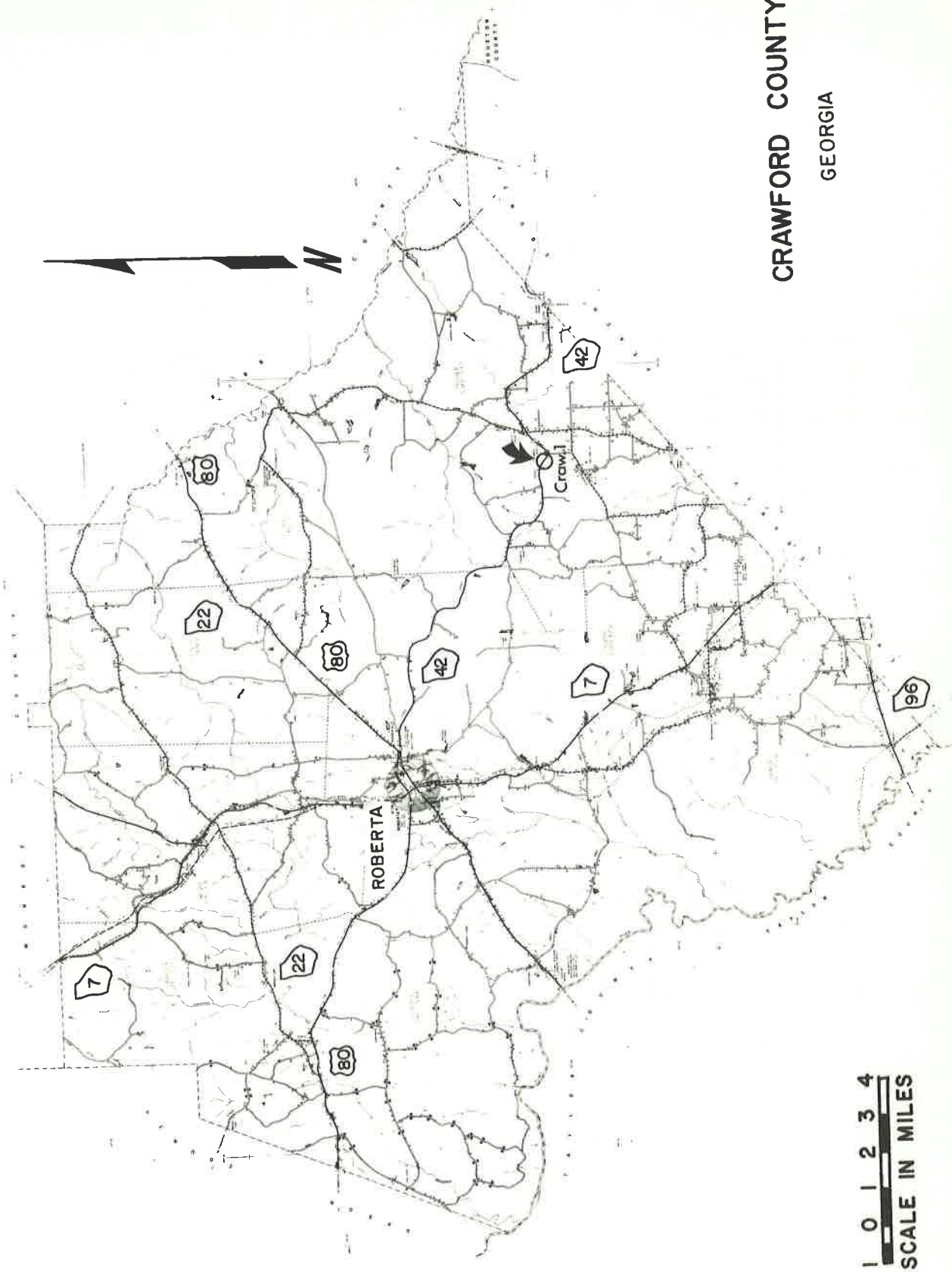


Figure CRAW-1. Location of Holes - Crawford County

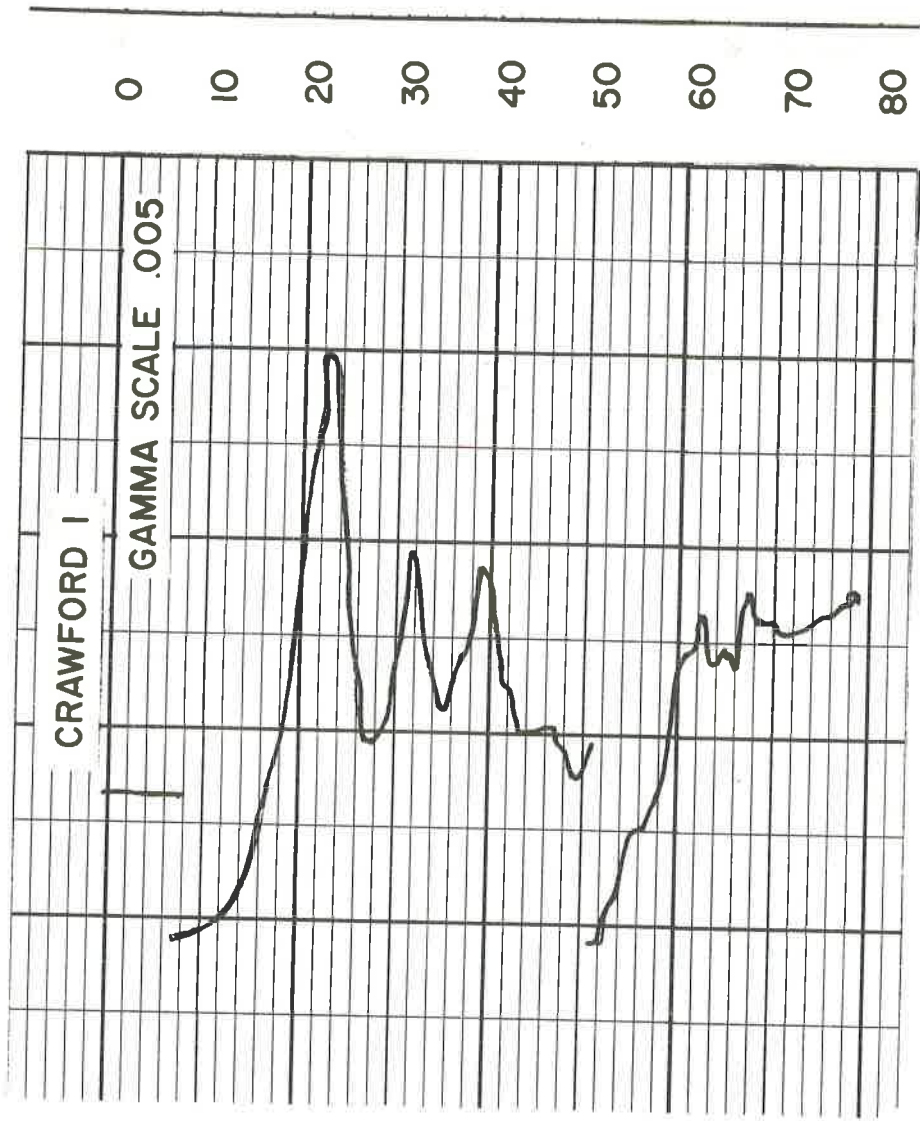


Figure CRAW-2. Gamma-Ray Logs - Crawford County Hole CRAW-1

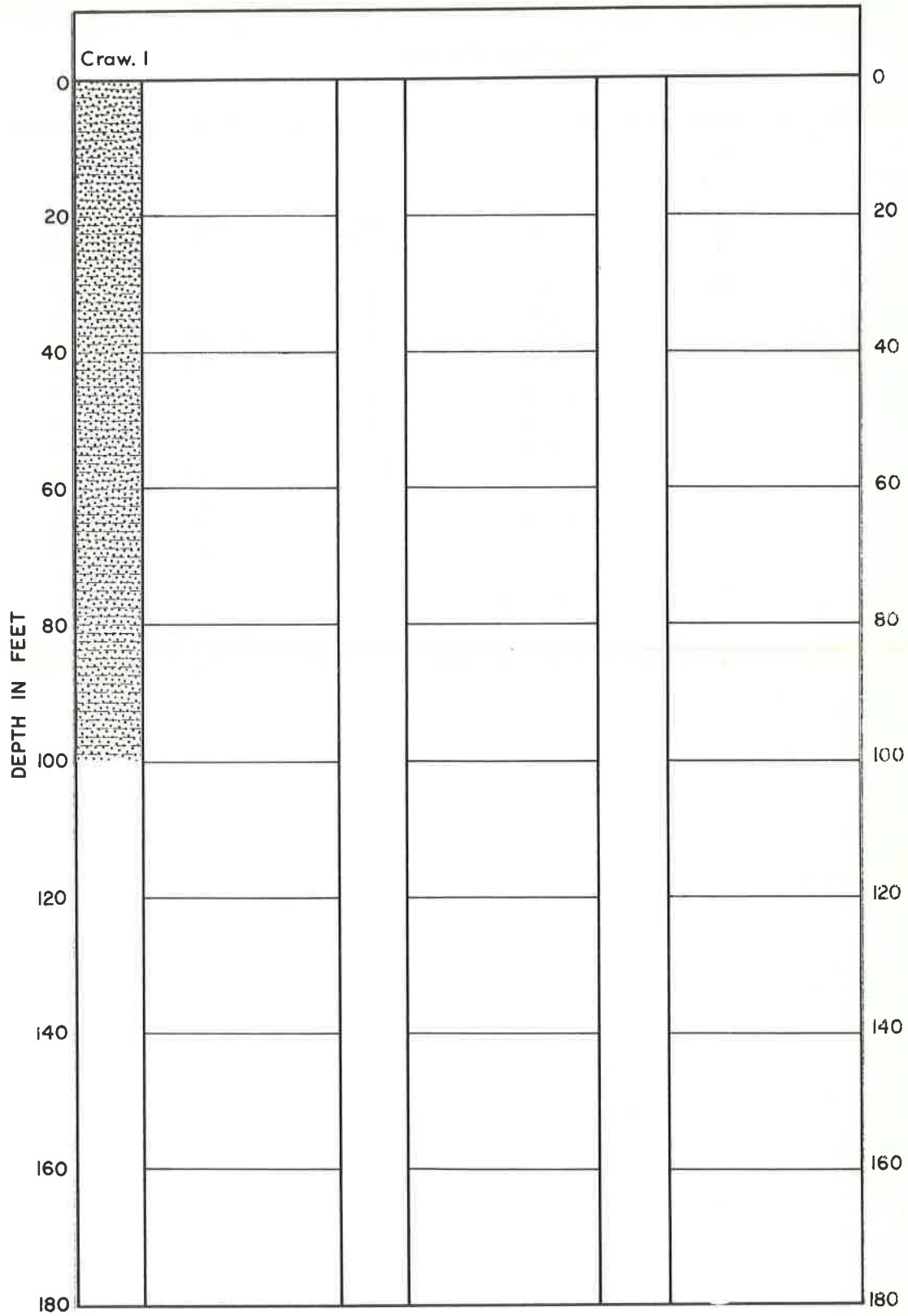


Figure Craw-3. Lithologic Logs - Crawford County

TABLE CRAW-I  
BPL DETERMINATION ON CORES  
Crawford County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Craw-1      | 564   | 0-3            | 2             | 67  | 0        |
|             |   | 3-6            | 2             | 67  | 0        |
|             |   | 6-9            | 3             | 100 | 0        |
|             |   | 9-12           | 2             | 67  | 0        |
|             |   | 12-15          | 2             | 67  | 0        |
|             |   | 15-30          | 6             | 40  | 0        |
|             |   | 30-45          | 2             | 13  | 0        |
|             |   | 45-60          | 11            | 73  | 0        |
|             |   | 60-65          | 5             | 100 | 0        |
|             |   | 65-70          | 5             | 100 | 0        |
|             |   | 70-75          | 5             | 100 | 0        |
|             |   | 75-90          | 15            | 100 | 0        |
|             |   | 90-100         | 9             | 90  | 0        |



HOUSTON COUNTY

HOUSTON COUNTY  
SUMMARY OF RESULTS

Holes drilled in this county were also for kaolin. Samples were systematically tested for phosphorite. Results were meager.

Cave-in of hole Ho-1 was the reason for not presenting electric log data of that hole. Gamma-ray logs were run inside the drill pipe.

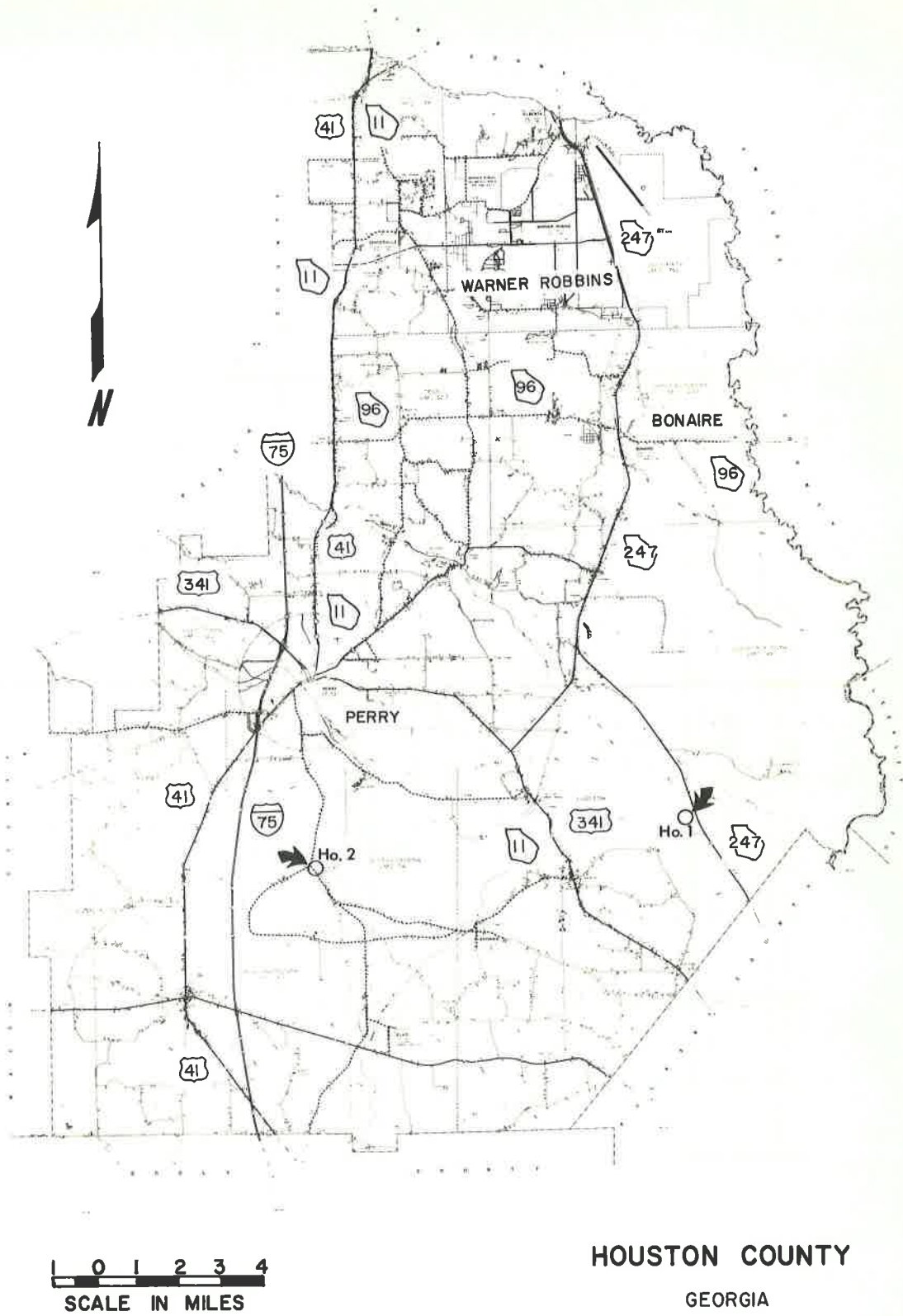


Figure HO-1. Location of Holes - Houston County

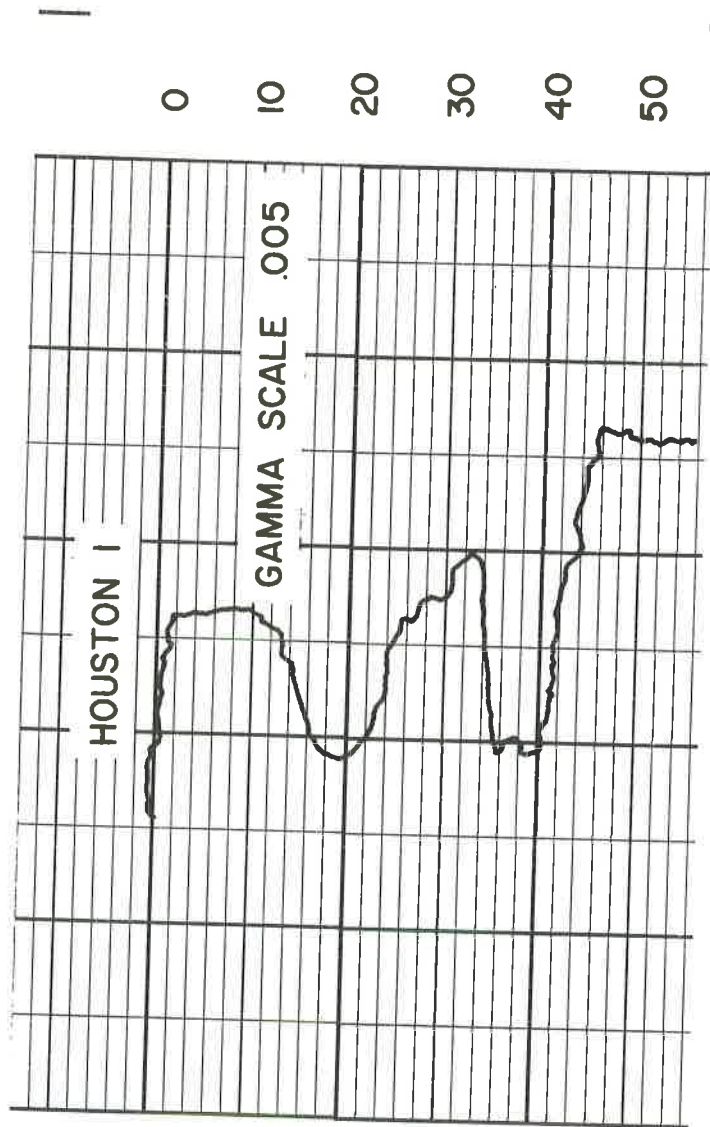


Figure HO-2. Gamma-Ray Logs - Houston County  
Hole Ho-1

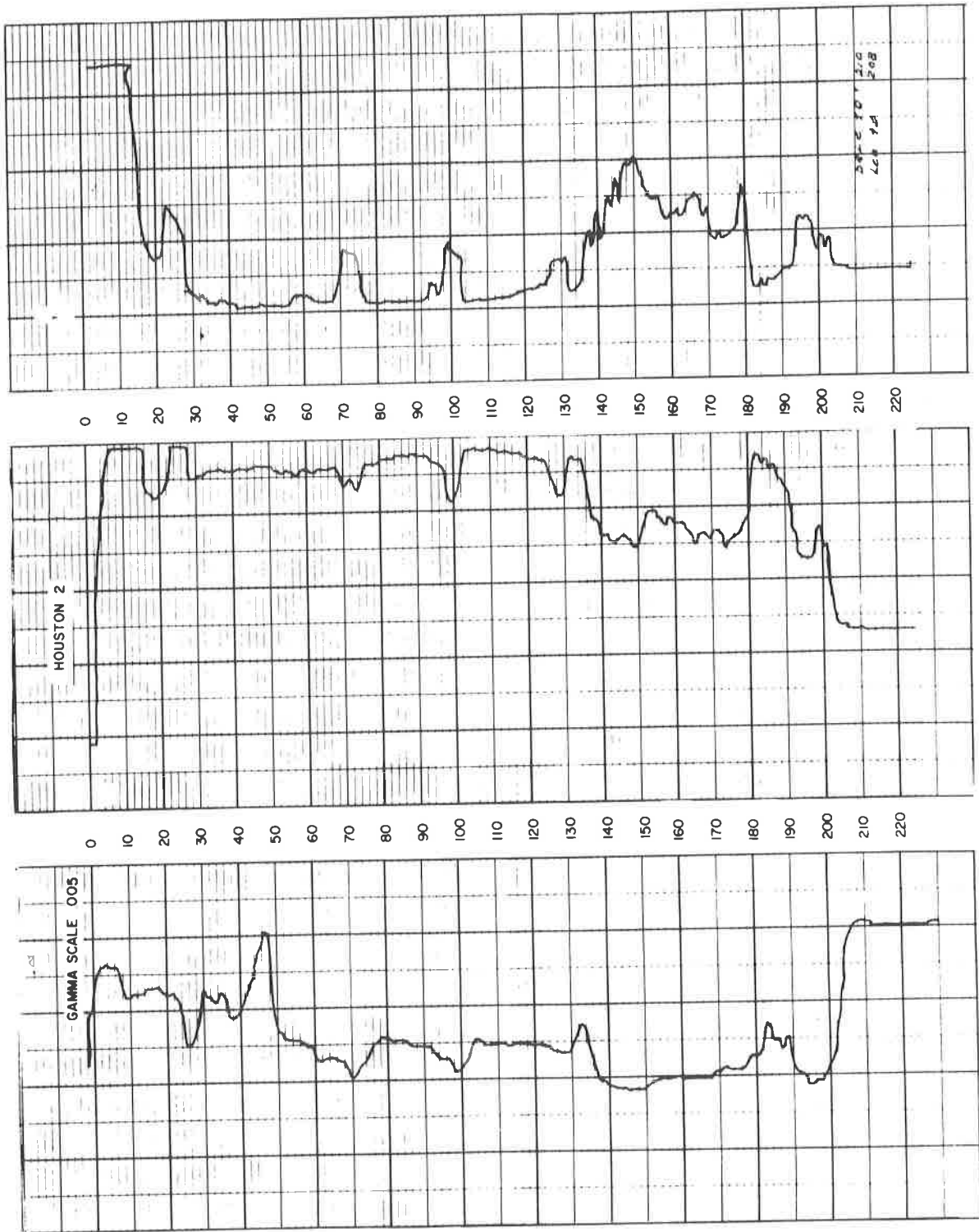


Figure HO-2. Electric and Gamma-Ray Logs - Houston County Hole Ho-2

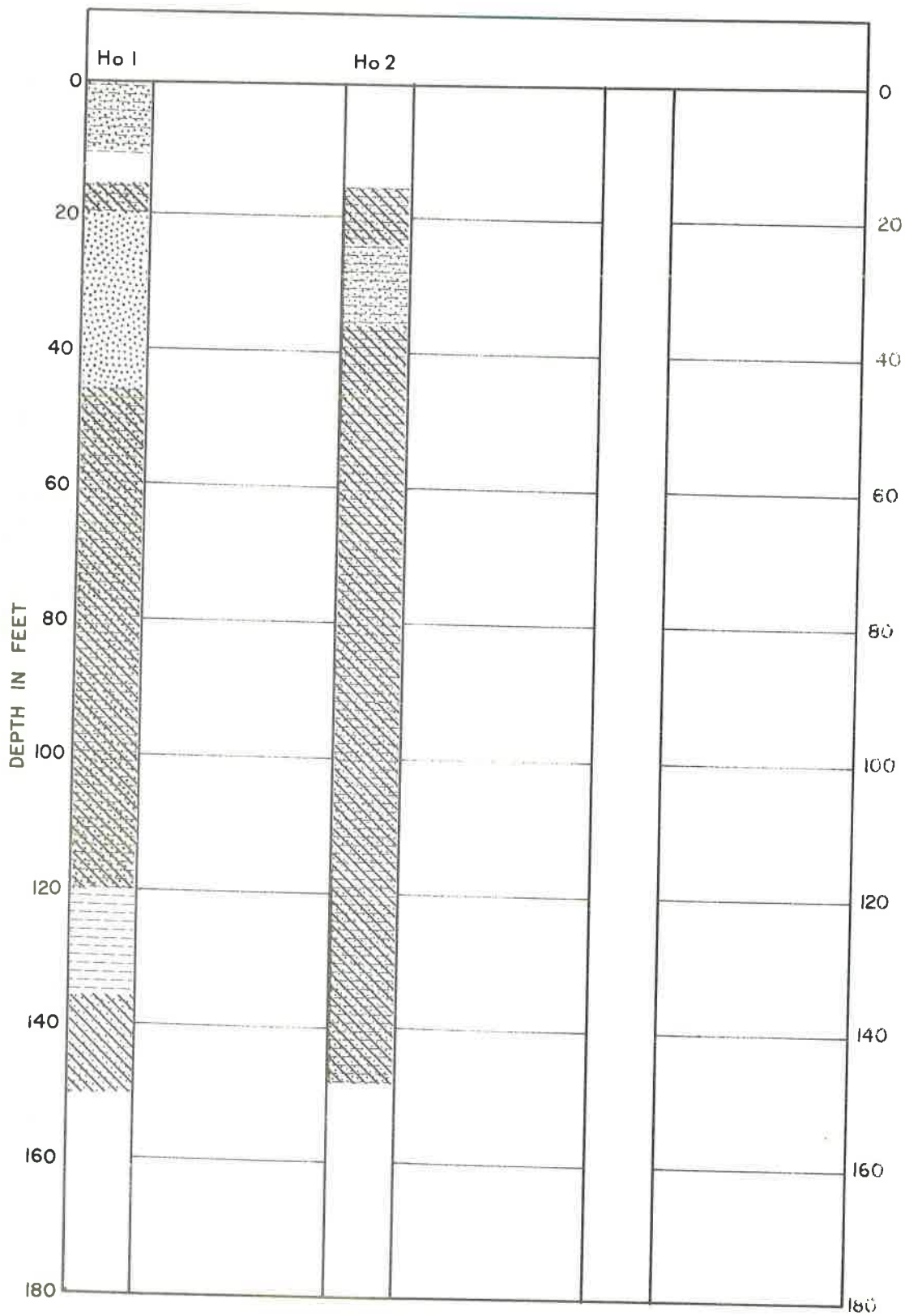


Figure Ho-3. Lithologic Logs - Houston County

TABLE HO-I

## BPL DETERMINATION ON CORES

Houston County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL         |
|-------------|---|----------------|---------------|-----|-------------|
|             |   |                | Feet          | %   | %           |
| Ho-1        | 400   | 0-10           | 7             | 70  | 0           |
|             |   | 10-15          | 0             | 0   | -           |
|             |   | 15-20          | 2             | 40  | 0           |
|             |   | 20-30          | 1             | 10  | 0           |
|             |   | 30-45          | 2             | 13  | 0           |
|             |   | 45-60          | 11            | 78  | 0.78        |
|             |   | 60-75          | 14            | 93  | 0.37        |
|             |   | 75-90          | 10            | 67  | 0           |
|             |   | 90-105         | 13            | 87  | 0           |
|             |   | 105-120        | 14            | 93  | 0           |
|             |   | 120-135        | 10            | 67  | 0           |
|             |   | 135-150        | 4             | 27  | 0           |
|             |   | Ho-2           | 434           | 0-5 | Wash Sample |
| 5-10        | Wash Sample                                 |                |               | -   | 0           |
| 10-15       | Wash Sample                                 |                |               | -   | 0           |
| 15-23       | 8   |                |               | 100 | 0           |
| 23-35       | 10  |                |               | 83  | 0           |
| 35-50       | 15  |                |               | 100 | 1.15        |
| 50-60       | 3   |                |               | 30  | 0.37        |
| 60-71       | 2   |                |               | 13  | 0.57        |
| 71-90       | 5   |                |               | -   | 0           |
| 90-105      | 9   |                |               | 60  | 0           |
| 105-125     | 10  |                |               | 50  | 0           |
| 125-142     | 5   |                |               | -   | 0           |
| 142-147     | 3   |                |               | 60  | 0           |
| 147-165     | -   |                |               | -   | -           |
| 165-170     | Wash Sample                                 |                |               | -   | 0           |
| 170-175     | Wash Sample                                 |                |               | -   | 0           |
| 175-180     | Wash Sample                                 |                |               | -   | 0           |
| 180-185     | Wash Sample                                 |                |               | -   | 0           |
| 185-190     | Wash Sample                                 |                |               | -   | 0.71        |
| 190-195     | Wash Sample                                 |                |               | -   | 0           |
| 195-200     | Wash Sample                                 |                |               | -   | 0           |
| 200-205     | Wash Sample                                 | -              | 0             |     |             |
| 205-210     | Wash Sample                                 | -              | 0             |     |             |





LOWNDES COUNTY

## LOWNDES COUNTY

## SUMMARY OF RESULTS

New Lowndes County holes drilled are 10 through 14. Only the area near hole 12 seems to warrant additional study. This is based on thickness of matrix, low overburden, and ability to be beneficiated to 75% BPL.

Electric logs were not run on hole Lo-14 because of caving hole conditions.

The gamma-ray log was run inside the drill pipe.

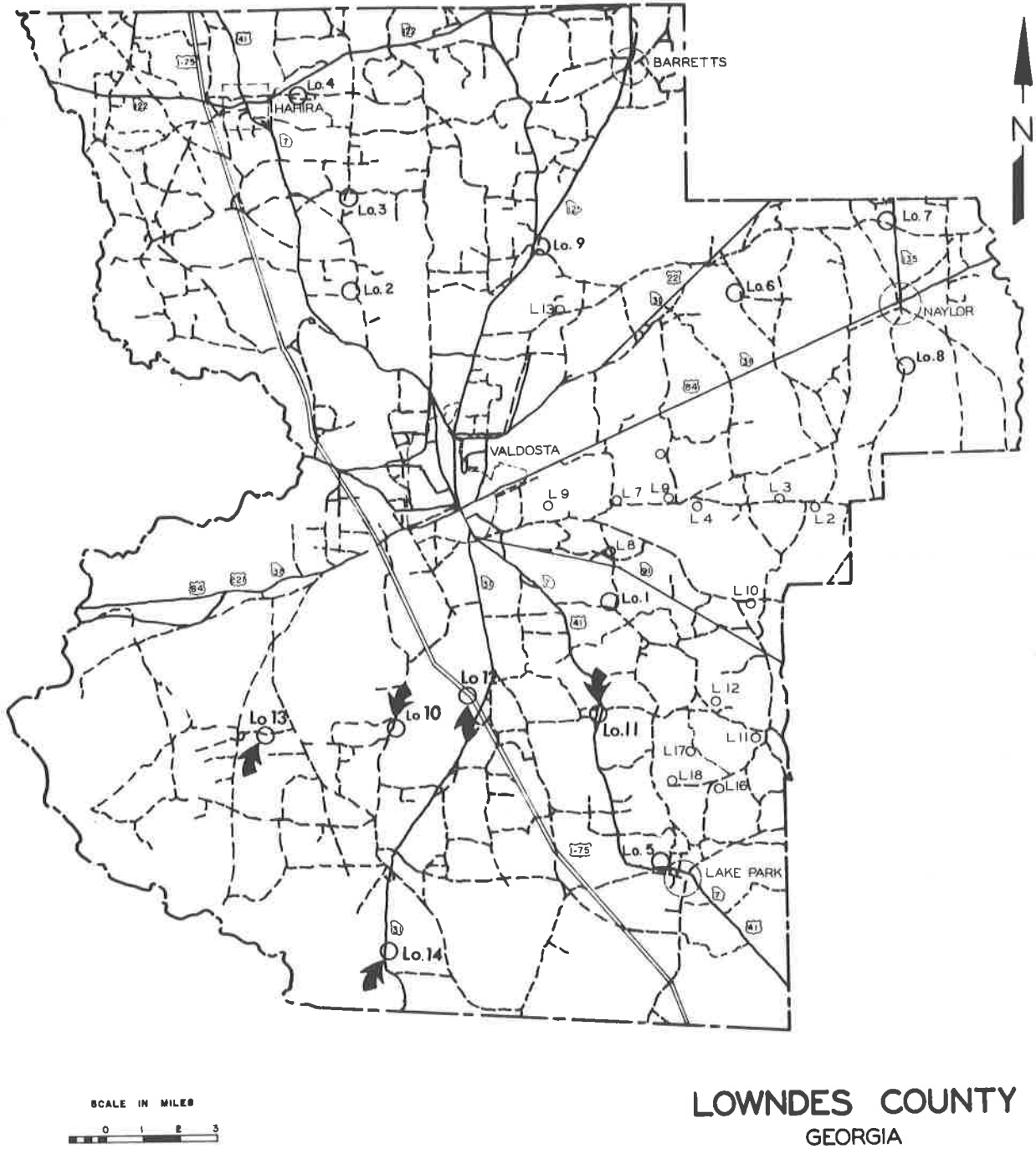


Figure LO-1. Location of Holes - Lowndes County

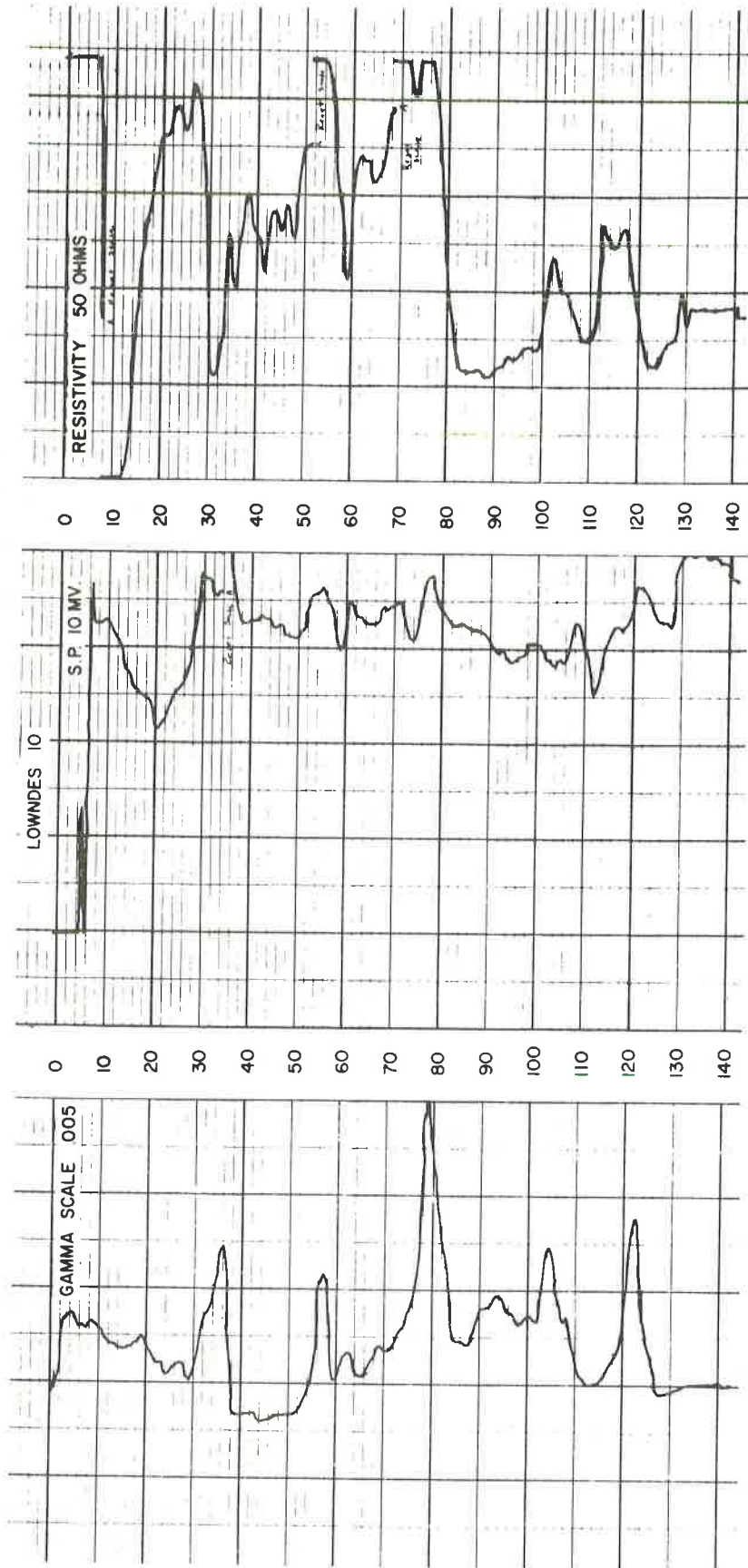


Figure 10-2. Electric and Gamma-Ray Logs - Lowndes County  
Hole 10-10

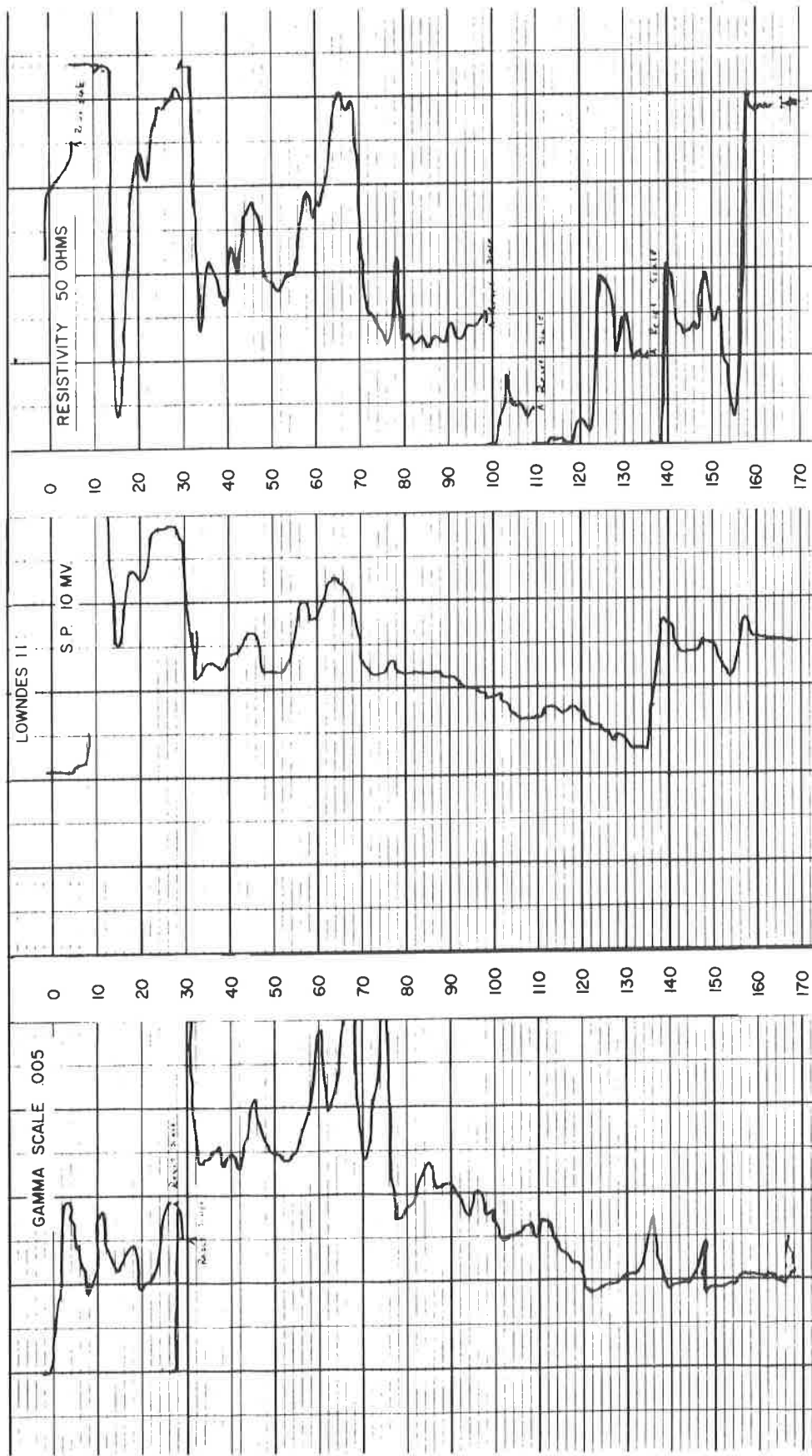


Figure 10-2. Electric and Gamma-Ray Logs - Lowndes County Hole 10-11

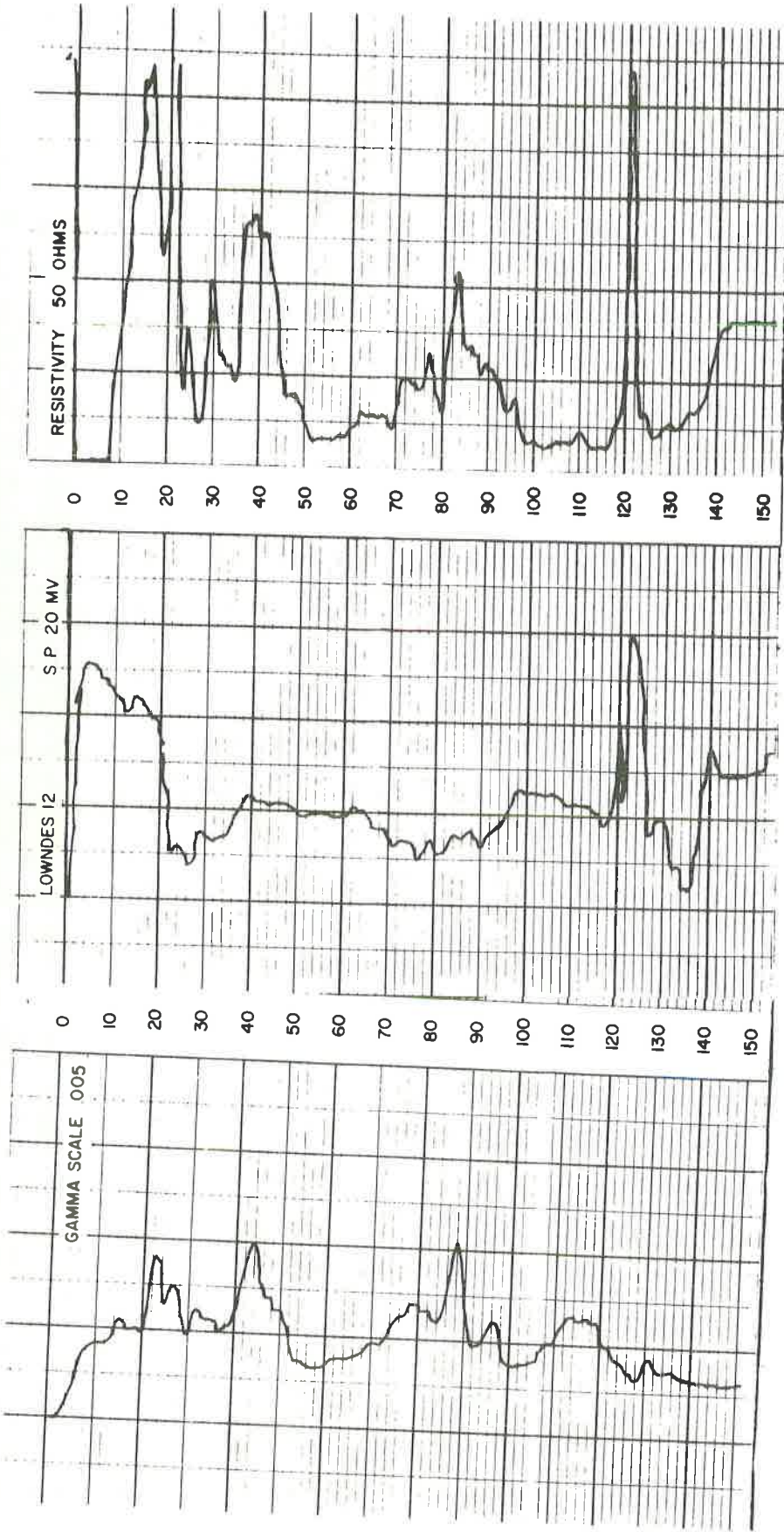


Figure 10-2. Electric and Gamma-Ray Logs - Lowndes County  
Hole 10-12

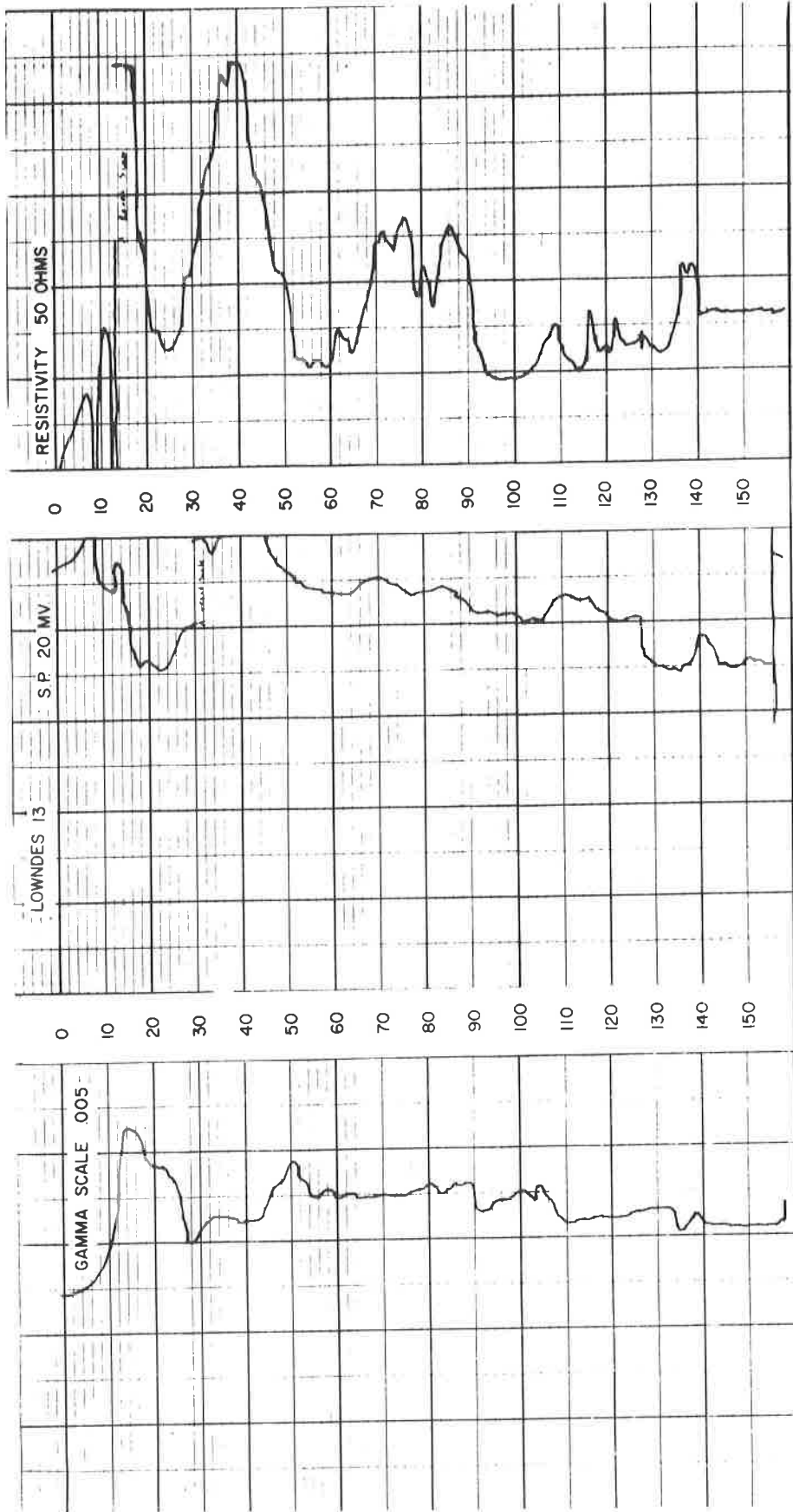


Figure 10-2. Electric and Gamma-Ray Logs - Lowndes County  
Hole Lo-13

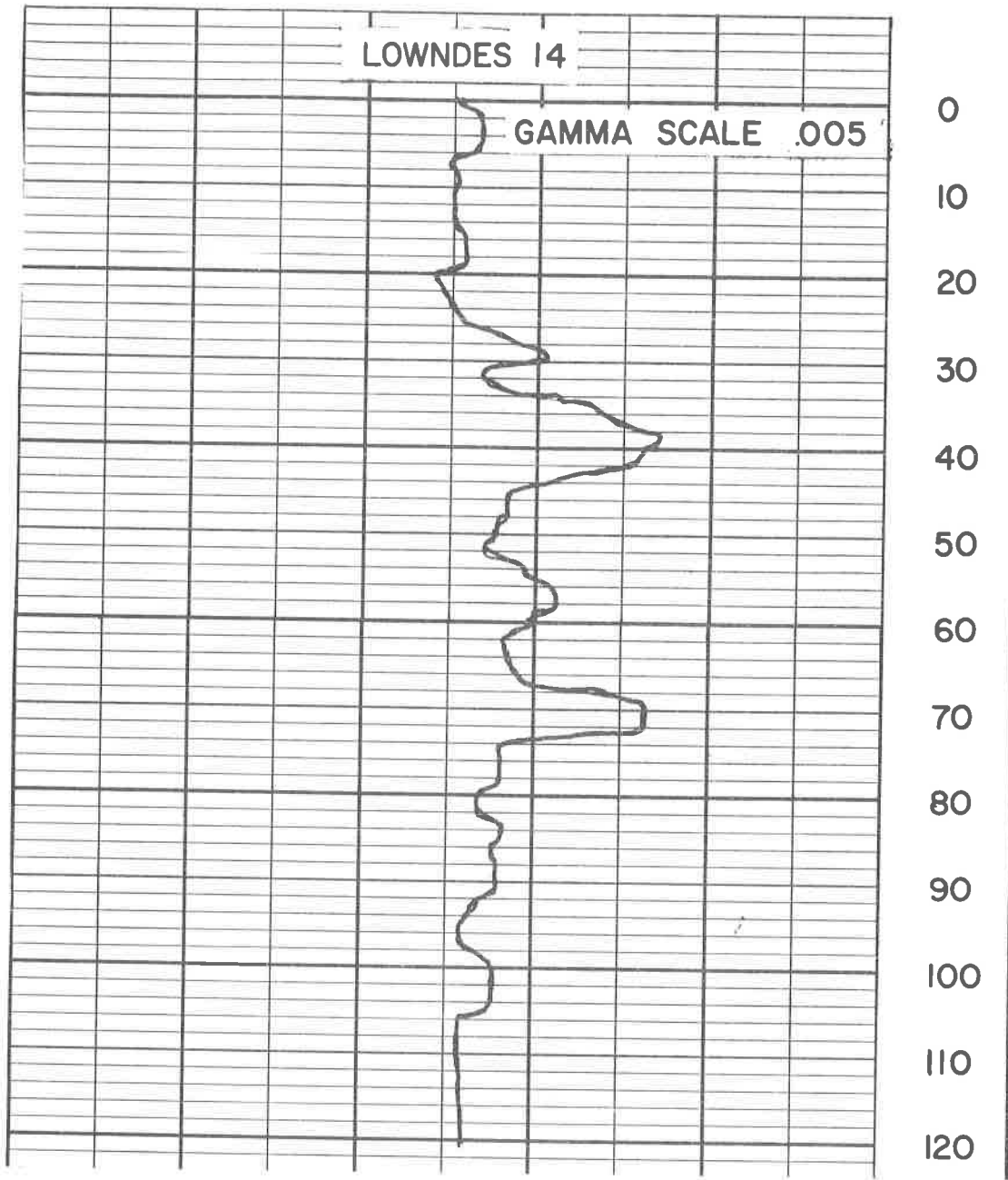


Figure LO-2. Electric and Gamma-Ray Logs - Lowndes County Hole Lo-14



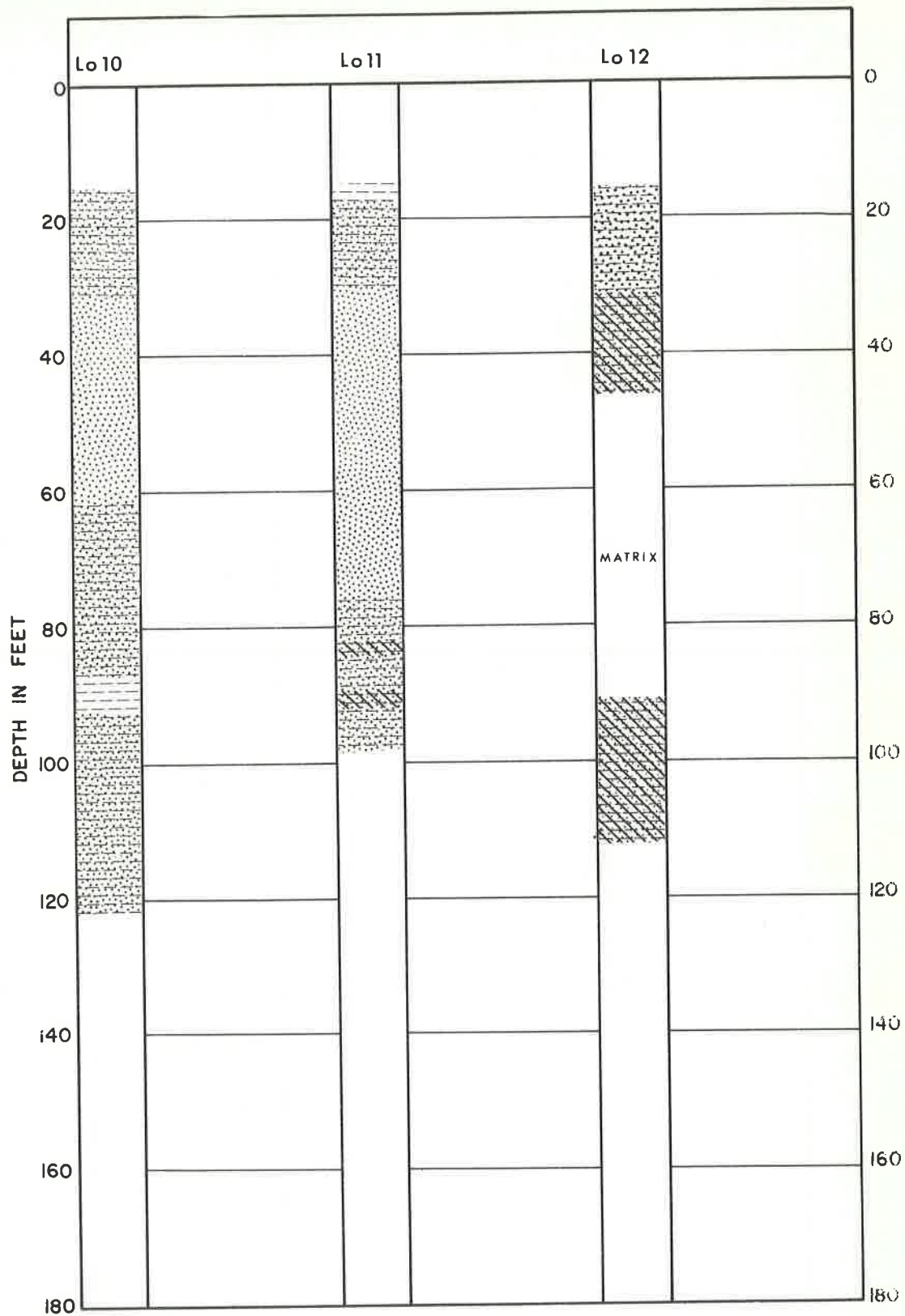


Figure Lo-3. Lithologic Logs - Lowndes County

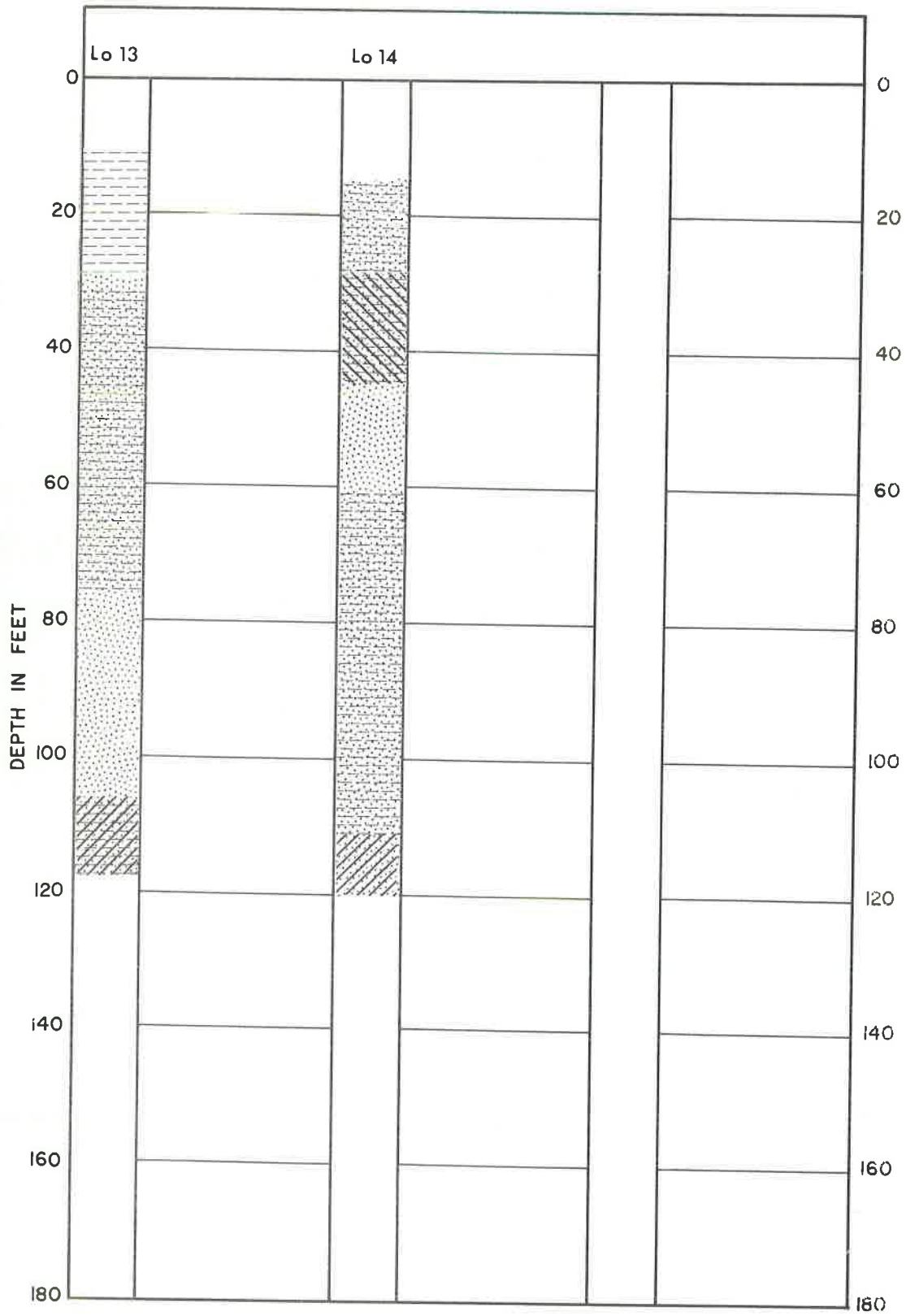


Figure Lo-3. Lithologic Logs - Lowndes County (Cont.)

TABLE LO-I  
BPL DETERMINATION ON CORES  
Lowndes County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |        | BPL<br>% |        |   |   |
|-------------|---|----------------|---------------|--------|----------|--------|---|---|
|             |   |                | Feet          | %      |          |        |   |   |
| Lo-10       | 208   | 0-15           | Wash          | Sample | -        | 0      |   |   |
|             |   | 15-19          | 3             | 75     | 0        |        |   |   |
|             |   | 25-31          | 5             | 83     | 0        |        |   |   |
|             |   | 31-51          | 5             | 50     | 0        |        |   |   |
|             |   | 51-61          | 4             | 40     | 0        |        |   |   |
|             |   | 61-76          | -             | -      | -        |        |   |   |
|             |   | 76-81          | 5             | 100    | 3.03     |        |   |   |
|             |   | 81-86          | 5             | 100    | 6.37     |        |   |   |
|             |   | 86-91          | 2             | 33     | 9.98     |        |   |   |
|             |   | 91-94          | 3             | 100    | 7.79     |        |   |   |
|             |   | 94-98          | 4             | 100    | 7.96     |        |   |   |
|             |   | 98-101         | 3             | 100    | 8.70     |        |   |   |
|             |   | 101-107        | -             | -      | -        |        |   |   |
|             |   | 107-112        | 3             | 60     | 3.71     |        |   |   |
|             |   | 112-121        | 2             | 22     | .34      |        |   |   |
|             |   | 121-125        | Wash          | Sample | -        | 1.01   |   |   |
|             |   | 125-130        | Wash          | Sample | -        | 1.01   |   |   |
|             |   | 130-135        | Wash          | Sample | -        | .67    |   |   |
|             |   | Lo-11          | 178           | 0-5    | Wash     | Sample | - | 0 |
|             |   |                |               | 5-10   | Wash     | Sample | - | 0 |
| 10-15       | Wash  |                |               | Sample | -        | 0      |   |   |
| 15-17       | 2   |                |               | 100    | .88      |        |   |   |
| 17-30       | 3   |                |               | 23     | 1.79     |        |   |   |
| 30-45       | 2   |                |               | 13     | 7.49     |        |   |   |
| 45-60       | -   |                |               | -      | -        |        |   |   |
| 60-75       | 3   |                |               | 20     | 16.29    |        |   |   |
| 75-82       | 7   |                |               | 100    | 7.01     |        |   |   |
| 82-84       | 2   |                |               | 100    | 32.17    |        |   |   |
| 84-90       | 6   |                |               | 100    | 4.18     |        |   |   |
| 90-92       | 2   |                |               | 100    | 9.61     |        |   |   |
| 92-94       | 2   |                |               | 100    | 9.27     |        |   |   |
| 94-96       | 1   |                |               | 50     | 3.37     |        |   |   |
| 96-98       | 1   |                |               | 50     | 3.17     |        |   |   |
| 98-105      | -   |                |               | -      | -        |        |   |   |
| 105-110     | Wash  |                |               | Sample | -        | 5.53   |   |   |
| 110-115     | Wash  |                |               | Sample | -        | 4.82   |   |   |
| 115-120     | Wash  |                |               | Sample | -        | 3.47   |   |   |
| 120-125     | Wash  |                |               | Sample | -        | 1.85   |   |   |
| 125-130     | Wash  | Sample         | -             | 1.69   |          |        |   |   |
| 130-135     | Wash  | Sample         | -             | 1.52   |          |        |   |   |

(Continued)

TABLE LO-I (Continued)  
BPL DETERMINATION ON CORES

## Lowndes County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Lo-11       | 178   | 135-140        | Wash Sample   | -   | 1.82     |
|             |   | 140-145        | Wash Sample   | -   | 1.52     |
|             |   | 145-150        | Wash Sample   | -   | 1.85     |
|             |   | 150-155        | Wash Sample   | -   | 3.14     |
|             |   | 155-160        | Wash Sample   | -   | 2.43     |
| Lo-12       | 201   | 0-5            | Wash Sample   | -   | .13      |
|             |   | 5-10           | Wash Sample   | -   | .61      |
|             |   | 10-15          | Wash Sample   | -   | .27      |
|             |   | 15-19          | 4             | 100 | 0        |
|             |   | 19-31          | 5             | 42  | 0        |
|             |   | 31-46          | 3             | 20  | 1.52     |
|             |   | 46-61          | 11            | 67  | 13.69    |
|             |   | 61-76          | 15            | 100 | 11.43    |
|             |   | 76-91          | 2             | 40  | 14.97    |
|             |   | 91-98          | 2             | 29  | 4.05     |
|             |   | 98-112         | 9             | 16  | 1.72     |
|             |   | 112-121        | 3             | 33  | 1.18     |
|             |   | 121-125        | Wash Sample   | -   | 3.37     |
|             |   | 125-130        | Wash Sample   | -   | 3.51     |
|             |   | 130-135        | Wash Sample   | -   | 2.56     |
| 135-140     | Wash Sample                                 | -              | 4.05          |     |          |
| 140-145     | Wash Sample                                 | -              | 4.82          |     |          |
| 145-150     | Wash Sample                                 | -              | 3.27          |     |          |
| Lo-13       | 196   | 0-15           | Wash Sample   | -   | 0        |
|             |   | 15-16          | -             | -   | -        |
|             |   | 16-29          | 13            | 100 | .67      |
|             |   | 29-31          | 1             | 50  | 0        |
|             |   | 31-46          | 3             | 43  | .34      |
|             |   | 46-49          | 3             | 100 | .67      |
|             |   | 49-61          | 7             | 58  | 1.35     |
|             |   | 61-76          | 14            | 93  | 3.17     |
|             |   | 76-91          | 10            | 67  | 9.48     |
|             |   | 91-106         | 10            | 67  | 3.20     |
| 106-117     | 7   | 63             | .44           |     |          |

(Continued)

TABLE LO-I (Continued)  
 BPL DETERMINATION ON CORES  
 Lowndes County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Lo-14       | 200   | 0-15           | -             | -   | -        |
|             |   | 15-18          | 1             | 33  | .27      |
|             |   | 18-21          | 2             | 67  | .27      |
|             |   | 21-25          | 2             | 50  | .34      |
|             |   | 25-29          | 1             | 25  | 0        |
|             |   | 29-45          | 4             | 25  | 1.55     |
|             |   | 45-60          | 4             | 27  | 2.29     |
|             |   | 60-75          | 5             | 33  | 11.46    |
|             |   | 75-90          | 7             | 47  | 6.17     |
|             |   | 90-99          | 9             | 100 | 8.50     |
|             |   | 99-111         | 5             | 42  | 2.66     |
|             |   | 111-113        | 1             | 50  | .54      |
| 113-120     | 1   | 14             | 1.35          |     |          |

TABLE LO-II  
 MATRIX BENEFICIATION RESULTS  
 LOWMEDES COUNTY

HOLE NO. 10-10 MATRIX INTERVAL = 86-91

|                      | <u>FEEU</u><br>5 | <u>+4</u> | <u>4XB</u> | <u>8A16</u> | <u>F F</u><br>16X150 | <u>(16X35</u><br><u>35X150)</u> | <u>SLIME</u><br><u>-150</u> | <u>(CONC</u><br><u>)</u> | <u>F.A.</u><br><u>TAILS</u> | <u>AMINE</u><br><u>FLOAT)</u> |
|----------------------|------------------|-----------|------------|-------------|----------------------|---------------------------------|-----------------------------|--------------------------|-----------------------------|-------------------------------|
| TOTAL MATRIX FOOTAGE | 100.0            | 0         | .03        | .25         | 8.15                 |                                 |                             |                          |                             |                               |
| DRY DENSITY LB/CU FT | 11.23            |           |            | 2.70        | 1.01                 |                                 |                             |                          |                             |                               |
| PERCENT DRY WEIGHT   | 71.75            |           |            | 93.10       | 97.51                |                                 |                             |                          |                             |                               |
| PERCENT LPL          |                  |           |            |             |                      |                                 |                             |                          |                             |                               |
| PERCENT ACID INSOL   |                  |           |            |             |                      |                                 |                             |                          |                             |                               |
| PERCENT IRON OXIDE   | 6.72             |           |            |             |                      |                                 |                             |                          |                             |                               |
| PERCENT ALUM OXIDE   | 14.10            |           |            |             |                      |                                 |                             |                          |                             |                               |
| PERCENT CALC OXIDE   | 74.41            |           |            |             |                      |                                 |                             |                          |                             |                               |

NOTE: WORK ON THE MATRIX WAS DISCONTINUED AFTER THE FLOTATION FEED WAS FOUND TO CONTAIN LESS THAN 7% BPL.

TABLE LO-II (CONT.)  
 MATRIX BENEFICIATION RESULTS  
 LOWMEDES COUNTY

| HOLE NO. LO-11       | MATRIX INTERVAL = 60-84 | FEED  |    | 4X8   | 8X16  | F F<br>16X150 | (16X35 | 35X150) | SLIME<br>-150 | (CONC | F. A.<br>TAILS | AMINE<br>FLOAT) |
|----------------------|-------------------------|-------|----|-------|-------|---------------|--------|---------|---------------|-------|----------------|-----------------|
|                      |                         | +4    | 24 |       |       |               |        |         |               |       |                |                 |
| TOTAL MATRIX FOOTAGE |                         | .00   |    | 1.19  | 1.38  | 57.69         |        |         |               |       |                |                 |
| DRY DENSITY LB/CU FT | 100.0                   | 1.55  |    | 65.32 | 62.32 | 5.19          |        |         |               |       |                |                 |
| PERCENT DRY WEIGHT   | 12.51                   | 19.98 |    | 17.37 | 20.58 | 93.56         |        |         |               |       |                |                 |
| PERCENT BPL          | 81.24                   | .39   |    | .46   | .60   | .22           |        |         |               |       |                |                 |
| PERCENT ACID INSOL   | 1.24                    | .96   |    | 1.22  | 1.35  | .96           |        |         |               |       |                |                 |
| PERCENT IRON OXIDE   | 4.46                    | 43.02 |    | 42.32 | 40.58 | 1.82          |        |         |               |       |                |                 |
| PERCENT ALUM OXIDE   | 4.90                    |       |    |       |       |               |        |         |               |       |                |                 |
| PERCENT CALC OXIDE   |                         |       |    |       |       |               |        |         |               |       |                |                 |

NOTE: WORK ON THE MATRIX WAS DISCONTINUED AFTER THE FLOTATION FEED WAS FOUND TO CONTAIN LESS THAN 7% BPL.

TABLE IO-II (CONT.)  
MATRIX BENEFICIATION RESULTS

LOWMEDES COUNTY

| HOLE NO. IO-11       | MATRIX INTERVAL = 90-94 | FEED<br>4 | +4    | 4X8   | 8X16  | F F    |                | SLIME<br>-150 | F.A.<br>TAILS<br>(CONC) | AMINE<br>FLOAT) |
|----------------------|-------------------------|-----------|-------|-------|-------|--------|----------------|---------------|-------------------------|-----------------|
|                      |                         |           |       |       |       | 16X150 | (16X35 35X150) |               |                         |                 |
| TOTAL MATRIX FOOTAGE |                         | 100.0     | .88   | .80   | 2.67  | 28.99  |                |               |                         |                 |
| DRY DENSITY LB/CU FT |                         | 9.31      | 1.11  | 5.70  | 9.00  | 3.98   |                |               |                         |                 |
| PERCENT WY WEIGHT    |                         | 74.38     | 11.42 | 33.74 | 52.17 | 88.34  |                |               |                         |                 |
| PERCENT WPL          |                         | 2.26      | .37   | 1.52  | 2.43  | .81    |                |               |                         |                 |
| PERCENT ACID INSOL   |                         | 6.46      | .92   | 3.67  | 5.72  | 2.58   |                |               |                         |                 |
| PERCENT IRON OXIDE   |                         | 4.69      | 29.03 | 20.64 | 10.98 | 1.86   |                |               |                         |                 |
| PERCENT ALUM OXIDE   |                         |           |       |       |       |        |                |               |                         |                 |
| PERCENT CALC OXIDE   |                         |           |       |       |       |        |                |               |                         |                 |

NOTE: WORK ON THE MATRIX WAS DISCONTINUED AFTER THE FLOTATION FEED WAS FOUND TO CONTAIN LESS THAN 7% BFL





TABLE IO-II (CONT.)  
 MATRIX BENEFICIATION RESULTS  
 LOWMEDES COUNTY

| TOTAL MATRIX FOULAGE<br>DRY DENSITY LB/CU FT<br>PERCENT LRY WEIGHT<br>PERCENT CPL<br>PERCENT ACID INSOL<br>PERCENT IRON OXIDE<br>PERCENT ALUM OXIDE<br>PERCENT CALC OXIDE | HOLE NO. IO-14 |     | MATRIX INTERVAL = 72-75 |      | F P    |        | SLIME<br>-150 | (CONC | F.A.<br>TAILS | AMINE<br>FLOAT) |
|---|----------------|-----|-------------------------|------|--------|--------|---------------|-------|---------------|-----------------|
|   | FEEU<br>3      | +4  | 4X8                     | 8X16 | 16X150 | (16X35 |               |       |               |                 |
|   | 100.0          | .03 | .17                     | .73  | 65.30  |        |               |       |               |                 |
|   | 14.67          |     |                         |      | 5.73   |        |               |       |               |                 |
|   | 79.95          |     |                         |      | 92.40  |        |               |       |               |                 |
|   | .82            |     |                         |      |        |        |               |       |               |                 |
|   | 2.84           |     |                         |      |        |        |               |       |               |                 |
|   | 5.95           |     |                         |      |        |        |               |       |               |                 |

NOTE: WORK ON THE MATRIX WAS DISCONTINUED AFTER THE FLOTATION FEED WAS  
 FOUND TO CONTAIN LESS THAN 7% BPL

TABLE LO-III  
ECONOMIC FACTORS - FIGURES OF MERIT

WELL NO. LO-12

## INDIVIDUAL MATRICES

1  
46- 91MATRIX NO.  
DEPTH INTERVAL, FT.

UNIT (M=1000)

|                                 |                  |               |
|---------------------------------|------------------|---------------|
| * OVERBURDEN                    | FT.<br>MT/AC     | 46.00<br>90.2 |
| * MATRIX                        | FT.<br>MT/AC     | 45.00<br>67.0 |
| * BPL IN MATRIX                 | PERCENT<br>MT/AC | 12.98<br>8.7  |
| * OVERBURDEN/MATRIX             | RATIO            | 1.02          |
| WASH-SCREEN PRODUCTS            |                  |               |
| +16 MESH                        | MT/AC            | .3            |
| -16+150 MESH                    | MT/AC            | 30.3          |
| -150 MESH (LOSS)                | MT/AC            | 36.4          |
| * FLOTATION CONCENTRATE PRODUCT | MT/AC            | 3.1           |
| * TOTAL USEFUL PRODUCTS**       | MT/AC            | 3.4           |
| BPL RECOVERY                    |                  |               |
| +16 MESH                        | MT/AC            | .1            |
| -16+150 (FLOT. CONC.)           | PERCENT BPL      | 75.9          |
| -16+150 (FLOT. CONC.)           | MT/AC            | 2.4           |
| * TOTAL                         | MT/AC            | 2.5           |
| * RECOVERED FROM MATRIX         | PERCENT          | 28.56         |
| * OVERBURDEN / PRODUCT          | CU YD/T          | 28.9          |
| * MATRIX / PRODUCTS             | CU YD/T          | 21.46         |
| * I+A IN FLOT. CONC.            | PERCENT          | 2.21          |

## FIGURES OF MERIT

## ECON. LEVEL

|                        |         |             |
|------------------------|---------|-------------|
| OVERBURDEN             | UNIT    | ECON. LEVEL |
| MATRIX BPL             | FT      | 88 MAX      |
| BPL IN FLOT. CONC. (1) | FT      | 3 MIN       |
| BPL IN FLOT. CONC. (2) | PERCENT | 10 MIN      |
| OVERBURDEN/MATRIX      | PERCENT | 66 MIN      |
| OVERBURDEN/PRODUCTS    | RATIO   | 2 MAX       |
| I+A IN FLOT. CONC.     | CU YD/T | 17.5 MAX    |
| PRODUCTS RECOVERY      | PERCENT | 5 MAX       |
| BPL (+150) RECOVERY    | T/AC-FT | 400 MIN     |
| MATRIX/PRODUCTS        | PERCENT | 63 MIN      |
|                        | CU YD/T | 6 MAX       |
|                        |         | 1.91        |
|                        |         | 15.00       |
|                        |         | 1.30        |
|                        |         | 1.15        |
|                        |         | 1.46        |
|                        |         | 1.96        |
|                        |         | .61         |
|                        |         | 2.26        |
|                        |         | .19         |
|                        |         | .45         |
|                        |         | .28         |

(1) FOR WET ACID PROCESS, (2) FOR ELECTRIC FURNACE PROCESS, (\*\*) SUM OF +16 MESH AND FLOT. CONC.  
NOTES: OVERBURDEN WEIGHT BASED ON 90 LB/CU FT. MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

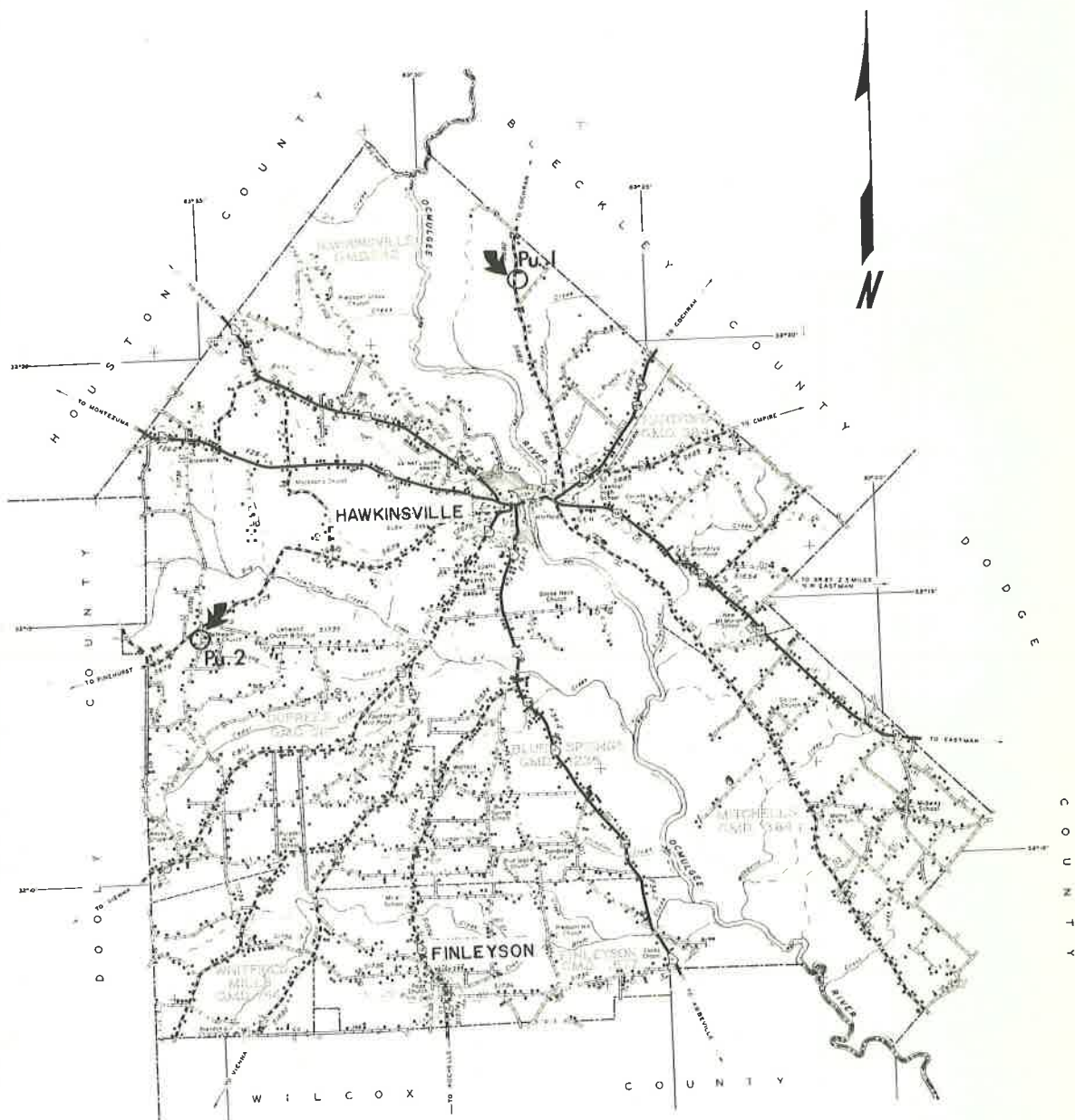


PULASKI COUNTY

PULASKI COUNTY  
SUMMARY OF RESULTS

Two holes were drilled in Pulaski County for kaolin and routinely tested for phosphorite. Only Pu-1 showed traces.

No electrical logs were run on both holes, due to cave-in conditions, but the gamma-ray logs were run inside the drill pipe.



1 0 1 2 3  
SCALE IN MILES

PULASKI COUNTY  
GEORGIA

Figure PU-1. Location of Holes - Pulaski County

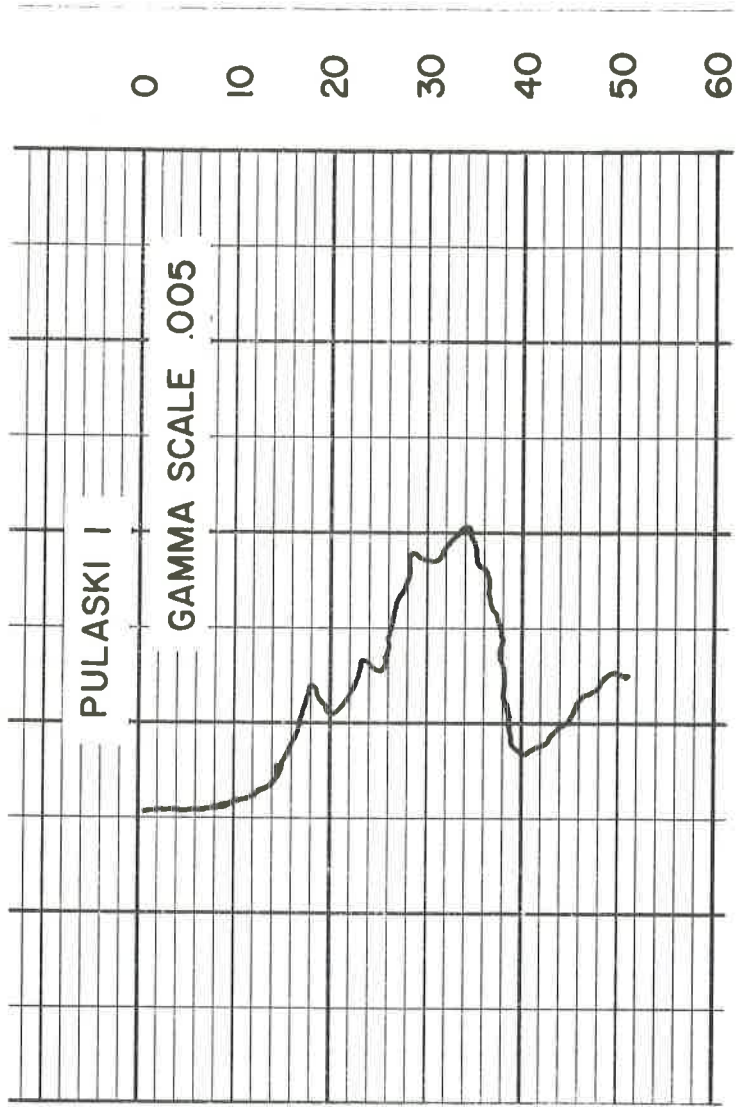


Figure PU-2. Gamma-Ray Logs - Pulaski County  
Hole Pu-1



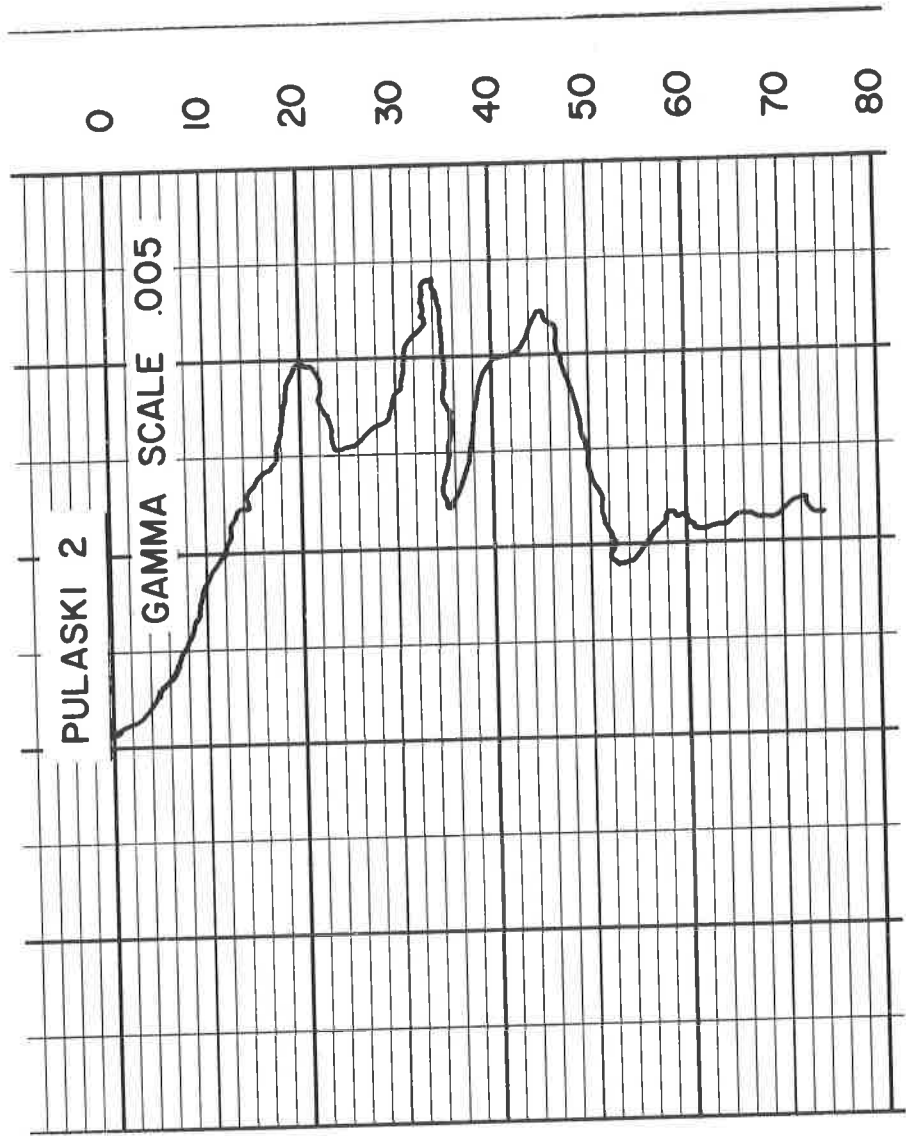


Figure PU-2. Gamma-Ray Logs - Pulaski County  
Hole Pu-2

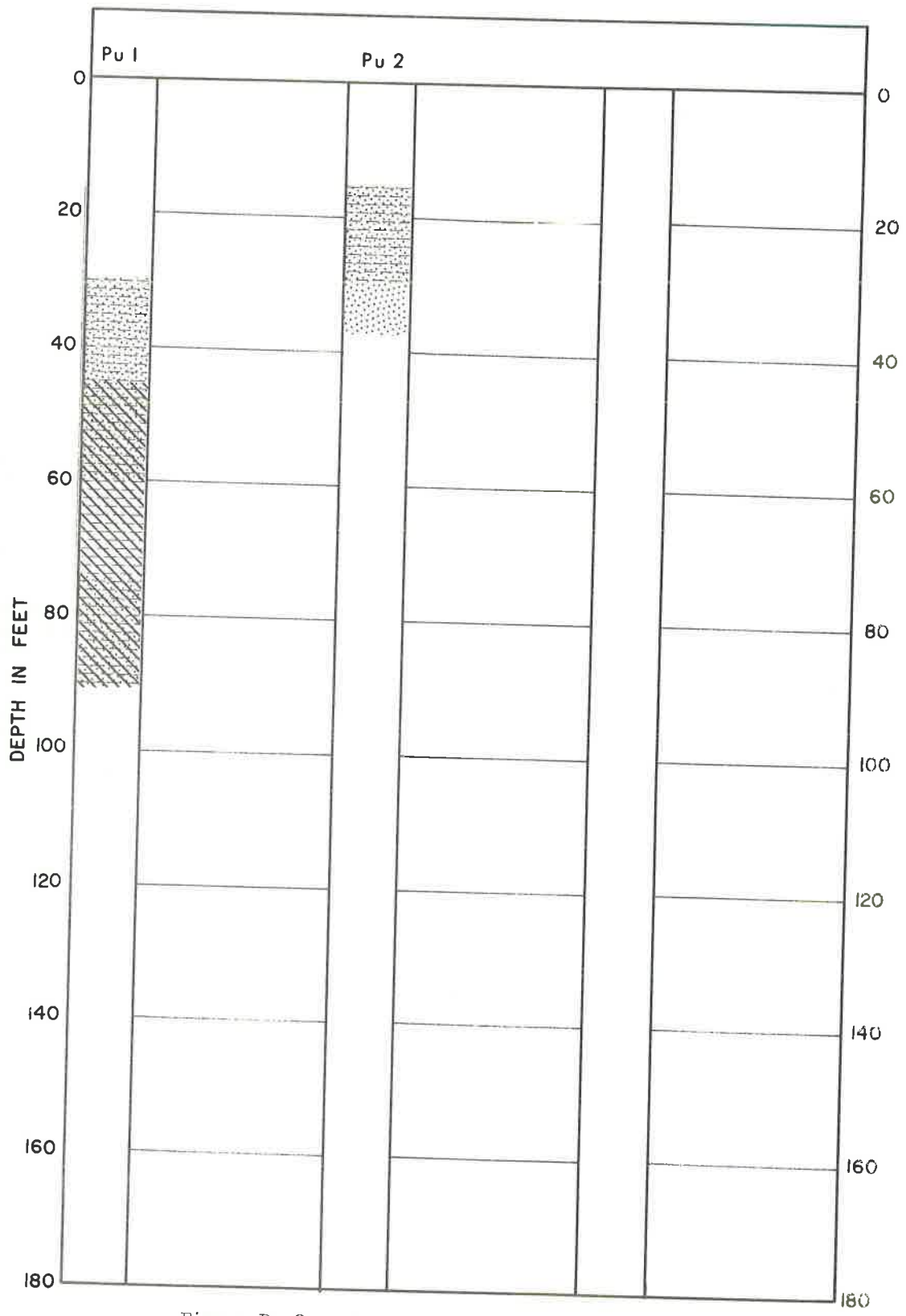


Figure Pu-3. Lithologic Logs - Pulaski County

TABLE PU-I  
 BPL DETERMINATION ON CORES  
 Pulaski County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |    | BPL |
|-------------|---|----------------|---------------|----|-----|
|             |   |                | Feet          | %  | %   |
| Pu-1        | 299   | 0-30           | -             | -  | -   |
|             |   | 30-45          | 1             | 7  | 0   |
|             |   | 45-60          | 11            | 73 | .81 |
|             |   | 60-75          | 14            | 93 | .44 |
|             |   | 75-90          | 4             | 27 | .71 |
| Pu-2        | 321   | 0-5            | Wash Sample   | -  | -   |
|             |   | 5-10           | Wash Sample   | -  | -   |
|             |   | 10-15          | Wash Sample   | -  | -   |
|             |   | 15-30          | 8             | 53 | 0   |
|             |   | 30-37          | 1             | 14 | 0   |
|             |   | 37-40          | Wash Sample   | -  | 0   |
|             |   | 40-45          | Wash Sample   | -  | 0   |
|             |   | 45-50          | Wash Sample   | -  | 0   |
|             |   | 50-55          | Wash Sample   | -  | 0   |
|             |   | 55-60          | Wash Sample   | -  | 0   |
|             |   | 60-65          | Wash Sample   | -  | 0   |
|             |   | 65-70          | Wash Sample   | -  | 0   |
|             |   | 70-75          | Wash Sample   | -  | 0   |

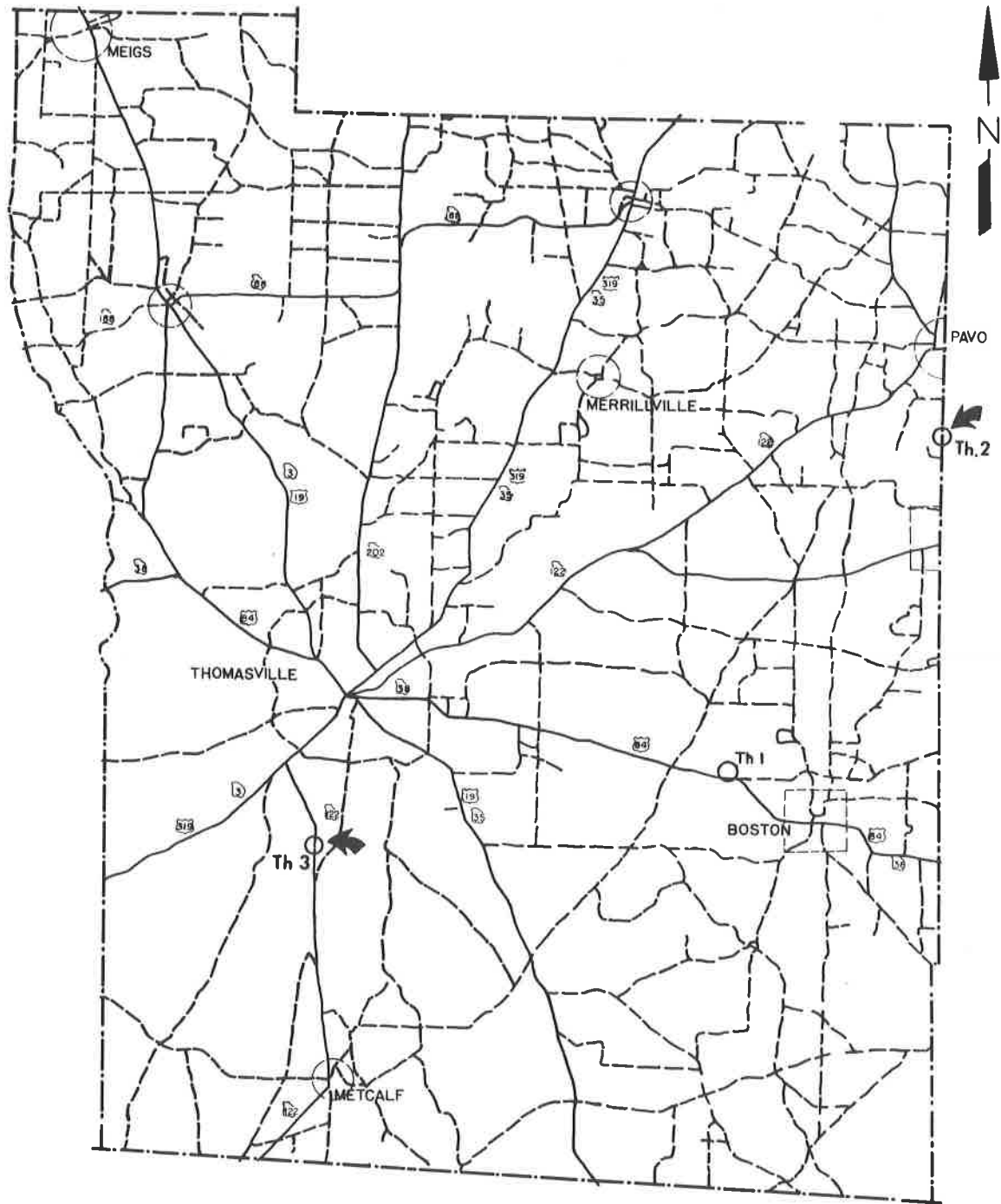


THOMAS COUNTY

THOMAS COUNTY  
SUMMARY OF RESULTS

Thomas County holes 2 and 3 are reported herein. Only Th-3 had matrix of sufficient interest to be beneficiated and the results indicate a sub-marginal deposit.

Electrical logs were not run on Th-3 because of caving hole conditions. The gamma-ray logs was run inside the drill pipe.



### THOMAS COUNTY GEORGIA

Figure TH-1. Location of Holes - Thomas County

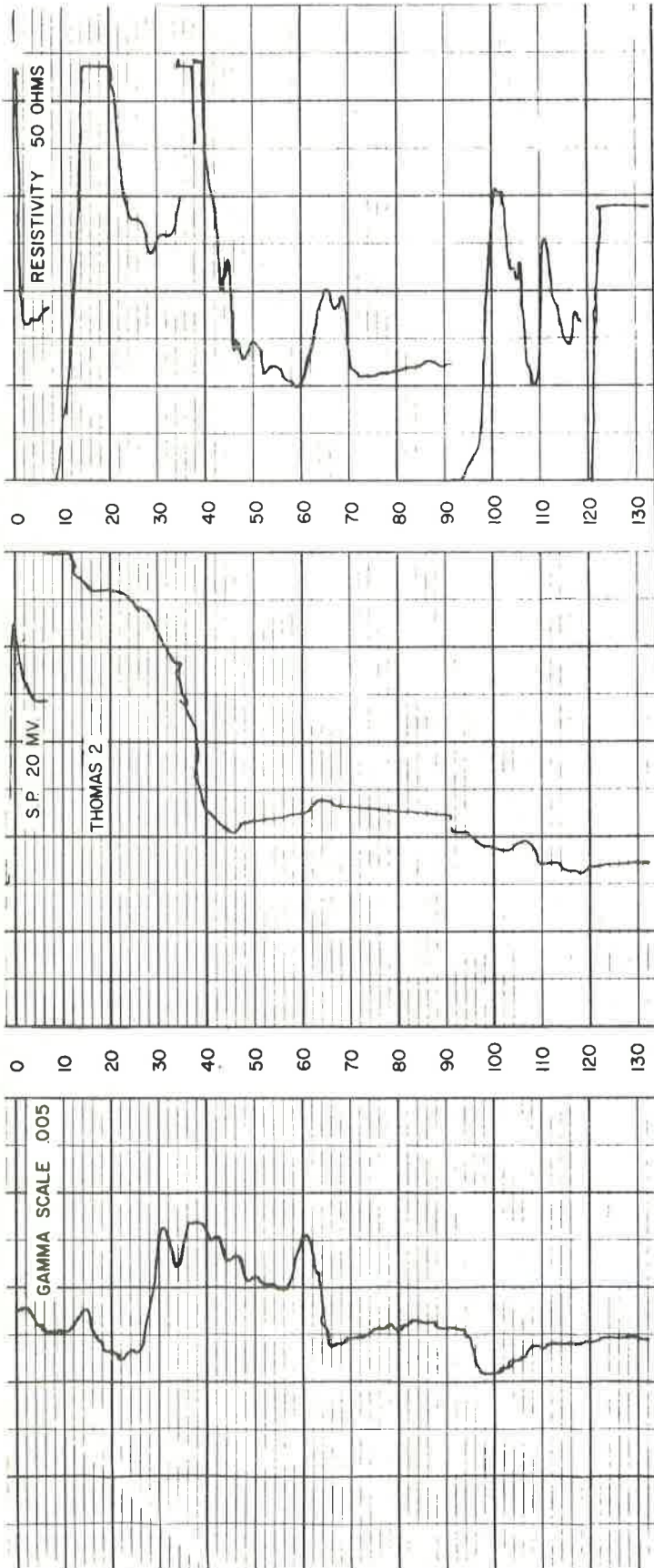


Figure TH-2. Electric and Gamma-Ray Logs - Thomas County Hole Th-2



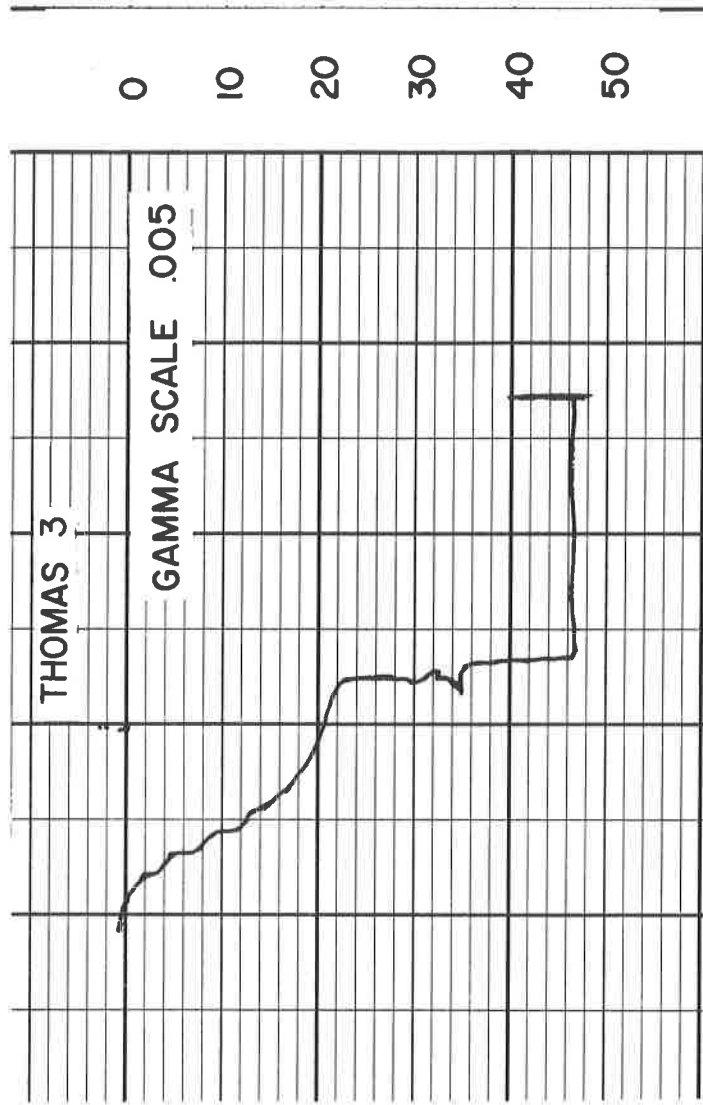


Figure TH-2. Gamma-Ray Logs - Thomas County Hole Th-3

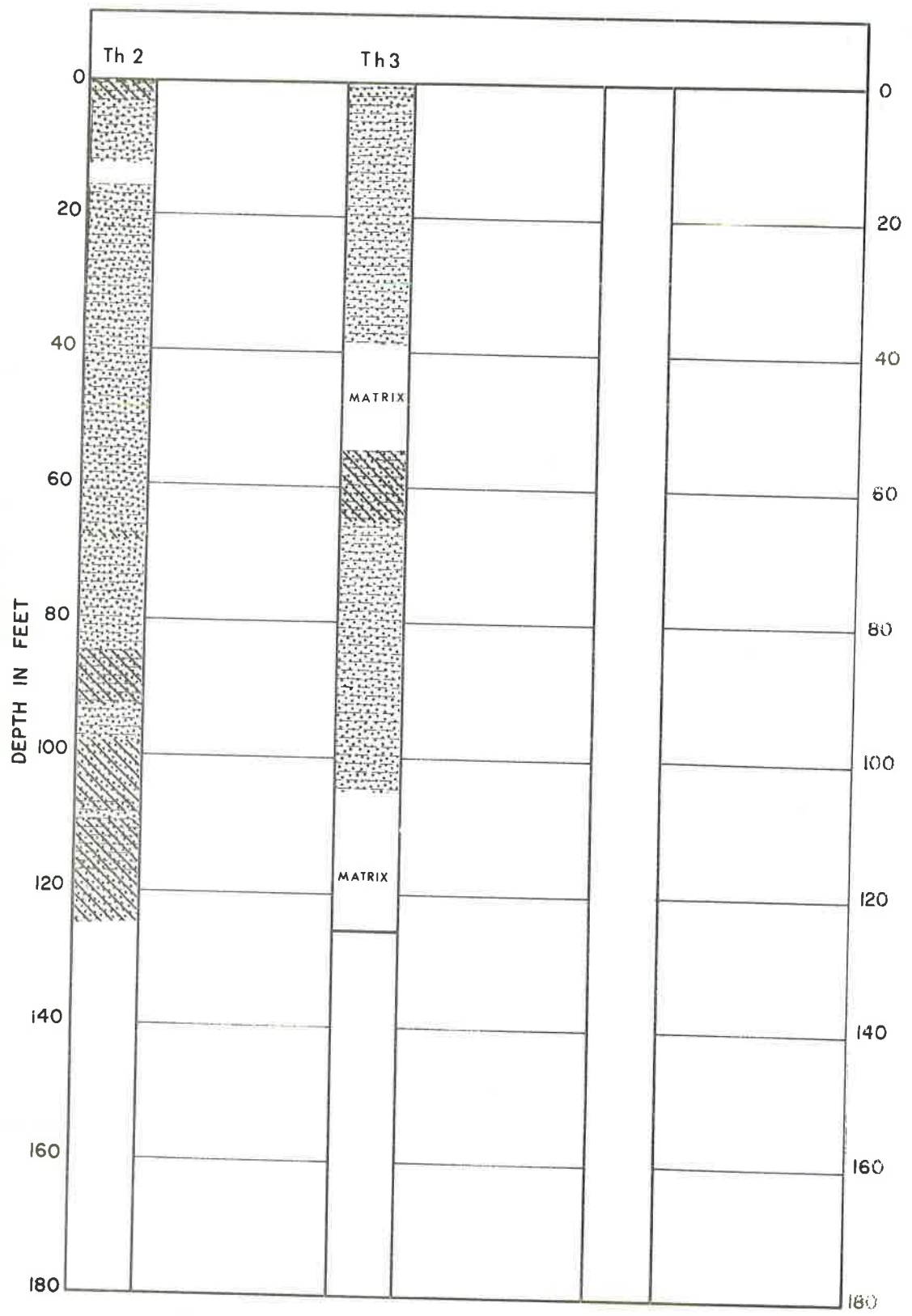


Figure Th-3. Lithologic Logs - Thomas County

TABLE TH-I  
 BPL DETERMINATION ON CORES  
 Thomas County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Th-2        | 239   | 0-3            | 2             | 67  | 0        |
|             |   | 3-6            | 3             | 100 | 0        |
|             |   | 6-9            | 3             | 100 | 0        |
|             |   | 9-12           | 3             | 100 | 0        |
|             |   | 12-15          | 0             | 0   | -        |
|             |   | 15-30          | 3             | 20  | 0        |
|             |   | 30-45          | 2             | 14  | 0        |
|             |   | 45-55          | 10            | 100 | 1.45     |
|             |   | 55-66          | 11            | 100 | 8.06     |
|             |   | 66-77          | 10            | 92  | 0.57     |
|             |   | 77-83          | 6             | 100 | 0        |
|             |   | 83-91          | 8             | 100 | 2.76     |
|             |   | 91-98          | 7             | 100 | 1.96     |
|             |   | 98-106         | 1             | 12  | 0        |
|             |   | 106-109        | 3             | 100 | 0.44     |
|             |   | 109-110        | 0             | 0   | -        |
|             |   | 110-118        | 4             | 50  | 0        |
| 118-125     | 3   | 43             | 0             |     |          |
| Th-3        | 194   | 0-3            | 2             | 67  | 0        |
|             |   | 3-6            | 2             | 67  | 0        |
|             |   | 6-9            | 3             | 100 | 0        |
|             |   | 9-23           | 6             | 43  | 0        |
|             |   | 23-33          | 9             | 90  | 0        |
|             |   | 33-39          | 6             | 100 | 0        |
|             |   | 39-49          | 9             | 90  | 13.15    |
|             |   | 49-54          | 5             | 100 | 10.52    |
|             |   | 54-65          | 8             | 42  | 3.24     |
|             |   | 65-74          | 9             | 100 | 1.72     |
|             |   | 74-82          | 8             | 100 | 2.56     |
|             |   | 82-90          | 8             | 100 | 9.24     |
|             |   | 90-105         | 9             | 60  | 4.99     |
|             |   | 105-115        | 10            | 100 | 9.98     |
| 115-125     | 9   | 90             | 10.25         |     |          |

TABLE TH-II  
 MATRIX BENEFICIATION RESULTS  
 THOMAS COUNTY

| TOTAL MATRIX FOOTAGE<br>DRY DENSITY LB/CU FT | FEEJ<br>15 | MATRIX INTERVAL = 39-54 |       |       |               |        |         | SLIME<br>-150 | (CONC) | F.A.<br>TAILS | AMINE<br>FLOAT) |
|--|------------|-------------------------|-------|-------|---------------|--------|---------|---------------|--------|---------------|-----------------|
|  |            | +4                      | 4XB   | 8X16  | F F<br>16X150 | (16X35 | 35X150) |               |        |               |                 |
| PERCENT WY HEIGHT                            | 43.65      | .27                     | .46   | 1.34  | 57.34         | 2.03   | 55.31   | 10.21         | 86.13  | 3.66          |                 |
| PERCENT CPL                                  | 11.93      | 3.03                    | 10.95 | 13.99 | 10.11         | 29.84  | 10.29   | 50.41         | 2.87   | 31.53         |                 |
| PERCENT ACID INSOL                           | 79.93      | 87.20                   | 73.89 | 71.49 | 84.08         | 52.66  | 85.68   | 35.53         | 96.58  | 58.88         |                 |
| PERCENT IRON OXIDE                           | 1.57       | .79                     | .36   | .41   | .48           | 1.61   | .46     | .44           | .09    | 2.22          |                 |
| PERCENT ALUM OXIDE                           | 4.22       | 1.32                    | 4.30  | 7.56  | 2.46          | 4.72   | 2.41    | 1.44          | 2.46   | 6.61          |                 |
| PERCENT CALC OXIDE                           | 5.95       | 2.24                    | 5.60  | 7.70  | 5.25          | 19.94  | 4.55    | 31.83         | .62    | 20.99         |                 |

NOTE: FLOTATION FEED HAD TO BE SCRUBBED, DESLIMED, AND RE-SCRUBBED FOR FLOTATION TO BE SUCCESSFUL.

TABLE TH-II (CONT.)  
 MATRIX BENEFICIATION RESULTS

THOMAS COUNTY

| HOLE NO. TH-03       | MATRIX INTERVAL = 105-125 |       |       |       |               | SLIME<br>-150 | F.A.<br>TAILS<br>(CONC) | AMINE<br>(FLOAT) |
|----------------------|---------------------------|-------|-------|-------|---------------|---------------|-------------------------|------------------|
|                      | FEED<br>-20               | +4    | 4X8   | 8X16  | F F<br>16X150 |               |                         |                  |
| TOTAL MATRIX FOOTAGE | 100.0                     | 3.98  | 1.88  | 1.65  | 47.25         |               |                         |                  |
| DRY DENSITY LB/CU FT | 11.60                     | 2.87  | 7.92  | 11.46 | 4.22          |               |                         |                  |
| PERCENT DRY WEIGHT   | 80.64                     | 92.34 | 85.13 | 82.15 | 94.07         |               |                         |                  |
| PERCENT PPL          |                           |       |       |       |               |               |                         |                  |
| PERCENT ACID INSOL   |                           |       |       |       |               |               |                         |                  |
| PERCENT IRON OXIDE   |                           |       |       |       |               |               |                         |                  |
| PERCENT ALUM OXIDE   |                           |       |       |       |               |               |                         |                  |
| PERCENT CALC OXIDE   |                           |       |       |       |               |               |                         |                  |

NOTE: WORK ON THE MATRIX WAS DISCONTINUED AFTER THE FLOTATION FEED WAS FOUND TO CONTAIN LESS THAN 7% REL.

TABLE TH-III

ECONOMIC FACTORS - FIGURES OF MERIT

WELL NO. TH-03

INDIVIDUAL MATRICES

| MATRIX NO.<br>DEPTH INTERVAL, FT.    | UNIT (M=1000)    | 1<br>39- 54   |
|--------------------------------------|------------------|---------------|
| <b>ECONOMIC FACTORS *</b>            |                  |               |
| * OVERBURDEN                         | FT.<br>MT/AC     | 39.00<br>76.4 |
| * MATRIX                             | FT.<br>MT/AC     | 15.00<br>14.3 |
| * BPL IN MATRIX                      | PERCENT<br>MT/AC | 11.53<br>1.6  |
| * OVERBURDEN/MATRIX                  | RATIO            | 2.60          |
| WASH-SCREEN PRODUCTS                 |                  |               |
| +16 MESH                             | MT/AC            | .3            |
| -10+150 MESH                         | MT/AC            | 8.2           |
| -150 MESH (LOSS)                     | MT/AC            | 5.8           |
| <b>FLOTATION CONCENTRATE PRODUCT</b> |                  |               |
| TOTAL USEFUL PRODUCTS**              | MT/AC            | .8            |
| BPL RECOVERY                         | MT/AC            | 1.1           |
| +16 MESH                             | MT/AC            | .0            |
| -10+150 (FLOT. CONC.)                | PERCENT BPL      | 50.4          |
| -16+150 (FLOT. CONC.)                | MT/AC            | .4            |
| TOTAL                                | MT/AC            | .5            |
| RECOVERED FROM MATRIX                | PERCENT          | 27.73         |
| * OVERBURDEN / PRODUCT               | CU YD/T          | 114.8         |
| * MATRIX / PRODUCTS                  | CU YD/T          | 21.41         |
| * I+A IN FLOT. CONC.                 | PERCENT          | 1.88          |
| <b>FIGURES OF MERIT</b>              |                  |               |
| OVERBURDEN                           | UNIT             | ECON. LEVEL   |
| MATRIX                               | FT               | 89 MAX        |
| BPL IN FLOT. CONC.(1)                | PERCENT          | 3 MIN         |
| BPL IN FLOT. CONC.(2)                | PERCENT          | 10 MIN        |
| OVERBURDEN/MATRIX                    | PERCENT          | 56 MIN        |
| I+A IN FLOT. CONC.                   | RATIO            | .76           |
| PRODUCTS RECOVERY                    | CU YD/T          | .97           |
| BPL (+150) RECOVERY                  | PERCENT          | 2 MAX         |
| MATRIX/PRODUCTS                      | T/AC-FT          | 17.5 MAX      |
|                                      | PERCENT          | 5 MAX         |
|                                      | CU YD/T          | 400 MIN       |
|                                      | PERCENT          | 63 MIN        |
|                                      | CU YD/T          | 6 MAX         |
|                                      |                  | .28           |

(1)FOR WET ACID PROCESS, (2)FOR ELECTRIC FURNACE PROCESS, (\*\*)SUM OF +16 MESH AND FLOT. CONC.  
 NOTES, OVERBURDEN WEIGHT BASED ON 90 LB/CU FT, MATRIX WEIGHT BASED ON ACTUAL DRY DENSITY

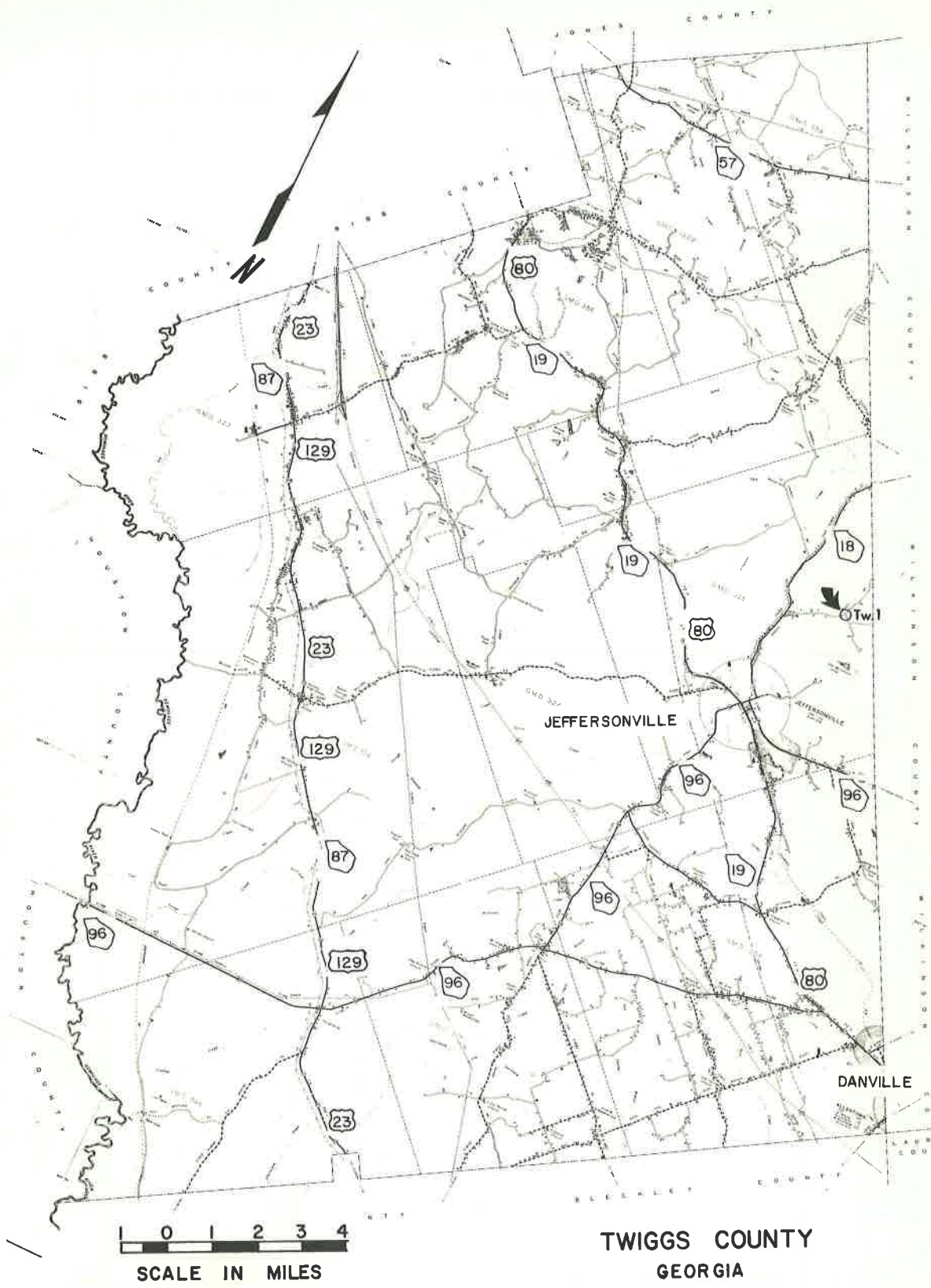
TWIGGS COUNTY

TWIGGS COUNTY  
SUMMARY OF RESULTS

The Twiggs County hole was drilled on the basis of reported phosphorite in GGS Well No. 416. Although phosphorite was found almost continuously in both Upper Eocene and Upper Cretaceous, the quantity is slight.

Electric and gamma-ray logs were not run on these holes because of caving hole conditions. The holes were drilled with Failing 250 rig and pipe inside diameter was not large enough for the gamma-ray probe.





**TWIGGS COUNTY  
GEORGIA**

Figure TW-1. Location of Holes - Twigg County

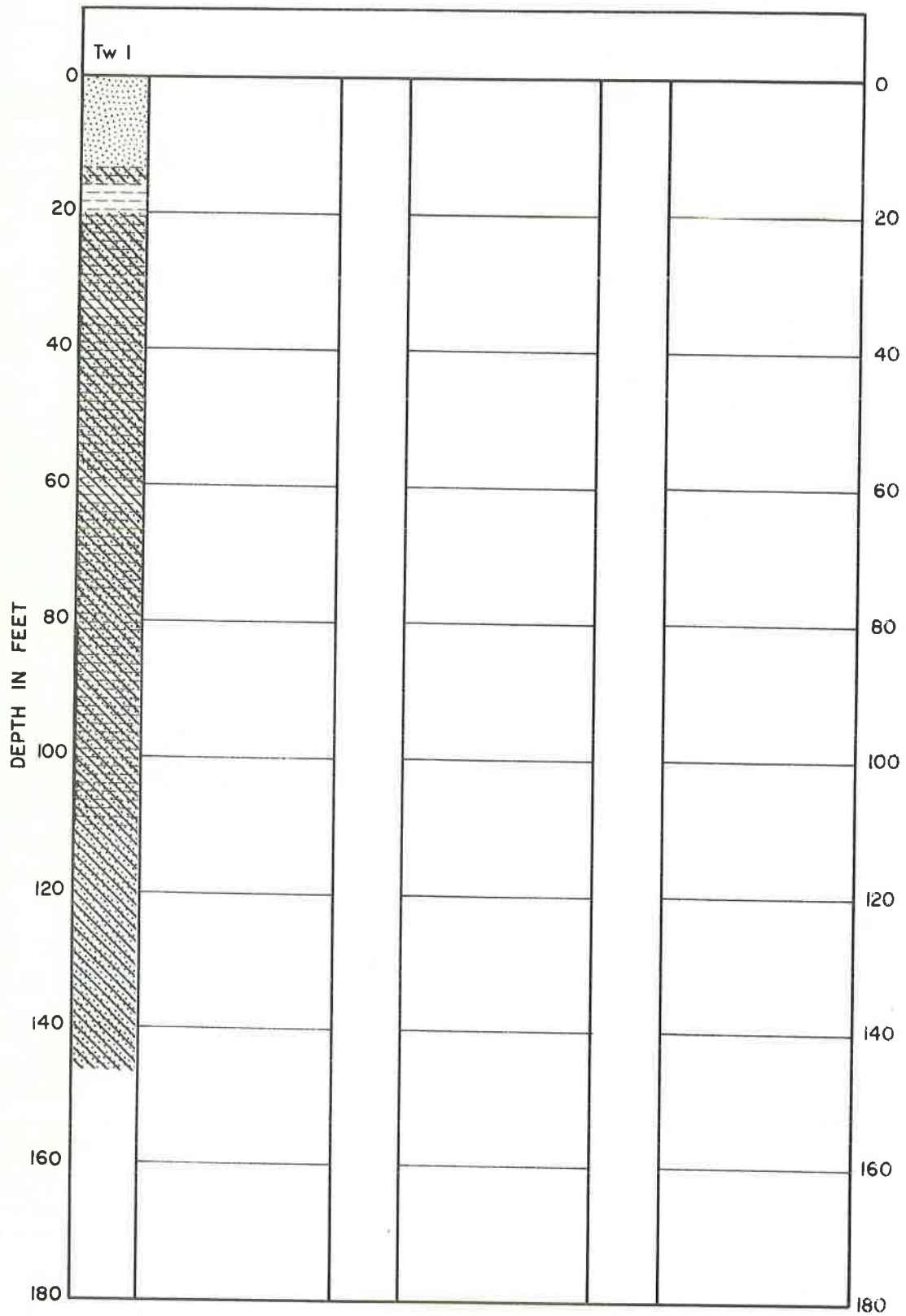


Figure Tw-3. Lithologic Logs - Twiggs County

TABLE TW-I

## BPL DETERMINATION ON CORES

## Twiggs County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL<br>% |
|-------------|---|----------------|---------------|-----|----------|
|             |   |                | Feet          | %   |          |
| Tw-1        | 502   | 0-4            | 3             | 75  | 0        |
|             |   | 4-7            | 3             | 100 | 0        |
|             |   | 7-9            | 2             | 100 | 0        |
|             |   | 9-11           | 2             | 100 | 0        |
|             |   | 11-13          | 2             | 100 | 0        |
|             |   | 13-15          | 2             | 100 | 0        |
|             |   | 15-20          | 5             | 100 | 1.01     |
|             |   | 20-25          | 5             | 100 | 0.71     |
|             |   | 25-30          | 5             | 100 | 1.25     |
|             |   | 30-32          | 2             | 100 | 0.54     |
|             |   | 32-34          | 2             | 100 | 0.50     |
|             |   | 34-39          | 5             | 100 | 0.30     |
|             |   | 39-40          | 1             | 100 | 0.13     |
|             |   | 40-46          | 6             | 100 | 0        |
|             |   | 46-49          | 2             | 67  | 0.27     |
|             |   | 49-59          | 8             | 80  | 0.41     |
|             |   | 59-62          | 2             | 67  | 0.91     |
|             |   | 62-68          | 4             | 67  | 0.37     |
|             |   | 68-69          | 1             | 100 | 0.34     |
|             |   | 69-75          | 5             | 83  | 0.40     |
|             |   | 75-80          | 5             | 100 | 0.44     |
|             |   | 80-84          | 3             | 75  | 0.50     |
|             |   | 84-86          | 2             | 100 | 0.54     |
|             |   | 86-90          | 4             | 100 | 0.47     |
|             |   | 90-92          | 2             | 100 | 0        |
|             |   | 92-96          | 3             | 75  | 0.54     |
|             |   | 96-102         | 5             | 83  | 0.44     |
|             |   | 102-109        | 5             | 71  | 0.30     |
| 109-112     | -   | -              | -             |     |          |
| 112-117     | 4   | 80             | 0.34          |     |          |
| 117-120     | 1   | 33             | 0             |     |          |
| 120-131     | 3   | 27             | 0             |     |          |
| 131-140     | 4   | 44             | 0.30          |     |          |
| 140-145     | 2   | 40             | 0             |     |          |



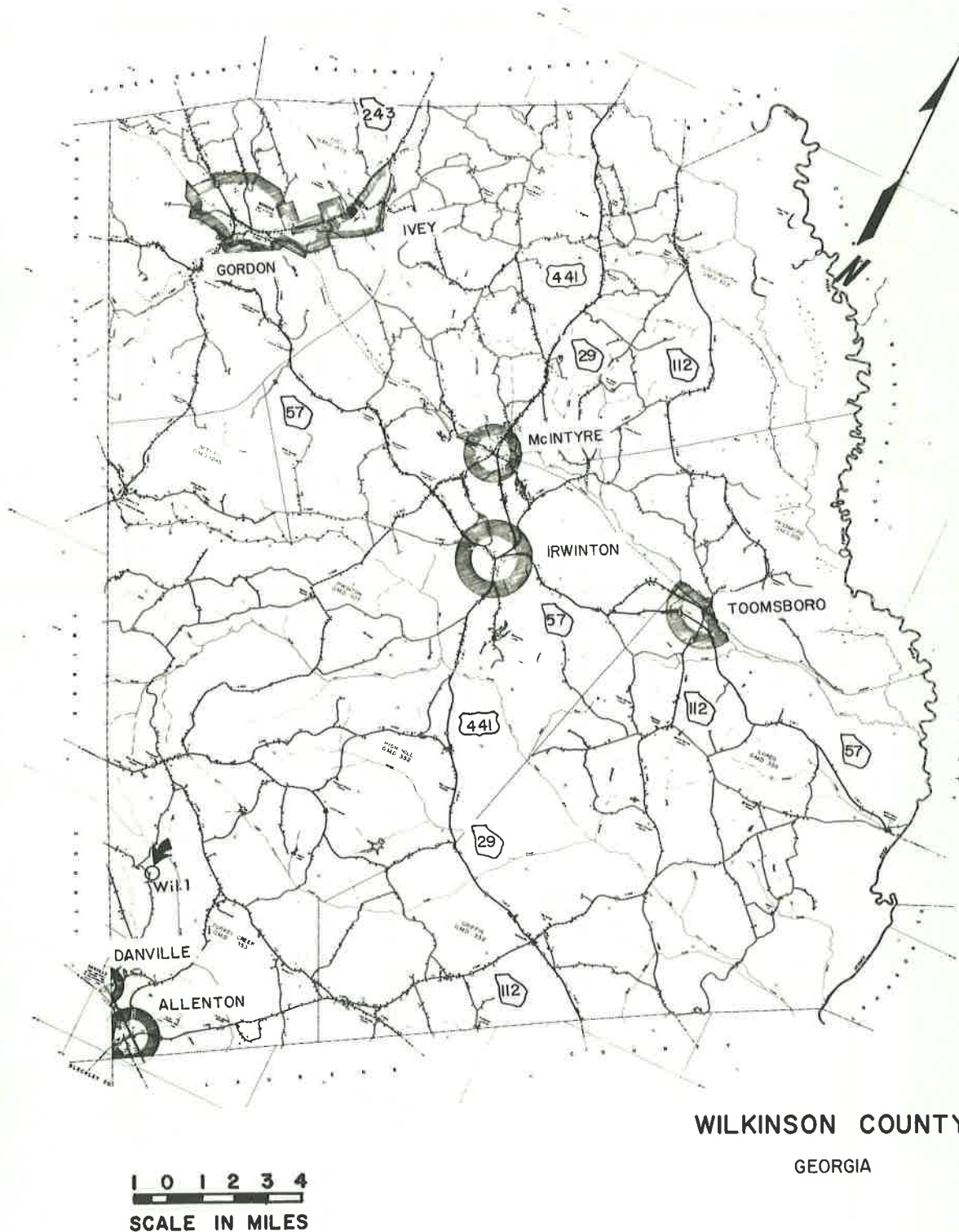
WILKINSON COUNTY

## WILKINSON COUNTY

## SUMMARY OF RESULTS

The Wilkinson Hole was drilled because of reported phosphorite in GGS Hole No. 529. It did not go as deep as the Middle Eocene sediments where the phosphorite was reported, but did sample the current economic mining depth. Small amounts of phosphorite were found between 16 and 57 feet of depth.

Electrical and gamma-ray logs were not run on this hole because of caving conditions and the use of the smaller rig.



**WILKINSON COUNTY**  
GEORGIA

Figure WILK-1. Location of Holes - Wilkinson County

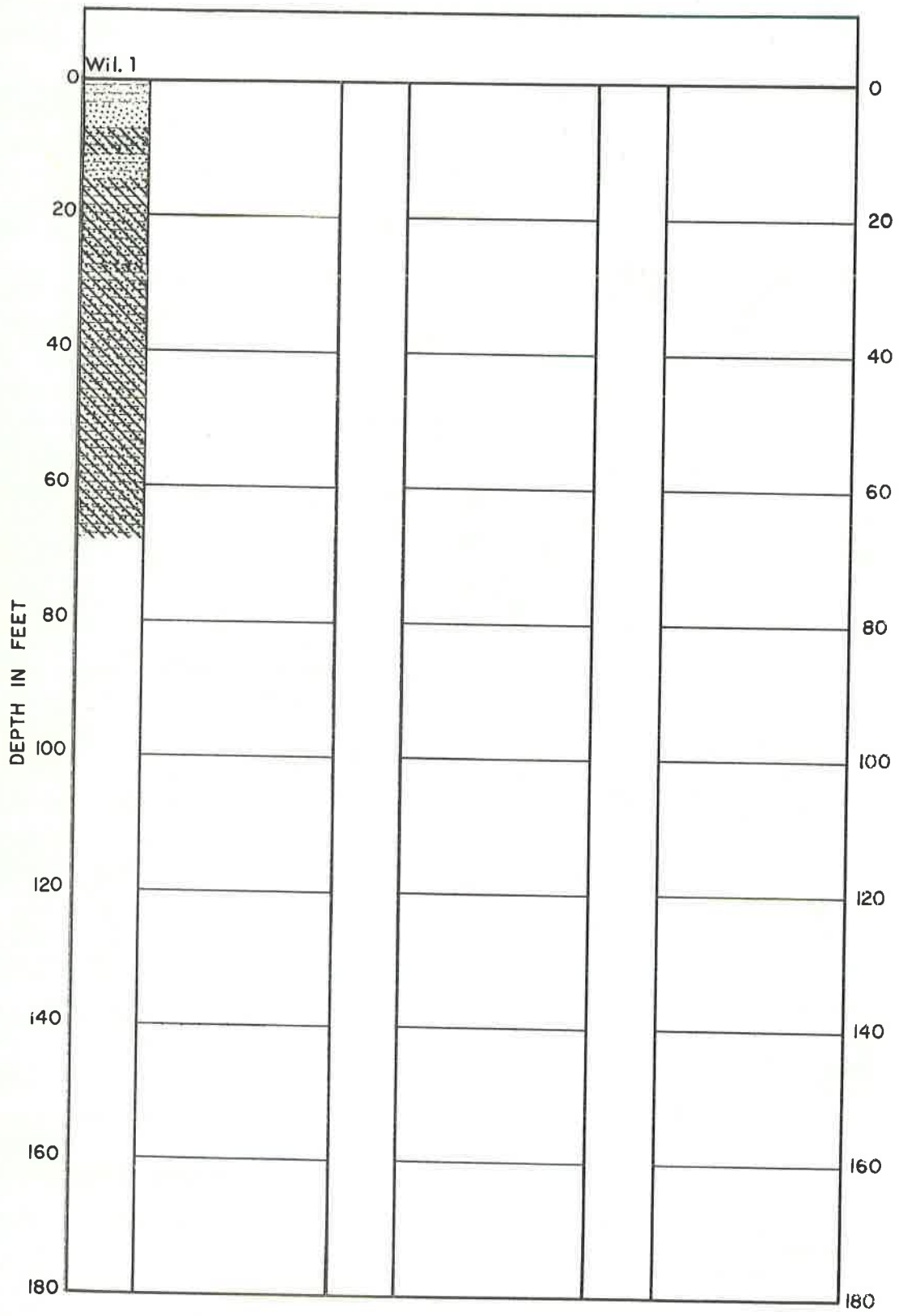


Figure Wil-3. Lithologic Logs - Wilkinson County



TABLE WILK-I  
 BPL DETERMINATION ON CORES  
 Wilkinson County

| Hole<br>No. | Surface<br>Elevation<br>(Sea Level)<br>Feet | Depth,<br>Feet | Core Recovery |     | BPL  |
|-------------|---|----------------|---------------|-----|------|
|             |   |                | Feet          | %   | %    |
| Wilk-1      | 333   | 0-1            | -             | -   | -    |
|             |   | 1-3            | 1             | 50  | 0    |
|             |   | 3-6            | 2             | 67  | 0.20 |
|             |   | 6-9            | 2             | 67  | 0    |
|             |   | 9-13           | 3             | 75  | 0    |
|             |   | 13-16          | 2             | 67  | 0    |
|             |   | 16-23          | 7             | 100 | 0.13 |
|             |   | 23-28          | 4             | 80  | 0.24 |
|             |   | 28-37          | 7             | 78  | 0.10 |
|             |   | 37-47          | 7             | 70  | 0.27 |
|             |   | 47-57          | 8             | 80  | 0.07 |
|             |   | 57-67          | 4             | 40  | 0    |
|             |   | 67-100         | -             | -   | -    |
|             |   | 100-105        | Wash Sample   | -   | 0    |
|             |   | 105-110        | Wash Sample   | -   | 0    |
|             |   | 110-115        | Wash Sample   | -   | 0    |
|             |   | 115-120        | Wash Sample   | -   | 0    |
|             |   | 120-125        | Wash Sample   | -   | 0    |
|             |   | 125-130        | Wash Sample   | -   | 0    |
|             |   | 130-135        | Wash Sample   | -   | 0    |
|             |   | 135-140        | Wash Sample   | -   | 0    |
|             |   | 140-145        | Wash Sample   | -   | 0    |
| 145-150     | Wash Sample                                 | -              | 0             |     |      |



APPENDIX

APPENDIX  
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| County   | Holes   | Report Number | Location of Holes | Gamma and Electric Log | Lithologic Logs | Particle Size | Visual and Microscopic Observation | Physical Properties | EPL Determination | Matrix Beneficiation | Economic Factors | Chemical Composition | Mineral Percent | Chemical Analysis of Heavy Minerals | X-Ray Diffraction |
|----------|---------|---------------|-------------------|------------------------|-----------------|---------------|------------------------------------|---------------------|-------------------|----------------------|------------------|----------------------|-----------------|-------------------------------------|-------------------|
| Appling  | A 34-35 | 8             | 7                 |                        |                 |               |                                    | 27                  |                   |                      |                  |                      |                 | 39                                  |                   |
| Atkinson | 1-3     | 5             | 21                | 23                     | 22              |               |                                    |                     | 25                | 26                   |                  |                      |                 |                                     |                   |
| Atkinson | 1-3     | 6             |                   |                        |                 | 39            | 42                                 |                     |                   |                      |                  | 53                   |                 |                                     |                   |
| Atkinson | A 53    | 8             | 9                 |                        |                 |               |                                    | 28                  |                   |                      |                  |                      | 32              | 39                                  |                   |
| Bacon    | A 48-50 | 8             | 8                 |                        |                 |               |                                    | 28                  |                   |                      |                  |                      | 32              | 39                                  |                   |
| Ben Hill | 1-3     | 5             | 28                | 30                     | 29              |               |                                    |                     | 32                |                      |                  |                      |                 |                                     |                   |
| Ben Hill | 1-3     | 6             |                   |                        |                 | 39            | 43                                 |                     |                   |                      |                  | 53                   |                 |                                     |                   |
| Berrien  | 1-3     | 5             | 34                | 36                     | 35              |               |                                    |                     | 38                | 39                   |                  |                      |                 |                                     |                   |
| Berrien  | 1-3     | 6             |                   |                        |                 | 39            | 44                                 |                     |                   |                      |                  | 53                   |                 |                                     |                   |
| Brantley | A 56-65 | 8             | 9                 |                        |                 |               |                                    | 28                  |                   |                      |                  |                      | 33              | 39                                  |                   |
| Brooks   | 1-2     | 3             | 17                |                        | 18              |               |                                    |                     | 19                |                      |                  |                      |                 |                                     |                   |
| Brooks   | 1-2     | 6             |                   | 57,58                  |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Bryan    | A 10-18 | 8             | 5                 |                        |                 |               |                                    | 24                  |                   |                      |                  |                      | 31              | 38                                  |                   |
| Bryan    | 1-2     | 10            | 7                 |                        | 8               | 12            | 13                                 |                     | 9                 |                      |                  | 11                   |                 |                                     |                   |
| Bulloch  | A 1-3   | 8             | 5                 |                        |                 |               |                                    | 24                  |                   |                      |                  |                      | 31              | 38                                  |                   |
| Camden   | 1-2     | 3             | 21                |                        | 22              |               |                                    |                     | 23                |                      |                  |                      |                 |                                     |                   |
| Camden   | 1-2     | 6             |                   |                        |                 |               |                                    |                     | 59,60             |                      |                  |                      |                 |                                     |                   |
| Camden   | A 77-80 | 8             | 11                |                        |                 |               |                                    | 30                  |                   |                      |                  |                      | 34              | 40                                  |                   |
| Charlton | A 73-76 | 8             | 11                |                        |                 |               |                                    | 30                  |                   |                      |                  |                      | 33              | 40                                  |                   |

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|-----------|---------------|---------------|-------------------|-------------------------|-----------------|---------------|------------------------------------|---------------------|-------------------|----------------------|------------------|----------------------|-----------------|-------------------------------------|-------------------|
| Charlton  |               | 4             | 5                 |                         |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Chatham   | A 19-22       | 8             | 6                 |                         |                 |               |                                    | 25                  |                   |                      |                  |                      | 31              | 38                                  |                   |
| Chatham   | 1-5           | 9             | 14                | 17                      | 15              |               |                                    |                     | 23                | 26                   | 37               |                      |                 |                                     |                   |
| Chatham   | 6-9           | 10            | 18                | 21                      | 19              | 28            | 29                                 |                     | 24                | 35                   | 36               | 27                   |                 |                                     | 33                |
| Clinch    | 1-3           | 3             | 25                |                         | 26              |               |                                    |                     | 27                |                      |                  |                      |                 |                                     |                   |
| Clinch    |               | 4             | S                 |                         |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Clinch    | 1-3           | 6             |                   | 61-63                   |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Clinch    | A 72          | 8             | 11                |                         |                 |               |                                    | 30                  |                   |                      |                  |                      | 33              | 40                                  |                   |
| Coffee    | 1-2           | 5             | 42                |                         | 43              |               |                                    |                     | 44                |                      |                  |                      |                 |                                     |                   |
| Cook      | 1-5           | 5             | 46                | 48                      | 47              |               |                                    |                     | 50                |                      |                  |                      |                 |                                     |                   |
| Echols    | 1-14          | 2             | 5,22              |                         | 31              |               |                                    |                     | 25                | 64                   |                  |                      | 36              |                                     |                   |
| Echols    |               | 4             | S                 |                         |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Echols    | 1-11<br>13-14 | 6             |                   | 64-77                   |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Echols    | 15-17         | 9             | 48                | 50                      | 49              |               |                                    |                     | 53                | 55                   | 57               |                      |                 |                                     |                   |
| Effingham | 1             | 3             | 31                |                         | 32              |               |                                    |                     | 33                |                      |                  |                      |                 |                                     |                   |
| Effingham | 2-7           | 6             | 8                 | 11                      | 9               | 40            | 45                                 |                     | 18                |                      |                  | 54                   |                 |                                     |                   |
| Effingham | 4-7           | 8             | 5                 |                         |                 | 50-58         |                                    | 24                  |                   |                      |                  |                      | 31              | 38                                  |                   |
| Effingham | 8             | 10            | 39                | 41                      | 40              | 45            | 46                                 |                     | 42                |                      |                  | 44                   |                 |                                     | 48                |
| Evans     | 9             | 8             | 5                 |                         |                 |               |                                    | 24                  |                   |                      |                  |                      | 31              | 38                                  |                   |

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|------------|---------|---------------|-------------------|-------------------------|-----------------|---------------|------------------------------------|---------------------|-------------------|----------------------|------------------|----------------------|-----------------|-------------------------------------|-------------------|
| Glynn      | A 66-70 | 8             | 10                |                         |                 |               |                                    | 29                  |                   |                      |                  |                      | 33              | 40                                  |                   |
| Irwin      | 1-3     | 5             | 53                | 55                      | 54              |               |                                    |                     | 58                |                      |                  |                      |                 |                                     |                   |
| Irwin      | 1-3     | 6             |                   |                         |                 | 41            | 49                                 |                     |                   |                      |                  | 55                   |                 |                                     |                   |
| Jeff Davis | A 33    | 8             | 7                 |                         |                 |               |                                    | 26                  |                   |                      |                  |                      | 32              | 39                                  |                   |
| Jeff Davis | 1-3     | 9             | 77                | 79                      | 78              |               |                                    |                     | 85                |                      |                  |                      |                 |                                     |                   |
| Lanier     | 1-7     | 3             | 35                |                         | 36              |               |                                    |                     | 38                |                      |                  |                      |                 |                                     |                   |
| Lanier     | 2,4,6,7 | 6             |                   | 78-81                   |                 |               |                                    |                     |                   |                      |                  |                      | 33              |                                     |                   |
| Lanier     | A 71    | 8             | 11                |                         |                 |               |                                    | 30                  |                   |                      |                  |                      |                 | 40                                  |                   |
| Lanier     | 8       | 9             | 59                | 61                      | 60              |               |                                    |                     | 62                | 63                   | 64               |                      | 32              |                                     |                   |
| Liberty    | A 27-32 | 8             | 7                 |                         |                 |               |                                    | 26                  |                   |                      |                  |                      |                 | 39                                  |                   |
| Liberty    | 1       | 9             | 87                | 89                      | 88              |               |                                    |                     | 95                |                      |                  |                      |                 |                                     |                   |
| Long       | A 23-26 | 8             | 6                 |                         |                 |               |                                    | 26                  |                   |                      |                  |                      | 32              | 39                                  |                   |
| Long       | 1,2     | 9             | 90                | 92                      | 91              |               |                                    |                     | 95                |                      |                  |                      |                 |                                     |                   |
| Lowndes    | 1-7     | 3             | 49                |                         | 50              |               |                                    |                     | 52                |                      |                  |                      |                 |                                     |                   |
| Lowndes    | 4       | 8             |                   |                         |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Lowndes    | 1-7     | 6             |                   | 82-88                   |                 |               |                                    |                     |                   |                      |                  |                      |                 |                                     |                   |
| Lowndes    | 4       | 6             |                   |                         |                 | 41            | 51                                 |                     |                   |                      |                  | 55                   |                 |                                     |                   |
| Lowndes    | 8-9     | 9             | 65                | 67                      | 66              |               |                                    |                     | 69                | 71                   | 74               |                      |                 |                                     |                   |
| McIntosh   | A 42-47 | 8             | 8                 |                         |                 |               |                                    | 27                  |                   |                      |                  |                      | 32              | 36                                  |                   |

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|------------|---------|---------------|-------------------|-------------------------|-----------------|---------------|------------------------------------|---------------------|-------------------|----------------------|------------------|----------------------|-----------------|-------------------------------------|-------------------|
| Montgomery |         | 1             | 9                 | 81                      |                 |               |                                    |                     |                   | 85                   |                  |                      |                 |                                     |                   |
| Pierce     | A 51-52 | 8             | 9                 |                         |                 |               |                                    | 28                  |                   |                      |                  |                      | 32              | 39                                  |                   |
| Screven    | 1-5     | 10            | 51                | 54                      | 52              | 64            | 66                                 |                     | 58                |                      |                  | 63                   |                 |                                     | 72                |
| Tattnall   | A 8     | 8             | 5                 |                         |                 |               |                                    | 24                  |                   |                      |                  |                      | 31              | 38                                  |                   |
| Thomas     | 1       | 3             | 60                |                         | 61              |               |                                    |                     |                   | 62                   |                  |                      |                 |                                     |                   |
| Ware       | 1       | 3             | 65                |                         | 66              |               |                                    |                     |                   | 67                   |                  |                      |                 |                                     |                   |
| Ware       | A 54-55 | 8             | 9                 |                         |                 |               |                                    | 28                  |                   |                      |                  |                      | 33              | 39                                  |                   |
| Wayne      | A 36-41 | 8             | 8                 |                         |                 |               |                                    | 27                  |                   |                      |                  |                      | 32              | 39                                  |                   |
| Wayne      | 1       | 9             | 93                |                         | 94              |               |                                    |                     |                   | 95                   |                  |                      |                 |                                     |                   |
| Wheeler    | 1       | 9             | 82                | 84                      | 83              |               |                                    |                     |                   | 85                   |                  |                      |                 |                                     |                   |

Note: A = Auger Hole  
 S = Southern Railroad Holes

