# GEORGIA OFFSHORE MINERALS ASSESSMENT

by

ZELLARS-WILLIAMS COMPANY

Division of

JACOBS ENGINEERING GROUP INC. LAKELAND, FLORIDA

> Department of Natural Resources Environmental Protection Division Georgia Geologic Survey

Project Report No. 14

## GEORGIA OFFSHORE MINERALS ASSESSMENT

Project Report No. 14

by

ZELLARS-WILLIAMS COMPANY

Division of

JACOBS ENGINEERING GROUP, INC.
LAKELAND, FLORIDA

In cooperation with
Minerals Management Service
U.S. Department of the Interior
under MMS Agreement No. 14-12-0001-30399

Department of Natural Resources J. Leonard Ledbetter, Commissioner

**Environmental Protection Division Harold F. Reheis, Assistant Director** 

Georgia Geologic Survey William H. McLemore, State Geologist

**Atlanta** 

1988

<u>(i)</u>					
					i
.1					
ac .					
0.0)					
bi.					
.a					
.8 R					
1 14.					
gara or					
1					

# GEORGIA OFFSHORE MINERALS ASSESSMENT TABLE OF CONTENTS

		OUTTUE OUT AND	Page 1
SECTION 1	EXE	CUTIVE SUMMARY	
SECTION 2	SCO	PE OF STUDY	2-1
	2.1 2.2	Overview and Objectives Data Collection	2-1 2-3
SECTION 3	RES	OURCES OF GEORGIA CONTINENTAL SHELF	3-1
	3.3 3.4	Introduction Database Model Construction Phosphorite Potential Heavy Minerals Potential	3-1 3-3 3-8 3-28 3-32
SECTION 4	OFF	-SHORE MINING TECHNOLOGY	4-1
	4.1 4.2 4.3 4.4 4.5 4.6	Introduction State-of-the-Art Dredges Currently Available Mineral Dredging Systems Borehole Mining Applicability of Existing Technology	4-1 4-2 4-4 4-17 4-22 4-27
SECTION 5	PHC	SPHATE DEVELOPMENT FEASIBILITY	5-1
	5.3 5.4		5-1 5-2 5-37 5-51 5-58 5-69 5-79
SECTION 6	HEA	AVY MINERAL DEVELOPMENT FEASIBILITY	6-1
	6.3 6.4	· ·	6-1 6-1 6-24 6-31 6-34 6-39

### TABLE OF CONTENTS - continued

		Page
ENV	IRONMENTAL IMPACTS	7-1
7.1 7.2 7.3 7.4	Environmental Setting Phosphate Mining Heavy Minerals Mining Permitting	7-1 7-7 7-9 7-13
BIBL	JOGRAPHY	8-1
APP	ENDIX	
9.1 9.2 9.3	Modelled Data Raw Data, Sea Floor Characterization Grab Sample Mineralogy	
	7.1 7.2 7.3 7.4 BIBL APP 9.1 9.2	7.2 Phosphate Mining 7.3 Heavy Minerals Mining 7.4 Permitting  BIBLIOGRAPHY  APPENDIX  9.1 Modelled Data 9.2 Raw Data, Sea Floor Characterization

### **EXECUTIVE SUMMARY**

An assessment of mineral resources in the sea-bed on the continental shelf offshore Georgia was undertaken by Zellars-Williams Company, division of Jacobs Engineering Group Inc., pursuant to a contract dated August 12, 1988. The award was made following a request for proposals by the Georgia Department of Natural Resources and the Minerals Management Service, U.S. Department of the Interior, acting cooperatively with other participants, as the TASK FORCE for Offshore Mineral Resources.

Owing to budgetary constraints, the work assesses the economic viability of commercially exploiting offshore phosphorites and heavy minerals utilizing, to the greatest extent possible, commercially available proven technology.

The premises upon which the occurrences of potentially economic resources are located and their areal extent and volume quantified are based entirely on data made available by others. It is emphasized that this study is based on a minerals occurrence inferred by scattered, widely-spaced data points. The conceptual mining and beneficiation flowsheet designs were formulated based on analysis of these data and assumptions as to ore grade, minerals distribution, and ore continuity.

The phosphate-bearing Middle Miocene area targeted for this study is located within a 3-nautical mile radius of a point which is the intersection of  $80^{\circ}40^{\circ}$  latitude, and  $32^{\circ}$  longitude lines. The ore (matrix) zone identified for mining is 5-7 meters thick, under 8-10 meters of overburden. Water depth, below MSL, is 14-16 meters. The 507 million cubic meters of matrix have the potential of yielding 162 million tonnes of 30%  $P_2O_5$  grade phosphate rock product after mining and beneficiation losses.

For phosphate exploitation, all of the required mining, beneficiation, waste disposal, product storage, ship loading, and supporting infrastructure facilities are entirely offshore. Similarly designed, hybrid cutterhead suction-type hydraulic dredges remove overburden and mine matrix independently. Overburden is pumped through a trailing pipeline about 1.5 nautical miles to a floating, constant level head tank and flexible tremie discharging into previously mined cuts at sea bottom. Matrix is pumped to the beneficiation plant through a pipeline, which lengthens as mining

progresses to a maximum distance of 3 nautical miles. The overburden dredge must excavate about 1.6 cubic meters for each cubic meter of ore mined by the matrix dredge.

A 15-acre man-made island, located in the center of the proposed mining area, houses all the beneficiation processing units required to produce wet phosphate The phosphate beneficiation facility consists of washer, feed concentrate. preparation, flotation and product storage, and loading areas. The beneficiation facility is designed to receive slurried ore from the matrix dredge, disaggregate the ore, wash and grind the oversize rock, remove the clay, and separate the sand from the feed to produce a marketable phosphate concentrate product. Fresh water, produced by a reverse osmosis desalination plant, is used to rinse the concentrate to remove surficial salt residue remaining from the beneficiation process. Concentrate is loaded aboard ocean-going vessels berthed at a wharf from a walled-in type open storage yard. Clay and sand-sized particles, rejected with sea water in the beneficiation process, are thickened with the aid of flocculants, dewatered, mixed, and then discharged through a submerged pipeline into mined cuts. The dredges and island facilities are self-sustaining and are designed to operate 6,000 and 7,000 hours per year, respectively, in all but the most severe weather conditions. The facilities are designed to yield product at the average annual rate of 4.8 million tonnes.

World-wide and domestic phosphate supply-demand projections support the premise that market entry in about the year 2000 is reasonable. The most optimistic estimate of the time required to implement the exploration, development, and preliminary engineering phase of this enterprise could support start-up in the year 1996. Economic sensitivity analyses, based on constant 1988 dollars, for sales prices (FOB vessel off-shore island) of \$36.00 per tonne in 1996, and \$42 per tonne in 1999, demonstrate a promise of economic viability. Construction capital, production cost, and after-tax discounted cash flow return on investment for each of five scenarios, with final production in 1999, and revenue based on a \$42 per tonne sales price, are summarized below.

Case No.	Sales Price _\$/tonne	Construction Capital \$ Millions	Production Cost \$/tonne	DCFROI
II	42	280	16.60	12.2
IIa	42	280	15.15	13.3
IIb	42	280	18.05	11.1
IIc	42	252	16.60	14.1
IId	42	308	16.60	10.6

An implied occurrence of surficial sea-bed sands containing heavy minerals and rare earths most amenable to mining by conventional ocean-going dredges targets the area considered in this study. This heavy mineral line, about 30 nautical miles from shore, is about 0.8 nautical miles wide, 8.1 nautical miles long, and 10.4 meters thick. Water depth, below MSL, is 26-30 meters. The 292 million cubic meters of mineral-rich sands have the potential of yielding 15 million tonnes of a suite of heavy minerals and rare earth products, after mining and milling process losses. The dredge is a suction hopper vessel with a leading suction head arm operating from anchored positions to excavate the full depth in panels created in a series of pits.

Dredged sands are processed first in an on-board wet mill and then pumped to a nearby dry mill for final up-grading. The wet mill concentration process rejects oversize and fine sediments, which are collected, thickened, and discharged into the mined cuts. The resulting intermediate product is pumped through a trailing pipeline to a dry mill situated on a semi-submersible platform anchored nearby. The platform is moved, as mining advances, when the distance from mining exceeds about 1.1 nautical miles. This requires the platform to move every five years. The platform is a fully self-contained floating production platform with crew quarters, and product storage and vessel loading equipment.

The heavy mineral facilities are designed to recover rutile, ilmenite, leucoxene, monazite and zircon from heavy mineral sand deposits. Processing facilities include an initial concentration plant (wet mill) located onboard the mining dredge, and a remote-located platform-mounted recovery plant (dry mill). Sea water is used for processing at both the wet and dry mills. The configurations of mine and beneficiation facilities are designed to produce 811,100 tonnes per year of products consisting of a mix of the heavy minerals identified in the study.

Economic analyses are based on capital construction cost of 235 million dollars and a production cost of \$42.53 per average tonne of heavy mineral products. Sales price for the average tonne of heavy mineral product was constructed by applying the current quoted market price for each of the five products to the quantities of each. The resulting artificial average sales price of \$127.00 per tonne is increased by 30% in increments of 10% to test sensitivity. The resulting after-tax discounted cash flow in percent return on investment is given following.

Artificial Average Sales Price \$/tonne	Construction Capital\$ Millions	Production Cost \$/tonne	DCFROI %
127.00	235	42.53	4.2
130.70	235	42.53	4.2
152.40	235	42.53	6.8
165.10	235	42.53	9.0
		42.33	11.7

The results of this study indicate that economics for both phosphate and heavy minerals support further explorative work offshore in the described target and other areas. The technical and economic risk associated with the mining, beneficiation, and infrastructure facilities proposed may be reduced to acceptable levels by more detailed engineering study. This effort is not warranted until further exploratory work is carried on to reduce the uncertainties of the minerals occurrences. This exploration work would focus on developing data upon which to base a scientific determination of level-of-confidence as to the quantity and quality of sea-bottom ore.

Limited areal investigation and complete profile core drilling to recover adequate samples in several locations are required to confirm assumptions made as to grade and quality. Properly located drill holes will aid in reducing uncertainties of continuity and variability. Favorable results of bench scale laboratory analysis and beneficiation process testing would then support more engineering.

Concurrent with the initial phases of the exploration program, limited environmental baseline studies are required to identify, evaluate and quantify biota and marine environments on a site-specific basis. These preliminary studies will provide the data with which potential impacts on marine life may be evaluated. Further, these data will provide the means of analyzing and costing mitigative alternatives to various exploitation plans. The success of, and the cost of, mitigation and environmental monitoring may be a significant additional operating cost in the offshore mining of minerals.

The bibliography, contained as Section 9, is intended to recognize Zellars-Williams Company key professional contributors, in addition to J.M. Williams, P.E., as a principal investigator, and all the sources of reference used in preparing the report.

The Draft Final Report was delivered and reviewed in Atlanta at a Task Force meeting on May 17, 1988. A second Task Force meeting in Atlanta was held on June 14, 1988 to receive input and to consider modifications and amendments to the Draft. The Final Report, reflecting comments of the Task Force, was published on July 20, 1988.

"THIS RESEARCH WAS FINANCED THROUGH A GRANT FROM
THE GEORGIA GEOLOGIC SURVEY, ENVIRONMENTAL PROTECTION
DIVISION, DEPARTMENT OF NATURAL RESOURCES.
FUNDED BY THE MINERALS MANAGEMENT SERVICE
DEPARTMENT OF THE INTERIOR
UNDER MMS AGREEMENT NO. 14-12-0001-30399"

"V - "			
9			
Ų.			
n w			
ne i			
Texas (			

### SECTION 2

### SCOPE OF STUDY

### 2.1 OVERVIEW AND OBJECTIVES

In August 1987 Zellars-Williams Company, a member of Jacobs Engineering Group Inc., (ZW), contracted with the Department of Natural Resources, State of Georgia, to provide a resource assessment study for Georgia offshore minerals. The specific study area (Figure 2.1) is defined as the Continental Shelf off Georgia, lying between Universal Transverse Mercator (UTM) grid lines N 3,362,400 meters and N 3,675,000 meters. The western and eastern study-area boundaries, respectively, are the three geographical-mile line (measured seaward from the coast as depicted on U.S.G.S-U.S.N.O.S. topographic-bathymetric maps) and the shelf break.

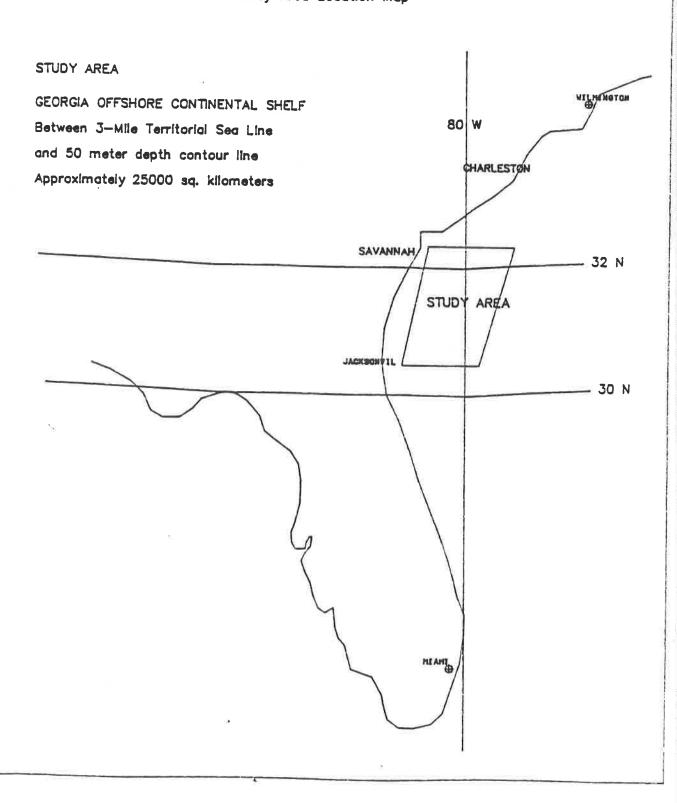
Two primary services are defined by the scope of study:

- o preparation of resource assessment studies (for heavy mineral sands and phosphorites), which include quantity, chemical analyses and physical properties, and
- o a general economic feasibility analysis (for both heavy minerals and phosphorites) which consists of a discussion of mining technologies, infrastructure, and other facilities, as well as economic sensitivity analyses of factors relative to exploitation of mineral resources.

Project deliverables are limited to the following items:

- o a computerized geologic database,
- o digitized resource maps, and
- o a final project report describing the physical resource and presenting the economic feasibility analyses.

FIGURE 2.1
Study Area Location Map



### 2.2 DATA COLLECTION

Resource assessment studies in this report are based on published and unpublished reports and databases. The only two potential mineral resources that have been reported for the Atlantic Continental Shelf (ACS) offshore of Georgia are heavy mineral sands and phosphorites. Deposits of materials such as gravel and shell have been located in other ACS areas, but no descriptive evidence of these materials in exploitable concentrations exists for the study area.

Steps leading to the resource description included identification of available data, collection of them, standardization to provide comparable formats, assessment of data quality and assignment of consequent limitations on its use, integration of data sets of comparable character and quality, and assessment of the natural resource in terms of location and probable quantity and quality.

Available data related to potential mineral resources offshore of Georgia were identified by several means. Bibliography and literature reviews were conducted to assess the availability of published information. Data survey forms were prepared and submitted to certain organizations to determine the availability of unpublished data. Additionally, a number of personal contacts were made in order to obtain specific data or samples, or to follow-up on data survey forms.

The Request for Proposal specified eight potential data sources for evaluation during the course of the first phase of the Resource Assessment Study. Contacted potential sources are listed in Table 2-1, with persons contacted at each, as well as an assessment of the current holdings of each.

### A. Georgia Geological Survey, EPD, DNR, Atlanta, Georgia

Contact: Mr. Jeff Kellam, 404/656-3214

Holdings of the Georgia Geological Survey are generally duplicative of published information that may be as easily acquired elsewhere. However, a careful file review will be conducted with Survey staff to ensure that essential materials do not escape attention.

Table 2-1

# Organizations Contacted for Data Relevant to

# GEORGIA OFFSHORE MINERAL, ASSESSMENT STUDY

Data Used	N/A	N/A	8	No - data being reduced, not avail- able until Sept. E8	N/A	N/A	Geologic Model Phosphate mine model Heavy minera! model	Data set of interpreted sparker and airgun profiles covring the Georgia shelf and Slope, Heavy mineral information from data file phosphate analyses on shelf drill cores.	No - not relevant to study.	No - not released.	No - not relevant.
Type of Data Held	Holdings generally available from published sources or available from other sources.	No independent relevant data.	High resolution seismic (HRS) profiles, side scan records, (CCTV) tapes, bathymetric profiles.	Box cores, vibracores, HRS profiles, side scan records, gamma-sled traverses.	Same investigation and data as Marine Extension Service	Same as Geology Dept. Univ. of Georgia, Atlanta	Vibracore and grab samples, HRS profiles, side scan sonar	Data set of interpreted seismic profiles covering the Georgia shelf and Biake Plateau. Data file of analyzed shelf grab samples	Published data announcements	Proprietary	Cores and geophysical logs. F.RS profiles
Respondent	J. Kellam	A. Barsotti	J. Harding	J. Harding	J. Harding	J. Herding	A. Grosz	P. Popenoe F. Manheim	R. Warnken	J. Herding	R. Amato
sponse Telephone	×	×					×	*			
Method of Response Letter Telec			×	×	×	×				×	
DSF			)5 (%				×		×		×
Contacts	J. Kellam	A. Barsotti L. Lind	V.J. Henry	J. Harding	J. Noakes	V.J. Henry	A. Grosz E. Force J. Wynn	P. Popenoe F. Manneim	R. Warnken	C. Woolsey	R. Amato
Grganization	, Georgia Geologic Survey * Atlanta	. U.S. Bureau of Mines * Washington, D.C.	. Geology Dept., Univ. of * Georgia, Atlanta	. Marine Extension Service * Univ. of Georgia, Savannah	Center for Applied Isotope * Studies, Univ. of Georgia Athens	Skidaway Institute of * Oceanography, Univ. of Savannah	, U.S. Geological Survey-ENR * Reston, Virginia	U.S.G.S., Office of Marine * Geology, Woods Hole, Mass.	NDAA, Boulder. Colorado	Mississippi Minerals Research Institute	K. MMS, Vienna, Virginia DSF = Data Survey Form
	Ą.	В.	ပ	å	ய்	۱.,	ပံ	i	<u> </u>	J.	. A OSF

DSF = Data Survey Form N/A - Not Applicable \* Organizations listed in Request for Proposal for evaluation of data relevant to study.

### B. U.S. Bureau of Mines, Washington, D.C.

Contact: Mr. Aldo Barsotti, Division of Minerals Availability 202/634-1138; Mr. Langtrey Lynd, Titanium Commodities Specialist, 202/634-1055.

Mr. Barsoti and Mr. Lynd have jointly reviewed DMA data holdings, along with Mr. Don Rogich (Chief, DMA). They concluded that they have no independently developed information that is relevant to the requirements of the Georgia Offshore Minerals Assessment Study. They hold no samples.

### C. Geology Department of Georgia State University, Atlanta, GA.

Contact: Professor Vernon J. Henry, 404/658-227 2

There are virtually no unpublished data in the files of Georgia State. Rather, all assessment work is accessible through published information on file there, or elsewhere.

The recent work of Georgia State is based on two data gathering campaigns, the first reported upon in June, 1983. This was work performed for the U.S. Geological Survey (USGS), in a cooperative program with the Bureau of Land Management (BLM), which consisted of a survey conducted to determine the occurrence and distribution of biological and geological hazards on the ocean bottom between Cape Hatteras, N.C. and Jacksonville, Florida from the three-mile inner-shelf boundary seaward to the 50 meter isobath. During the course of this work nearly 6,000 kilometers of trackline were covered, providing the following information:

- o 3.5 khz, 5662 kilometers
- o Uniboom air gun system, 5734 kilometers
- o Sidescan sonar system, 5872 kilometers

In addition, underwater television camera work was performed, as well as data gathering from 22 dives of the research submersible, <u>Diaphus</u>.

In 1986 Georgia State reported the results of a survey along 420 kilometers of trackline proceeding from the vicinity of the Altamaha River northward into Port Royal Sound, S.C. This work was supplemented by data from 1984 borings by the South Carolina Water Resources Commission, performed in cooperation with the U.S. Geological Survey.

Interpretation of the seismic data gathered for the BLM has contributed to numerous important reports since 1981. Most notable among those, the 1986 publication by Kellam and Henry, "The Interpretation of Seismic Stratigraphy of the Phosphatic Middle Miocene on the Georgia Continental Shelf". This document contains stratigraphic sections derived from the seismic profiles, as well as contour maps showing the structure of important sedimentary strata. These contour and isopach maps represent two levels of refinement beyond the basic uninterpreted raw seismic data.

## D. Marine Extension Service, University of Georgia, Savannah, GA Contact: Professor James Harding, 912/362-2496

Data collected jointly by Dr. Harding and Dr. Noakes are presently being reduced. Data consists of box cores, vibracores, HRS profiles, side-scan sonar records, gamma-sled traverses, all of which were obtained on a grant to investigate the occurrence of heavy mineral placer deposits offshore Georgia. The investigation is 50 percent complete. Data will be available when investigation is complete (end of August, 1988).

### E. Center for Applied Isotope Studies, University of Georgia,

Athens, GA.

Contact: Professor John Noakes, 404/542-1395

Work being done jointly with Dr. Harding. Not available until end of August, 1988.

### F. Skidaway Institute of Oceanography, University of Georgia,

### Savannah, GA

Contact: Prof. James Harding, 912/362-2496; Prof. Vernon J. Henry, 404/658-2272

All raw data obtained from high resolution seismic surveys conducted by the University of Georgia are on file at Skidaway. Files containing interpreted seismic data are believed to be located there, as well. Virtually all trackline data have been incorporated into publications.

### G. U.S.G.S. Eastern Mineral Resources, Reston, VA

Contact: Mr. Andrew Grosz, 703/648-6314; Mr. Eric Force, 703/648-6325; Mr. Jeff Wynn, 703/648-6389

The U.S.G.S. holds a large body of raw data and interpreted information, as well as a limited amount of unpublished information, that is pertinent to the Atlantic Continental Shelf overall. Certain elements of this work are relevant to the area offshore of Georgia. The most recent data pertinent to offshore Georgia are derived from a survey conducted offshore in June, 1985 in which 26 samples were acquired, including 10 vibracore, three of which have been fully processed. In each instance, surface grab samples were obtained at the location of vibracores. Samples were subjected to mechanical classification on shipboard, with a three-turn spiral classifier; the heavy mineral fraction was then subjected to microscopic analysis and heavy media separation, in order to determine total heavy mineral fraction and other characteristics of the sample.

### H. U.S.G.S. Office of Marine Geology, Woods Hole, Massachusetts

Contact: Mr. Peter Popenoe, and Dr. Frank Manheim - 617/548-8700 The Woods Hole, MA office of the U.S. Geological Survey has a large data set of both raw and interpreted seismic profiles as well as the database of analyzed shelf grab samples for the continental shelf off Georgia. The raw seismic data has all been released to the public through the National Geophysical Data Center (NGDC) in Boulder, CO, and most of the interpreted data have been published.

Intepreted, but unpublished, seismic data covering the Georgia continental shelf and slope were also located in Woods Hole, held by Peter Popenoe, who was actively working on the analyses of these data. As a large part of these unpublished data were pertinent to the Georgia Shelf investigation, ZW made an appeal for the unpublished data through the joint Department of Interior-State of Georgia Task Force. These data were released in Open-File (Popenoe and Spalding, 1988), and form the basis for compiling the structure contour and isopach maps.

The unpublished data file of analytical data on Georgia shelf grab samples used in this report was also obtained from the USGS Woods Hole office.

### ATTACHMENT "A"

### GEORGIA OFFSHORE MINERAL ASSESSMENT

### DATA SURVEY FORM

ORGAN	I	ZAT	١	ON	:
-------	---	-----	---	----	---

			ሮ፣	

TEL. NO.:

	s your organization possess borehole data in the EEZ offshoring.
	answer to above is NO, proceed to Question II.)
Α.	Type of boring
в.	Number of borings
c.	General location of borings
D.	Average depth of boring
E.	Geophysical log?
	1. Type
F.	Geological log?
	1. Correlations completed?
G.	Geologic Data Format (hard copy, computer, etc.)
н.	Sieve analysis
1.	Heavy mineral analysis
J.	Phosphorite analysis
Κ.	Other mineral analysis (specify mineral)
L.	Have these data been reduced?
	1. Maps:
	Type
	Scale
	Quantity
	2. Cross sections:
	Scale
	Quantity

9	11	Does your organization have bottom grab sample data in the EEZ offshore Georgia?
e se		(If answer is NO, proceed to Question III)
19		A. Approximate number of samples
		B. General sampling location
		C. Sieve analysis (specify)
		D. Heavy mineral analysis
		E. Phosphorite analysis
		F. Other mineral analysis (specify)
		G. Data format (Analysis sheets, computer, etc.)
		H. Have these data been reduced?
	f.(	1. Maps:
		Type
		Scale
		Quantity
		2. Cross sections:
		Scale
		Quantity
	111	Does your organization possess samples taken from the EEZ offshore
		Georgia?
		(If answer to above is NO, proceed to question IV.)
		A. TypeQuantity
		B. Method of preservation and storage
		C. General sampling location
		D. Typical length
		E. Diameter
		r. Storage location
		G. Have samples been described geologically?
27		1. Method employed
		H. Have the samples been correlated to geologic strata?

IV	Does	s your organization possess geophysical data in the EEZ offshore
	Geor	gia?
	(If	answer to above is $\underline{NO}$ , proceed to Question V.)
	Α.	Type
	В.	Number of surveys
	C.	Length of each survey
	Đ.	Have the data been interpreted?
	E.	Data storage format
	F.	Format of presentation of interpreted data
*		
	G.	Maps:
		1. Number
	V	2. Scale
	9	3. Size
Ä	н.	Cross Sections:
	341	1. Number
		2. Scale
		3. Size
V		your organization integrated interpreted data of various types
	for	presentation concerning the EEZ offshore Georgia?
	(If	answer to above is NO, proceed to Question VI.)
	Α.	Location
	8.	Maps:
		1. Number
		2. Scale
		3. Size
	C.	Cross Sections:
		1. Number
		2. Scale
		3. Size

91	oes your organization possess any unpublished papers (i.e., these						
/14	dissertations) pertaining to the EEZ offshore Georgia?						
(17	answer to above is <u>NO</u> , proceed to Question VII.)						
Α.	Method of access						
8.	Type(s)						
C.	Titles & Authors (please list)						
İs	VOUE OF CARTIZATION OF CAREF						
ls the	your or ganization, or staff, aware of any other data concerning						
ls the	your or.ganization, or staff, aware of any other data concerning EEZ offshore Georgia?						
the	EEZ offshore Georgia?						
the	Identify						
the	Identify  1. Type						
the	Identify  1. Type  2. Location						
the	Identify  1. Type						

Please submit this completed questionnaire to:

Mr. Thomas P. Oxford Zellars-Williams Company P. O. Box 2008 Lakeland, FL

Phone: 813/665-2194

### SECTION 3

### RESOURCES OF THE GEORGIA CONTINENTAL SHELF

### 3.1 INTRODUCTION

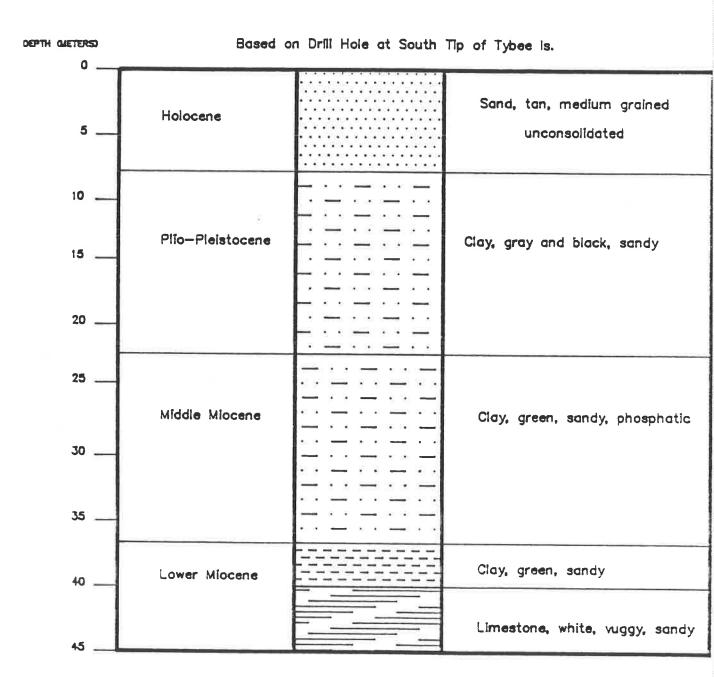
Georgia's present-day coast is characterized by tidal inlets and sand shoals associated with numerous barrier islands. The barrier islands tend to be broad nonlinear features unlike the long, narrow islands bordering the Florida coast. This development is due to heavy river sediment loads and coastal energy input favoring constructional rather than erosional features (Pirkle, 1970; Swift, et al, 1972). Oertel and Howard (1972) discuss, in detail, shoal development and morphology on the Georgia coast. Shoals extend two to four miles seaward of estuary entrances at major tidal inlets. Formation and maintenance of these shoals is due to generation of sediment circulation cells which result from dynamic dispersion of tidal and transient currents (Oertel, 1972).

Off of Georgia, the continental shelf extends seaward from the barrier islands between 100 and 200 kilometers to the shelf break where the ocean depth is about 60 meters. Near barrier islands top sediments are generally fine-grained Holocene sands that thin seaward (Foley, undated). Beyond these fine-grained deposits, more coarsly-grained sands, believed to be primarily of fluvial origin, become typical. This textural change occurs at water depths of about 14 meters (Kellam, 1981). Today's shelf morphology and topography resulted from modification of coastal features formed at previously lower sea levels (Swift et al, 1972).

Figure 3.1 shows generalized stratigraphy for the region. For more detailed discussions the reader is referred to Henry and Kellam (1987), Kellam (1981), and Popenoe (1986). Henry and Kellam (1987) provide a good general overview of the geology of the Georgia coastal plain and continental shelf. Discussions include regional structural features, the Floridan Aquifer, and regional stratigraphy. Greater detail related to the Miocene is given by Popenoe (1986).

Figure 3.1

GENERALIZED STRATIGRAPHY



### 3.2 DATABASE

### 3.2.1 Purpose and Scope

The database for the Georgia offshore resource assessment study is to be used for making estimates of quantity and quality of potential resources and to identify targets for further exploration. In order to accomplish this goal, the database must be easy to access and manipulate, and must provide the means for input and integration of new data as they become available.

Potential resources of the Georgia continental shelf are economic heavy minerals and phosphorite. Data relevant to these two types of deposits can be grouped into two general categories: geological and analytical. Geological refers to data that relate to the thickness and structure of stratigraphic units. Examples are seismic records and descriptive logs of cores from drill holes. Analytical data are derived by laboratory procedures that quantify mineral or chemical constituents, determine percentage of grains within specified size ranges, or determine sediment age by paleontological or other methods. Analytical data serve to verify interpretations of geological data, and they facilitate economic evaluations of mineral resources. Analyses are conducted on cores from drill holes and on grab samples of ocean bottom sediments.

Commercially economic concentrations of phosphorite can occur in Middle Miocene strata, and heavy minerals have been observed in grab samples of Quaternary sediments from the ocean floor. Since seismic interpreted data provide thicknesses of and depths to geologic strata of interest, they are useful for preliminary assessment of both phosphorites and heavy minerals. When these interpreted seismic data are digitized into a computerized geologic model they provide a means for estimating phosphorite source bed and overburden thicknesses, and heavy mineral sand deposit thickness. Because of the paucity of available analytical data from core drilling, there are gross limitations to the reliability of such estimates. Vertical and horizontal distributions of phosphorite within Middle Miocene strata cannot be determined without abundant core analysis data. Likewise, although grab

sample analyses are available, there are on four published vibracore analyses within the study area (Ayers, 1977) to make reliable predictions of heavy mineral vertical distributions in Quaternary sediments.

The available data for this assessment study are adequate for making only gross estimations of resource quantities. The great value of existing data is that it provides a sound and essential basis for identifying targets for further exploration.

Zellars-Williams has integrated the unpublished analytical database into a usable database format. These data come from two primary sources, as follow:

- o interpreted and annotated seismic profiles provided by Peter Popenoe of the U.S. Geological Survey (Popenoe and Spalding, 1988), and
- o tabulated grab sample analyses jointly obtained by the U.S. Geological Survey and Woods Hole Oceanographic Institution (Hathaway, 1971).

Targets for further exploration have been identified by the preparation of maps using data from this database and from review of published reports. Once target locations for heavy minerals and phosphorite were established, hypothetical models of economic deposits were placed at the target locations to establish the economic feasibility of mining at these locations if, by intensive core sampling, the deposits are proven to exist.

### 3.2.2 Database Structure

The database prepared by Zellars-Williams contains two separate and distinctly different type of data. The first type is composed of the tabulated analytical data from Hathaway (1971). These quantitative data relate to particle size characterizations, gross mineralogy, heavy mineral concentrations and grab sample locations. For each grab sample location, 45 identified fields of data have been provided for in the database. Fields include those recommended by Grosz and Escowitz (1983), as well as others. The 45 fields are as follow:

1)	Sample I.D.	16)	Magnetite	31)	Glauconite
	Latitude	17)	Ilmenite	32)	Sphene
	Longitude	18)	Apatite	33)	Sulfides
	UTM North		Monazite		Phosphate
	UTM East	20)	Rutile		Amphibole
6)	Depth	21)	Zircon	36)	Limonite
	Wt. % Gravel	22)	Sillimanite	37)	Zoisite
	Wt. % Sand	23)	Kyanite	38)	Augite
9)	Wt. % Silt	24)	Staurolite	39)	Hypersthene
	Wt. % Clay	25)	Leucoxene	40)	Anadalusite
	Quartz	26)	Titanite	41)	Spinel
12)	Potassium Feldspar	27)	Mica	42)	Dumortierite
	Plagioclase Feldspar	28)	Garnet	43)	Glaucophane
	Heavy Minerals	29)	Epidote	44)	Hornblende
	Phosphorite		Tourmaline	45)	Aegerite
	•				

Data for all of these fields are not presently available for the Georgia continental shelf. Edit, retrieve, input and report writing functions have been developed to key on sample number, location, and location ranges. Data entry windows, menus and retrieval queries facilitate these functions for user friendliness. Standard report formats have been developed and ADVANCED REVELATION permits specialized reports to be easily developed by the user.

The second type of data contained in the database is derived from the three-dimensional computer model (Section 3.3) developed for the Georgia offshore area. From the computer model, data were retrieved and stored for each UTM block within the OCS blocks of the study area, as shown in Figure 3.2. Each block is described by its boundary and geographical center-point, both in latitude and longitude and in the AMS coordinate system. The data for each OCS block consist of 25 fields grouped under major headings, as follows:

### o Location and area

- oo Area
- oo UTM East coordinate of block center
- oo UTM North coordinate of block center
- oo Latitude of block center
- oo Longitude of block center

8				
i i				
2 (1) 3 (2)				
*				
			po	
			P	
н				
) 0				
5				
		*		
tr.	×			
- 10				
	20			
	*			

- o Ocean floor character
  - oo Weight percent gravel
  - oo Weight percent sand
  - oo Weight percent silt
  - oo Weight percent clay
- o Stratigraphy and bathymetry
  - oo Water depth
  - oo Quaternary thickness
  - oo Pliocene thickness
  - oo Upper Miocene thickness
  - oo Middle Miocene thickness
  - oo Lower Miocene thickness
  - oo Middle Miocene bottom structure
  - oo Overburden thickness (thickness of stratigraphic units overlying Middle Miocene)
- o Major heavy minerals on ocean floor
  - oo monazite
  - oo rutile
  - oo staurolite
  - oo titanite
  - oo zircon
- o Gross mineralogy
  - oo quartz
  - oo heavy minerals
  - oo potassium feldspar
  - oo plagioclase feldspar
  - oo phosphorite.

There are no provisions for input of new data for the second data type because such provisions would result in inappropriate mixing of raw and modeled data. Menus have been developed to access retrieval utilities and generate reports concerning the modeled database.

Included with this report (Appendix A) are hard copies of both the raw and modeled databases. In addition, these data, on magnetic media, accompany the report to the Georgia Geologic Survey. Raw data have two magnetic media forms: ASCII files for input into the Georgia Geologic Survey's prime computer and REVELATION database files. Modeled data are in ASCII format accessible through REVELATION and specialty access programs developed by Zellars-Williams.

### 3.3 MODEL CONSTRUCTION

ZW uses the EAGLES-PC software to develop numerical models for natural resource evaluations. The EAGLES-PC program, GRID, provides the capability to produce regular grids from randomly-spaced data points. One grid is produced for each physical and analytical parameter to be evaluated. The grid consists of rows and columns with a calculated numerical value at each intersection. These grids are used to produce maps, cross-sections, volumetric calculations, mine plans, mining sequences, blending and stockpiling alternatives, product quality forecasts, and operating cost evaluations.

There is a virtually unlimited set of equations and parameters to be used to calculate the grid from the data points. For the Offshore Georgia Minerals Assessment project, ZW studied several different sets of equations and parameters prior to selection of the set which provided the best fit with the raw drill-hole data. In general, the selected set is defined as follows:

- Eliptical linear inverse distance weighting
- o Anisotropic angle of 140 degrees
- Anisotropic factor of 5
- o Direct assignment distance of 240 meters
- o Maximum search distance of 48,000 meters
- o Extrapolation distance of 22,000 meters
- Minimum number of points for gridding is 2
- o Fixed sectors used
- Selection for gridding by number sector
- o Number of points per sector is 2

- Number of sectors is 8
- Shadow angle is 10.0 degrees
- Deterministic weight function applied to power of 0.5.

Grids can also be produced using an EAGLES-PC program called GENGRD. As the name implies, this program generates grids from digitized contour Creation of new grids by operations involving original grids is accomplished in GRDMOD (GRID MODification). Grid-to-grid operation capabilities consist of modifications based on:

0	In	te	rs	e	ct	10	Π	S

Division

o Unions

o Identity

o Targets

o Lower values

Operands

Upper values

o Constants

o Basement limits

o Addition

o Ceiling limits

o Subtraction

o Data extensions

Multiplication

### 3.3.1 Geological Model

The study area geologic model contains nine grid files, as follows:

o Thickness of:

Quaternary

Pliocene

Upper Miocene

Middle Miocene

Lower Miocene

- o Bathymetry
- o Structural countour elevation of the base of Middle Miocene
- o Overburden thickness
- Total depth to phosphate matrix.

Thickness grids for individual stratigraphic units were created from discrete point data using the GRID program. Point data were scaled from interpreted, high-resolution, sparker seismic strip charts provided by the U.S. Geological Survey. Thicknesses were scaled assuming the seismic velocity for sea water (1500 meters per second) for the entire thickness. Some of the data points in the northernmost part of the study area came from Gilliss lines 1-P, 7-P, and 9-P. The majority of data points, however, are from FAY lines 23, 24, 25, 26, 27, and 28. Figure 3.20, at the end of Section 3, shows all of the data points used to create the geological model.

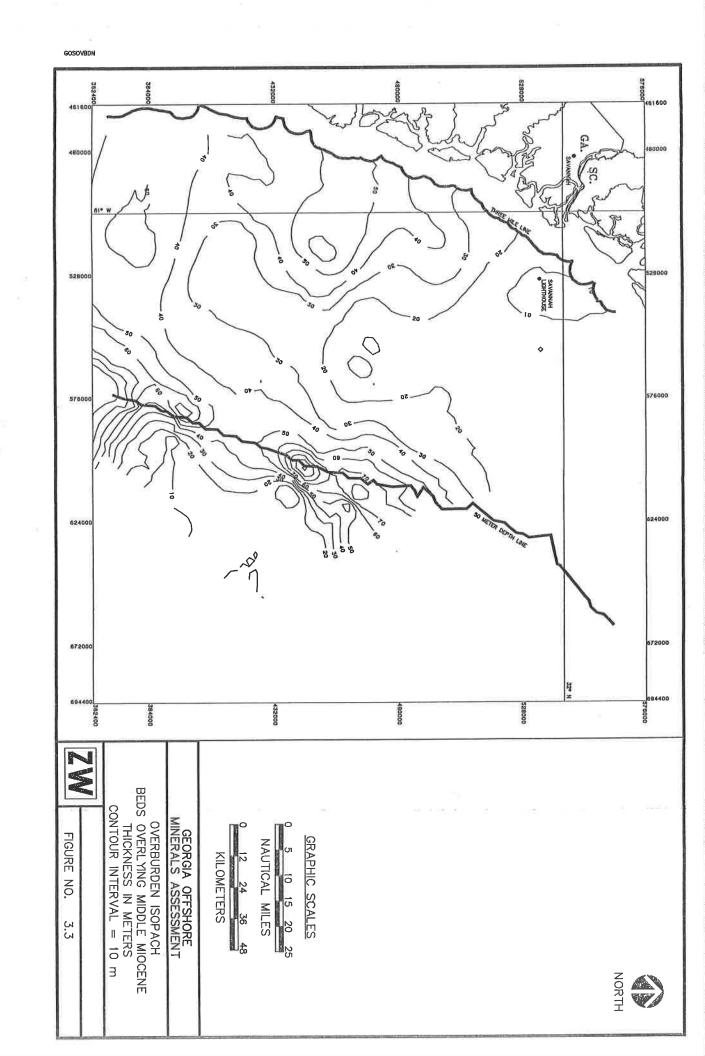
The bathymetry grid was produced using GENGRD. Contours were digitized from several U.S. Geological Survey-National Oceanographic Survey topographic-bathymetric maps that cover the study area.

Grids of overburden thickness, total depth to matrix, and the Middle Miocene base structure were produced in GRDMOD. Overburden thickness (Figure 3.3) is the sum of Quaternary, Pliocene and Upper Miocene thicknesses (Figures 3.4, 3.5, and 3.6, respectively). Total depth to ore (Figure 3.7) is the sum of bathymetry (Figure 3.8) and overburden thickness. The base structure (elevation) contour grid for the Middle Miocene (Figure 3.9) was generated by summing bathymetry, overburden thickness and Middle Miocene (Figure 3.10) thicknesses and multiplying this sum by a negative one.

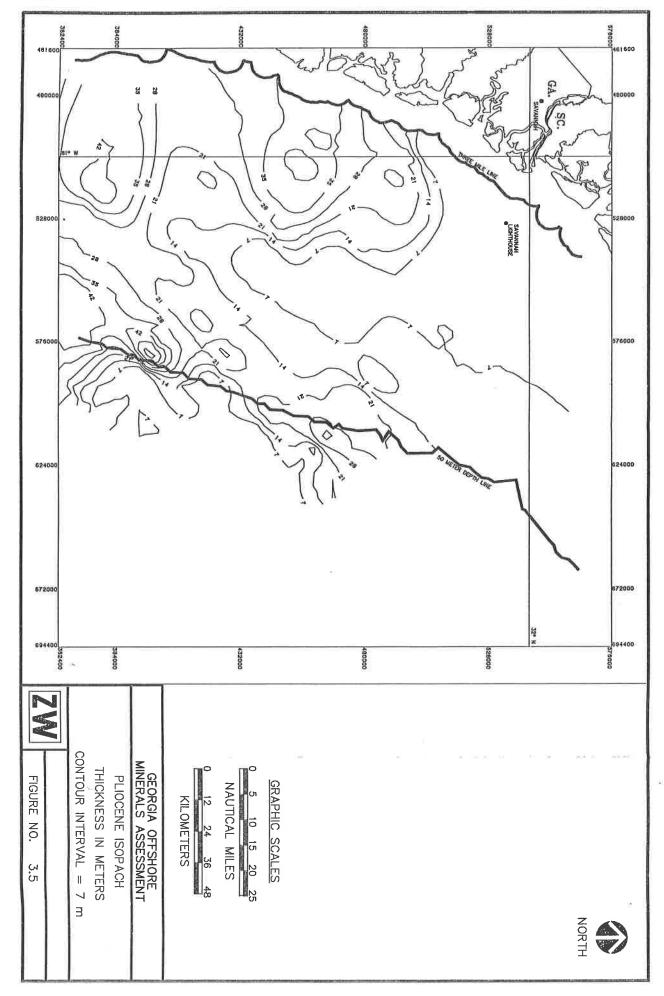
### 3.3.2 Analytical Model

The analytical model of the study area was built using sample mineralogical and grain size analyses data files listed in Hathaway 9971). This database is very extensive in terms of both area covered and number of constituents analyzed. However, since the database results from analysis of grab samples of surficial deposits it relates only to the locating of a hypothetical heavy mineral deposit. It is not relevant for development of a phosphorite deposit model in Middle Miocene strata. To remain within the scope of this study, only sample points within the Georgia ACS study area were considered, and only those constituents relevant to evaluation of economic minerals were modeled.

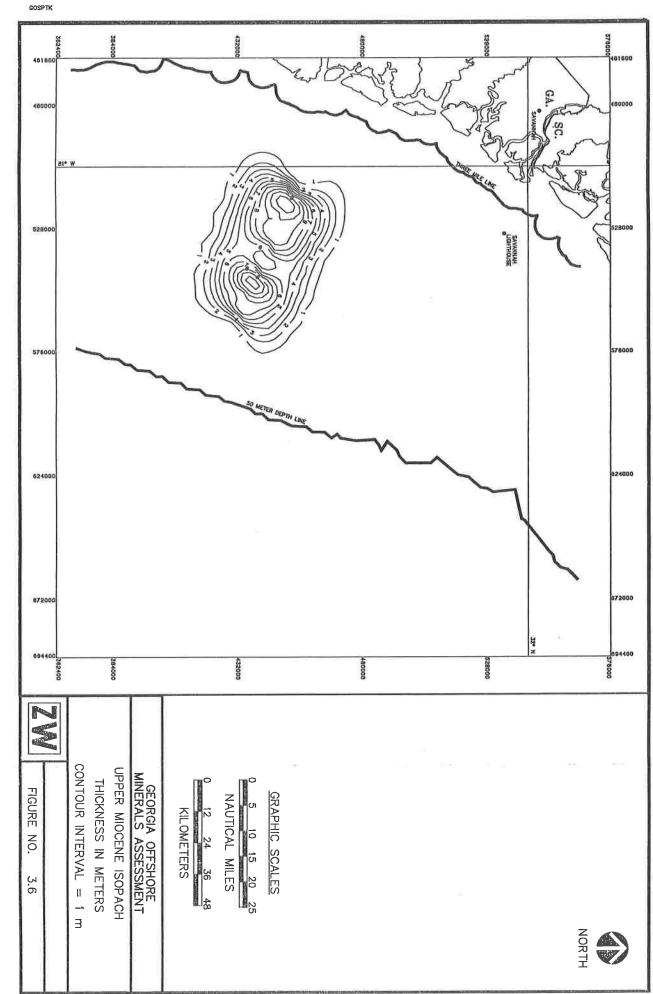
Grids were created from discrete data points for thirteen different constituents. These constituents are summarized below under their respective data file code lines and the approximate number of data points used within the study area. Data file code lines used here are those presented in Hathaway (1971) and are not related to the database prepared in conjunction with this report. They are included here for reference.

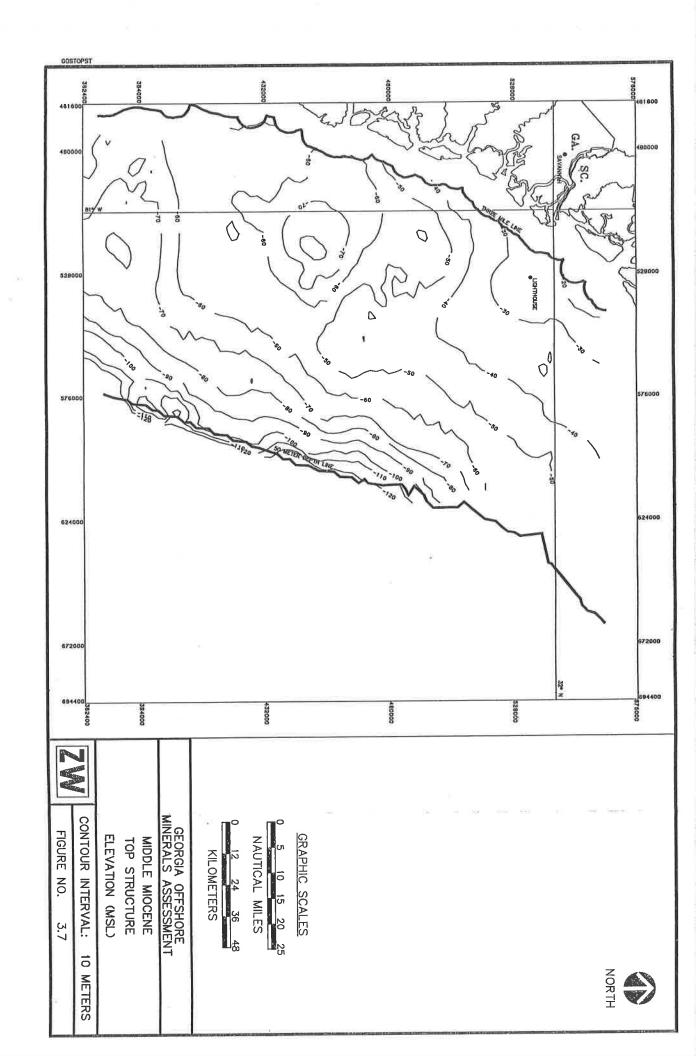


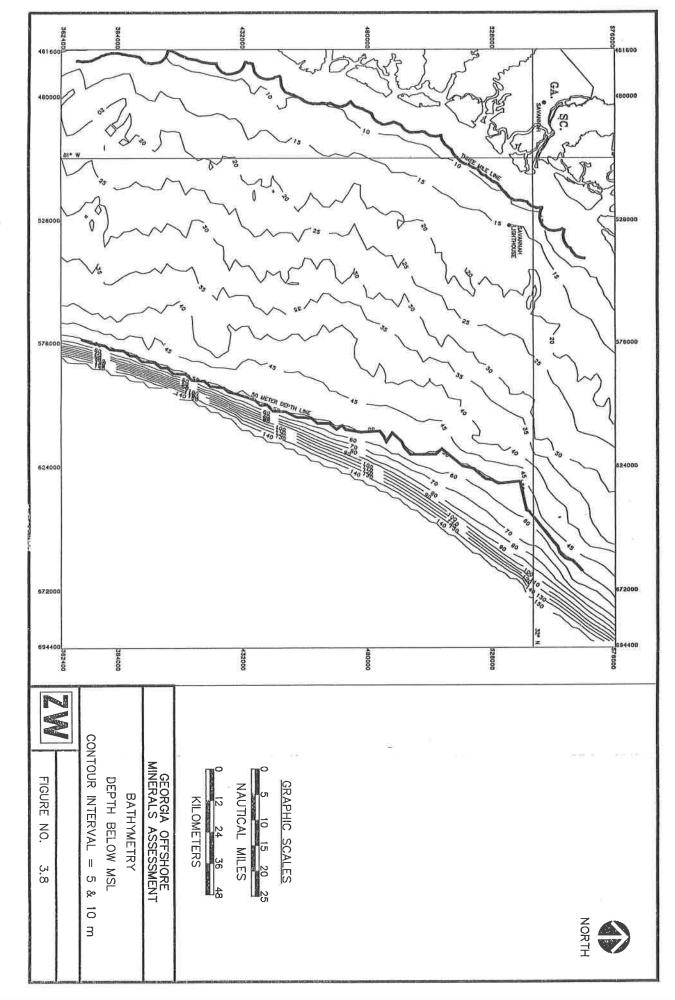
NORTH

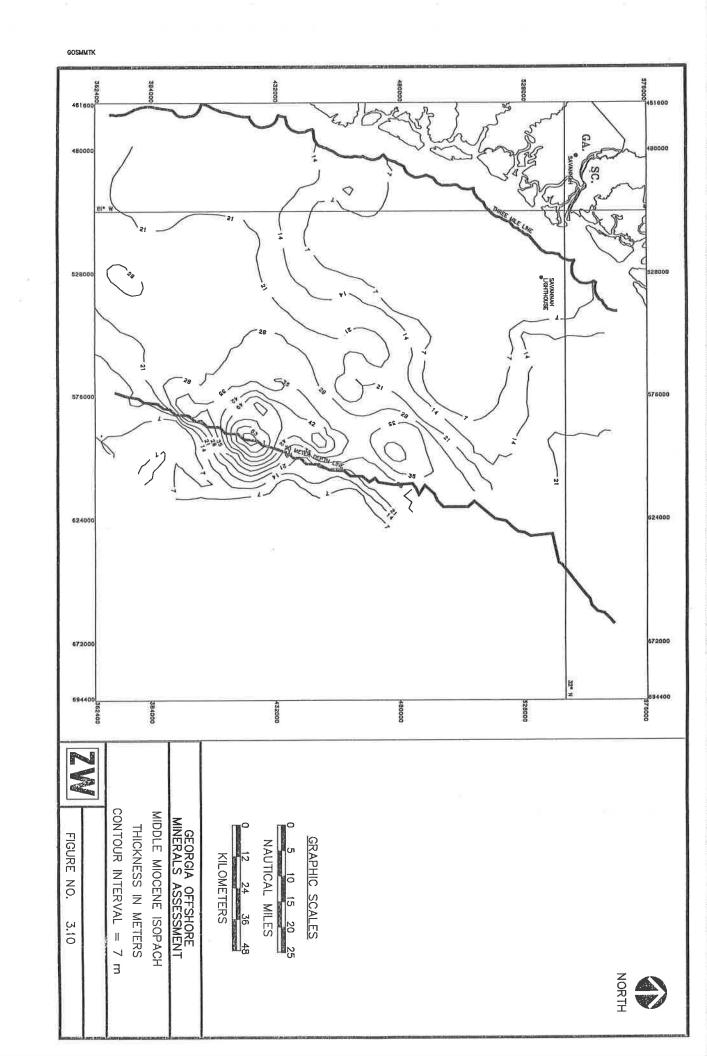


•		







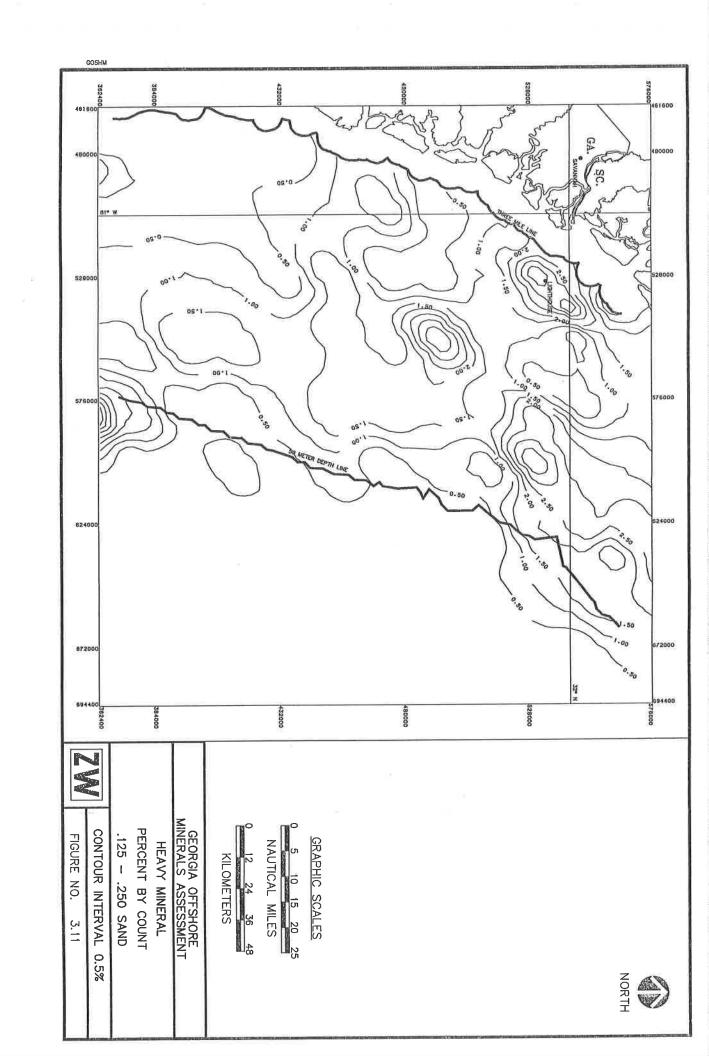


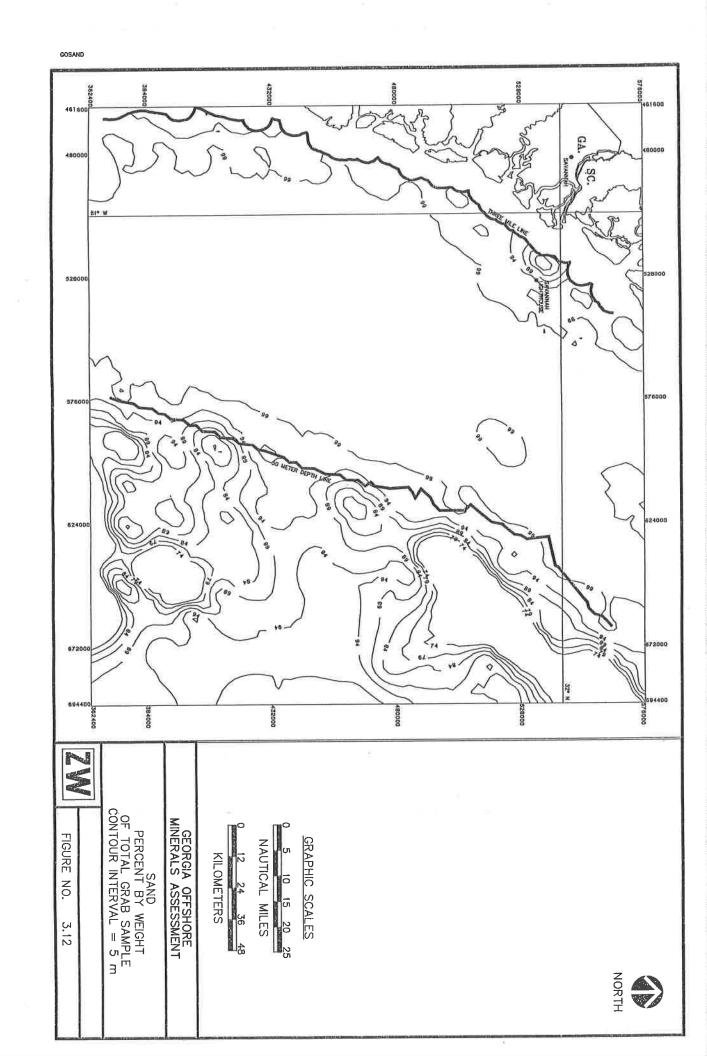
- o Code line 320 91 sample points; components given in percent by point count of the fine grain sand fraction (.125-.250 mm)
  - oo Quartz
  - oo Phosphorite
  - oo Potassium feldspar
  - oo Plagioclase
  - oo Heavy minerals
- o Code line 210 80 sample points; constituent in percent by weight of total sample
  - oo gravel (greater than 2mm)
  - oo sand (0.062 to 2 mm)
  - oo silt (0.004 to 0.062 mm)
  - oo clay (less than 0.004 mm)
- o Code line 560 17 sample points; mineral in percent by weight in the sand fraction (62 um to 2 mm) of the whole sample
  - oo monazite
  - oo rutile
  - oo staurolite
  - oo titanite
  - oo zircon

Figure 3.11 is an isopleth map, built from 91 data points in this database that shows the heavy mineral concentration within the sand fraction. Occurring at water depths between 25 and 40 meters is a linear trend of relatively high heavy mineral concentration (greater than 3%). A detailed bathymetric map (USGS, NOS, 1978) of the study area reveals that within this depth range there are topographic features that could be interpreted as relict sand shoals. Note in Figure 3.12 that between the three-mile line and the 50-meter water-depth contour the sand content is 100%. Development of these features parallels the trend of the higher heavy mineral concentration.

The hypothetical heavy mineral mining location used in this study was selected, in part, because of the distinct heavy-mineral concentration trend seen in Figure 3.11. For this project, this trend has been divided into two parts based on bottom bathymetry and geological interpretations related to

(20)						
9						
, i	32				*	
	e					
2						
				*		
1						
		(#)				
- x						
, K* 						
*						
3 1 1 3						
2 W. X						





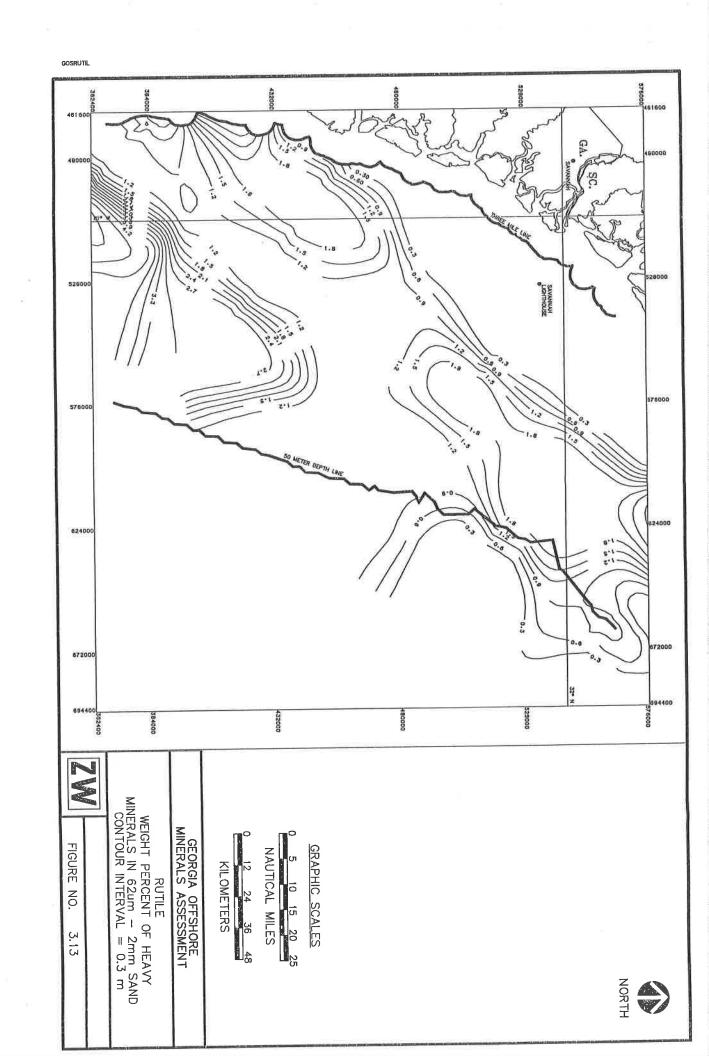
onshore heavy-mineral deposit trends. However distinct this trend is, it must be noted that it is based on grab samples with an average area of influence of 507 square kilometers.

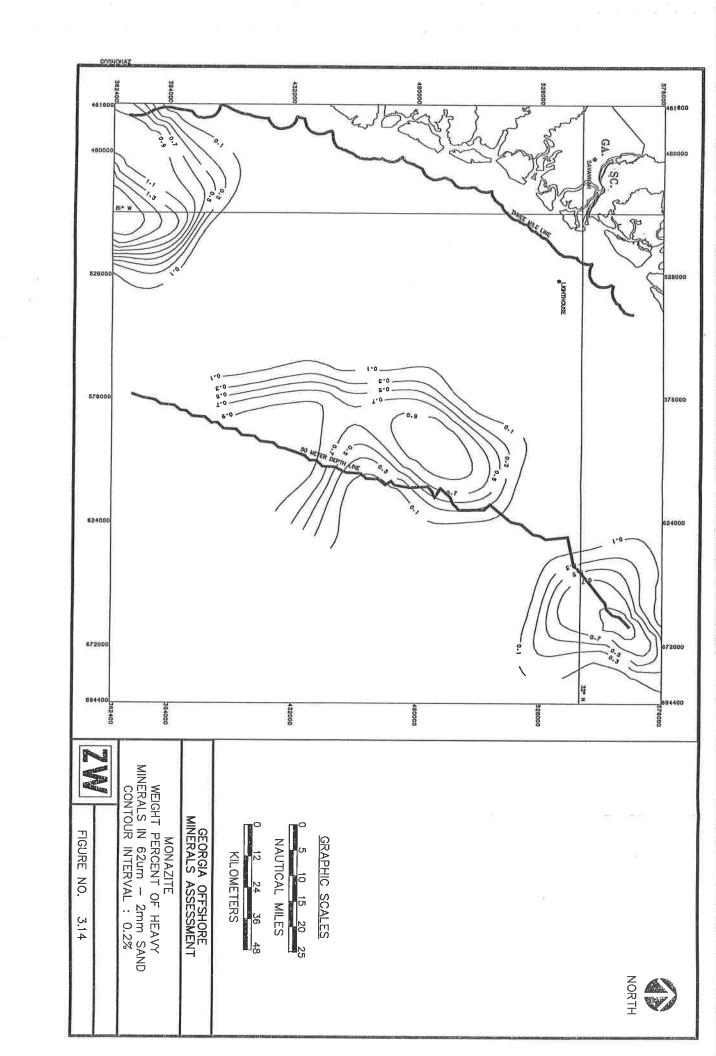
The aforementioned trend is very pronounced using total heavy mineral content and is supported, in general, by trends in the mineral species rutile, monazite, zircon, and staurolite (Figures 3.13 through 3.16). Unfortunately, the mineral species database does not contain a field for ilmenite, and leucoxene is listed under titanite (Figure 3.17). While the trends in the species data approximate the total heavy mineral trend, they do not exactly overlay due to sampling frequency and distribution differences between the data sets. In the area of interest, there are species data at six locations, an average of about 105 kilometers apart. The average area of influence for each site is over 11,000 square kilometers. None of the points lie within the defined heavy mineral trend.

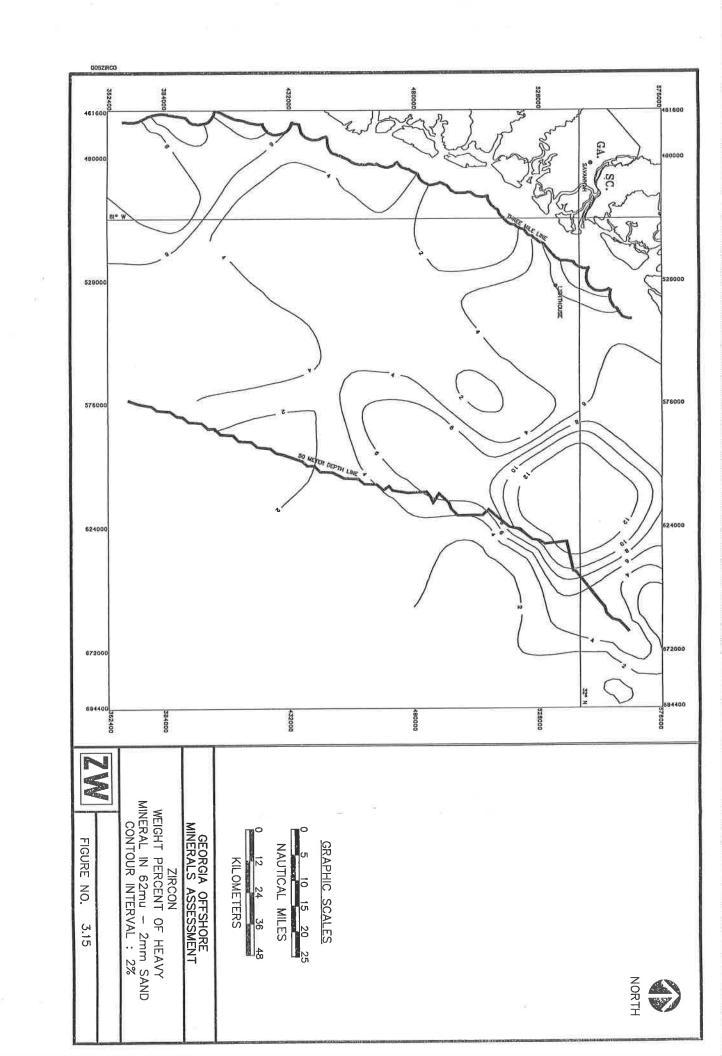
Another notable difference between the two data sets is that the total heavy mineral analyses are percentages of only the fine grained (0.125 to 0.250 mm) sand fraction, while the species analyses are a percent of the total (0.062 to 2.0 mm) sand fraction. Without knowing the heavy-mineral content of sand sizes outside of the 0.125 to 0.250 mm range and the ratio of this size range to total samples, it is not possible to determine in-situ heavy-mineral concentration. If heavy-mineral grains are predominantly in the 0.125 to 0.250 mm size range, then materials outside of this size range decrease the overall in-situ heavy-mineral concentration. Alternatively, in-situ concentration could be the same as, or even higher, than in the 0.125 to 0.250 size range.

In a plan for exploiting East Coast heavy mineral placers, the U.S.B.O.M. (1987) designed a plant to operate aboard a dredge. This plant was designed to recover heavy minerals from sand deposits typical of those found off the coast of Virginia. As designed, material greater than 10 mesh (2 mm) and less than 200 mesh (0.075 mm) would be discarded overboard. It was assumed that only 50 percent of the total material could be eliminated without significantly reducing heavy mineral recovery.

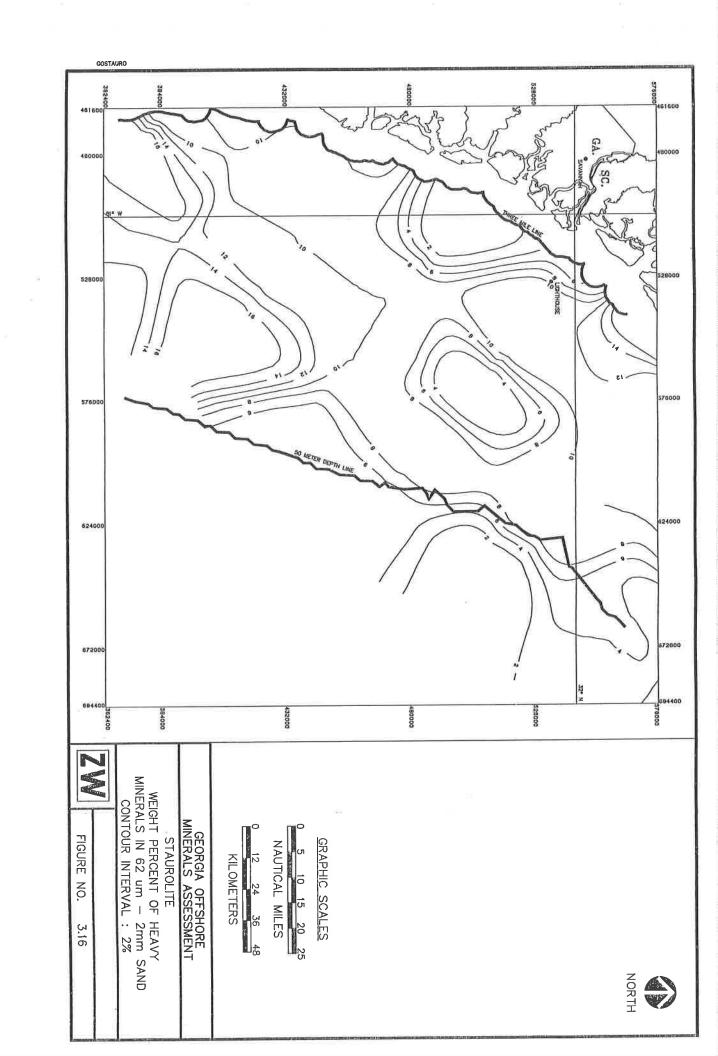
<u>«</u>				
		94		¥.
		5		
		0		
			$\bar{X}_1$	
		F		
		a 31 (1€5		
6			5	
E .			*	
* H		9	*	
×.				
	<u>~</u>			
5				
X g = 1				
				-

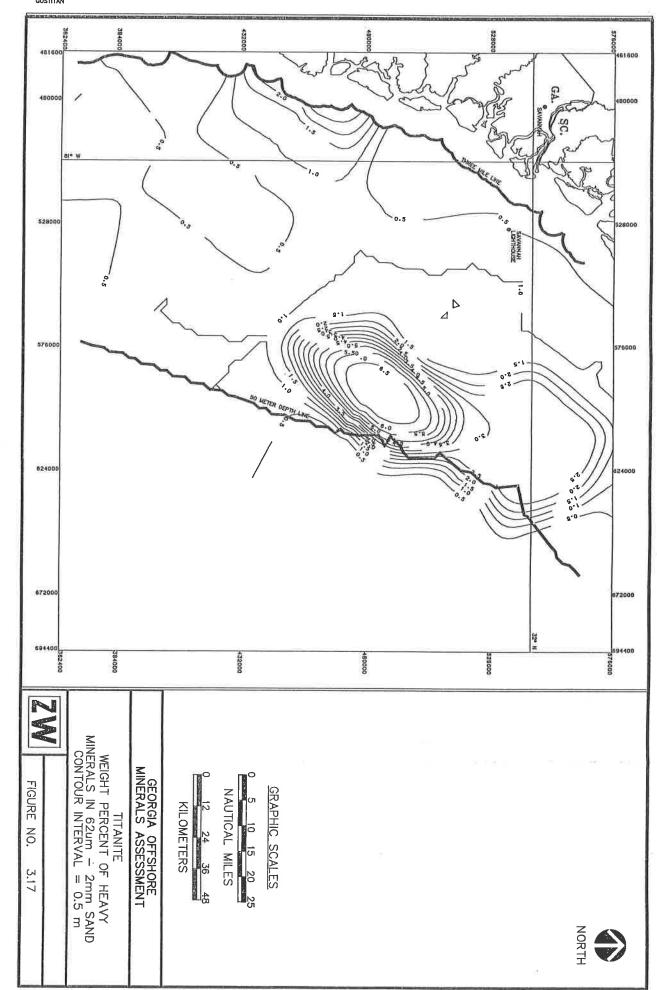






Ř		





Pirkle and Yoho (1970) present analyses of twenty surface sand samples of the Trail Ridge type which were selected from localities as far north as southern Georgia, and as far south as central peninsular Florida. In these samples, the heavy minerals tend to be concentrated in the plus 230 to minus 120 mesh (0.062 to 0.125 mm) fraction. Percentages of heavy minerals in total samples were significantly less than in the 0.062 to 0.125 mm fraction.

For the purposes of this study, a hypothetical deposit model has been built using the following assumptions:

- o The mining site has been sized to fit the orebody outline of the Green Cove Springs heavy-mineral deposit in northeastern Florida (Figure 3.18).
- o Orebody thickness is considered to be the entire thickness of the Quaternary sands within the orebody outline.
- o Species distribution is calculated from U.S.B.O.M. 1987 using annual production estimates for mean grades of mineral species. For annual mining of 5 million short tons the following species recoveries are realized:

Tons Recovered	Tons Recovered as Percent of Total Mined	Percent HM Recovery	Tons In-situ	Percent In-situ
221,862	4.44	83.6	265,400	5.31
14,119	0.28	80.8	17,500	.35
35,398	0.70	80.8	43,800	.87
25,994	0.52	83.6	31,000	.62
6,772	0.14	83.6	8,100	.17
	Recovered 221,862 14,119 35,398 25,994	Tons Recoveredas Percent of Total Mined221,8624.4414,1190.2835,3980.7025,9940.52	Tons         as Percent of Total Mined         Percent HM Recovery           221,862         4.44         83.6           14,119         0.28         80.8           35,398         0.70         80.8           25,994         0.52         83.6	Tons Recovered         as Percent of Total Mined         Percent HM Recovery         Tons In-situ           221,862         4.44         83.6         265,400           14,119         0.28         80.8         17,500           35,398         0.70         80.8         43,800           25,994         0.52         83.6         31,000

## 3.4 PHOSPHORITE POTENTIAL

Zellars-Williams' (1978) report on known occurrences of phosphate deposits in Georgia, North Carolina and South Carolina was prepared for entry into the U.S. Bureau of Mines' Minerals Availability System. Data were collected from known literature, mineral interests previously

		::	
×.			5
*			
			76 6
38			* *
			A A
			(*)
	78		
,			e
×			
**			
- St			

NORTH

prospected in the region, and governmental agencies on a regional, deposit summary, or individual prospect hole database. Estimated resources for the "Savannah District" included an offshore portion which had almost no control (two drill cores and seismic profiling).

Subsequently, Zellars-Williams, under the auspices of the U.S. Geological Survey, conducted a technical feasibility and economic potential study (Zellars-Williams, 1979) in the Georgia-South Carolina area near Savannah. This study employed the extrapolation of knowledge of onshore ore characteristics to an inferred offshore deposit because very little data were available offshore.

In general, phosphate minerals occur in marine sedimentary rocks of the Atlantic Coastal Plain from the Florida Keys to North Carolina. The known deposits of marginal or economic grade are confined to sediments of Middle Miocene or, in some cases, younger phosphate containing sediments derived from reworking of middle Miocene beds (Cathcart, 1968). Middle Miocene deposits on the continental shelf of Georgia are represented by The Coosawhatchie Formation (Henry and Kellam, 1987). The Coosawhatchie Formation contains marine sands and clays with variable amounts of phosphate mineral. It has been divided into four members, the most important of which is the Tybee Phosphorite Member. Lithology of the Tybee member is discussed by numerous authors, including Kellam (1981), Henry and Kellam (1987) and Woolsey. (1977).

Savannah is underlain by thousands of feet of sedimentary beds ranging in age from Late Cretaceous to Holocene. Near the center of Chatham County, the top of the phosphate matrix is at Elevation -45 meters. Because the overburden is excessively thick and the matrix thickness is less than 5 meters at this location, the phosphate is not considered mineable under present-day mining criteria. However, to the east and northeast the phosphate matrix thickens and overburden decreases. The higher elevation of the matrix at the coast would appear to contradict the influence of the regional dip to the southeast. The reversal in this case is caused by the north-south trending Beaufort Arch, the axis of which passes beneath the Savannah Light Tower, about 16 kilometers offshore from Savannah Beach on

Tybee Island. Although the limited wide-spaced drilling onshore and the drill data at the Light Tower suggest this structural trend, the seismic profiling work by Woolsey (1976) has provided clear evidence of the structure. It is quite probable that the phosphate matrix in the area north of the Light Tower constitutes the stable sea floor which is being abraded by migrating sand waves.

## 3.4.1 Techniques for Phosphorite Exploration

Seismic reflection surveys yield worthwhile broad-based information on stratigraphy of offshore areas. Middle Miocene strata, which typically contain the phosphate matrix, have seismic signatures that are recognizable and traceable on a regional basis (Kellam, 1981; Woolsey, 1977). Therefore, interpreted seismic data can be used to approximate depth to, and thickness of, Middle Miocene strata. In this manner, favorable sites for detailed exploration can be established. Seismic data, however, do not provide any information on the actual phosphate content of the Middle Miocene.

In phosphate prospecting there is no substitute for a well-designed program to obtain suitable cores of phosphate matrix. Cores are typically retrieved in four-inch core barrels, and coring is continuous between the top and bottom of the phosphate matrix. A properly executed coring effort will not only provide excellent records of matrix characteristics, but more importantly, it will deliver essential samples for determining the processability of the matrix and contained phosphate rock.

## 3.4.2 Phosphorite Exploration Targets

Exploration targets indicated by Henry and Kellam (1987) are the eastern flank of the Beaufort Arch, subsurface topographical features (The Tybee Trough, for example), and basal units along the edge and seaward of the Sea Island Scarp. The eastern flank of the Beaufort Arch is considered to be a primary target because phosphorite deposits tend to accumulate on the nose and flanks of structural highs.

Initial exploration for phosphorite should be conducted in locations where, if a deposit is proven, it will have the most economically favorable potential for development. Since analyses of core samples providing data on phosphate ore

grade and quality are very limited, exploration targets must be selected on the basis of relative accessibility. One such site has been selected using unpublished, high-resolution "sparker" seismic-reflection profiles which were collected and interpreted by the U.S. Geological Survey (Popenoe, personal communication).

This location, shown in Figure 3.19, has been used in this report for studying the feasibility of phosphate mining on the continental shelf of Georgia. The site selection was confined by an area of zero Middle Miocene thickness immediately to the south, the Corps of Engineers channel widening dump to the southwest, thickening overburden to the east and west, and the South Carolina border immediately to the north. This area contains the shallowest Middle Miocene deposits in the entire study area, as well as the thinnest overburden.

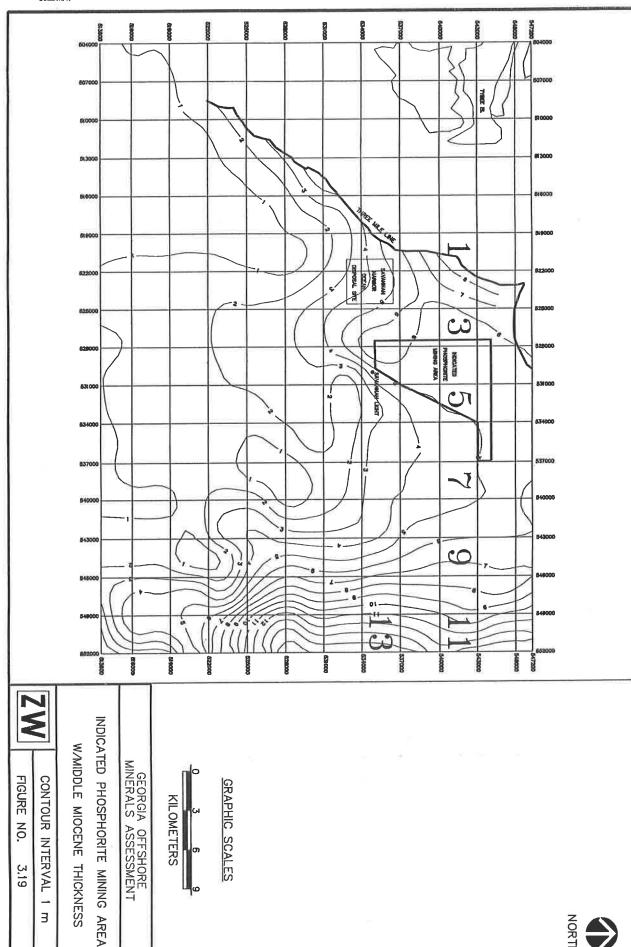
### 3.5 HEAVY MINERAL POTENTIAL

Three heavy-mineral provinces are generally recognized for the Atlantic Continental Shelf (ACS) of the United States: northern, central and southern. The Georgia coast lies within the southern ACS. Grosz, (1983) cites a number of older studies that refer to economic potential of heavy-mineral accumulations within sediments of the ACS, but do not convey sufficient information for making quantitative resource estimates. Recently published studies of ACS economic heavy-minerals contain very limited information specific to Georgia.

A reconnaissance study conducted by the U.S.G.S. (Grosz, 1983) involved analysis of 71 ACS sediment grab samples from Florida, North Carolina and Virginia. Although none of the samples represent the Georgia ACS, the study is important because results indicate that concentrations of heavy minerals occur in surficial ACS sediments in areas offshore of land areas that contain no economic concentrations.

Over the past few years, U.S.G.S. researchers have made significant progress in defining heavy mineral distributions on the ACS. Two characteristics of the southern ACS reported by Grosz (et al, 1986) are pertinent to this study. These are:

ii ji			
#			
V)			
ë			
- 180			
,			
91			
g II			
.3			
£			
2 11			
. 17.			
*			
177			
			PC



W/MIDDLE MIOCENE THICKNESS

GEORGIA OFFSHORE MINERALS ASSESSMENT

KILOMETERS

GRAPHIC SCALES

CONTOUR INTERVAL 1 m FIGURE NO.

NORTH

		- St	
	+g)		

- o elevated heavy mineral concentrations in the southern ACS appear to be limited to inner-shelf sediments (less than 60 meters water depth), and
- o heavy mineral assemblages of the southern ACS are more economically attractive than those of the northern provinces.

Ongoing studies are being conducted by the U.S.G.S. (Grosz, et al, 1986; Grosz, 1987) to assess the potential for the existence of heavy mineral placer deposits in continental shelf sediments. These studies include analyses and interpretations of grab samples, vibracores and seismic reflection profiles. Vibracore analyses have not been completed for the Georgia ACS. However, preliminary reports, based on grab sample analyses, indicate that elevated values of rutile, zircon, monazite and phosphorite are found offshore of central Georgia.

# 3.5.1 Techniques for Heavy Mineral Exploration

Sediment sampling on the ACS is done by either grab sampling or vibracoring. Grosz (et al, 1986) have concluded that grab sample analyses are of limited use in ACS placer resource estimation and the technique should be limited to very broad regional studies of qualitative aspects of heavy-mineral assemblages. The same report further concludes that, at the present time, no substitute for vibracoring is presently available for resource estimation and geologic studies in the marine environment. Vibracores are an essential element for evaluation because they provide important information on the vertical extent of heavy-mineral concentration.

Development of geophysical techniques specifically for heavy-mineral exploration on continental shelves is in its infancy. Radiometric data obtained using towed submersible sleds have shown promise as a tool for offshore ilmenite exploration (Tixeront, et al, 1978). Grosz (et al, 1986) documents testing of induced polarization (IP) with a prototype marine IP electrode streamer. Results indicate that the IP method has potential for application as an offshore exploration system and as a shipboard assaying tool.

# 3.5.2 Heavy Mineral Exploration Targets

In a thorough review of published reports and publically available unpublished documents, no accounts of ACS heavy mineral placer discoveries have been found. The U.S.B.O.M. (1987) reported that two companies explored in 1986 for heavy-mineral placers on the southern ACS. According to Grosz (et al, 1986), the prospect for finding commercially exploitable heavy-mineral deposits in ACS sediments appears favorable.

Attanasi (et al, 1987) suggest three types of sediment deposits that are likely to contain offshore titanium mineral placer deposits. These are:

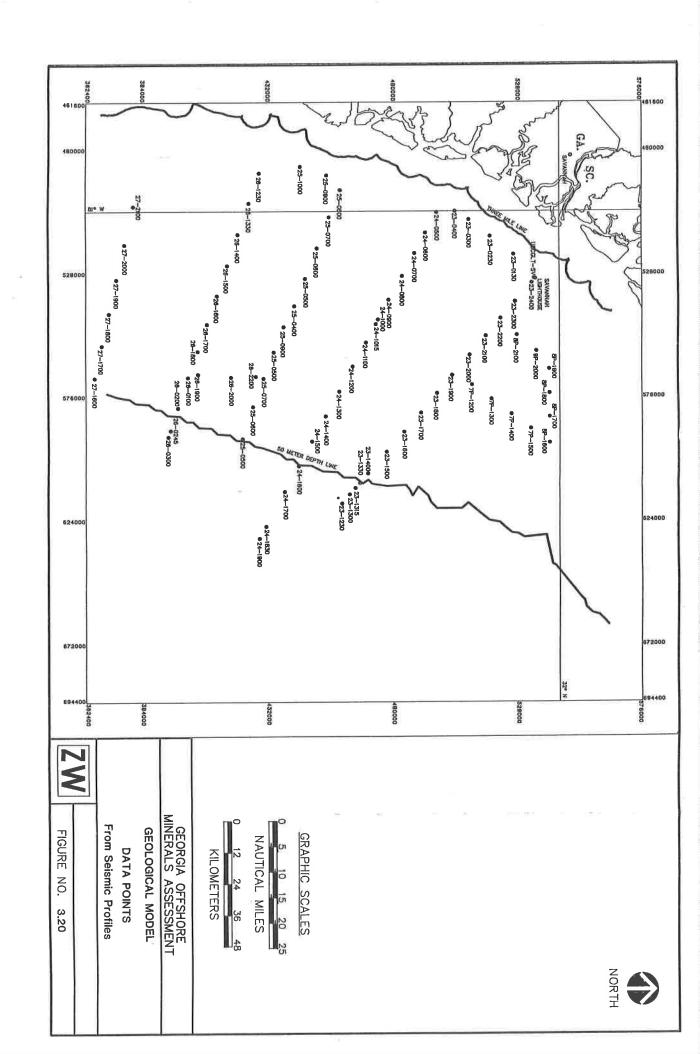
- o beach complex or strand-line deposits formed during a previously lower stand of sea level,
- linear shore-tied or isolated sand shoals, and
- o older fluvial deposits.

The world's major sources of titanium minerals are onshore beach complex or strand-line deposits (U.S.B.O.M., 1987). In a broad definition presented by Attanasi (et al, 1987) beach complex deposits include beach, aeolean dune, inlet and washover fan deposits. These deposits are generally characterized by fine-grained, well-sorted sands.

Regardless of the exact mechanism, heavy mineral accumulations offshore would have developed during, and as a result of, sea level stands lower than today's. Considering that elevated heavy-mineral concentrations in the southern ACS appear to be limited to inner-shelf sediments, i.e., less than 60 meters water depth (Grosz, 1986), and considering that there is a recognized textural change seaward of 14 meters water depth (Kellam, 1981), primary exploration targets are apparent strand-line deposits lying at water depths between 14 and 60 meters. The location designated as a hypothetical deposit (Figure 3.18) in the Heavy Mineral Analytical Model (Section 3.3.2) is one such exploration target.

An interesting and important feature of the location map for the hypothetical heavy mineral deposit (Figure 3.18) is the relative size of the Green Cove Springs deposit compared to the heavy mineral concentration trend and to the overall study area. Exploration for a heavy-mineral placer deposit having the dimensions of the Green Cove Springs deposit compares to the proverbial needle in the haystack.

6			
- ×			
	<b>6</b>		
all o			
# 10 V #			
, st			



#### **SECTION 4**

#### OFFSHORE MINING TECHNOLOGY

#### 4.1 INTRODUCTION

The two types of mineral resources that exist off the coast of Georgia are heavy minerals placer deposits and phosphorite sands deposits. Heavy minerals deposits occur when a heavy mineral source is eroded and the resulting sands are transported to the depositional site by vigorous hydraulic conduits such as waves, tides, or wind. Sediments are generally sorted, weathered, and form concentrations of heavy minerals having economic values. Heavy metals are known to exist off the coast of Georgia, but none have been explored sufficiently to warrant construction of a site-specific geologic model. Consequently, the geological model used in this study is hypothetical and is based on current strandline models from other areas of the world. A strandline deposit is one which was formed during srands at or above sea level. The strandline placers, which form the basis for the geologic model, are the primary sources for the world's supply of titanium, zircon, and other heavy minerals.

A typical heavy mineral strandline deposit contains 140,000,000 tonnes of sands located beneath 80 feet of ocean. The deposit thickness is from 3-12 meters, with no defined overburden. Deposits at much deeper ocean depths, and those with overburden, are considered economically unattractive for the present hypothetical conditions.

More information is known about phosphorite, which also occurs offshore Georgia. Extensive work on phosphorite has been done at Onslow Bay off the Atlantic Coast of North Carolina, a geologically similar area. In addition, drilling at Tybee Island and near Savannah indicates that deposits of potential economic value exist off the coastline.

The deposit parameters for phosphorite deposits offshore Georgia are similar to the characteristics listed above for heavy minerals in regard to ocean depth and deposit thickness, except that some overburden above the phosphorite exists. The type of mining systems and equipment that are applicable to heavy minerals mining may also be suitable for phosphorite mining. However, in phosphorite mining, provisions must be made for overburden disposal.

To a considerable degree, the selection of mining equipment is affected by oceanographic and meteorological conditions. Unfavorable conditions may require shutdown and movement to a safe harbor. At other times conditions may result in a lower production rate. In any case, mining equipment must be designed to meet the oceanographic conditions described in Section 5, and/or be capable of moving to safe harbor in the event of a major storm.

## 4.2 STATE-OF-THE-ART

Technical advances in offshore oil production have resulted in advanced technology that is currently available for application in the exploitation of offshore marine deposits. Mining must proceed from a central platform, or working area, from which mining and dispatching operations are controlled. These platforms or working stations consist of three general types:

- 1) floating platforms
- fixed platforms
- 3) walking platforms.

Floating platforms generally take the form of especially designed vessels on flotation hulls with dredging equipment mounted or attached. Pontoon or barge-type hulls are used for dredging work in estuaries, harbors, rivers, ship-channels and in-land waters, as these are not suitable for offshore ocean conditions. Dredged material is pumped as a water-solids mixture (slurry) via trailing pipeline to the point of deposition, or is transferred to tugboat-towed scows for transport. Conventional sea-going transport vessel configuration

modified to accommodate dredging equipment is widely used for offshore ocean deep-water dredging. These vessels usually contain compartments to store dredged material and to transport the contents to shore.

In some experimental cases, the actual mining is directed from submersible vessels or bottom-supported vehicles that are attached to the platform by pipelines, power supplies, and mechanical material handling systems such as bucketlines or dippers. While these systems have obtained samples and engaged in exploration activities at depths of over 1000 feet, presently the technology is insufficient to support similar large scale mining operations. Dredges are the only proven mining system that utilize the concept of floating platforms.

Fixed platforms have been used in sulfur mining and oil production for some time. Because they are immobile and above the surface, fixed platforms provide a working area free from movements of the ocean surface and currents. However, this immobility results in a high operating cost when conventional mechanical and hydraulic mining techniques are used. On the other hand, borehole mining can be operated from fixed platforms. In this mining technique, boreholes are drilled through the overburden to the mineral formation (matrix) by mining tools. High presssure water jets, attached to the mining tools, disaggregate the matrix and remove it from the host rock. The slurry is then pumped to the processing plant. Although it has never been successfully applied to commercial phosphate operations, the borehole mining method is being successfully used in commercial mining of sulfur and potash. Borehole mining may be applicable in phosphate deposits with deep overburden. Since it is not necessary to remove overburden, borehole mining techniques result in no overburden removal costs.

A unique walking platform is being developed by IHC Holland. It can be described as a self-elevating platform on which all motions are eliminated because it uses the sea bottom as a supporting structure. In addition, the platform has the ability to walk without being lowered into floating position, a feature that is required since the digging tool must continuously move over the mining area, similar to a land-based dragline. Power for this platform is provided by a surface vessel, which also will receive the material mined for

further processing. These supply lines are the only connection between the surface vessel and the walking mining platform. Although several variations of this machine have been developed and tested, currently no commercial walking platforms are in use.

Ellicott Machine Corporation of Baltimore, Maryland has proposed conceptual designs of platform dredges incorporating design features of conventional dredges and offshore exploration platforms. The design is suitable for mining in shallow offshore waters. This design shows a great deal of promise, and if supported by the viability of Atlantic coast OCS mining may be commercially developed in the near future.

#### 4.3 DREDGES

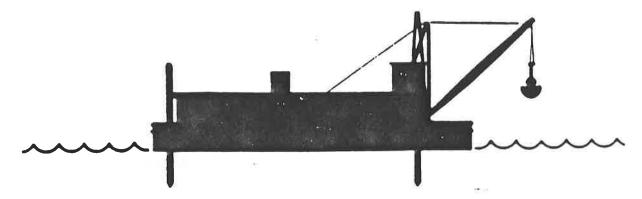
The dredge, of one type or another, is the only system proven to be successful for offshore mining. Several types of dredges have been developed and commonly employed for under-water excavation. Very few of these are suitable for deep water and ocean conditions.

Dredges may be classified as two general types. These are mechanical dredges and hydraulic dredges. The classification is based on the method used to handle excavated material.

# 4.3.1 Mechanical Dredges

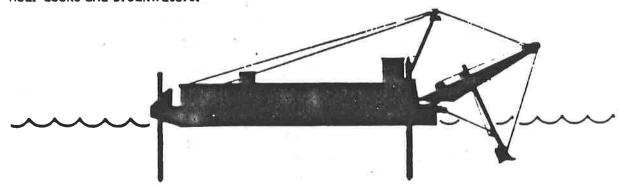
Mechanical dredges consist of three general types, as illustrated on Figure 4.1. These, as a class, are not suitable for production mining of phosphorites or heavy minerals in the offshore ocean environment. They are included here to describe their capabilities, applications, and limitations.

- grapple dredge
- 2) dipper dredge
- bucket dredge.



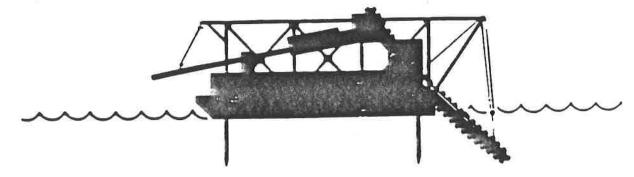
The Grapple Dredge

In this type, the work is done by a clamshell bucket suspended from a derrick mounted on a barge. It is most suitable for excavating medium-soft materials in confined areas near docks and breakwaters.



The Dipper Dredge

A powerful dipper bucket mounted at the forward end gives the dipper dredge its main advantage: strong "crowding action," produced as the bucket is forced into material being moved. This permits efficient removal of rock and other hard materials. For its size, a dipper dredge can handle larger pieces, thus reducing blasting needs.



The Bucket Dredge

Buckets mounted on an endless chain do the work here. Each bucket digs, conveys and dumps its own load. A continuous work cycle makes the bucket dredge an efficient mechanical dredge, when used in operations such as sand and gravel production.

### Grapple Dredge

The grapple dredge is a flat-topped barge upon which a derrick is mounted to support the clamshell bucket by means of wire rope lines. The clamshell derrick is attached to a revolving machinery deck similar to a land-based dragline tub. Similarly, the bucket swings around the derrick to load barges anchored nearby, or to spoil material.

Two general types of grab buckets are used -- the clamshell, for mud or stiff mud, and the orange peel, for loose rock or other hard or bulky materials. The grab dredge is used extensively around docks, piers, and particularly in the corners of cuts where it has the ability to get in close without damaging structures. This dredge works well in silts and stiff muds and is particularly effective where there are obstructions and trash. Production is poor, and an irregular bottom is left, making it unsuitable for stiff hard materials.

Since digging action depends upon bucket weight, the grapple dredge does not have sufficient penetration to obtain a "full bite", or full load in hard materials. Dredging depth is restricted only by the length of the hoisting wire. However, deeper dredging will result in lower production due to increased hoisting time. Dredging depths of 100 feet are not uncommon.

## Dipper Dredge

Dipper Dredges - The dipper dredge is a power shovel or backhoe operating from the forward end of a barge. Like its land counterpart, the dipper dredge has good crowding action, making it suitable for handling large rocks, and casting them into nearby barges for removal. To obtain stability, spuds anchor the dredge when excavating. It is most effective in hard materials such as till, soft and broken rock, and shales, but also works well in areas where obstructions such as boulders, snags or timbers exist.

Located on the hull are two forward spuds and one stern or kicking spud, similar to those on grab dredges. The two forward spuds are used to lift the barge above its normal flotation and thereby obtain additional weight for

absorbing the reactions of the digging operation. The kicking spud is used to move the dredge forward. Digging depth is limited by the length of the boom, 65 feet being about the maximum.

Both the grapple dredge and the dipper dredge are unsuitable for offshore operations. The grapple dredge is unproductive in large tonnage and deep water deposits, while the dipper dredge has mechanical limitations and limited digging depth.

### **Bucket Dredge**

These dredges excavate with a continuous chain of buckets supported on an inclined ladder that moves up and down around two pivots called tumblers. As the buckets go around the lower tumbler, they scoop up the material, carry it up the ladder, finally dumping it into an ore chute as the buckets pass over the upper tumbler. The continuous action at the bucket chain provides good production and efficient operations. The bucket dredge is extensively used for sand and gravel deposits, and diamond and heavy metal (tin) deposits.

One of the disadvantages of this dredge is that it has to be moored with five or more lines and anchors. These moorings hinder traffic, and moving and resetting the dredge is time-consuming. Not only does this dredge have poor mobility as a result of the moorings, but it is not stable when being towed, principally because of the high center of gravity caused by the ladder, A-frame, and buckets. A second disadvantage is that it is not a rough-weather dredge. In active water the material washes out of the buckets. Waves of three feet or more make it non-productive, although recent design has improved this condition.

#### 4.3.2 Hydraulic Dredges

Hydraulic dredges can be classified into two main types - cutter head and suction head - based on the "head" attachment at the end of the suction pipe. For offshore marine applications, both types of hydraulic dredges consist of ocean-worthy self-propelled vessels on which a large centrifugal pump and suction pipes are mounted. The centrifugal pump draws a mixture of water

and suspended solids from the sea bottom, which is pumped as a slurry to on-board hoppers, nearby barges, or into slurry pipelines. Loose material can be drawn into the suction head with a plain hydraulic suction head. Hard materials require a cutter head to dislodge and direct material into the suction head.

## Plain-Suction Dredges

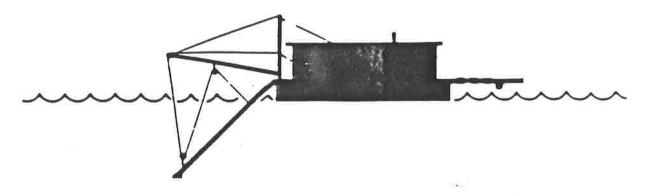
Plain-suction dredges are similar in hull construction to a regular ship, but they often differ from other dredges in the location of the suction pipe. The plain-suction dredge often has its suction pipe in a well at the bow, whereas other types have their suction pipes alongside. The suction pipe, regardless of its location, extends through the hull to the dredge pump.

For compacted material, the plain-suction dredge often has water jets installed at the lower end of the suction. High-pressure water is forced through the jets to break up the material. The suction end is also often flattened in a rectangular shape, similar to the mouthpiece of a vacuum cleaner, with the jets attached around the perimeter.

The dredge pump creates a pressure drop resulting in the movement of water and solids material into the suction pipe head. The dredge pump pushes the slurry along the discharge pipe to on-board hoppers or barges moored alongside the barge. Technology for dredge pumps is advanced, with special alloy castings available for pumping abrasive material. Most dredge pumps cannot lift slurry much more than 7 meters above the ocean level. To increase lift, pumps are mounted on the suction pipe boom below water level; however, motors must also be of the submersible type or extended power transmission shafts constructed. Economics is a prime determinate in design of dredge pumping systems. Dredge technology is well advanced.

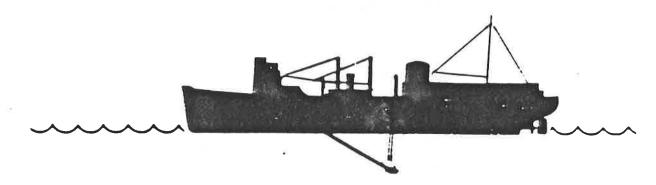
Figure 4.2 illustrates three types of hydraulic dredges.

The plain suction dredge shown is commonly employed for civil works excavation in and around harbors and marine facilities. Owing to the design



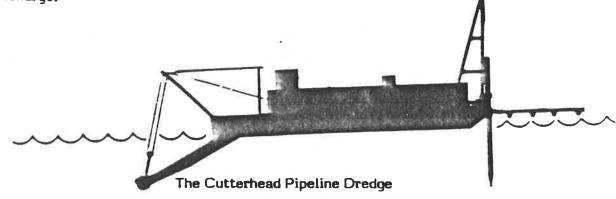
### The Plain Suction Dredge

In this type of dredge, a suction pipe is lowered to the surface to be worked. A powerful dredge pump draws up the material, mixed with water, and discharges through a pipeline. Units of this type are used for digging soft, free-flowing materials.



# The Self-Propelled Hopper Dredge

Resembling an ocean-going ship, this vessel functions in a way similar to a plain suction dredge. Material is gathered from the bottom by dragged suction heads, then pumped into storage hoppers. When filled, the dredge proceeds to a deep-water dumping area, where the hopper doors in its hull bottom are used d for rapid discharge.



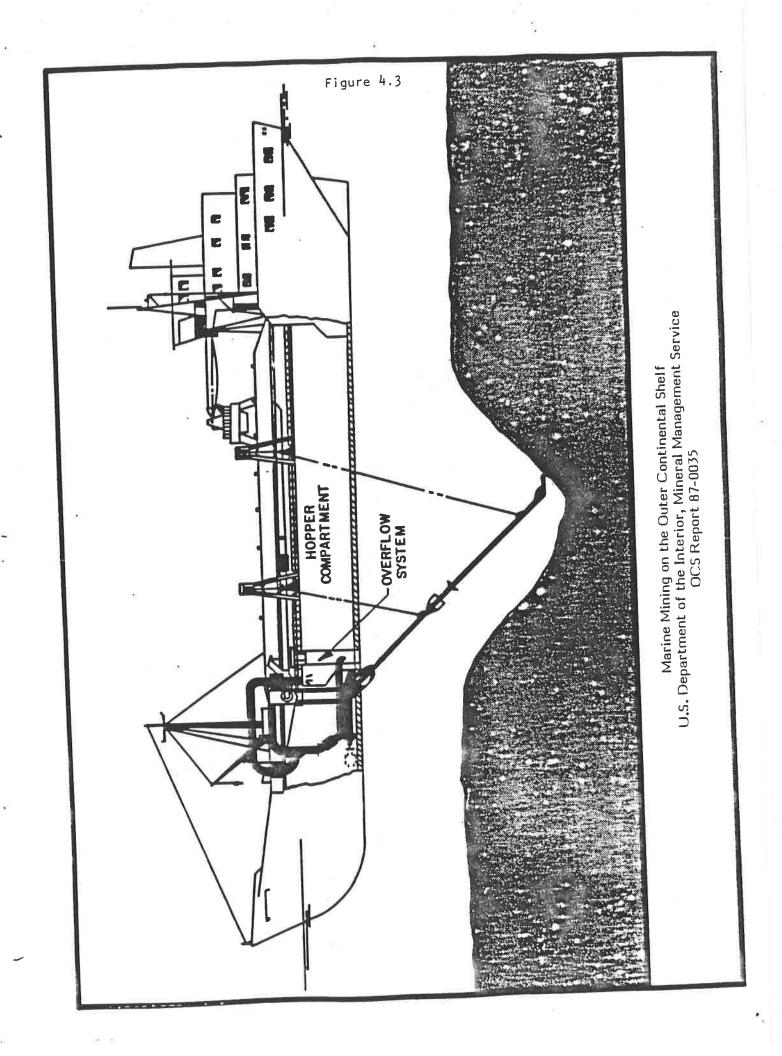
The most versatile and widely used excavating unit for transporting waterbound solids. A rotating cutter loosens the material, which is then sucked through the dredging pump, discharged via a pipeline at the stern. These dredges can dig and pump all types of alluvial materials, also, clay, hardpan and other compacted deposits.

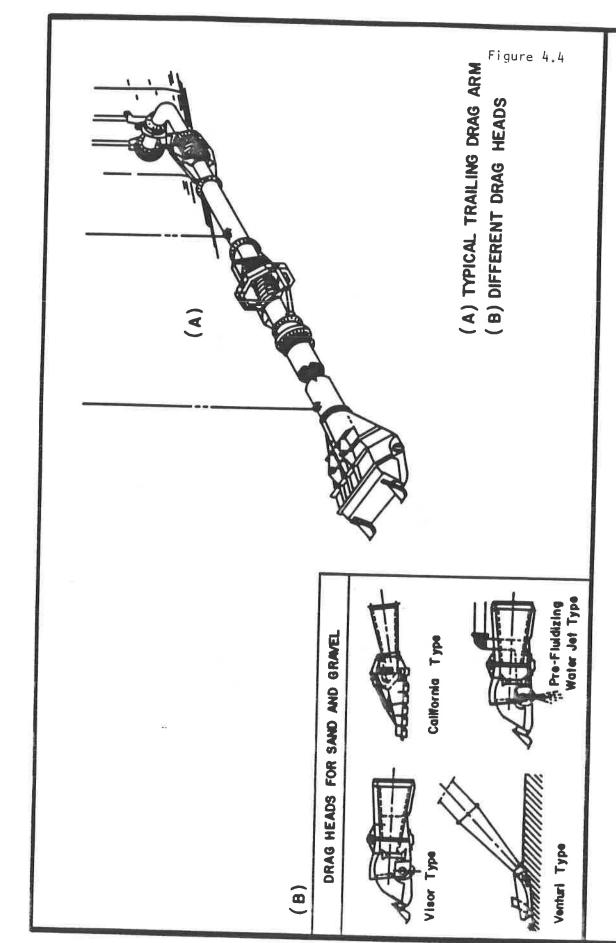
of the hull, which is often a single barge-shaped pontoon, this type suction dredge is not suitable for operating in the offshore ocean environment. The hull is not seaworthy enough to permit safe operation. This dredge may be self-propelled, but is more often towed and positioned by tugboats. The depth capability of this dredge is limited to the net positive suction head available at the dredge pump mounted on the deck, usually 5-8 meters. Depth is theoretically unlimited when the pump is submerged. Submergence is limited by design considerations, such as size of structural components, and the floating platform. Capacity is dictated by pump size, and power available.

The self-propelled hopper dredge is also known as the trailing suction head dredge.

This dredge operates while the vessel is underway, moving forward at about 1-3 knots. As the name indicates, the suction pipe trails behind the vessel dragging along the sea bottom. Figure 4.3 illustrates this type of dredge. Because dredging takes place as the vessel is underway, a deep excavation such as that illustrated is not typical. This shape and depth excavation would result from a fixed position with the vessel anchored.

Specially designed heads, depending upon the material being dredged, are mounted on the pipe and are referred to as dragheads. Figure 4.4 illustrates a typical trailing drag arm and several types of drag heads. For certain applications, a submerged dredge pump is added to the drag arm to increase effective depth and capacity. Dragheads can normally be adjusted and generally cut a path 1 meter wide by 1/3 meter deep. The resulting cuts are numerous shallow trenches in the sea bottom. Mining control is limited with the trailing suction head dredge. The dredged material is pumped into a hopper onboard the vessel, dewatered, washed and screened, then transported to shore when the hopper is full. When material is washed, waste material can be discharged through a pipe/pumping system to the bottom of the ocean, thus avoiding turbulence. The rejected sands partially settle in the mined trenches.





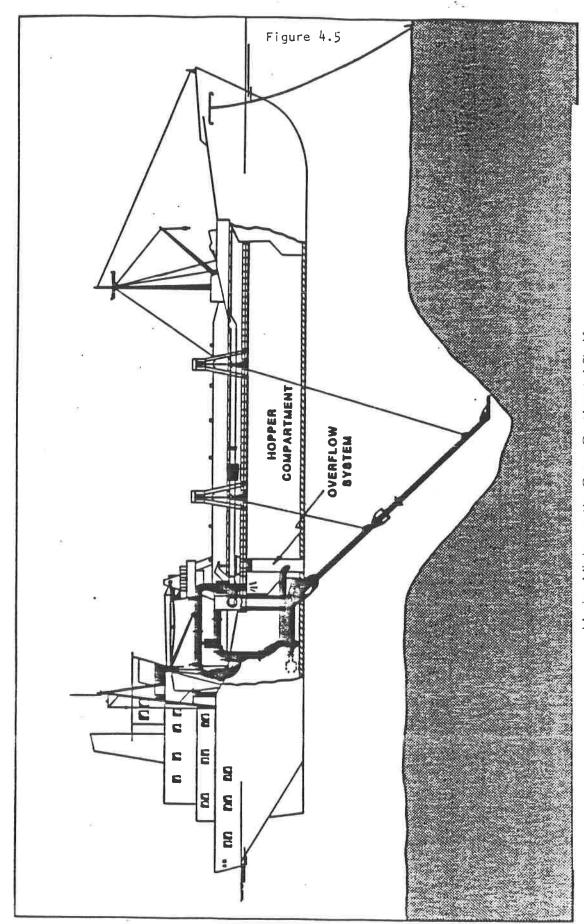
Marine Mining on the Outer Continental Shelf U.S. Department of the Interior, Mineral Management Service OCS Report 87-0035

Trailing suction head dredges are common in channel dredging operations. An example is the DCI Dredge IX built by IHC Holland for the Dredging Corporation of India. This is the fifth trailing suction head dredge bought by this company. The primary function of this dredge is to maintain shipping channels and approaches to several ports. The DCI Dredge IX is a twin-screw trailing suction dredger with a hopper capacity of 4,500 m<sup>3</sup>. Two 800 mm diameter suction pipes are capable of dredging to a depth of 25 meters. The DCI Dredge IX is equipped with an automatic light mixture installation which ensures that only a mixture with a predetermined solids concentration goes into the hopper. The hopper can be filled in about 40 minutes. Spoil is discharged through 18 conical valves arranged in two rows in the bottom of the hopper. Air conditioned living quarters for the crew of 50 men are built in the rear of the vessel. Complete instrumentation allows the dredge master to optimize the entire hopper charging process. Overall length is 102 meters, with an 18 meter beam. Power is provided by two 1070 kW electric motors operated from the two main 3850 kW propulsion engines.

Another use for trailing suction head dredges is in mining of aggregates off shore in the United Kingdom (U.K.). Twenty million tons of aggregate are mined by trailing suction head dredges in the U.K. The trailing suction dredge is an efficient mining tool and has the ability to operate under almost all conditions in the rough North Sea waters. An example, the Arco Avon has a submersible dredge pump installed in the trailing-suction pipe.

This enables the Arco Avon to dredge approximately 43 meters deep. The 1,000 kW centrifugal pump has a suction mouth diameter of 700 mm and is capable of pumping sand/gravel at a rate of 2,000 tons/hour. An automatic swell compensator raises and lowers the suction pipe so dredging can continue in sea conditions of up to 6 m swells. The vessel is is 98 meters with length, with a 17 meter beam.

Anchored suction head dredges operate much the same as trailing suction head dredges except that dredges are anchored to a location and angular movement is restrained by those anchors. Figure 4.5 illustrates the configuration of a sea-going anchor-type suction head hopper dredge operating at anchor. The suction head is held in one location longer so pits



Marine Mining on the Outer Continental Shelf U.S. Department of the Interior, Mineral Management Service

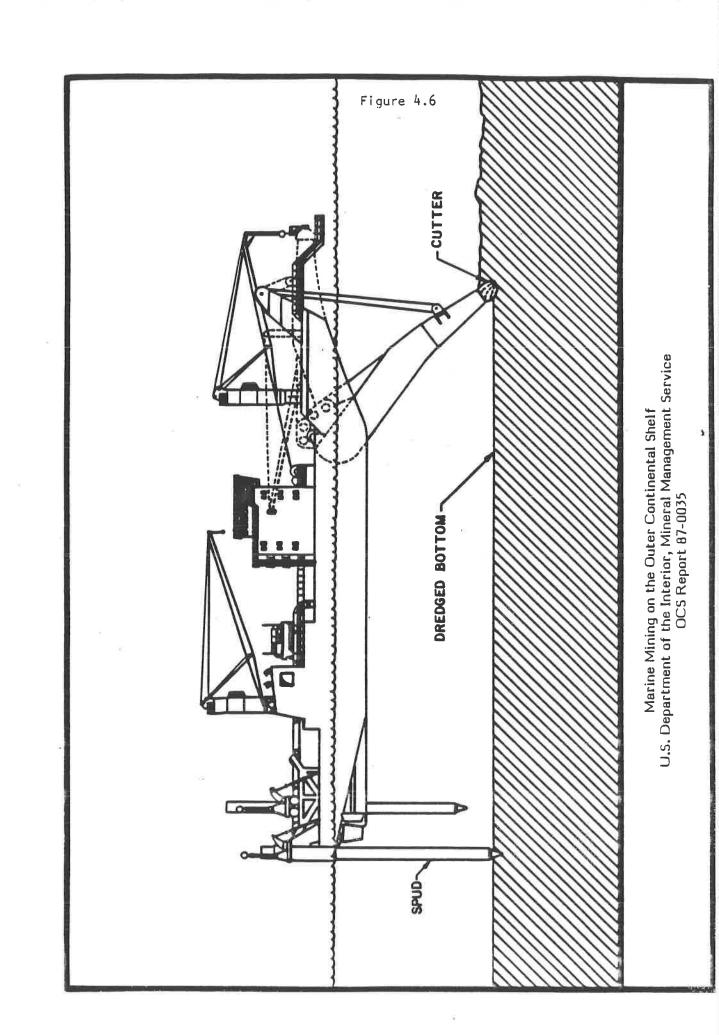
are dug instead of trenches. The dredge can mine panels about 80 meters wide and 1000 meters long in about 60 meter blocks.

As the desired depth is reached for the panel, the anchor is pulled and the dredge relocated to the next block. The mining process is repeated for each new block. Since the suction head is dragged over the bottom only by the swing motion of the dredge, it has less digging capability than the trailing suction head dredge. Operation of this dredge often requires the use of a separate tug to remove, re-position, and re-set the anchors.

Anchored suction dredges are used in Japan for aggregate mining, usually at depths of around 30 meters. In Europe, these dredges have been used, but in recent years all mining dredges operating offshore the United Kingdom and the European coast have been of the trailing suction head design.

## Cutter Head Dredges

The cutter head dredge is essentially a combination of other dredges, adapted so that material is excavated mechanically and transported hydraulically to another location. The cutters are mounted near the suction intake of the dredge pump and attached to the bottom of a ladder which, in turn, is attached at the bow of the vessel. Cutters are connected by a shaft to the cutter motor. Rotation of the cutter agitates loose material and cuts hard material. Cut material is directed to the suction intake through the motion of the cutter and the design of the suction intake pipe. Material is pumped aboard the vessel and handled in the same manner as the plain suction head dredges. A typical cutter head hydraulic dredge is shown on Figure 4.6. This dredge utilizes a basket type radial cutter head. The blades of the cutter may be plain for semi-compacted material, or may be studded with replaceable teeth for harder material. Spuds are used to position the platform and to resist the reactive force of the cutter head.



In addition to the cutter head, the ladder carries the suction pipe, lubricating lines, motors and reduction gear. The aft, or upper end of the ladder, is supported by heavy trunions set in a well in the bow of the dredge hull. The dredge is held in position by spuds. Movement of the cutter head is from side to side over an arc angle of 90°-100°, and is controlled by winching anchored swing lines attached to winch drums on board the vessel.

The A-frame is the main support for the block-and-tackle that supports the ladder. It is usually pinned to the forward end of the dredge hull rather than being fixed rigidly. This arrangement allows for movement while the dredge is operating. It is tied back to an H-frame by flexible wires or steel rods. Angular rotation of the vessel about a spud permits the dredge platform and attached ladder to advance, thereby forming a mining pit.

A cutter head dredge which utilizes a bucket wheel to excavate material is shown on Figure 4.7. This dredge is essentially the same as the basket cutter head dredge. The cutting wheel is designed for the material to be excavated, with or without teeth, and directs the excavated material to a suction pipe. The ladder, or boom, supports the bucket wheel, bucket wheel motor, suction pipe and, if required by depth and capacity, a submerged dredge pump and submersible motor. In recent years many of these type dredges have been built for high capacity or difficult digging conditions. This type dredge has also been adopted to sea-going vessels for mining in offshore ocean conditions.

Cutter head dredges of both types have been used extensively for mining onshore, including heavy minerals and phosphorite and are, in recent years, being extensively adopted to offshore ocean dredging applications.

#### 4.4 CURRENTLY AVAILABLE MINERAL DREDGING SYSTEMS

There are many examples of modern dredging applications, many of which are for the purpose of mineral recovery. Table 4-1 lists some of the more important mining dredges world-wide, with statistics of interest. Examples of each type; bucket ladder dredge, cutter suction dredge, bucket wheel dredge.

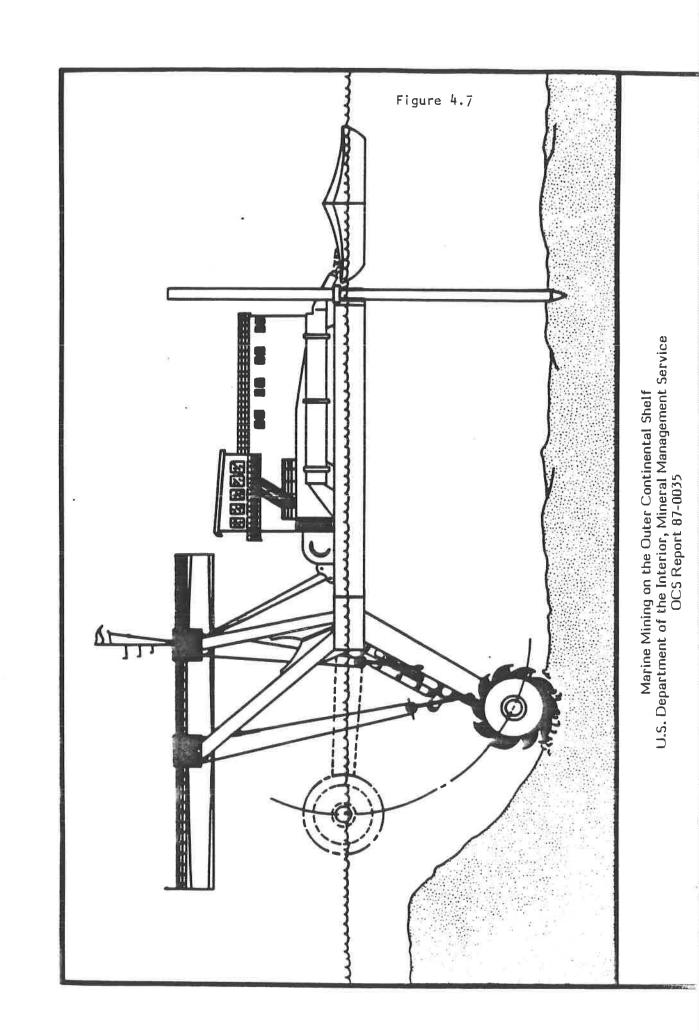


Table 4-1 Commercially Available Mineral Dredging Systems

Cutter Suction Dredges (contd)  Ellicott Machinery Corp.  1600 Bush Street Baltimore, Maryland 21230 USA HP HOlland P.O. Box 3, 3360 AA Sleidrecht Holland International Inc. 1600 Bush Street Baltimore, Maryland 21230 USA Humphreys Mineral Industries, Inc. 2219 Market Street Denver, Colorado 80205 USA IHC Holland Holland P.O. Box 3, 3360 AA Sleidrecht Humphreys Mineral Industries, Inc. 2219 Market Street Denver, Colorado 80205 USA IHC Holland P.O. Box 3, 3360 AA Sleidrecht Holland P.O. Box 3, 3360 AA Sleidrecht Holland P.O. Box 3, 3360 AA Sleidrecht Holland P.O. Box 3, 2000 mm Wheel, 18.6 rpm Wheel, 18.6 rpm Holland P.O. Box 3, 3360 AA Sleidrecht Achon Operatein & Koppell AG Series 200-300 Series 200-300 Conenstein & Koppell AG Series 200-300 Conenstein & Conenstein & Conenstein & Conenstein & Conenstein & Conenstein & Conenst	Description of Dredge	Ore	Depth T	Throughput M3/ Month (600 Hrs)
rp. 21230 USA leidrecht 1230 USA lustries, Inc. 15 USA eidrecht td. 3				
leidrecht  Pr. 1230 USA lustries, Inc. 15 USA eidrecht td.		Various	02-9	22,800- 1,101,000
p. 1230 USA lustries, Inc. 15 USA eidrecht d.		NS NS	S	SZ
P. 1230 USA lustries, Inc. 15 USA eidrecht td.				
lustries, Inc.  J5 USA eidrecht td.  alia	_	Various 8	8-21 plus	45,600- 1,836,000
eidrecht td. alia		Ba/Sn/Au	30	s Z
td. Series 200-300 200-450 mm suction. 35% s alia  UWS 250, 5,000 mm wheel. 250 liter buckets 380 KW	el class. 2,200 mm NS 6 rpm 1 suction 750-4,000 KW	2	10-16	S Z
CG UWS 250, 5,000 mm wheel. 250 liter buckets 380 KW	000 n suction. 35% solids	S	6-15	to 200,000
	$000 \text{ mm}$ wheel. $10 \times \text{NS}$ uckets $380 \text{ KW}$	S	SZ	NS
wheel, submerged pump, 2,400 KW	planned) 8,000 mm Sn merged pump,	c	100	1,350,000

Manufacturer	Description of Dredge	Ore	Depth Meters	Throughput M3/ Month (600 Hrs)
Deep Water Dredges				
Alluvial Mining and Shaft Sinking	AMROD 305 mm discharge,	Au/diam/Ti	to 300	200,000
Co. High Pavement, Basildon Essex 5514 IEA, England	submerged centrifugal DOD series, 150 mm suction and jet. Diver operated.	NS	200-300	SN
Fuchs Systems Inc.	Air lift	NS	15-120	160,000-180,000
P.O. Box 379 Salisbury, N.C. 28144, U.S.A.		397		
OCP Group - FW Payne (UK) Ltd. 34 Southborough Rd., Bickley Bromley Kent BRI 2EB, England	Remote control underwater suction	Various	50-150	SZ .
Orenstein & Koppell AG Karl Funke Strasse 30 D-4600, Dortmund, FRG	Multiple head collector 30 m wide Submerged suction with vibrator and jetting	Mn nodules Red Sea muds	6,000 m 3,000 m	NS NS
Orenstein & Koppell "Draga D-9"	Split hopper suction dredger 2-700 mm suction dredge pump 1200 hp each.	SZ	28 m	1,480,000

NS = Not specified

#### 4.5 BOREHOLE MINING

During the past several years there has been a considerable amount of interest in the United States and Canada on the extraction of minerals through a borehole from deeper sedimentary deposits. Several private companies evaluated borehole mining methods for mining deep phosphate rock in North Carolina back in the 1960's, as well as other locations. The concept of mining through a borehole is obviously not novel as Frasch sulfur has been mined commercially through a borehole since the 1890's. The extraction of slurried minerals through a borehole, however, has not achieved any significant commercial success.

In 1973, the United States Bureau of Mines (USBM) took an active interest in the development of this technology as part of their program to increase the domestic availability of critical minerals. In 1976, they developed a tool specifically designed to mine coal, that was built by Flow Industries Inc. (Flow). This early work indicated that coal could be slurried in place by high pressure water and transported by use of an eductor pump. Experimental test work was also conducted in the slurry mining of California oil sands by the USBM.

Emphasis at the USBM then shifted to adapt the concept to the mining of uranium ore-bearing sandstone in Wyoming. The initial tests were conducted during 1977 in conjunction with Rocky Mountain Energy Co. (RME). The result of these tests encouraged RME to develop a prototype system with Flow which was operated over a several month period. The test results indicated that uranium bearing sandstone could be eroded with high pressure water at a standoff distance in excess of 70 feet when the nozzle was operated in an air environment. A satisfactory production rate was achieved when the operating conditions were optimized. They were able to elevate the slurried sandstone with the eductor pump from the air-filled cavity at a depth in excess of 200 feet. The energy required to elevate this slurry by this method was high. Unfortunately, at about that time, the price of uranium dropped dramatically, causing RME to discontinue their program prematurely. At about the same time this test work was being conducted, the USBM became interested in re-evaluating the technology as it could be applied to phosphates.

In 1980 a test program was conducted at a northeast Florida site using the USBM equipment developed for coal and uranium sands. The test results indicated that in that particular environment, borehole mining had to be conducted in a flooded cavity to maintain roof support. It was encouraging to determine that even when operated in a flooded condition, a surprisingly good production rate could be achieved, and that a radius approaching 20 feet was obtainable. When the system was operated with the cavity filled with water to the top of the casing, the energy required to lift the slurry created by the cutting jet action by the eductor pump was considerably less than in earlier tests.

Encouraged by these results, a joint venture research program between Agrico and International Minerals and Chemical Company was established to conduct a new test program. The actual borehole test work was conducted in late 1984.

The results of this test program were encouraging. In all cases, a consistent hole radius of approximately 20 feet was obtained. No subsidence occurred as all the cavities were developed in a flooded environment with a positive casing overflow. The production rates were adequate for the cutting jet flow rates available, and it was apparent that with increased cutting jet nozzle flow rates, and with a system specifically designed for that site, production rates could be substantially improved. In early 1985 most of the waste clay (a major environmental and disposal storage problem in the central Florida strip mines) was successfully thickened and re-injected back into the cavities created by extraction. The drilled holes (16 inches in diameter) were plugged after backfilling and the casings removed. By removing the steel casings (PVC also used and pulled) and repeatedly recycling them, the economics of borehole extraction are decidedly more attractive.

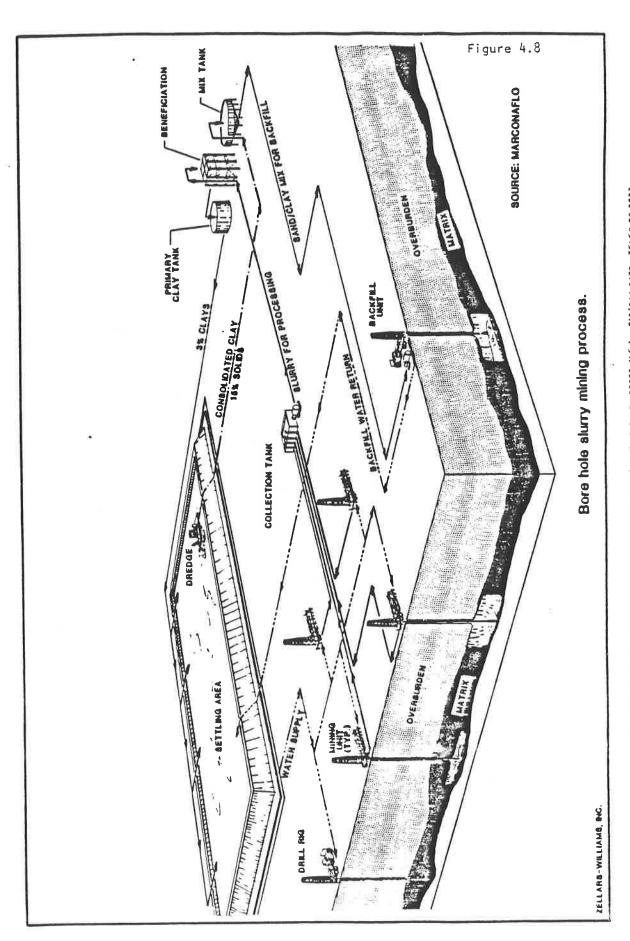
Upon the completion of the test program, an overall conceptual analysis was made to determine how the above results could be converted into a practical commercial development. A mining plan was conceived indicating that a multi-unit system with a portable centralized distribution and receiving unit was the most likely approach. Economic projections made, based on this

plan, were encouraging. These projections indicated that land based, large, previously unmineable resources had the potential of being a cost effective, environmentally acceptable, long-term phosphate rock supply.

The basis of the design would be a system having a high operating factor with a minimum mobilization time between pre-drilled boreholes. The mining concept calls for a separation of the four unit functions deemed necessary to mine phosphate rock at that site. The extraction unit's only function is to mine; the other three functions - drilling and casing, backfilling, hole plugging and casing pulling - would be conducted separately.

A land-side borehole slurry mining process would use a 12-inch to 16-inch diameter cased borehole drilled to the matrix and uncased through the ore zone. Figure 4.8 is an illustration of a conceptual arrangement for borehole mining in north Florida. Because of the depth to the base of the orebody (occasionally over 200 feet), a multi-stage turbine pump is required to lift the ore slurry back to the surface. The ore is slurried by a high pressure (275 psi) water jet making an arc of 270° to 360°. This jetting action creates a cavity approximately 50 feet in diameter at a height determined by the matrix thickness in each hole. Due to the limited size of down-hole equipment, some 20 mining units are necessary to produce 2.5 million tons per year of product. This quantity is based on a 60 percent matrix recovery with each slurry unit producing the equivalent of 50 product tons per hour in recovered ore.

Dedicated mining units produce matrix to a centralized delivery system for transport to the plant. A separate drilling and casing unit is advancing in front of each of the three groups. When a unit finishes mining, a four-hour move is required to set up the next hole in the series. Behind each group is a backfilling unit, placing a mixture of tailings and consolidated clays into the finished boreholes. The 18 to 20 percent solids clay material is dredged from a single 500-acre settling pond that could possibly be used throughout the life of the project. This type of waste disposal may create permitting problems because of the material being placed into an aquifer. But, this type of procedure using sand tailings from the mill, is presently being evaluated as an alternative means of preventing subsidence problems at the surface.



ZEILARS : WILLIAMS INC. 4222 SOUTH FLORIDA AVENUE LAKELAND FLORIDA 33803, U.S.A.: 813/844 8478 · TELEK 92 2532

A typical mining equipment scheme provides 932 tonnes per hour of matrix in a 20% solids slurry to the beneficiation plant.

Some of the positive features that a land-based borehole extraction system would offer industry are partially listed as follows:

- o Low capital cost per unit of material moved.
- No surface disturbance. Surface can be utilized for practically any use immediately after mining.
- o Waste material resulting from mining and mineral processing can be disposed of back into the mined-out cavity.
- o Small, erratic, or highly faulted deposits can be selectively mined with a minimum of surface infrastructure required.
- o Development drilling necessary to delineate an orebody to justify open pit mining could be reduced when borehole mining is considered. The definition of "proven ore" would take on a different meaning.
- Only the material that needs to be moved for subsequent processing has to be handled.
- o The system would be very adaptable for automated operation.
- o The concept appears to be environmentally acceptable. It allows potential development of valuable commodities that could not be mined by conventional methods.
- o Borehole extraction could have many other uses besides mining. Any time it would be desirable to create an artificial cavity within a favorable horizon for waste disposal, storage of recoverable material, well field regeneration, etc., through a restricted orifice, this concept should be considered.

The Georgia offshore area of interest between the 3-mile territorial sea line, and the 50-meter contour, indicates some phosphorite occurrence at depths which might fit the borehole mining concept. These areas appear to occur as pockets of what might be phosphate-rich, deep Middle Miocene. Little or nothing is known or available at this time to warrant consideration of borehole mining to Georgia offshore phosphates. The discussion above is given only to acquaint the reader with the general state-of-the-art as it may

apply to phosphate mining. Development Planning and Research Associates, Inc., (DPRA) 1987, in their offshore North Carolina phosphate feasibility report, describe a conceptual system for borehole mining a phosphate resource. The 20-meter thick phosphate zone proposed for borehole mining is in 30 meters of water, under 50 meters of overburden, and is centered on an exploratory borehole about 60 kilometers east of Cape Fear. This kind of investigation and work is beyond the scope of this study.

### 4.6 APPLICABILITY OF EXISTING TECHNOLOGY

For a continuous mining operation offshore Georgia, only two types of dredges are feasible - the trailing or anchored suction head dredge, and the cutter head dredge. These dredges can be built on ocean-going vessels with large receiving hoppers and washing plants to reduce the volume of material transported. These dredges can also be integrated into transportation systems utilizing slurry pipelines, barges, or a self-contained load/unload hopper-dredge.

The principal problem with the cutter wheel and bucket line dredges is that being digging dredges they require heavy mechanical equipment and supporting steel structures, resulting in a high bottom contact pressure by design. However, being digging dredges by design, they will dig in response to hull movements making it difficult to maintain permanent contact with the dredging face. Oceanic conditions such as waves, swell currents, and wind causes the dredge hull to surge, heave, pitch, roll, sway and yaw in relation to the ocean bottom. This movement prevents contact with ocean bottom and stresses mechanical and structural components.

Solutions to this problem have been advanced, one of which is to build a semi-submersible hull configuration instead of a surface pontoon. Analysis of response curves for waves striking the hull at 1350 (considered the most severe angle) indicates a vast improvement in pitch and heave with the semi-submersible hull design. Solutions to this problem appear to be within the state-of-the-art technology and one dredge operating in moderate oceanic conditions has been built to mine tin in Thailand using a large cutter head dredge. A spud is used to keep the dredge on station balance by shock

absorbers which were built into the ladder suspension and swing wires. While not really flexible, this mechanical innovation prevents undue shock loading of critical mechanical components. Further testing and investigation would be necessary to apply this technology to offshore Georgia coastal conditions. Currently, work is being done to create a truly flexible dredge by using a rigid bucket ladder with the supporting pivot shaft connected to the pontoon by link bars and hydro-pneumatic cylinders. Movement in relation to the pontoons is permitted by the pivot shift. In addition, the support bracket is supported by a buffer cylinder which permits the bow to move vertically and keeps the digging force on the bottom by adjusting the pressure on the cylinders.

The trailing suction head dredge, equipped with a draghead, has a low bottom contact pressure and does not sink into the bottom, but maintains contact with the bottom despite dredge hull movements. Because of low weight, the trailing suction head dredge can be equipped with a universal hinge, a horizontal hinge, sliding and turning glands and swell compensation buffer gear. This keeps the draghead on the bottom at constant pressure while the bow moves up and down.

The principal disadvantage of the seagoing trailing suction head dredge is that excavation of material at sea bottom generally occurs while the host vessel is travelling at 1-3 knots. The suction head is dragged along the bottom and the depth of cut depends on the effective contact weight and the consolidation of the material. The suction drag head can not remove (cut) more than a few feet with each pass. The width of the cut is limited by the size of the drag head and the angle of repose of the material being excavated. A single pass may make a cut 1 to 2 meters deep and 5 to 8 meters wide in free-flowing sands and gravels. Many passes are required to mine any significant depth.

The seagoing trailing suction drag head dredge is most effective when operated from a vessel which contains compartments for storing dredged material. Dredged material is deposited directly in the on-board integral hopper either directly or after mechanical sizing to reject oversize material. The dredge hopper vessel, with or without on-board processing, is designed to

remain at sea long enough to fill its hoppers. The vessel, when loaded to capacity, returns from the mine site to a designated land-side dump where the hopper is unloaded. Some vessels are designed to bottom dump hopper contents, while others transfer material from the hopper by self-contained slurry pumps, Marcona-flow, or by other conventional methods.

One version of the seagoing suction drag head dredge is the anchor dredger. The seagoing vessel is similarly equipped with a suction head and hopper. This dredge works at anchor and does not move while dredging, other than periodically to winch itself forward as required to keep the flow of material feeding into the suction pipe head. This type of dredge has the advantage that it can work in a deep deposit and covers very little area of the sea bed. The disadvantage is that the sea bottom is left with a series of holes.

The seagoing suction dredge, whether of the anchor type or trailing suction type, is suitable for mining loosely compacted surficial sands containing heavy minerals which do not require removal of overburden.

A system which can operate safely in the offshore Atlantic Ocean coastal water environment is the first requirement which must be met by any equipment assemblage. For the mining of phosphorite, an equally important requirement is that the system be capable of engaging the total horizon of material to be excavated and to do so with an acceptable level of recovery. In other words, overburden and matrix each should be excavated in a single pass, while leaving a minimum of ore having value behind and/or diluting at a minimum the desired ore with barren material. Additional characteristics of the system must be: high level of reliability, and ease of maintenance and component replacement; ability to partially upgrade ore onboard; ability to efficiently transfer or transport upgraded ore to a nearby moored vessel or barge, or to a centrally located offshore beneficiation plant; capable of quickly suspending operation, riding out sudden storms, and quickly resuming work.

The selected systems for mining offshore Georgia phosphorites and heavy minerals are described in Sections 5 and 6, respectively, of this report.

+					
40 14					
	*				
	*1				
			25		
				7.5	
					, e
	j.				

#### **SECTION 5**

#### PHOSPHATE DEVELOPMENT FEASIBILITY

### 5.1 INTRODUCTION

This section deals with the work leading to the selection of a preferred configuration for mine, beneficiation, and related infrastructure components required for the commercial exploitation of Middle Miocene phosphorite occurrences offshore the coast of Georgia in the Atlantic Ocean. The reader is taken through a description of the proposed mining area and a comparison of production-configuration schemes. This comparison is based on information and data developed and published in previous studies. Much of this comparative work relies on reports of the Bureau of Mines and Minerals Management Service of the U.S. Department of Interior, Zellars-Williams Company, and Development Planning and Research Associates, Inc.

The configuration selected as a result of the comparative study is that of hybrid dredges mining to an offshore beneficiation facility from which finished product is shipped.

Each component is fully described and capital and operating costs estimated. Economics and viability are based on current phosphate rock sales prices and on supply-demand projections, which indicate the year 2000 as the time-frame in which realization of this enterprise may become viable.

Dredge design and excavating-pumping rate expectations, which underly the premises of the proposed annual production of 4.8 million tonnes of phosphate rock, assume that coquina or similar cemented conglomerates do not occur in the overburden or ore zone horizons scheduled for mining. A phosphate mining enterprise at Santo Domingo on the west coast of Baja Sur California, Mexico, failed to enter production after expenditures of about 60 million dollars because the overburden and ore zones were improperly characterized as uniform beach sands. This soils classification came about as a result of drilling and sampling techniques which failed to characterize in-situ coquina.

The coquina turned out to be impenetrable by the dredges designed and built for this project. Coquina lenses reportedly occur frequently enough to create problems for Texasgulf in mining the marine deposits at their Lee Creek, N.C. mine.

This experience adds emphasis to the importance of a properly designed and executed exploration program for offshore minerals.

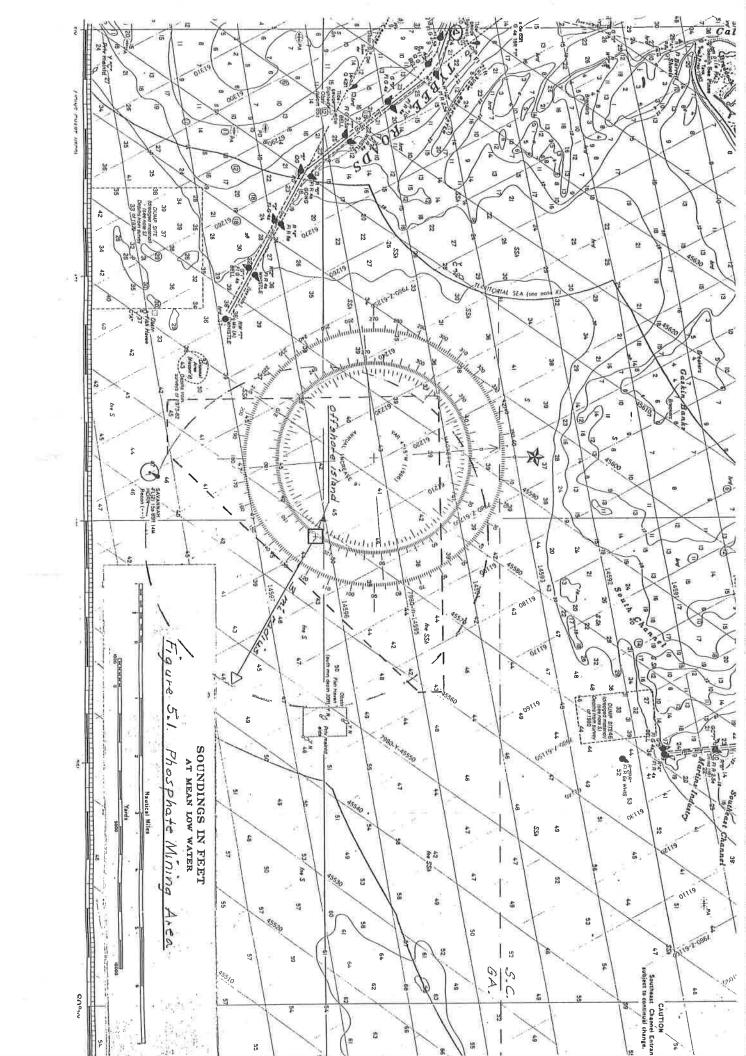
### 5.2 MINING

## 5.2.1 Selection of Mining Area

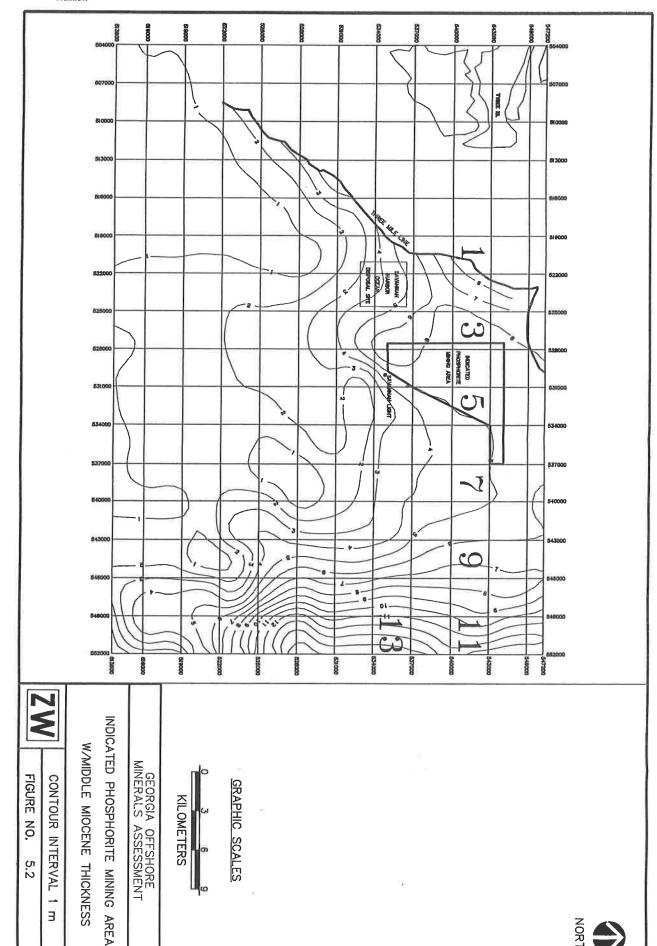
Figure 5.1 shows the area under consideration for phosphate mining. This location contains the thinnest overburden and shallowest phosphate in the study area. Due to the seaward slope of the Miocene sediments, as well as increasing water depths, areas seaward of the model area are increasingly difficult to mine by surface techniques. A more complete review of the model area and geology is given in Section 3.

The area modeled ranges from 6 to 25 nautical miles from shore. Figure 5.2 is a geologic map of this area containing about 180 3-kilometer square blocks. Twenty years of mining to yield 3-5 million tonnes of product per year covers a small fraction of the total blocks identifying Middle Miocene phosphorites. The number of blocks required depends upon the matrix thickness, which is taken as the Middle Miocene thickness. Since matrix thickness, overburden thickness, and depth of water are not constant in the model area, a methodology was developed to select the most favorable economic mining site.

Each block has an overburden thickness, a matrix thickness, and a water depth. The relative proportion of these determines dredge operating and capital costs. By examination of these data, 13 blocks were selected for economic evaluation. Table 5-1 lists the boundary limits of each selected block. These blocks were analyzed for dredge capital costs, and dredge operating costs. Zellars-Williams computerized dredge model was used to calculate production rates and costs. All plant costs are assumed to be location independent. An incremental waste disposal charge was added to the



5.2





capital and operating costs, when the mining depth exceeded 27 meters. The sum of dredge operating cost, dredge capital cost, and incremental waste disposal cost, expressed in dollars per tonne of product, was added to give the total cost. Results are summarized in Table 5-2 for each block.

Table 5-1
Block Coordinates

Blocks	Northing	Southing	Easting	Westing
1	543,000	540,000	522,000	519,000
2	543,000	540,000	525,000	522,000
3	543,000	540,000	528,000	525,000
4	543,000	540,000	531,000	528,000
5	543,000	540,000	534,000	531,000
6	543,000	540,000	537,000	534,000
7	543,000	540,000	540,000	537,000
8	543,000	540,000	543,000	540,000
9	543,000	540,000	546,000	543,000
10	543,000	540,000	549,000	546,000
11	543,000	540,000	552,000	549,000
12	540,000	537,000	552,000	549,000
13	537,000	534,000	552,000	549,000

Table 5-2

Mining Area Dredge Operating Costs

						Increm.	
				Total	Dredge	Waste	Total
	De	epth		Mine	Cost	Cost	Cost
Block	Ore	Ovbd.	Strip	Depth	\$/t	\$/t	\$/t
#	m	m	Ratio	m	Matrix	Matrix	<u>Matrix</u>
1	9.0	15.5	1.72	32.2	\$2.06	\$.06	\$2.12
2	7.2	12.0	1.67	30.0	1.88	.04	1.92
3	5.9	11.3	1.92	27.3	1.88	.04	1.92
4	5.6	8.5	1.52	26.3	1.66	.00	1.66
5	5.2	8.0	1.54	27.7	1.68	.01	1.69
6	4.6	7.5	1.63	28.3	1.93	.02	1.95
7	4.7	8.2	1.74	29.6	2.01	.03	2.04
8	5.3	8.7	1.64	32.0	2.18	.06	2.24
9	6.3	9.7	1.54	35.0	2.10	.09	2.19
10	8.1	11.3	1.40	39.0	2.14	.13	2.27
11	11.0	12.2	1.11	43.0	1.94	.17	2.11
12	12.0	12.0	1.00	43.5	1.84	.17	2.01
13	12.2	12.0	.98	44.2	1.83	.18	2.01

Note: Total mine depth includes water depth from MSL to sea floor (top of overburden) at each location.

Using the lowest total cost/tonne of matrix (ore) as the selection criteria, Blocks 4 and 5 were chosen as the core of the initial mining site. The size of the site was matched to an area required to support a 3.5 million tonne (product, dry) per year operation for twenty years. This area contains the shallowest Middle Miocene location, as well as the thinnest overburden in the entire model area.

The initial area is approximately triangular in shape, with the hypotenuse being the 5 meter Middle Miocene thickness contour on the southeastern side. The southwestern and northeastern corners are described as:

	AMS Coo	ordinates	Lat. and Long.
	_East_	North	
sw	527500	535000	80°42'32.45", 31°57'8.34"
NE	537000	544000	80036'29.34", 32001'59.68"

The site contains parts of the following OCS blocks: NI 17-11 - 951, 952, 953, 995, 996, and 997 NH 17-2 - 27 and 28

The site is characterized by the following in-situ parameters:

		Meters		Meters <sup>3</sup>
Item	Average	Min.	Max.	Volume
Water Depth	13.97	11.4	16.4	
Overburden	8.02	7.1	9.9	366,746,720
Matrix	5.44	5.0	7.0	249,040,020
Stripping Ratio (m:m)	1.47	1.42	1.41	,
Total Mining Depth	27.43	26.4	28.8	

All overburden material is sand material with no cementing. There is no Pliocene or Upper Miocene material present within the confines of the site.

Using the "Design Basis Data" from Table 10, page 54, of the 1979 ZW report, a target production rate of 3.5 million tonnes for 20 years, and the summarized site data listed below, an annualized production summary was prepared.

## Summarized Site Data

Total Matrix Volume (meters <sup>3</sup> )	249,040,020
Matrix "X" m <sup>3</sup> ore to produce 1 ton product	3.37
Percent Clay Waste	21.29
Total Product Tonnes (dry)	73,899,000
Total Area (meters <sup>2</sup> )	45,741,096
(acres)	11,303

The initial mining area described above includes parts of eight blocks having the most favorable mining characteristics and is the area targeted for earliest exploitation. The total mineable area, however includes at least eight additional blocks to permit increasing mine life and/or annual yield. Experience in early years will result in improved technology, increase the mineable area, and permit exploitation of as much as 500,000,000 m<sup>3</sup> of phosphorite matrix in the Middle Miocene. The product yield over the life of a single enterprise would be as much as 150,000,000 tonnes.

## 5.2.2 Configuration and Production Rate Comparison

The annual production of any mineral beneficiation facility is dependent upon the ability of the mine to supply ore. Normally, plant production is based on operational efficiency which is largely independent of mining because of the ease of providing large stockpiles of plant feed. Most phosphate rock production is based on a link between the mining dragline - ore transportation system and the plant washer. High operating factors are typical and ore storage is not a requirement. Operating factors for most ocean mining equipment, however, are low by comparison. Climatic and other conditions beyond the control of the operator are the major contributors to the reduced operating factor.

Production based on mining of ore at sea for beneficiation at a remotely located land-based facility is greatly dependent on the effective operating factors of the excavating and transporting equipment and systems employed.

As a basis for uniform comparison of alternative configuration schemes certain criteria were established. The criteria adopted for comparative evaluation given in Table 5-3 are based on previous work and on reported experience with ocean-going dredges and transportation systems. These criteria were later modified to better fit the preferred mining equipment and systems configuration.

Table 5-3
Criteria Basis for Configuration Comparison

Annual Mining Equipment Availability	
Days lost: annual dry dock/repairs	30
adverse weather/sea conditions	<u> 36</u>
Days operational	299
Hours/day operational	21
Mechanical availability Effective operating hours	90%
(299 × 21 × .90)	5,651

Item Description	Unit	Value
Average overburden thickness	meters	8.02
Average matrix (ore) thick.	meters	5.44
Matrix "X"	m <sup>3</sup> ore/l_tonne product	3.37
Matrix & overburden density	tonnes/m <sup>3</sup>	1.36
	lb/ft <sup>3</sup>	85
Mining recovery	percent	85
Stripping ratio	m <sup>3</sup> ; overburden/m <sup>3</sup> matrix	1.73
Suction head pipe or dredge		
pump discharge diameter	mm	900
inches	36	
Pipeline velocity	m/sec	4.92
	ft/sec	15.0
Dredge production dry solids	m <sup>3</sup> /yr	12,118,000
	tonnes/hr	2,196
Average slurry solids	percent	26
Washer rejects	percent	20
Distance to land-based beneficiation plant	nautical miles	27
Average vessel speed	knots	12

Typically, offshore dredges are ocean-going vessels equipped for mining and contain hoppers for collecting dredged material. Since these vessels also serve as transports, their availability for mining is limited. Investment is high and utilization for mining is low. This appears to be the norm as is experienced by operators who use these types of foreign-built dredges in the North Atlantic, Pacific Ocean and Sea of Japan. These systems are most effective where: there is little or no overburden; where the ratio of ore to product is low; and where concentration takes place on board. This is not the case for phosphate.

However, because sea-going suction head hopper type dredges have a long and successful history of operating under ocean conditions, they are considered here in evaluating alternative configuration schemes.

The four major project configuration schemes considered for offshore phosphorite production are:

- Sea-going hopper dredge for mining and transportation to an onshore plant.
- 2. Sea-going hopper dredge mining and barge transportation of ore to an onshore plant.
- 3. Dredge mining and pipeline transportation of ore to onshore plant.
- 4. Dredge mining and pipeline transportation of ore to nearby offshore island plant.

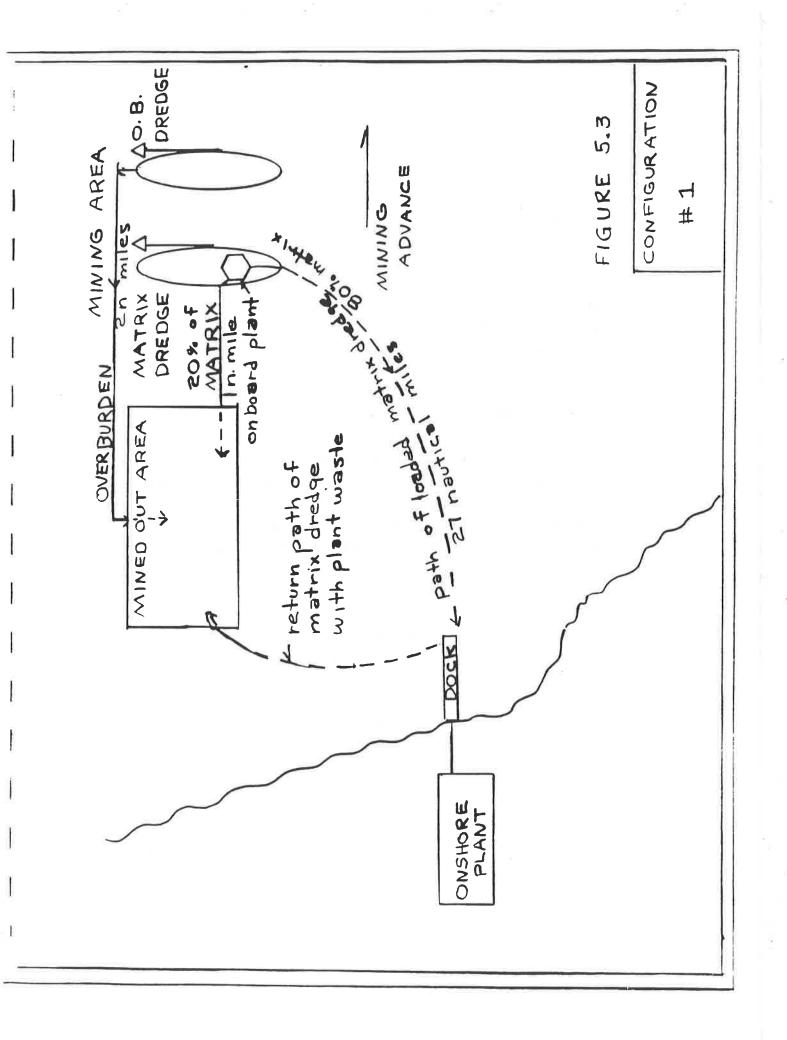
The mining dredge vessel or platform in each of the four major configurations is equipped with an onboard processing (washing) plant. Flowsheet data indicate that about 20% of the dredged material can be eliminated by washing. This reject material, a mixture of oversize and slimes, would be disposed of in nearby mined-out areas. In Configurations 1, 2, and 3, matrix is transported, after washing, to a land-based plant for further processing. The dredge vessel size is determined by the necessity of making the vessel seaworthy, not by the dredging equipment. In Configuration 1, a large hopper is required for storage as the dredge is also the vessel used to transport ore, after washing, to shore.

Since dredge vessel size is larger than required for the dredging equipment alone, the addition of a washing plant costs only slightly more than if located onshore. Plant operating costs are identical. However, with onboard processing, material transported to shore decreases by 20%, resulting in a corresponding reduction in transportation costs of 20%. In addition, waste disposal of the 20% fraction rejected by washing at an onshore plant must be either re-transported from the plant and disposed of in the mined-out areas, or disposed of in tailing impoundments onshore. Either way, the offshore washing plant reduces costs considerably by wasting the 20% fraction rejected in nearby mine areas.

For Configuration 4, costs are expected to be about equal, with or without onboard processing. This is because the processing plant is located near the mine area. Therefore, for Case 4, either onboard or offboard washing can apply.

# Sea-going hopper dredge for mining and transportation to an onshore plant.

Figure 5.3 shows this configuration. An anchor suction dredge removes overburden, pumping it to mined-out areas. One anchor suction dredge is dedicated to overburden removal. A second matrix dredge follows at least 2,000 feet behind the overburden dredge. The anchored suction head dredge slurries and pumps the ore to a distribution box, and then the ore is screened, washed and deslimed. About 80 percent of the material is loaded into a hopper on board the vessel. Here, through a series of weirs, the washed matrix is dewatered to 75% solids. When the hopper is full, the suction head and pipes are raised from the bottom to the deck. The dredge now functions as a normal merchant ship and carries the material 27 nautical miles to the plant site. The plant site was selected in an industrial area where permitting problems and land acquisition problems are minimized. It was felt that an onshore plant located closer to the mining operation on the barrier islands would be environmentally unacceptable.



Costs for hopper dredges were taken from the open file report "An Economic Reconnaissance of Selected Heavy Mineral Placer Deposits in the U.S. Exclusive Economic Zone" by the Bureau of Mines Washington Staff, released 4-87.

For a hopper dredge, cycle times consist of loading, travel, unloading and return travel. The hopper size increases capacity, but also increases capital. In an attempt to optimize hopper size, four loading capacities were analyzed. Table 5-3 shows the design criteria used to determine productivity and costs.

Loading and unloading is done by a 900 mm pump using the criteria in Table 5-3 at the rate of 2,916 tonnes per hour.

Table 5-4 shows the time required for each element in the cycle. The cycles per year are based upon 5,651 hours. The tonnes per cycle are based upon the loading time, which is different for each case. Table 5-4 also lists the tonnes per year of product produced for each capacity. As Table 5-4 shows, increases in loading times (hopper capacity) result in only a slight increase in tonnes per year of product.

Table 5-4
Cycle Time Configuration 1

Item	Hours	Hours	Hours	Hours
Load Ore	5.00	10.00	15.00	20.00
Travel to Plant	2.25	2.25	2.25	2.25
Unload Ore	5.00	10.00	15.00	20.00
Load Tails	5.00	10.00	15.00	20.00
Travel to Mine	2.25	2.25	2.25	2.25
Dump Tails	5.00	10.00	15.00	20.00
Total Cycle Time	24.50	44.50	64.50	84.50

Table 5-4 (continued)

Cycles per year	230.65	127	87.6	66.88
Tonnes per cycle	11,666	23,300	35,000	46,600
Tonnes hauled	2,690,691	2,962,400	3,066,000	3,120,000
Tonnes prod. produced	734,000	808,000	836,000	851,000

The following USBM equations from Open File Report 4-87 were used:

#### Where

DHC = short tonnes hauled divided by operating days

L = one way haul distance in nautical miles

Operating Days = 299
Short tonnes hauled will be determined

Dredge capital cost = 7,052 (P).9421

Plant capital costs are based upon \$20,000,000 for an onshore plant, \$4,000,000 for an onboard plant and \$15,000,000 for dock construction. Infrastructure is estimated at 30% of the total of these costs. These costs are based on a phosphate plant yielding 4,000,000 tonnes of product per year. To allow for other product rates, an exponent of .7 was usd. The general formula is:

Capital Cost A = (Production/yr A + 4,000,000)•7 \* B where A = production/year from Table 5-6 B = base cost (\$20,000,000, \$4,000,000, \$28,000,000) for the 4,000,000 tpy case

Table 5-5 is a summary of calculated hopper sizes and the resulting capital required for each production rate from Table 5-4. The overburden dredge does not require a large hopper and its cost is estimated from other sources. Dollars per ton capital is based on 20 years of mine production for each production scenario.

Table 5-5
Capital Costs Configuration 1

Product		Millions of Dollars								
	Tonnes	Hopper	Mat.	Ob.	Ob.		OS			\$/M
Annual	20 Yrs.	<u>ST</u>	Dredge	Dredge	Plant	<u>Dock</u>	Plant	Misc	Tot	Ton
734 808 836 851	14,680 16,160 16,720 17,020	8,780 9,668 10,005 10,183	36.60 40.08 41.39 42.08	40.00 40.00	1.31 1.34	5.02		27.84 28.33	115.05 120.65 122.77 123.87	7.47 7.34

Table 5-7 combines the capital cost per tonne with the operating cost per tonne, to provide a basis for cost comparison.

Operating costs for the suction head hopper type matrix mining dredge are based on the following U.S.B.O.M. formula (from Open File Report 4-87).

Dredge operating cost (
$$\frac{s}{s.t.}$$
) =  $\frac{2.7534 (P) + 5,453}{Daily Dredge Capacity}$ 

where P = payload or hopper capacity in short tons daily dredge capacity = annual capacity in short tons + days.

Operating costs for the overburden dredge and for processing are based on Zellars-Williams operating cost model. Table 5-6 lists a summary of operating costs for the different production rates.

Table 5-6
Operating Cost - Configuration 1
Operationg Cost \$/Metric Ton Product

Tonnes Matrix*	Mat. Dred.	O.B. Dred.	Plant	Waste Disp.	Prod. <u>Hand.</u>	Admin.	Total
3,363,000	10.65	3.91	5.71	0.40	.45	1.30	22.42
3,703,000	10.45	3.91	5.71	0.40	.45	1.30	22.22
3,832,000	10.38	3.91	5.71	0.40	.45	1.30	22.15
3,900,000	10.35	3.91	5.71	0.40	.45	1.30	22.12

 <sup>4.6</sup> tonnes matrix mined results in one tonne of product.

Table 5-7
Total Comparative Cost per Tonne, Configuration 1

Tonnes Matrix	Capital	Operation	<u>Total</u>
3,363,000	\$ 7.84	\$22.42	\$30.26
3,703,000	7 - 47	22.22	29.69
3,832,000	7.34	22.15	29.49
3,900,000	7.28	22.12	29.40

### Sea-going Hopper Dredge Mining, Barge Transportation of Ore to an Onshore Plant

Figure 5.4 shows this configuration. An anchor suction dredge removes overburden, pumping it to mined-out areas. One anchor suction dredge is dedicated to waste and the other is used mostly for matrix. Since no large hoppers are required, as in Configuration 1, both dredges can be identical in design. To maximize production, the matrix dredge is required to operate in overburden some of the time. Table 5-3, shows the design criteria used for production and operating cost calculations.

The stripping ratio expressed in terms of cubic meters waste to cubic meters matrix is defined by the following equation:

Stripping Ratio = 
$$\frac{\text{Overburden Thickness}}{\text{matrix thickness} \times \% \text{ recovery}}$$
  
=  $\frac{8.02}{5.44 \times .85} = 1.73$ 

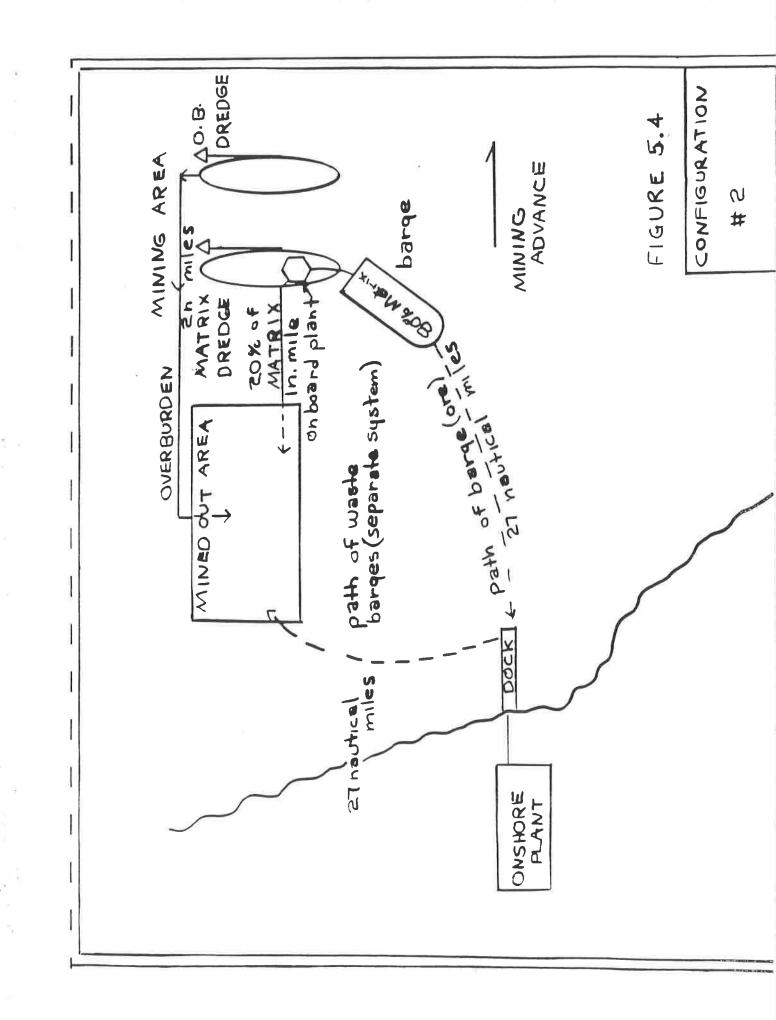
For each cubic meter of matrix mined, 1.73 cubic meters of waste needs to be removed. The total production from the overburden and matrix dredge is:

$$2 \times 12,118,000 \text{ m}^3/\text{yr} = 24,236,000 \text{ m}^3$$

This approach assumes that 15% of the ore zone is not recovered, as compared to the alternative approach of adding this volume to the overburden.

This is the total annual production from both dredges. Taking in account the required stripping ratio, the annual ore production is:

$$24,236,000 + (1+1.73) = 8,877,000 \text{ m}^3/\text{yr}$$



Annual matrix tonnage is:

 $8.877,000 \text{m}^3 (1.36 \text{ t/m}^3) = 12,074,000 \text{ tonnes}$ 

Annual product tonnage is:

 $8.877.000m^3 + (3.37 t/m^3) = 2,634,000 tonnes$ 

From these calculations, it is apparent that the matrix dredge must operate in overburden part of the time in order to maximize production.

The matrix dredge pumps matrix into a distribution box from which it is screened, washed, and deslimed. About 20% of the matrix is removed by onboard washing and disposed of in mined-out areas. The remaining 80% of the matrix is dewatered to 75% solids aboard 26,000 tonne barges. These barges are towed to the on shore beneficiation plant by tug boats. After matrix is unloaded by pumping it from the barge into live storage containment, the barge is towed back to the overburden dredge and another cycle begins. In order to avoid a large tailings area, an independent fleet of barges and tugs load, transport, and dump the plant tailings in the mined-out areas. By providing storage at the plant and a separate waste disposal sytem, the plant operation is not directly tied to the mine.

Table 5-8 shows the time required for each element in the cycle. The cycles per year are based upon 4,140 hours (the hours dredging in matrix). The tonnes per cycle are based upon the cycle time. Criteria from Configuration 1 apply here with the exception that barges move at 8 knots.

Table 5-8

Cycle Time Configuration 2

Item	Hours
Load barge	8.36
Barge to plant	3.38
Unload barge	8.36
Barge return	3.38
Total cycle time	23.48
Cycles per year	176.3
Tonnes per cycle	19,500
Tonnes hauled per year	3,439,000

Since the dredge mines 12,074,000 tonnes of matrix annually, the number of dredges required is:

12,074,000 (.8) + 3,439,000 = 2.81 or 3

The waste cycle is assumed to be similar to the matrix cycle. Although the waste from the onshore plant is only 7,029,000 tonnes (as shown below), the loading-dumping times and percent solids are expected to compensate for these differences.

washed matrix - product = waste 12,074,000 (.8) - 2,630,000 = 7,029,000

In all, a total of seven barges and tugs are required, three for matrix handling, three for waste disposal, and one for a spare. Dredge, barge, and tug capital costs are estimated from updating previous studies. Plant capital costs are based on \$20,000,000 for an on-shore plant, \$4,000,000 for an onboard plant, and \$28,000,000 for infrastructure and \$15,000,000 for dock. These costs are based on a phosphate plant yielding 4,000,000 tonnes of product per year. To adjust cost for other production rates, an exponent of .7 was used. The general formula to estimate capital cost for 2,634,000 tonnes per year production is:

Capital Cost =  $(2,634,000 + 4,000,000) \cdot 7*B$ where B = the base cost of capital items.

Table 5-9 itemizes the capital required for comparison of Configuration 2.

Table 5-9
Capital Cost Configuration 2

Item	mm \$ Unit <u>Cost</u>	No.	Total Cost
Barges Tugs Matrix dredge Overburden Dredge Beneficiation Plant Onboard Plant Infrastructure & Misc. Vessel Berths, loading dock	16.2 5.5 40.00 40.00 14.93 2.99 20.90 11.20	7 7 1 1 1	\$113,400,000 38,500,000 40,000,000 40,000,000 14,930,000 2,990,000 20,900,000 11,200,000
Total			\$281,900,000
\$ per tonne annual produc	etion		107.03
\$ per tonne mine life (20	years)		5.35

Operating costs are computed using Zellars-Williams operating cost model. Table 5-10 summarizes the operating costs.

Table 5-10
Operating Costs Configuration 2

	Cost per tonne product
Mining	6.64
Plant	4.94
Waste/Water	.25
Product Handling	.45
Administration	1.30
Total	\$13.58

The total comparative cost for Configuration 2 is \$18.93 per tonne product.

# 3. Dredge mining, pipeline transportation of ore to onshore plant

Because the location of the plant is upstream of the river, a pipeline system is not feasible. A substantial part of the pipeline would lie across shipping channels and industrial installations. For this reason, as well as environmental considerations, the pipeline system was not considered in further detail for this report. This is the same conclusion reached by other investigators, i.e., Zellars-Williams 1979, and Development Planning and Research Associates, Inc., 1987 North Carolina Offshore. Figure 5.5 illustrates the configuration.

# 4. Dredge mining, pipeline transportation to offshore plant

Figure 5.6 shows this configuration. An overburden dredge mines overburden sands ahead of the matrix dredge. Overburden is pumped back to the nearby mined-out areas. Trailing about 2,000 feet behind, in the same cut, the matrix dredge mines and pumps directly to a nearby offshore plant. This plant is built on an island formed by dredged material, located equi-distant an average of two nautical miles from the mining areas. The pipeline is flexible and most of it is submerged. Only the flexible portion near the dredge is floating. At the beneficiation plant, matrix is processed, and a saleable product produced. Waste is pumped through a separate pipeline to mined-out areas and released. All processing is done at the island-based processing plant. Product from the beneficiation plant is barged to shore for sale. The dredge production is identical to Configuration 2.

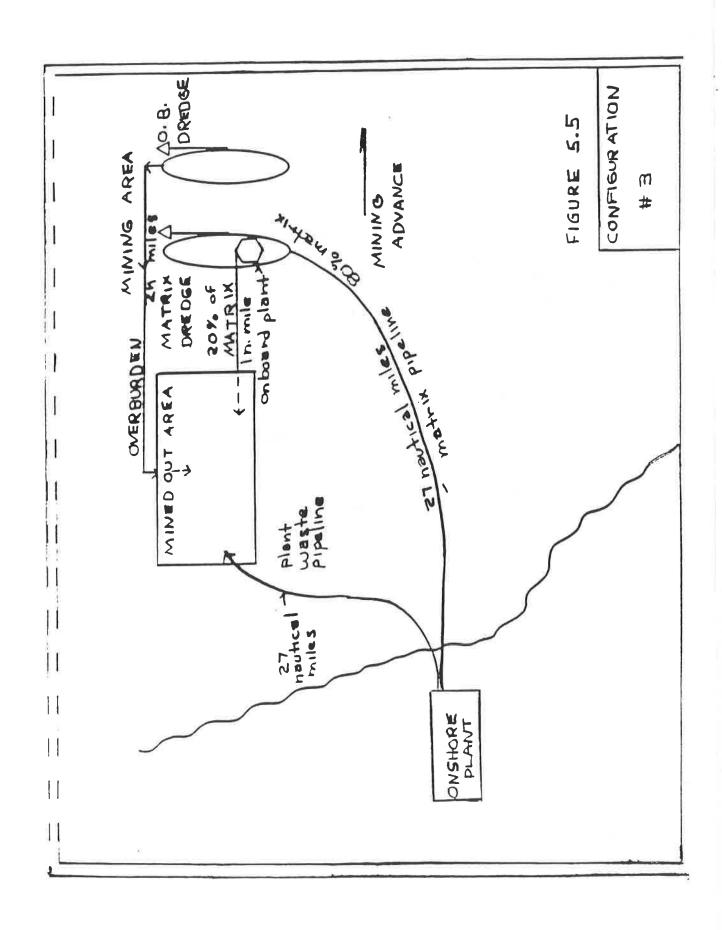
Barges are only needed to transport the product to Savannah Harbor. The cycle time is based on the same criteria as for Configuration 1.

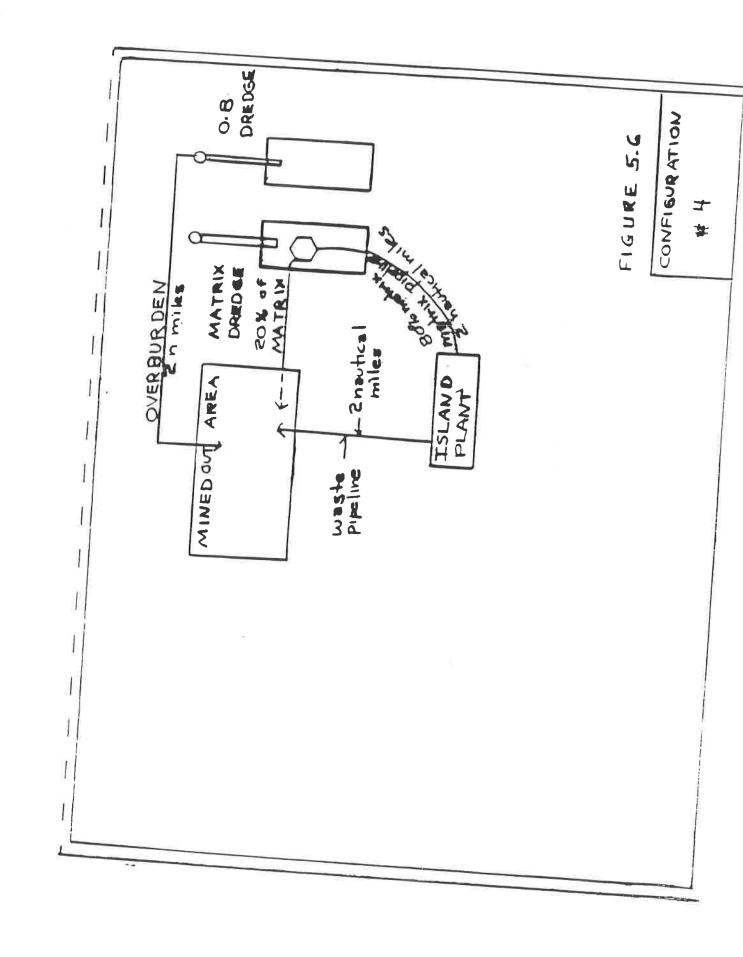
Loading time is:

barge capacity \* loading rate = hours Tonnes  $(26,000 \times .75) * (2916) t/hr = 6.69 hours$ 

Travel time is:

distance + speed = hours
27 (nautical miles) + 12 knots = 2.25





Assuming that unloading and loading are equivalent, cycle time is:

	Hours
Loading	2.25
Plant to harbor	6.69
Unloading	6.69
Harbor to plant	2.25
Total Cycle Time	17.88
Cycle per year	316
Tonnes per cycle	19,500
Tonnes hauled per year	6,162,000

Since only 2,634,000 tonnes of product require transport, one tug and one barge is adequate. Employment of contract transport carrier systems for product may be indicated.

Capital costs are summarized in Table 5-11. The only difference from Configuration 2 is the number of barges, tugs, island cost, and pipeline cost.

Table 5-11
Capital Cost Configuration 4

Item	mm \$ Unit <u>Cost</u>	No.	_Total Cost
Barges Tugs	16,200,000 5,500,000	1	\$ 16,200,000 5,500,000
Matrix dredge	40,000,000	1	40,000,000
Overburden dredge	40,000,000	1	40,000,000
Beneficiation plant	14,930,000	1	14,930,000
Onboard plant	2,990,000	1	2,990,000
Infrastructure & Misc.	20,900,000	1	20,900,000
Island	30,000,000	1	30,000,000
Pipelines	2,500,000	2	5,000,000
Vessel berth & loading dock	11,200,000	1	_11,200,000
Total Capital			\$186,720,000
<pre>\$ per tonne annual production \$ per tonne mine life (20 year</pre>			70.89 3.54

Operating costs were computed using Zellars-Williams operating cost model. Table 5-12 summarizes the operating costs.

Table 5-12
Operating Cost Configuration 4

Item \$Co	ost per tonne
Mining	5.76
Plant	4.94
Waste/water	.25
Product handling	.46
Administration	1.30
Total	12.71

The total cost for comparison of Configuration 4 is \$16.25 per tonne of product.

# 5.2.3 Selection of Configuration

It is evident that, from a material handling standpoint, the offshore plant should be more efficient. Material is processed near the plant and wasted near the plant in mined-out areas. With onshore plants, washed matrix is hauled 27 nautical miles by barge and tug, processed, and the waste hauled 27 miles back to the mined-out pits for disposal. Table 5-13 outlines comparative capital and operating costs for each configuration. Based upon this trade-off study, Configuration 4, utilizing an offshore plant, was selected as the basis for examining the economic feasibility of exploiting off-shore phosphorites. This configuration is developed in further detail in the following parts of this section.

Table 5-13
Configuration Selection

	Annual Production		Tonne Conce	
Configuration	Tonnes	Capital	Operating	Total
1	851,000	7.28	22.42	29.70
2	2,634,000	5.35	13.58	18.93
3	Not feasible	e (no econo	mics done)	
4	2,634,000	3.54	12.71	16.25

Configuration 1)	Sea-going hopper dredge for mining and transportation to
	an onshore plant.
Configuration 2)	Seagoing hopper dredge mining and barge transportation
	of ore to an onshore plant.
Configuration 3)	Dredge mining, pipeline transportation of ore to onshore
	plant.
Configuration 4)	Dredge mining, pipeline transportation of ore to nearby
	offshore island plant.

Zellars-Williams, 1979, treated Configuration 2 in considerable detail and concluded that favorable economics could result if all the assumptions made proved to be valid. The beneficiation process flowsheet suggested by Zellars-Williams, 1979, is adopted for this study, with minor modification in the degree of final processing. Most modern chemical fertilizer production plants use wet phosphate rock as feed stock. Calcination to improve grade of phosphate rock after wet processing is a matter of economics not considered essential to evaluating feasibility.

Capital and operating costs of beneficiation plants of various production rates, together with ancillary facilities and supporting infrastructure, are well known, and no attempt is made in this report to construct new estimates. Capital and operating costs are developed from current in-house data, factored for the production rates and unit costs applicable to the selected configuration and local conditions.

## 5.2.4 Design Criteria

Table 5-14 lists the design criteria used for determining production limits, operating costs, equipment needs, and capital requirements of the selected configuration. As with any mining project, the physical and chemical geologic parameters are site-specific, having been determined by nature. These characteristics were based upon the initial mine site selected in Section 5.1.1.

Operating factors were determined by past experience, as well as consideration of the unique mining environment. In the case of offshore dredging, it is necessary to consider the size and design of the dredge from a seaworthy standpoint. A large vessel is necessary to accommodate the mining depths; therefore, required size is somewhat independent of production. The largest dredge pumps operating in ocean mining today have a suction head pipe diameter of 1200 mm (48"). For the conditions of offshore Georgia, a 900 mm diameter (36") suction head pipe was used to determine productivity. The design philosophy is to use the largest practical dredge pump, mounted on a seaworthy vessel. For example, a dredge pump producing half the capacity of a 900 mm dredge pump gives only a small reduction in capital and operating costs. Therefore, the design philosophy maximizes production while minimizing the costs.

Table 5-15, Climatic and Physical Oceanographic Data, for the southeastern United States continental shelf, indicates conditions which may cause dredge mining operations to shut down which depends upon the specific equipment and configuration utilized.

The production rates are determined from the design criteria. In most land-based phosphate operations, the beneficiation plant is optimized and, because its maintenance and operations are easier, operating hours exceed the dragline (mining) operating hours. Often, several draglines feed the same plant. Stockpiles and surge bins cushion the difference between operating hours and production hours.

# Table 5-14 Design Criteria

## o Ore (matrix) assumed distribution

Size Fraction	Percent	BPL	Disposition
+4 Mesh	2.74	17.03	Grind to feed
4x8 Mesh	0.64	33.38	Grind to feed
8x16 Mesh	2.05	30.18	Grind to feed
16x150 Mesh	68.52	25.53	Flotation Feed
16x150 Mesh	4.76	6.00	Feed dilution
-150 Mesh	21.29	15.07	Clay Waste

## o Grade Criteria (Estimated)

Feed Head 16x150 - 24.20 BPL Rougher Concentrate - 55.00 BPL Final Concentrate (Float) - 66.0 BPL Final Concentrate (if Calcined) - 68.00 BPL

#### o Recoveries

Mining Recovery - 90%
Primary Cyclone Recovery of Feed - 98%
Secondary Cyclone Recovery - 99%
Rod Mill Weight Recovery - 85%
Flotation Recovery (Overall) - 80% of BPL values in the total feed

#### o Annual Operating Hours

Days lost: annual dry dock/repairs hurricane gale force winds fog other	30 1 5 1 1 38
Days operational Hours operational/year (327 x 24) Mechanical availability Overburden dredge Operating factor *	327 7,848 90 83
Matrix Dredge Operating factor * Dredge operating factor - average, use Overall operating factor90 x.85 =	87 85% 76.5%
Effective production hours/year (7.848 x .715)	6,000

\* Note: operating factor for dredges is based on allowing time for resetting spuds at end of each mining cycle.

# Table 5-14 (continued) Design Criteria

## o Beneficiation Plant

	Washer production hours	6,000	
	Production hours feed prep. flotation and product to storage	7,000	
0	Mining Data		
	Average Water Depth Average Overburden Depth Average Matrix (ore) Depth Average Mining Depth (below MSL) Matrix "X" (m <sup>3</sup> /t prod.) Matrix Density - 1.44 tonnes/m <sup>3</sup> (90 lbs/ft <sup>3</sup> ) Stripping Ratio - 1.64 m <sup>3</sup> overburden/m <sup>3</sup> matrix Overburden Density - 1.6 tonnes/m <sup>3</sup> (100 lbs/ft <sup>3</sup> )	13.97 m 8.02 m 5.44 m 27.43 m 3.13 1.44 1.64 1.60	n

Note: Oceanographic information is contained in Table 5-15.

Table 5-15

## Climatic and Physical Oceanographic Data \*

Much of the following information applies generally to the Savannah, Georgia region rather than specifically to the proposed offshore mining site. Local measurements within the area of interest have not been made.

Precipitation:	Average annual rainfall is 51 inches, half of which falls during
	the June 15 through September 15 thunderstorm season.
	Snowfall is rare and occurs, on an average, less than once a year.
Wind:	Winter surface winds are chiefly out of the west while the

summer months experience north and east winds alternating with those from the west. Average wind speed during the year is about 7 miles per hour with peaks each month ranging up to 30 to

38 miles per hour.

Storms: During an 84-year period to 1970, all tropical cyclones occurred between May 28 and October 19. Severe tropical storms affect the area about once in 10 years. In the period 1954-1975, seven

cyclones passed through the Savannah area.

Fog: Heavy fog is common along the coast and Savannah experiences 44 foggy days a year. The distribution of foggy periods is fairly

even through the year, although July and August have less.

Temperature: The climate is temperate with a seasonal mean of 51°F in the winter and 80°F in the summer. The record minimum and

maximum are 8°F and 105°F.

Tides: The maximum spring tidal range along the southeastern coast is 8 feet and occurs in the Savannah area. Strong onshore winds

can raise the water level a significant amount above the

maximum normal tide level.

Waves: Spring and summer waves from the southeast are generally small. Although more severe wave conditions result from the strong fall and winter winds from the north and west, the proposed mining site is relatively well sheltered by land from this direction. Offshore from Savannah the recorded percent

frequency of two levels of wave height is:

Wave Height	Feb.	May	Aug.	Nov.	Annual
4 foot	40%	66%	74%	48%	57%
12 foot	5%	2%	1%	1.5%	2.4%

<sup>\*</sup> From Zellars-Williams (May 1979)

For ocean mining, the plant is dependent on feed from a single dredge, so stockpiling is impractical. Therefore, the washer or front end of the plant must reduce operating hours from the normal of about 7,000 hours per year to match the dredge, which is limited to 6,000 hours per year. A quick look at capital costs from previous studies shows that dredging and transportation comprise a much larger percent of total project capital than does the beneficiation plant. Therefore, the dredging/transportation systems are optimized at a slight reduction in plant capital cost efficiency.

Section 4 lists the available state-of-the-art technologies. The only currently utilized system capable of mining phosphate in off hore Georgia is a plain suction head dredge. There is considerable doubt that this dredge is capable of mining the phosphorite which is consolidated. If this is true, then no currently utilized systems exist for mining offshore Georgia phosphorite.

## 5.2.5 Mining Systems

The system proposed for offshore phosphate mining in the areas identified is an advanced version of a hydraulic dredge of the cutter head suction type.

The platform would be constructed of steel, taking the shape of a large hull comprising a series of watertight compartmentalized buoyant sections fastened together to make a semi-rigid structure. The buoyancy and structural integrity of the platform must be capable of supporting the spuds, pumps, prime movers, deck machinery, operator's house, ladder and superstructure, and as required, certain ore washing and screening equipment. This structure must be capable of floating, with safe freeboard, in moderate seas while being towed or otherwise moved by tug. During operation, the platform will be supported on legs extending to the bottom of the cut and must be structurally capable of carrying the dead load, wind and wave loads, and the dynamic loads imposed by the excavating machinery. The design and construction of this kind of platform is entirely within the technological expertise and experience of U.S. contractors and manufacturers.

The platform-hull will be equipped with a ladder supported by cantilevered overhead structural members. The ladder will pivot on a swivel located on or near deck level at the front end of the platform-hull to permit the ladder to

articulate. The ladder, about 250 feet in length, when lowered to 45° below horizontal, will swing port to starboard over an arc angle of 80°-90°. At digging depth of about 130 feet (below water surface), the chord distance of the arc swing will permit a cut width of about 360 feet. With the ladder lowered to 60°, digging depth of 165 feet and cut width of about 360 feet can be realized.

An hydraulic or electric motor driven cutter head mounted at the end of the ladder engages and excavates the material to be extracted. The cutter head directs excavated material to the flared open end of a pipe which leads to the suction side of a centrifugal pump. The pump is also submerged and is located about one-third the distance up the ladder. The pump is a high capacity, low head end suction centrifugal pump capable of passing large solids. This pump is direct driven through an extended mechanics shaft arrangement or directly by a variable speed submerged electric motor and gear box mounted on the ladder.

The platform-hull is designed to accommodate eight spuds. The entire platform is supported by four spuds extending to the ocean bottom. The lower end of each spud has an enlarged pad providing the area required for bearing to support the platform-hull. The spuds are of a length, when retracted, to permit floating with minimum draft, and when extended, to provide clearance above high tide and severe weather seas. Four of the spuds (working spuds) are mounted in carriage systems which will facilitate controlled horizontal movement of the platform. This movement, with working spuds extended, will permit advancing the mining face of the cut about 50 feet without resetting spuds.

When the full limit of horizontal travel is completed, the other four spuds (fixed or positioning spuds) are extended, the working spuds retracted, and the platform repositioned.

The working spuds are extended, the positioning spuds are retracted and the advance cycle by manipulation of the carriage system is repeated.

This platform-hull cutter head suction dredge will operate in all but the most severe weather conditions. When gale or hurricane force wind and wave

action occurs, the platform will ride out these conditions above the sea, supported on eight legs.

The cutter head may be an open radial multi-blade basket-type with cutter teeth designed for loose sand, sandy-clay and moderately cemented sands and gravels. Since the cutter head is axially mounted and rotates in one direction, excavation occurs when the ladder sweeps in the same direction. During the return sweep, no engagement of the cutter head occurs and the pump will collect material previously loosened. The matrix dredge will be equipped with a radial basket-type cutter head.

The cutter head may be of a bucket wheel design. The rotating axis of the wheel is perpendicular to the ladder and the buckets engage the excavating face in both sweeping directions. Bucket configuration and spacing is arranged for the type of material to be excavated and buckets spaced on the wheel to reject oversize particles. Production from this type of cutter is expected to be better than from a basket-type. The overburden dredge will be equipped with a bucket-wheel type cutter head.

The proper cutter type is a matter of design based upon accurate knowledge of soil conditions. For the purpose of this study, dredge production is based on experience with these two cutter heads in unconsolidated sandy material and on practical limits of centrifugal pump capacity, average solids content of 30-40% by weight in the slurry.

The mining system described above is based on a design proposed by Ellicott Machinery Corporation of Baltimore, MD, for mining sands offshore U.S. Atlantic coastal waters for beach nourishment. The design and construction of the dredge platform described is well within the capability of this manufacturer, who will combine its own dredge construction experience with the experience of offshore gas and oil exploration and production platform contractors.

Production is limited by the capacity of the ladder-mounted dredge pump. The capacity of the dredge pump is restricted by its size (weight) and the power output of the prime mover (motor, speed reducer and power transmission system). GIW Industries, Inc., of Grovetown, Georgia has

recently supplied deck and ladder pumps (30  $\times$  34 TBC 84, and 34  $\times$  34 LHD-60) to Shipyard Stapel B.V., The Netherlands, for the dredge "Amazone" built for Dredging International, N.V., Belgium. These pumps have slurry pumping capacity in the range of 50,000-70,000 gpm at discharge heads up to 500 feet.

The practical upper limit of currently manufactured submersible electric motors is about 3000 kW.

The combination of these state-of-the-art currently manufactured components indicates that dredge slurry pump capacities of 70,000 gpm at 40% solids, and 7,200 tonnes (dry solids) per hour are realistic. Total head, and therefore discharge head, is limited for practical purposes only by the amount of energy available at the pump shaft, i.e., by the horesepower (kW) of the prime mover.

The mining and ore transport system described above envisages an arrangement which is an assembly of cutter head, ladder pump and deck pump sized for maximum performance consistent with available power and the practical limitations of the platform and its structural components working in an ocean environment. This is the premise for mining which is the basis for determining the annual production capacity of the selected configuration used in evaluating feasibility of the enterprise.

#### 5.2.6 Mining Dredges

Two dredges will be required for the mining of phosphorites from the offshore areas described in Section 5.2.1. One dredge will excavate and remove overburden, the other will mine matrix and remove it to the beneficiation plant.

Overburden from the initial mining area will be used as hydraulic fill in the construction of the off-shore island.

The overburden dredge will excavate overburden and discharge through a trailing pipeline for deposition in mined-out cuts. The pipeline would be supported at a semi-submerged level by floats to minimize wave action effects. The pipeline would discharge to a barge-mounted hopper and tremie.

The tremie would direct discharge of the slurry below water near the bottom of the cut being backfilled. The discharge pipeline and tremie hopper barge would be tended by a tugboat which "shepherds" the pipeline and moves the tremie hopper barge.

The overburden dredge must remove about 7 cubic yards (5.1 cubic meters) for each tonne of final product produced. Average water depth is 45.8 feet, and the average depth of overburden is 26.3 feet (23.3 feet minimum to 32.5 feet maximum) in the area designated for mining. The platform must be capable of operating safely above the water surface with a clear distance of about 6-10 feet. Tide variance of +7.4 feet and wave height of 15 feet should be allowed. This will put the bottom of the platform at Elevation +30.4 (8 + 7.4 + 15). Assuming a depth of the platform-hull of 24 feet, the top of the platform would be at Elevation +54.4. Average overburden digging depth from top of platform to Elevation -72.1 is 126.5 ft. (54.4 + 45.8 + 26.3). Maximum digging depth to Elevation -86.3 is 140.7 feet (54.4 + 53.8 + 32.5).

The overburden dredge will excavate about 11,200 cubic yards (8,564 m<sup>3</sup>) from one position; the spud carriage system will advance the platform approximately 50 feet, before repositioning. This cycle will take 30-60 minutes.

This dredge is equipped with a GIW  $34 \times 34$  LHD-60 ladder pump and 2500 kW variable speed submersible motor. The pump capacity is 65,000 gpm at about 85 feet head (26 meters). A bucket wheel cutter head, at the end of the ladder, powered by a 1500 kW motor excavates and directs overburden to the ladder pump suction.

The ladder pump discharges directly into the suction of a GIW  $30 \times 33$  MDH 72 slurry pump mounted on the deck. This pump is fitted with an impeller capable of 65,000 gpm at 200 feet head (61 meters) at 350 rpm. The prime mover for this pump is a 4500 kW variable speed electric motor and speed reducer.

The overburden dredge is capable of mining at the average rate of 6,560 tonnes per hour at 35% solids, and transporting this slurry through a trailing pipeline about 1.5 nautical miles (9,120 feet) to waste in nearby mine cuts.

The matrix excavating dredge will excavate matrix and discharge through a trailing pipeline to a central processing plant. The area to be mined over a 20-30 year period will be within a radius of about 3 nautical miles (18,240 feet) from an artificial island on which the plant is built. The maximum pipeline length will be about 25,000 feet. The matrix mining dredge will operate from a stationary position above the water surface as described for the overburden dredge. The matrix dredge must remove about 4 cubic yards (3.1 cubic meters) for each tonne of final product produced. Average depth of matrix is 17.8 feet (16.4 ft. min. to 23 ft. max.). The average bottom of the matrix is at Elevation -90.1. From the top of the platform at Elevation +54.4, the average matrix digging depth is 144.1 ft. Maximum digging depth to Elevation -109.3 is 163.7 feet (54.4 + 53.8 + 32.5 + 23).

For each move, the matrix dredge will excavate about 7,500 cubic yards  $(5735 \text{ m}^3)$ . The repositioning cycle, which occurs at the end of the spud carriage system travel (about 50 ft.), will take about 30-60 minutes.

This dredge is equipped with a GIW 30 x 33 MDH 72 ladder pump and 1500 kW variable speed submersible motor. The pump capacity is 45,000 gpm at about 90 feet head (27 meters). A radial basket-type cutter head, at the end of the ladder, powered by a 1500 kW motor excavates and directs matrix to the ladder pump suction. The ladder pump discharges directly into the suction of a GIW 30 x 34 T8C 84 slurry pump mounted on the deck. This pump has a capacity of 45,000 gpm at 450 feet head (137 meters), and is driven by a 6,500 kW variable speed motor and speed reducer at 425 rpm. The matrix dredge is capable of mining at the average rate of 3,600 tonnes per hour at 30% solids, and transporting this slurry three nautical miles (18,240 feet) to the island-based beneficiation plant.

The two dredges are to be similar in design and construction. Average digging depth for the overburden dredge from top of deck is about 127 ft. (39 m) and for the matrix dredge about 144 ft. (44 m). Ladder length would be matched to the cut depth. Cutter head power would be the same. Ladder pumps would be similar, the overburden dredge having more capacity. Deck pumps would be sized to accommodate the slurry and pipeline distance.

The overburden dredge requires about 9500 kW diesel engine powered electric energy generating capability to provide power to all equipment. Maximum

power demand, which occurs when dredge pumps are being started while the other machine is operating, is about 9400 kW. During normal operation over mine life the power demand is about 7500 kW. Fuel consumption is about 1.4 tonnes per hour.

The matrix dredge requires installed diesel engine electric generating capability of about 10,500 kW. Mine life average power demand is about 8400 kW. Maximum power demand occurs when mining at the extremities of the oredoby, about 3 nautical miles, is estimated to be about 10,500 kW. Fuel consumption for mine life average is about 1.8 tonnes per hour.

The two dredges will be similarly equipped with diesel fuel powered electric generators having a nominal continuous rating of 10,000 kW and standby rating of 12,000 kW. Fuel storage capacity of about 1360 tonnes (10,000 bbls) to permit one month of operation without re-supply is provided.

Fuel is to be supplied by a commercial operator such as Belcher Company of Georgia, Inc., who will contract for delivery to the offshore dredges by fuel barge (10,000-17,000 bbl capacity). This fuel barge would normally deliver and transfer diesel to each dredge on a 10-15 day cycle.

Crew accommodations for three shifts are provided in 2-bed cabins. Crews work two weeks offshore, 14 days @ 12 hours/day, and go ashore for seven days. Shifts are staggered so that while two shifts are on duty offshore, one shift is at rest on shore. Cooking and mess facilities are provided to serve about 40 persons, three meals each day. Provisioning and re-supply occurs on a two-week cycle when crew shifts change. Crews and provisions are transported from Port Savannah by motor launch.

Each dredge has a helicopter landing deck platform positioned in cantiliverfashion off the stern.

For purposes of estimating capital cost, it is assumed the two dredges are identical; sized for the maximum conditions. Operating cost will be estimated separately for the two machines based on materials handled and distances transported.

#### 5.3 BENEFICIATION

The beneficiation facilities have been grouped into the following areas: washer, feed preparation, flotation, reagent, waste disposal, water recirculation, and product storage and loading.

These areas are designed to receive slurried ore from the dredge, disaggregate the ore, wash and grind the oversize rock, remove clay from the feed, and separate the sand from the feed to produce a marketable phosphate concentrate product.

Sea water will be used in the beneficiation process, which will result in a higher level of chlorides in the concentrate. Chlorides will be removed from the concentrate by filtering and rinsing with fresh water supplied by desalination units.

Waste products (clay and sand tailings) will be returned to the mine cuts.

#### 5.3.1 Washer

The phosphate rock ore (matrix) is dug and slurried by the dredge and then pumped to the washer for initial processing. The purpose of the washer is to separate the +20 mesh rock from the -20 mesh fines and to grind the +20 mesh rock to pass 20 mesh.

Large clay balls and other deleterious material are discarded at the washer. This material is recovered from the discard pile and used as fill to repair erosion, and/or is placed as fill along the toe of the outer slopes of the island.

The slurried matrix is received from the dredge at the matrix distributor where it is diverted to the trommel screens. The trommel screens separate the material at 2 inch. The +2 inch oversize is conveyed to a reject pile, while the -2 inch undersize from the trommels gravity flows to the flume screens. The flume screens separate the material at about 20 mesh. The flume screens facilitate a quick reduction in flow and removal of a large percentage of the solids. The +20 mesh material from the flume screen

oversize is re-screened at the primary vibrating screens. Plus 20 mesh oversize from the primary vibrating screens is then pumped to the milling section which consists of a rod mill in closed circuit with vibrating screens (secondary screens).

The secondary vibrating screens feed a surge bin. Feed retrieval from the bin is achieved by a weigh-belt feeder which is designed to deliver a controlled rate of feed to the rod mill. The rod mill discharge reports to a pump box which recycles the ground pulp to the secondary vibrating screens. The ground -20 mesh material passing the secondary vibrating screens is combined with the -20 mesh undersize from the flume screens and primary vibrating screens and is pumped to feed preparation. The +20 mesh material from the secondary vibrating screens reports to the mill feed surge bin.

The flowsheet for the washer is shown in Figure 5.7.

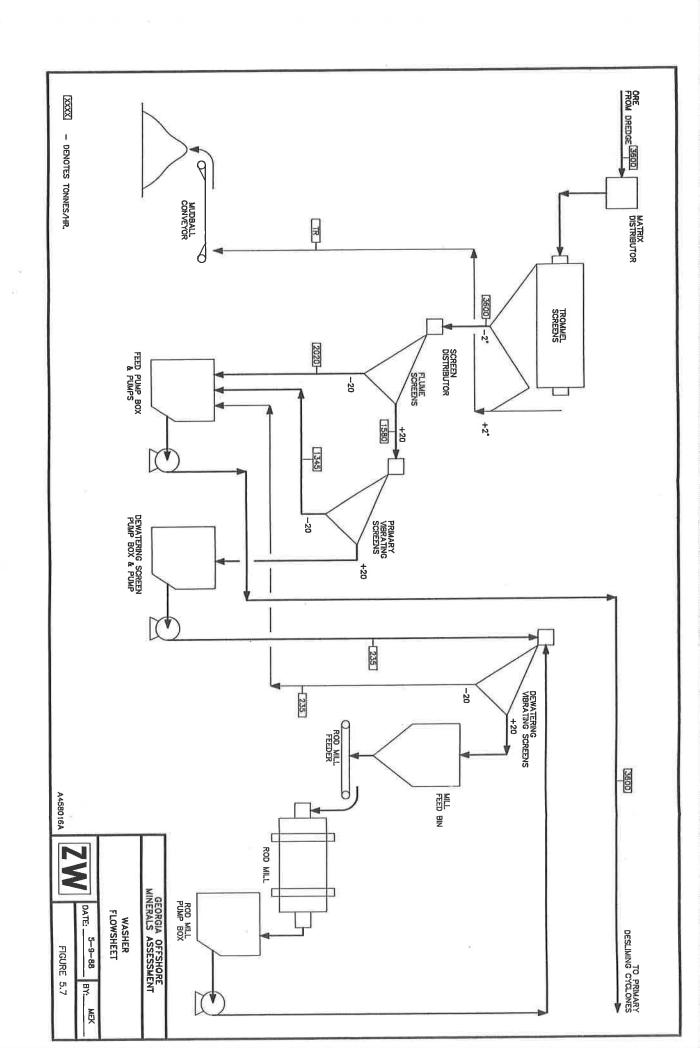
# 5.3.2 Feed Preparation

The -20 mesh feed from the washer is pumped to the feed preparation area. Primary activities conducted in the feed preparation area are:

- Removal of the -150 mesh particles (slimes) from the flotation feed. The
   -150 mesh slimes are removed in order to improve flotation efficiency
   and to reduce reagent consumption.
- o Perform attrition scrubbing of the flotation plant feed.
- o Provide feed to the flotation plant at a uniform rate by feed surge storage and control of feed tonnage rate.

This discussion describes one train. More than one train is required.

Feed from the washer is pumped to the primary desliming cyclones. The cyclones are used to remove -150 mesh slimes (clays) from the feed. The primary desliming cyclone underflow, at about 65% solids, gravity flows to the feed surge bin. The feed surge bin is designed to provide about 24 hours of live feed storage, smooths out upstream process surges, and helps to maintain a constant rate of feed to the feed preparation circuit. When the bin overflows, it also functions as a desliming operation.



Feed is reclaimed from the storage bin as a slurry and is pumped to the secondary desliming cyclones. The cyclones remove additional -150 mesh slimes and dewater the feed prior to attrition scrubbing. The secondary desliming cyclone underflow, at about 65% solids, gravity flows to the attrition scrubbers. Scrubbing of the feed removes any tramp clay particles, removes some of the friable carbonates by reducing it to slime particle size, and effectively scours the particle surfaces to enhance flotation performance.

Scrubbed feed is then repulped with recycle water and pumped through the tertiary desliming cyclones to remove the slimes produced during the scrubbing step.

The primary, secondary and tertiary desliming cyclone overflows and bin overflows contain slimes and fine solids entrained in dewatering. The combined slimes collect at the slimes stand tank and then gravity flow to the waste disposal station. Clarified water from the waste disposal station is returned to the plant for re-use in the process. Waste disposal and water distribution are reviewed in Section 5.3.5 and 5.3.6, respectively.

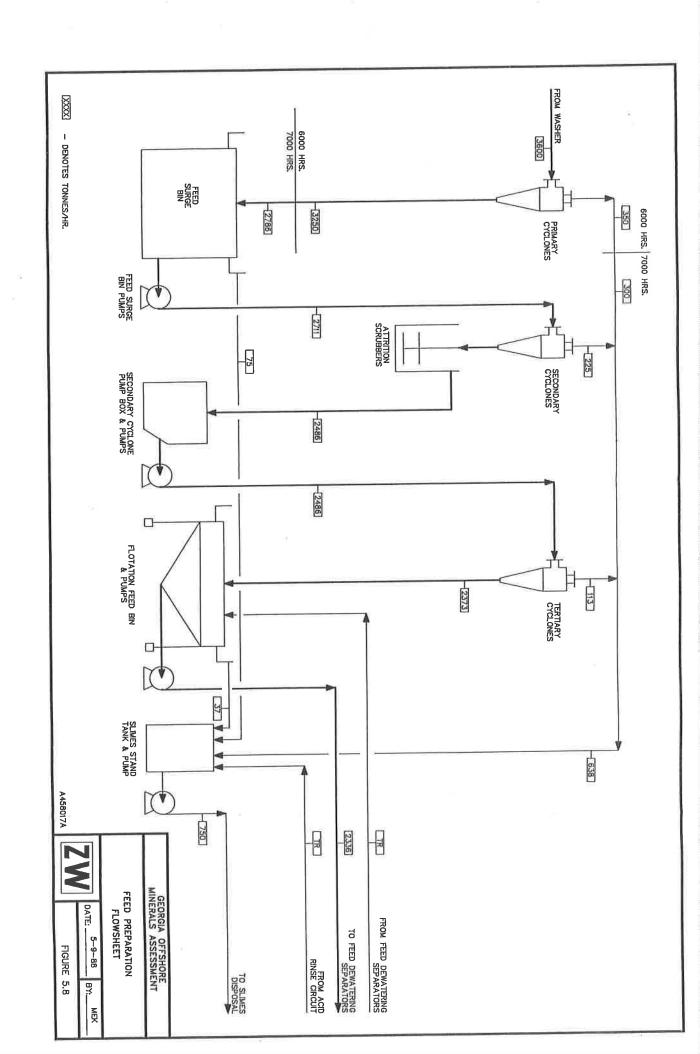
The tertiary desliming cyclone underflow reports to the flotation feed bins. The bins provide about 4 hours of live storage and are used to maintain a constant feed rate to flotation. The bins are designed to overflow, thereby functioning as a desliming operation as well. Feed from the bins is pumped to the feed dewatering separators in the flotation area.

The flowsheet for the washer is shown in Figure 5.8.

#### 5.3.3 Flotation

The flotation section is designed to recover the phosphate from the sized, deslimed feed delivered from the feed preparation area and produce a high grade saleable product. The conventional two-stage Crago process is employed for this purpose and consists of anionic rougher flotation of the phosphate particles followed by deciling and cationic cleaner flotation of the silica particles.

x						
8 2						
			×	×		
24						
10						
					2	
NO 6						
***						



		is <sup>N</sup>

The objective of rougher flotation is to obtain a bulk separation of the phosphate from the silica, achieving a reasonable recovery of phosphate without an attempt to produce a saleable concentrate. Significant rejection of silica is accomplished in this rougher step, but the concentrate is still high in silica. The rougher flotation reagents are removed by acid scrubbing and then the feed is subjected to cationic cleaner flotation where most of the remaining silica is floated and removed from the phosphate sink particles. The final concentrate product is relatively free of silica.

#### Reagents used in the rougher flotation circuit are:

- o Fatty Acid (or Fatty Acid Soap). An organic fatty acid (oleic acid, etc.) derived from wood pulp processing.
- o Fuel Oil. An extender used to aid in flotation and froth control.
- o Sodium Hydroxide or Ammonium Hydroxide. Used for pH adjustment.

Sulfuric acid is the deciling reagent. The acid attacks the reagents, solubilizing them, making it possible to wash the particle surfaces clean.

The reagents used in cationic cleaner flotation are:

- o Organic Amine Reagents. The primary silica flotation chemical.
- o Kerosense. An extender.
- o Sodium hydroxide for pH control, as necessary.

The deslimed feed from storage is pumped to the dewatering separators which dewater the feed to 68-72 percent solids prior to entering the reagent conditioners. Fatty acid, fuel oil and caustic are added at the conditioners and allowed to mix (condition) with the pulp for 3 to 4 minutes. The conditioned feed is then discharged into the rougher flotation machines. Flotation is conducted carrying the rougher concentrate to the overflow.

Rougher concentrate is then pumped through cyclones that dewater the solids to facilitate acid scrubbing. Reagentized water recovered from the cyclone overflow is returned to the flotation feed bin in the feed preparation area.

After scrubbing with sulfuric acid, the feed is washed free of spent rougher reagents by countercurrent flushing with water in primary and secondary wash boxes.

The de-oiled rougher concentrate is then fed to the cationic cleaner flotation cells where amine and kerosene are added to float the silica from the phosphate. Final concentrate reports to a pump box where it is pumped to the filtration section. The rougher tailings and cleaner tailings gravity flow to the general mill tailings pump box, and are combined and pumped to the GMT dewatering cyclones at the waste disposal station.

At the filtration area, the flotation concentrate is dewatered by cyclones followed by filtering and a two-stage countercurrent wash with fresh water to remove chlorides (sea salt). Horizontal table filters with sprays are used to filter and wash the concentrate. The washed and dewatered product is then conveyed to product storage. Wash filtrate from the filters is collected and returned to the plant hydraulic station.

The flowsheet for flotation is shown in Figure 5.9.

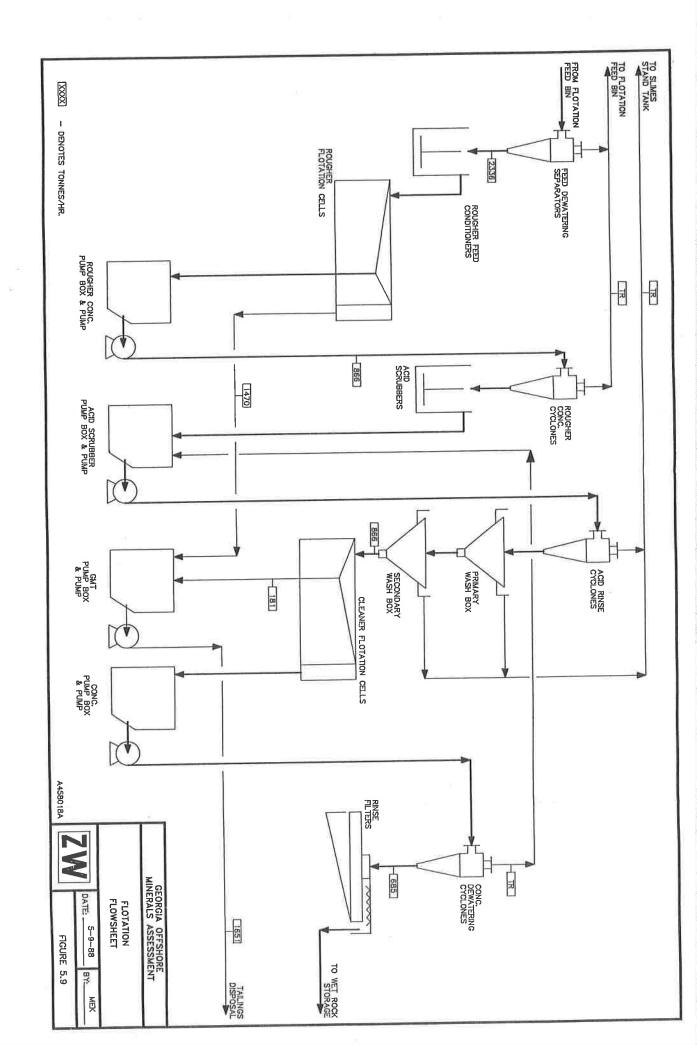
#### 5.3.4 Reagent Storage

## General

This area contains facilities to receive, unload, store, mix, and distribute reagents to the flotation plant and flocculants to the thickeners.

The system is designed to provide storage of reagents with capacity to receive shipments based on normal turnarounds. The mixed reagents storage capacity is based on the concept of one reagent operator five days per week preparing the reagent requirements for three shifts, seven days per week.

Stations for unloading are located to allow the receipt of reagents by ship/barge.



Electric heat is provided for No. 5 fuel oil, fatty acid, 50% caustic, and amine as required to pump and dilute these reagents for use in the flotation plant.

The tank farm will be enclosed by a wall for spillage containment and to aid in housekeeping.

## Fatty Acid

This reagent is delivered in 20,000 gallon lots. The fatty acid can be unloaded and stored in two 50,000-gallon storage tanks. Electric heat is provided to heat the fatty acid to about 120°F as necessary to unload, transfer, and store the chemical in a fluid state.

#### Fuel Oil

Number 5 fuel oil will be delivered in 20,000 gallon lots and unloaded using the fatty acid unloading pump. No. 5 fuel oil is viscous and must be heated to approximately 120°F for reasonable handling.

Fuel oil is stored in a 46,000 gallon insulated heated storage tank and is circulated to ensure consistency and to maintain fluidity. The fuel oil is furnished to the fatty acid-fuel oil mix tank as required. The resulting fatty acid/fuel oil mix is metered to the rougher flotation conditioners.

## Sulfuric Acid

Sulfuric acid (minimum of  $93\%\ H_2SO_4$ ) will be unloaded into a  $24,000\ gallon$  storage tank. It is fed to the acid scrubber circuit at the received concentration and the rate is controlled by a pH indicating/controller located at the acid scrubbers.

### **Amine**

Amine will be unloaded into a 24,000 gallon storage tank. The 100% amine will be maintained at approximately 100°F to maintain fluidity.

Temperature control and mixing by an agitator are provided in order to prevent overheating and degradation of the amine.

The 100% amine is pumped to the dilution/ mix tanks (10,000 gallons) where water is added to obtain a 5% solution of amine. The mixture is then transferred to a 14,000 gallon use tank for metering into the process.

#### Kerosene

Kerosene will be stored in a 12,000-gallon storage tank. From storage it will be metered to the flotation area for use as an extender in cleaner flotation.

### Sodium Hydroxide

Sodium hydroxide will be received as a 50% NaOH solution and stored in a 45,000 gallon storage tank. The 50% caustic must be heated in cool weather to prevent solidification; therefore, the system is provided with heated lines and the storage and mix tanks are heated.

The 50% caustic is diluted to 10% with water for plant use. After mixing, the 10% solution is transferred to a storage tank where it is metered to the rougher flotation section for pH control.

#### Flocculant

Flocculant is diluted directly with water to a low concentration suitable for metering into the thickener. The flocculant tank is provided with an agitator and recirculation capability.

## 5.3.5 Waste Disposal

The combined slimes from the feed preparation area gravity flow to the waste clay thickeners. The type of thickeners required are the high rate compact type that require less land area than conventional earth-bottom thickeners. The typical compact thickener consists of: a shallow,

cylindrical, cone-bottom tank; dewatering rakes and rake-drive; and an elaborate feed and discharge system for controlling slurry input, rate of addition of a flocculating agent, and the level and composition of the thickened slurry bed within the machine. Feed is typically injected into the center of the bed and clarified water is usually removed by way of a perimeter launder at the top of the tank. Clarified water from the thickener overflow water is returned to the plant hydraulic station.

The mill tailings (GMT) from the flotation area are pumped to dewatering cyclones. The cyclone overflow is returned to the hydraulic station while the cyclone underflow is fed into the waste clay thickeners. The thickener, therefore, acts as a mixing device, as well as facilitating a high-solids content sand-clay waste stream. It is believed that a high-solids content sand-clay waste stream, carefully deposited at or near ocean bottom, will undergo relatively little dispersion if water depth were sufficient and subsurface currents were not extraordinary.

An array of compact thickeners of adequate capacity could be constructed in various configurations. It is estimated (without specific knowledge of the character of the waste clays to be encountered offshore) that six units of 85-foot diameter, or three units of 140-foot diameter, would be sufficient for the proposed operation. The latter, disposed in a triangular array, would be less space-consuming than six units in a hexagonal configuration.

Whether waste clays are prethickened or not, and whether or not sand tailings addition were practiced, disposal of the waste streams would be within the mined-out areas. Typically, the discharge point would be well below sea level in order to minimize dispersion. The discharge line would require periodic tending to move the effluent point for even distribution of the mined-area backfill.

# 5.3.6 Water Requirements

Water is used extensively in mining and beneficiation as a processing medium and as a means of transporting solids in the form of aqueous slurries. The three main sources of water are: (a) sea water; (b) recirculated process water; and (c) fresh water.

Recirculated process water is collected at the plant hydraulic station where pumps lift the water, via independent distribution systems, to various areas of the beneficiation plant. Sea water is also pumped to the hydraulic station to replace system losses. Fresh water is used to wash the flotation concentrate and is required for reagent dilution, and for laboratory and potable water needs.

## Fresh Water

Fresh water is required for the following plant uses:

- o concentrate product wash
- o reagent dilution
- metallurgical laboratory use
- o potable water.

Systems that in normal circumstances would be supplied with fresh water, such as pump seal water, are not included in the total demand. It is also assumed that a source other than fresh water is used for sanitary fixtures.

A HydroFuge reverse osmosis (R/O) modular system is recommended to fill the planned fresh water needs. Water requirements, based on 150 ppm Cl-content in the treated (fresh) water are presented below.

Fresh (R/O Desalinated) Water Requirements

Description of Water Use	Rate (gpm)
Concentrate product washing	1,315
Reagent dilution	25
Met. lab	5
Potable water	5
Misc. (10% add. capacity)	135
Total	1,485
70	2,138,400 gpd

On a washed concentrate product tonnage basis, approximately 115 gallons of fresh water are used by the horizontal table filters for each tonne of product.

A 10 percent safety factor has been allowed in computing total fresh water requirements.

Each HydroFuge R/O module proposed will produce approximately 300,000 gallons per day (1,136 m<sup>3</sup>) of fresh water (Cl<sup>-</sup> content approximately 150 ppm) from average sea water feed of 1,000,000 (3,785 m<sup>3</sup>) gallons per day, at 19,000 to 21,000 ppm Cl<sup>-</sup>. The units operate at 30 percent recovery. Thirty percent recovery requires a 3-1/3:1 ratio of sea water delivered to the pump per unit of fresh water produced. This assumes a delivery pressure 75 psi (52 m).

In fact, actual operating recovery can be varied from 20 to 70 percent depending on output of water required and its contained chloride (or TDS) content.

The fresh water system installation required for concentrate product rinsing and other uses will require eight reverse osmosis modules.

The high Cl<sup>-</sup> filtrate from the R/O units will be discharged as waste. The wash filtrate from the two-stage countercurrent wash on the table filters is collected and returned to the plant hydraulic station.

#### **Process Water**

The main sources of process water are: recirculated water from the GMT cyclones overflow, recirculated water from the slimes thickeners overflow, and table filter wash filtrate. Process water make-up requirements are provided by the sea water pump station which supplies water to the hydraulic station.

The beneficiation plant hydraulic station consists of two tanks. Fresh water flows into the first tank which supplies water to a reagent water pump and to the laboratory. Excess water overflows the first tank into the second tank,

which satisfies the beneficiation process water supply pumps (high and low pressure) demand for water. The second tank also receives recycled water from the GMT cyclones overflow, the slimes thickeners overflow, table filter wash filtrate, as well as sea water from the sea water pump station.

# 5.3.7 Product Storage and Loading

Washed concentrate is conveyed from the filtration section to the wet rock product storage pile.

The storage pile will be contained in an open-top structure about 200 feet wide by 700 feet long, with concrete walls about 30 feet high. In normal operation, concentrate will be piled as much as 15 feet above the walls, resulting in a storage capacity of approximately 340,000 tonnes.

The storage system consists of a bridge-type dual bucket wheel stacker/reclaimer that spans the total width of the storage area and travels the length of the stockpile. Washed concentrate is stored via the bridge supported stacker conveyer, tripper car, and discharge chute. Concentrate is reclaimed via the bridge supported dual bucket wheels. The independent digging wheels feed a conveyor system which, in turn, feeds a shiploader with the capability of loading vessels at the rate of 3,000-3,500 tonnes/hour. The shiploader is equipped with a cantilevered section that extends out over the mooring berth to distribute the concentrate during loading of the vessel.

The mooring berth will be located along the full length of one side of the island, and adjacent to the wet rock product storage pile. The berth will also permit off-loading of fuel, reagents, and other supplies required to sustain the island operation.

#### 5.4 CONFIGURATION AND INFRASTRUCTURE

The preferred configuration of mine, beneficiation and support facilities is that which results in the least investment and the lowest cost of production. Accuracy in assessing and evaluating risks is a necessary and vital element of engineering the design and construction of the preferred configuration.

Depending on the specifics of location conditions, offshore dredging activities may be detrimental, beneficial, or have no determinable effect on fauna, the coastal environment, or the sea floor.

The offshore area targeted for initial exploitation of the phosphorite resource is located in 46 feet of water (average depth) just north of the Savannah Harbor navigation light tower, which marks the entrance to the Tybee Road ship channel. The northern extremity of the proposed mining area is about 2 nautical miles north of the 32° latitude line, and 4-7 nautical miles south and west of the Port Royal Sound navigation channel entrance.

The preferred configuration concept envisages the offshore location of all mining, beneficiation and support facilities. No production activity takes place on shore. Finished product is loaded on vessel for transport to the customer from the offshore location.

Zellars-Williams, 1979, under a contract to the U.S.G.S, based their work on mining a hypothetical orebody located in the same area identified and targeted for this study. Matrix, after washing aboard the dredge to reject oversize (+3/4") and fine colloidal material (-200 mesh), was transported by barge for final processing at a beneficiation plant located 27-30 nautical miles up the Savannah River on Hutchinson Island.

Comparative economics based on state-of-the-art technology and current conditions favor locating all of the processing and supporting infrastructure in a single facility on an offshore man-made artificial island. Construction of an island, in the center of the mining area, having a surface area of about 15 acres at Elevation +35.0 is proposed.

The same considerations apply to construction of the beneficiation plant, ancillaries, storage and load-out facilities on the island plant site as for a land side location. In addition to accounting for some increase in the cost of construction owing to the requirement for water-borne transportation of labor, equipment and materials, several specific additional requirements must be considered. These are; 1) getting electric power to the island, 2) providing potable water, and fresh water for de-salting concentrates, 3) standby power generation for minimum maintenance and safety during power outages, 4) worker accommodations, commissary, kitchen and dining facilities, and 5) transportation of workers and supplies. These extra facilities are no more than are ordinarily required of any remote plant site location.

Permitting requirements, once the concept is fully explained and understood, are likely to be less tedious and restrictive, and therefore less time-consuming and less costly. The post-mining use (after 25-30 years) of the island may prove to be an attractive and valuable asset to the environment, and local community.

Any one of several techniques may be employed for the design and construction of the island. One method is to simply dredge overburden material and place it hydraulically in the designated area. Overburden sands may be excavated by mining dredges and pumped to a single general location. The sands would pile up, assuming a natural angle of repose for fully saturated material until they were high enough above sea level to consolidate and permit spreading and leveling. The perimeter would be protected by continuous steel sheet piling, or by the construction of granite rip-rap, granite cobble and reinforced concrete armour.

Another technique would be to construct, on the perimeter, a rubble-mound breakwater using large granite rock and cobble. The inside of the breakwater cofferdam would be filled with dredged sand overburden material. Geotextile fabric placed on the inside stopes of the breakwater would contain the sand, and permit consolidation.

The estimate included in this report is based on island construction, using the average of the costs of the two techniques described above.

A technique which may offer the most potential for savings and economy of time is that of building all of the plant and support facilities, factory style, at land-side, and "sea-lifting" complete assemblies to the site. This concept has been around since the 1950's when refinery units were built in yards at Houston and shipped to Guatemala on commercial freighters. More recently, this concept, using barges on which oil refinery modules were assembled, was employed in the oil fields of Alaska's North Slope. This project could utilize this technology to advantage. All of the beneficiation plant process modules, support facility structures and wharfs would be constructed on the prestressed concrete "honeycomb" sandwich cell-type floating platforms. The platforms would be towed offshore to the plant site and grounded on the prepared sea floor. The advantage of precasting and segmental construction on-shore offers the opportunity for achieving high quality, economy, and speed. An additional feature of this construction is that it is likely to result in the least disruption of the marine environment. The honeycomb pattern lends itself to compartmentalization and can provide separate compartments for storage of different liquids.

Ocean-going vessel berthing will be accommodated by facilities located along the full length of one side of the island. Alongside and adjacent to the berths, a walled-in wet rock concentrate storage pile will be located. The wet rock storage capacity is based on the assumption that weather conditions occur to prevent vessels from arriving and berthing for loading a maximum period of 10 consecutive days. It is also assumed that an additional period of up to 5 consecutive days caused by mechanical breakdown, or other cause, would prevent ship loading. Ship loading would be conducted 320 days per year. Storage is provided based on production at 100% of design capacity (16,440 tonnes per day) for 15 days, or a total of 250,000 tonnes (1.9 tonnes/m³). The storage pile is contained in a concrete walled open-top structure, with a pitched floor to facilitate drainage and to collect water.

In plan, the storage structure will be 200 feet wide and about 700 feet long, with concrete walls about 30 feet high. Filled to wall height, about 250,000 tonnes of wet phosphate rock can be contained. In operation under normal conditions, concentrate would be piled an additional 15 feet to result in a trapezoidal cross-section. With this additional storage above the top of the wall, as much as 340,000 tonnes can be contained.

This storage pile will be served by combination stacker-reclaimer equipment, with a bridge spanning the total width which travels longitudinally the length of the pile. The bridge is supported by a hinged leg outside the storage wall. and a fixed leg on the wall. The bridge supports dual bucket wheel booms for reclaiming from the storage pile. The bridge also supports a tripper car, stacker belt, and chute. A belt conveyor from the beneficiation plant feeds the inflow cross belt via a tripper car. The cross belt at the back of the bridge's main girder loads the stack via a chute. The reclaiming bucket wheels feed a conveyor system which, in turn, feeds a ship loader with the capability of loading vessels at the rate of 3000-3500 tph. movements of the bridge type stacker/reclaimer, and its operating conditions, make automatic operation possible. The dual function of stacking and reclaiming are accomplished with the same traveling bridge mounted equipment. A trough, into which reclaimed material is collected for feeding the ship loader, permits reclaiming and ship loading. The bridge is about 260 feet long, spanning the storage pile and feeder trough (about 200 feet). The ship loader, with a cantilevered section extending out over the mooring berth, moves along the length of the dock to transfer and distribute concentrate for uniform loading of a vessel.

The berth, with mooring dolphins, will also permit off-loading of fuel, reagents, spare parts and other supplies required to sustain the island operation. Vessel loading and unloading can be accommodated in all but severe weather conditions, when vessels will be required to stand-off, under power, and/or at anchor until conditions permit returning to the berth.

- 1) Primary electric service will be supplied by a 750 MCM submarine cable at 115 kv, from Tybee Island by Savannah Electric and Power Co. The jacketed 750 MCM aluminum conductor will be encased in a 6" diameter conduit and cooled by a circulating oil bath. The conduit will be laid about five feet below the sea floor. A substation on the island will reduce voltage to 2.4, 4.16, and 6.9 kv, for distribution to load centers, as required.
- 2) Desalination of sea water will produce a high quality water suitable for human consumption, and for special uses such as boiler feed make-up, and

reagent solutions. Since the beneficiation process will use sea water for disaggregation, washing and flotation, the concentrate rock will contain a higher level of chlorides. The chlorides which are external to the phosphate particles may be removed by filtering and two-stage countercurrent washing with fresh water. Concentrate product washing by this process will require about 115 gallons of fresh water (desalinated to 150 ppm Cl-) per tonne of concentrate. Total fresh water required is estimated to be about 2,000,000 gpd. Desalination by state-of-the-art reverse osmosis HydroFuge units designed by World Water Treatment, Inc. of Concord, CA, is proposed. Each HydroFuge unit will produce approximately 300,000 gpd of fresh water (Cl- content less than 150 ppm) from 1,000,000 gpd of sea water containing about 35,000 ppm TDS, and 20,000 ppm Cl-. Six units are required to produce 2,140,000 gpd (1440 Eight units are provided; one for service during maintenance shutdown cycles and one as a standby to augment supply, if necessary. The HydroFuge R/O system and appurtenances is housed in a 10,000 ft<sup>2</sup> building. Raw water pumps capable of 6,000,000 gpd (4,200 gpm) are required to feed the R/O modules. Brackish water recovered after countercurrent filter-washing to de-salt concentrate is retained to supplement sea water make-up required for the beneficiation process. The enriched brine from the R/O system is returned to the sea. In addition, a fresh water ground storage tank of about 1,000,000 gallons capacity will be provided, (75' dia. x 30' side water depth.) The balance of the water supply system is the same as for any land side plant location.

- 3) Power outages are suffered by every user of commercially supplied power. The island location requires that minimum standby power be provided by an automatic starting diesel engine powered 60 Hz generator. Minimum power is required for lighting, heating, air-conditioning, potable and fire-fighting water systems, navigation lighting and personnel accommodations. This requirement will be met by a Caterpillar Model 3616 generator set, with automatic transfer switch, rated at 4000 kW. Fuel oil storage of 5,000 bbls in a 35' dia. x 30' high tank will be provided.
- 4) Personnel accommodations consisting of temporary housing, commissary, kitchen and dining facilities are required. Housing in dormitory type facilities will be provided for use by personnel during their two-week

tour (two 12-hour shifts, 14 days, 168 hours on three-week cycles). Housing will be sized to accommodate about 150 people. Cooking and dining facilities, including commissary with cold storage will also be designed to feed 150-160 people, 3 meals per day.

5) A motor launch will be provided to transport personnel and supplies from the island to the location of the turning basin in Port of Savannah. The launch will be seaworthy in all but severe weather conditions and capable of making ±30 knots so that a one-way trip takes no longer than one hour.

Matrix is pumped through a trailing pipeline terminating at the distribution head of the washer on the island. The matrix/slurry transportation pipeline is lengthened as mining progresses.

The two dredges are self-contained and, to a great extent, are self-sustaining. They require no direct service link to the island, or to land-side facilities, other than for re-supply and to transport workers. One ocean-going tugboat is assigned to service the mining operation. This tug is equipped with a rotating lift crane suited to at-sea maintenance and repair work. The tug moves and positions pipelines and the overburden waste discharge barge as mining progresses. This tugboat is also used to move the dredges to port for annual drydock maintenance and repairs.

All offshore operations will be based on work crew cycles of two weeks duty and one week off. This requires three completely staffed crews of operating, maintenance and supervisory personnel. While on duty, offshore personnel work 14 twelve-hour shifts, for a total of 168 hours each three week cycle. The wages for this work schedule is based on 40 hours per week, three weeks, 120 hours at regular time, and 48 hours at premium time. All meals and sleeping accommodations are provided by the enterprise at no cost to employees.

Accommodations, consisting of two-bed cabins, each complete with lavatory and shower, clothes lockers and desks are provided. Each offshore operating location contains its own accommodations. A fully-equipped kitchen,

provisioned commissary and staff will prepare and serve three meals each day in a dining room. Library, television, and indoor activity rooms will be provided. Physical exercise and conditioning facilities, both indoor and outdoor, will also be provided.

The island facilities will include a first-aid station, with a nurse, to attend to minor maladies and injuries. A heliport will enable the rapid evacuation of seriously sick, or injured, persons to mainland hospitals.

The configuration described above offers the opportunity to realize the commercialization of offshore mining. Mined matrix is delivered to a nearby beneficiation plant where it is upgraded to produce a commercial grade phosphate rock concentrate product. The wet beneficiation process uses sea water, except for final filter-rinsing with desalinated sea water to remove encrusted salt. The final product is loaded on commercial ocean-going transport vessels from an outdoor storage yard, by high capacity reclaimer and ship loader. The dock permits vessel loading of concentrate and vessel unloading of fuels, reagents, supplies, and other dry good commodities required to sustain operations. Utilization of the invested capital is maximized as the mining and beneficiation processes will continue to operate in all but hurricane weather conditions.

The final product is not calcined. Previous work by others, Zellars-Williams 1979, and DPRA 1987, considered calcination as a part of the beneficiation process. These reports indicate that grade is improved by about two BPL percentage points by calcination. No test work has been conducted to support this grade improvement. This report concludes that the benefit gained, solely that of improving  $P_2O_5$  grade, does not justify the expense incurred. Cash operating costs of calcination, as reported by Zellars-Williams 1979, adjusted to 1987, and DPRA 1987, vary from \$2.78 to \$3.22 per tonne. Return on the invested capital required for calcination adds \$2.50 to \$3.00 per tonne. The premium on penalty for each BPL grade percentage point is on the order of \$0.70-\$0.90.

The viability of this enterprise does not depend on producing 68 BPL phosphate rock concentrate. Many commercial chemical fertilizer plants use 66 BPL and lower grades for feed to manufacture phosphoric acid and diammonium phosphate (DAP). The supply demand forces of the world market, and particularly the requirements of chemical fertilizer producers within freight cost-effective shipping distances, will dictate viability.

The objective of the configuration selected for this economic feasibility evaluation is to produce a commercially marketable product at the least cost. Implementation economics will be satisfied when the demand for 4.8 million tonnes of 66 BPL phosphate concentrate becomes a reality.

#### 5.5 ESTIMATED CAPITAL COST

This section deals with the expenditures required to implement a phosphate mining-beneficiation operation having the configuration and features previously described. Estimated cost is based on conceptual and schematic designs, and is order-of-magnitude having an accuracy of plus or minus 25%.

#### 5.5.1 Capital Cost

Estimated capital cost has been prepared by a combination of generally accepted methodology. Island construction cost for building a 15-acre island by conventional civil-marine construction techniques has been prepared by preparing a survey of the quantities of the various work items and estimating the cost of each on an individual basis. Island construction cost includes all of the features required of an isolated offshore facility which would not be required of a conventional mainland site. The cost of island construction includes a ship loading dock as an integral part since no channel dredging is required. Table 5-16, Island Construction Cost Estimate, is a summary of cost by item for all the features included.

Beneficiation plant cost has been estimated for each production section; i.e., washer, feed preparation, flotation, reagents, water recirculation and waste disposal, product rinsing, wet rock storage, and support facilities, by

Table 5-16

Phosphate Mining Enterprise

Cost Estimate - Island Construction

Item	\$×1,000
Mobilization	\$ 350
Surveying	75
Navigation markers	30
Perimeter armor wall	7,500
Dredged fill	11,100
Vessel berth and dock	3,000
Mooring dolphins	250
Navigation aids	150
Submarine electric power service	12,500
Potable water plant and storage	150
Communications systems	100
Motor launch	500
Living accommodations	1,080
Kitchen, dining and recreation facilities	625
Standby generator 5000 kW	1,000
Fuel storage, 5000 bbl	125
Total	\$ 38,535

factoring techniques. Recorded costs of similar plants were compared by production process section for flowsheet applicability, adjusted for throughput or product capacity, and modified for specific dissimilarities. The resulting cost, reflecting the proposed capacity, was adjusted by applying the Engineering News Record (ENR) Construction Cost Index and the Chemical Engineering (CE) Plant Cost Index to determine current (May 1988) cost.

The procedure is to compare the process flowsheets and/or equipment requirements of the proposed plant section with that of a comparable plant section for which cost is known. The known cost estimate is modified to omit items not required of the proposed plant. Cost is adjusted for throughput (annual tonnes of matrix), or for product (annual tonnes of wet rock concentrate) by the ratio of these raised to the 0.7 power. This cost is modified for additions to the plant section, if required, of the proposed plant section. Current cost is determined by applying a multiplier. The multiplier reflects the difference in cost between the date of the known cost and May 1988 by a ratio of the average of ENR and CE indices. No attempt has been made to prepare an itemized equipment list for the beneficiation plant.

Dredge costs have been estimated by preparing a conceptual design with a general description of the principal components. Each dredge is a complete self-sustaining unit designed to remain at sea in all weather conditions. The principal machinery, equipment and structural components are identified, sized, and the weight of each estimated. Cost is the summation of the individual cost of the components. Table 5-17, Dredge Cost Estimate, is a summary of cost by item for each component. The design and construction of the dredges would be undertaken by one of several U.S. manufacturers as a result of a controlled procedure of design/construct competitive bidding. For purposes of this study, the cost of the two dredges is identical, whereas in the case of actual implementation, this may not be true. Dredge cost includes startup, acceptance testing, and commissioning.

The cost of special features and other items is estimated as the result of research of in-house data and telephone conversations with manufacturers, vendors, suppliers and other various experts.

Table 5-17

Dredge Cost Estimate

	Weight Short Tons	Cost \$X1000	_
<u>Hull-platform</u> (90' x 400' or 100' x 360')	3,000	\$ 9,000	0
Upper Deck House 9,2000 ft <sup>2</sup> houses bridge, operations, personnel accommodations, kitchen, dining, etc., including furnishings	235	920	0
Lower Deck House 8,000 ft <sup>Z</sup> house switchgear, generators, deck pump, other machinery	200	480	0
$\frac{\text{Heliport}}{40' \times 40'}, \text{ aft overhung}$	200	70	0
Fabricated Steel Components Ladder, ladder superstructure, 8 spuds, spud carriages, etc.	2,450	12,24	0
Machinery Dredge pumps, cutterhead, motors, speed transmission, generators, hydraulic systems, winches, hoists, etc.	610	7,24	0
Switchgear Electric controls and wiring	10	85	0
Navigation and Weather Equipment Radar positioning gear and weather station	3	15	0
Mass Flow Meter (Producion meter) meters, recorders, instrumentation	5	20	0
Communications VHF, AM-FM, TV, radio telephone	2	15	0
Heating, Ventilating and Air-conditioning Upper and lower deck houses	10	20	10
Spud Hoist and Carriage System Instrumentation and controls	1	15	0
Tools, Specialty Maintenance Equipment and Supplies	15	25	0

# Table 5-17 (continued)

	Weight Short Tons	Cost _\$X1000
Protective Coatings and Cathodic Protection	1	750
Engineering Preliminary engineering, modeling, design engineering and detailed engineering fabrication		1,500
Other		
Undefined development expense	N.	500
Transportation Shipyard to site by sea	***	180
Commissionning Startup, operating training and performance testing		2,000
Total Estimated Cost		\$ 37,460
Fuel, supplies, and personnel	1,808	
Total Estimated Weight	8,550	

Table 5-18, Phosphate Mining Enterprise Total Facility Capital Cost Estimate, is a summary of the total capital cost required to construct the offshore phosphate mining facilities described in this section. Fifteen percent is included as an allowance for costs which will be incurred for items not now predicted. Total capital costs include design, engineering, procurement, and construction management services as are applicable to each item.

## 5.5.2 Pre-production Cost

Pre-production cost in the amount of 10 million dollars is included as a part of the total investment required to implement the proposed enterprise mining scheme. This cost is intended to include the extensive drilling, sampling, and testing programs required to accurately identify the areal extent and gradequality characteristics of the Middle Miocene targeted for exploitation. This cost is also intended to include the cost of limited studies required to obtain This program would include exploratory drilling to the extent required to describe and define economically mineable reserves, based on the most effective beneficiation process flowsheet developed by the test work. This program includes the cost of bulk sample collection and a pilot plant test program to verify and refine the process flowsheet, material balances, reagent and water consumption, and recovery efficiencies such as are required to provide criteria and parameters for design and detail engineering. No interest is charged for the use of this money because it is assumed that these expenditures are in the nature of the regular research and development costs incurred by enterprises engaged in commercial minerals exploitation. Payback of pre-production/development cost is, however, included as a part of the total investment required by the enterprise.

The importance of environmental considerations and the related concerns of marine fisheries and others are not to be underestimated. The pre-production cost described herein does not include the cost of comprehensive environmental studies, or the preparation of an EA or EIS. It is unlikely that the private sector alone would undertake these kinds of studies without substantial incentive. Estimating the cost of such studies is beyond the scope of this report.

Table 5-18 Phosphate Mining Enterprise - Total Facility

Capital Cost Estimate
(4.8 x 106 tonnes/year product)

<u>Item</u>	_\$	Cost X1000_
Island Construction	\$	42,400
Overburden and Matrix Dredges		74,920
Trailing Pipelines		4,405
Overburden Water Barge and Tremie		1,210
Tugboats (2)		5,000
Washer Section		3,289
Feed Preparation Section		19,389
Flotation Section		26,565
Reagents Storage and Supply Section		2,240
Water Recirculation and Waste		18,471
Desalination and Water Storage		7,073
Desalt Rinsing Section		1,500
Wet Rock Storage		10,909
Stacker Reclaimer Shiploader		15,000
Buildings, Warehouse and Support Facilities	_	11,098
Totals	\$	243,469
Contingency - 15%	_	36,521
TOTAL	<u>\$</u>	279,990

This program will be conducted over a period fo 24-30 months and will be followed by a comprehensive economic analysis based on the latest market supply-demand price scenarios. A list of the tasks/objectives to be accomplished during this pre-production period before design and detailed engineering is undertaken is listed below.

- o drilling
- o sampling
- o geologic database update
- o bench scale test work
- o economic cutoffs applied
- o reserves estimates
- o bulk sampling
- o pilot scale test program
- o fresh water rinse tests
- acidulation test work to determine amenability of concentrate to acidulation of fertilizer manufacture
- o preliminary mine plan
- o preliminary design of dredges and ancillaries
- o island construction engineering alternatives evaluated
- o environmental issues identified
- o cost and likelihood of permitting estimated
- o lease and royalty fees/costs established
- o capital cost estimates
- o implementation plan and schedule
- o supply-demand and market scenarios
- o identify potential market
- o current product selling price
- o bankable document report.

The decision to move forward to implementation by contracting for detailed engineering, procurement, and construction can be taken with a high degree of confidence in the reliability of the economic analysis. Technological and economic risks will have been reduced to an acceptable level. If the economics are favorable and the market supports sales price and demand premises, the final phase of implementation can be initiated.

## 5.5.3 Replacement Capital

The employment of capital to replace equipment when its useful life has expired is replacement capital. Useful life is based on the concept that the level of maintenance is as required to keep the equipment (facilities) operational at an acceptable level of production. Useful or economic life is the period (time in years) until the failure rate increases to such an extent that it is no longer economical to operate.

The proposed mine-beneficiation complex operation and production is based on certain mechanical availability. This level of mechanical availability is the result of regular and scheduled shut-down maintenance. This maintenance for parts, supplies, and labor, in the amount of \$12,000,000 per year, is included in operating cost.

The severe service and adverse climatic environment requires a high level of regular and preventive maintenance. During one month of the year when all facilities are shut down while the dredges are in dry-dock, certain capital will be employed to sustain the equipment and facilities at design production capability. The additional sum of one million dollars per year is allowed as replacement capital. It is anticipated that this will maintain facilities at design level for a period of 30 years, without requiring the employment of additional replacement capital. The only exception is in the event technologically superior replacement equipment is warranted as justified by the economics of increased production.

#### 5.5.4 Working Capital

Ordinary operation of a business involves a circulation of <u>capital</u> within the current asset (capital cost) group. <u>Cash</u> is expended for materials (parts, supplies, expendibles), labor and services (electric energy, rental, fees, royalty, ...) and these expenditures are accumulated as costs. These costs are converted (wet rock inventory stock pile) into receivables and ultimately (back out by shipment) into cash again.

- o The average time intervening between the acquisition of materials or services and expenditure for labor entering this process and final cash realization constitutes an operating cycle.
- o The amount of capital committed (taken out of current funds or borrowed) to this cycle is working capital.
- o Cost of working capital (interest) is added.

To simplify economic analysis, the working capital requirement for this enterprise is estimated to be \$3.6 million, which is equal to the total production cost of 250,000 tonnes of phosphate rock concentrate for a period of 75 days (15 days supply in storage, plus 60 days for collecting receivables). To simplify economic analysis, working capital of \$3,600,000 is used throughout and recovered in the last year.

# 5.5.5 Comparable Capital Cost Estimates

Previous studies of the potential feasibility for commercial exploitation of offshore U.S. Atlantic coast phosphorites have produced capital cost estimates of the investment required.

ZW (1979) and DPRA (1987), each reported capital costs for development of phosphate mining and beneficiation facilities. The cost estimated for each of those studies envisaged offshore mining, on-board scalping/washing and partial desliming, transport of this intermediate product to land, beneficiation and product load-out from a central land-based complex.

The two estimates cover very similar methods of handling and processing matrix and the treatment of beneficiated concentrate. Each estimate has been adjusted for annual volume throughput, product output, and indexed to a comparable economic cost basis. Table 5-19 is a display of costs for annual finished product capacity of 4.8 million tonnes, comparable to the cost estimated for this study.

The table shows reasonable agreement, except for sea transportation cost. If this cost is equalized for the two estimates at the higher cost, the variance between the two estimates is within 5% for wet rock facility cost, and 14% for total facility cost.

Table 5-19

Comparable Capital Cost Estimates from Previous Studies

Adjusted for Capacity and Cost Index

(approximately 4.8 million tonnes product)

		\$ × 1,000	
<u>Item</u>	DPRA	Z-W	Equalize to DPRA
Dredge	\$ 36,660	\$ 31,340	
Scalping/Washer (on-board)	6,240	3,290	
Feed Preparation (land-based)	15,080	19,390	
Flotation Plant	13,280	26,570	
Reagents Section	-	2,240	• •
Water Supply, Recirculation and Waste	22,770	18,470	
Infrastructure	26,220		
Off-sites		14,040	**
Sea Transportation	232,950	51,460	181,490
Unloading Rock	25,750		==
Wet Rock Storage		14,230	
	\$378,950	\$181,030	\$362,520
Contingency	37,900	18,100	36,250
Total Wet Rock Facility	\$416,850	\$199,130	\$398,770
Calcination*	\$110,890*	\$ 68,620	
Contingency	11,090	6,860	
Total Calcination*	\$121,980*	\$ 75,480	
Total Facility	\$538,830	\$274,610	\$474,252

<sup>\*</sup> includes product storage/handling

NOTE: DPRA (1987) and ZW (1979) costs adjusted by ENR Construction Cost Index to 1988, and factored for through-put and production output to ZW (1988) study basis.

This discussion is not intended to be a critique of previous estimates, but is included here as a basis for comparison. Such variance is to be expected from estimates based on conceptual designs and preliminary definition of conditions.

The total costs estimated, at different times, by each of two investigators, are for comparable configurations providing conventional facilities at landside locations. The total wet rock facility cost of about \$400 million is comparable to the proposed totally offshore facilities' configurations estimated cost of \$280 million.

#### 5.6 ESTIMATED OPERATING COST

In view of the uncertainties in geology and production configuration, a detailed operating cost breakdown is not indicated. Zellars-Williams has compiled cost information on phosphate plants for many years and developed a relationship of costs to production for different geological and operating conditions. These relationships are broken down into operating modules and compiled in a computer model. This computer model has been used extensively in projects such as the World Phosphate Study 85, and the Assessment of Alternative Technology Study, for the Florida Institute of Phosphate Research (FIPR), as well as for evaluating performance of numerous operating mines.

Three cost modules specific to the offshore mining configuration were developed to make the cost model applicable to most of the operations. Cost of transportation and accommodations for personnel, and for product rinsing were estimated separately. All ZW operating cost models are based on short tons. Conversion to metric tons is performed for economic analysis. The expression ton in this report is for 2000 lbs. The expression tonne is for 2205 lbs. A copy of the cost model computer printout (pages 1 through 9 of 9) is included at the end of this section. The modules applicable to offshore Georgia are described in the following text.

#### Labor Costs

Labor costs are based on hours consumed for actual production functions. To this, a factor of 26% is added to allow for extra men, foremen, supervisors, and managers. The factors for each division follow:

Additional men	5%
Foremen	16%
Supervisors	3%
Managers	2%
Total	26%

The average rate used for labor is \$17.14 per hour, and includes overtime and fringe benefits.

The basis of this average rate is as follows:

Average hourly wage	\$	12.00
Burden, including fringes		3.00
Total Average Hourly Rate	\$	15.00
Premium Average Hourly Rate	\$	22.50
Work Cycle each 3 week period:		
120 hours @ \$15.00 =	\$1	,800.00
48 hours @ \$22.50 =	1.	,080.00
168 hours =	\$2.	,880.00

Average hourly wage:  $\frac{$2,880}{168 \text{ hr.}} = $17.14/\text{hour}$ 

## Administrative Costs

A figure of \$1.30 was used. This includes clerical, engineering support, planning, accounting, personnel, payroll, safety, legal, and all other local administrative, technical, and laboratory services. This does not include sales expense, taxes, insurance, exploration drilling, depletion, depreciation, or amortization.

#### Unit Costs

Unit cost for utilities, reagents, and other items are given on page 1 of the computer printout.

Estimated operating costs taken from the cost model, rounded and converted to metric units are given in Table 5-20. Indirect and offshore costs are individually estimated by other techniques. This is the basis of economic analysis.

The control units are the factors upon which the consumption factors are based. The consumption factors for each module are listed below.

#### Slurry Pumping of Matrix

This module covers the cost of pumping matrix slurry from the slurry well (pit) at the mine cut near the dragline to the washer, the first production unit in the beneficiation plant. Cost includes all the slurry pumps, pipeline, electric power supply, switchgear, control systems, and all appurtenances required for the matrix pumping system. All components are skid mounted. Cost includes seal water supply systems. Pit pump operation is included except for moving cost, which is a part of hydraulic monitor cost. Cost developed by this module is a function of distance based on transporting 1,000 tph of matrix (dry basis) at 30% solids average (by weight) and a pipeline velocity of 15 fps.

The model for this study is modified to cover the slurry density, pipeline size and lengths, and total system head conditions applicable to the offshore mining configuration described.

COST UNIT: Dry ton-miles matrix

UNIT CONSUMPTION:

Fuel

0.0866 gal.

Operating labor .00046 manhours

Operating supplies \$.00197

Maintenance labor .00046 manhours

Maintenance supplies \$.01194

Table 5-20
Operating Cost
4.8 million tonnes/year

# Direct Cost

Unit Operation/Item	\$/tonne product (wet rock, dry basis	)
Mining Overburden dredge and disposal Matrix dredge Matrix pumping	1.60 1.50 1.30	
Beneficiation		4.40
Washer	1.10	
Feed preparation Flotation	0.85 3.03	
In-process storage	0.20	
Hydraulic station	0.22	
Wasta Dispessi / Water Daylematics		5.40
Waste Disposal/Water Reclamation Tailing waste	0.60	
Slimes waste	0.51	
Make-up water	0.04	
Product Management		1.15
Rinsing and conveying	0.30	
Handling and storage	0.25	
Load-out	0.25	
		0.80
Supervisor, clerical and technical support		1.40
Offshore accommodations (personnel live and travel)		0.45
Direct Cost	\$	13.60
Indirect Cost		
Administration	0.20	0.20
Sales expense	0.25	0.25
Royalty @ 5% of sales price (\$35 & \$42)	1.75 to	2.10
Taxes (ad valorem, etc.)	0.20	0.20
Other (not specifically identified)	0.25	0.25
Indirect Cost	\$ 2.65 \$	3.00
Total Operating Cost:		
(a \$35 sales price)	\$16.25	
(a \$42 sales price)		16.60

#### Washer

This module consists of ore disaggregation, and separation and washing of pebble. A common washer includes a trommel, static screens, vibrating screens, and log washers. Battery limits are from the matrix pumping system discharge to the feed distributor for the primary cyclones and the pebble transfer conveyor.

COST UNIT: Tons matrix UNIT CONSUMPTION:

Electricity

2.25 KWH

\$.001

Operating labor

.00195 manhours

Operating supplies

Maintenance labor

.00199 manhours

Maintenance supplies \$0.05114

#### Feed Preparation

This module represents two stages of desliming and includes feed sizing and in-process storage of feed. Battery limits are from primary desliming cyclone feed distributor to the flotation feed dewatering or conditioning.

COST UNIT: Tons Flotation Feed

UNIT CONSUMPTION:

Electricity

3.00 KWH

Operating Labor

.00148 manhours

Operating Supplies

\$.00076

Maintenance labor

.00151 manhours

Maintenance supplies \$0.03881

#### Flotation

This module includes anionic rougher flotation for two size fractions, deciling, and cationic cleaner flotation. Battery limits are from discharge of flotation feed prep to the tails discharge point and the flotation concentrate discharge point.

COST UNIT: Ton Flotation Feed

UNIT CONSUMPTION:

Electricity

3.50 KWH

Operating labor

.00594 manhours

Operating supplies

\$.00305

Maintenance labor

.00606 manhours

Maintenance supplies

\$0.15577

### Reagents:

 Fatty Acid
 1.0 lb

 Fuel Oil
 1.25 lb

 NaOH/NH3
 .4 lb

 H2SO4
 1.3 lb

 Amines
 .17 lb

 Kerosene
 .1 lb

## In-Process Storage (Product Bins)

This module is for wet bin storage and retrieval of product. Battery limits are between product discharge from the washer and flotation plant to the product conveyor.

COST UNIT: Tons Product (as derived from flotation feed tons)

UNIT CONSUMPTION:

Electricity

.18 KWH

Operating labor

.00074 manhours

Operating supplies

\$.00030

Maintenance labor

.00075 manhours

Maintenance supplies

\$0.1941

## Hydraulic Station

This module is for operation of a plant hydraulic station. Battery limits are from the water collection points of recycled water from other modules, to the make-up water supply points in other modules.

COST UNIT: 1,000,000 gallons

UNIT CONSUMPTION:

Electricity

700 KWH

Operating labor

.30140 manhours

Operating supplies

\$.15498

Maintenance labor

.30743 manhours

Maintenance supplies

\$7.90

## Slurry Pumping of Tailings

This module is for hydraulic transport of tailings as a function of pumping distance to the disposal site. Tails are fed directly from the flotation plant. Battery limits are from the tails slurry pump to discharge from the tails pipeline at the sand-clay mix tank thickener.

## COST UNIT: Ton-Miles Tailings

#### UNIT CONSUMPTION:

Electricity

.76 KWH

Operating labor

.00046 manhours

Operating supplies

\$.00197

Maintenance labor

.00046 manhours

Maintenance supplies

\$.01194

Replacement pipe

\$.0015/ft.

## Slurry Pumping of Slimes

This module accounts for hydraulic transport of slimes as a function of distance to the disposal site. No credit is implicit in this module for gravity flow. Therefore, unit consumptions should be estimated on the basis of actual pumping distance. Battery limits are from the high grade sand-clay mix thickener to the end of the waste pipe discharge in mined-out cuts.

## COST UNIT: Ton-Miles Slimes

#### UNIT CONSUMPTION:

Electricity

1.15 KWH

Operating labor

.00141 manhours

Operating supplies

\$.00604

Maintenance Labor

.00142 manhours

Maintenance supplies

\$.03661

Pipe replacement

\$.00016/ft.

#### Make-up Water

This module accounts for fresh water pumped from deep wells as the source supply to make up for system losses. The basis is 7,500 gpm pumped a distance of one mile from a water level of 150 feet below the center line of discharge. The battery limits are from the deep aquifer water level surface to the hydraulic station. For the offshore situation this module is used for the cost of pumping sea water.

COST UNIT: 1,000,000 gallons

UNIT CONSUMPTION:

Electricity 850 KWH

Operating labor .301 manhours

Operating supplies \$.51591

Maintenance labor .30501 manhours

Maintenance supplies \$7.82

#### Conveyor

This module accounts for transportation by conveyor belt a distance of 600 feet with a 50-foot rise in elevation. The battery limits are from the product bin discharges to the conveyor belt discharge above the stockpiles.

COST UNITS: Tons of Product

UNIT CONSUMPTION:

Electricity .05 KWH

Operating labor .00011 manhours

Operating supplies \$.0023

Maintenance labor .00011 manhours

Maintenance supplies \$.00286

#### Storage

This module accounts for open pile storage of phosphate pebble and concentrate. Stacker and reclaimer factors are included. Battery limits are from the end of the transportation conveyor to the storage pile by stacker or tripper.

COST UNIT: Ton Product UNIT CONSUMPTION:

Electricity

Operating labor .00351 manhours

Operating supplies \$.02166

Maintenance labor .00355 manhours

Maintenance supplies \$.09114

#### Loadout

This module covers getting product from storage to the rail car. Battery limits are from the reclaimer which retrieves material from the wet rock pile to placement into the rail car. In this case, cost is for loading ocean-going vessels.

.22 KWH

COST UNIT: Ton Product UNIT CONSUMPTION:

Electricity .20 KWH

Operating labor .00351 manhours

Operating supplies \$.01203

Maintenance labor .00355 manhours

Maintenance supplies \$.09114

#### Offshore Dredge Mining Cost Modules

Three unique models were added for offshore Georgia. These are: dredge mining overburden, dredge mining matrix, and barge transportation. These modules are described below:

#### Dredge Mining Overburden

This module covers the cost of mining overburden and pumping it to nearby mine cuts. It is keyed-off of a dredge program for cost inputs. For the selected system, the unit consumptions follow.

COST UNIT: Cubic yards overburden

UNIT CONSUMPTION:

Fuel

.09798 gallons

Operating labor

.00489 manhours

Operating supplies

\$.01245

Maintenance labor

.00153 manhours

Maintenance supplies

\$.061

### Dredge Mining Matrix

This module convers the cost of mining matrix and pumping it to the surface. From here the matrix pumping module takes over. This module is keyed off the dredge program for cost inputs. For the selected system, the unit consumptions follow.

COST UNIT: Cubic yards matrix

**UNIT CONSUMPTION:** 

Fuel

.11286 gallons

Operating labor

.00796 manhours

Operating supplies

\$.02028

Maintenance labor

.00248 manhours

Maintenance supplies

\$.09936

#### Barge Transportation System

For configuration 2, barges were used to transport matrix from the dredge to the onshore plant, and transport waste back to the ocean disposal site. Loading and unloading costs are included in this module.

COST UNIT: Cubic yards matrix

UNIT CONSUMPTION:

Fuel

.2568 gallons

Operating labor

.0103 manhours

Operating supplies

\$.00722

Maintenance labor

.0088 manhours

Maintenance supplies

\$.05169

#### 5.7 ECONOMICS AND VIABILITY

### 5.7.1 Phosphate Market Evaluation

The United States, the leading world producer of phosphate fertilizers, supplies about 30% of world consumption. The long-established dominance of U.S. phosphate fertilizer producers in export markets, mainly from Florida and North Carolina, has been successfully challenged by the state-controlled phosphate producers of North Africa and the Middle East. The erosion of U.S. producers' share of total world markets by these state-controlled producers became evident as domestic consumption peaked in 1980-81, and since contracted. Global P2O5 fertilizer consumption appears to have levelled off and most forecasters suggest future growth at no more than 2-3% per year.

The U.S. phosphate rock industry capacity has grown from about 12 million tonnes per year in the 1950's to nearly 63 million tonnes per year in the 1980's. In the 1950's, U.S. production represented 50% of world-wide production. Today, U.S. production is only about 30% of world production.

The mature market demands of the U.S. agricultural sector for phosphate fertilizers are being met by domestic mines and rock producers, with minor exceptions. This demand accounts for about 19 million tonnes of phosphate rock (6 million P<sub>2</sub>O<sub>5</sub> tonnes). Morocco's OCP, from its Bou-Craa mine, is supplying a Gulf Coast U.S. fertilizer manufacturer with about 1 million tonnes of phosphate rock (370,000 P<sub>2</sub>O<sub>5</sub> tonnes). This rock is shipped after drying by OCP, but before washing to remove the salt water residue which results from beneficiation in sea water. Fresh water rinsing is accomplished at the site before the rock is fed to the chemical plant.

Current U.S. phosphate rock production is about 40 million tonnes per year (12.5 million  $P_2O_5$  tonnes), or 64% of capacity. Future demand and market scenarios which drive the industry are unlikely to require or justify any significant increase in this production. Meanwhile, however, exhaustion of economic reserves in areas being mined by present facilities will require that U.S. industry, mainly in Florida and North Carolina, invest in new

replacement mines and beneficiation plants. Some estimates indicate that as much as 30 million tonnes of new (replacement) capacity will be required between the years 1990 and 2005.

Total phosphate trade in  $P_2O_5$  tonnes (including rock, acids and fertilizer products) is projected in the following table.

## Total Phosphate Trade

	1975	<u>1980</u>	1985	1990	1995	2000
World (million tonnes $P_2O_5$ )	20.1	27.8	26.5	26.3	30.3	31.1
U.S. (million tonnes P <sub>2</sub> O <sub>5)</sub>	5.6	8.7	8.1	7.7	8.1	7.5
U.S. world share	28%	31%	30%	29%	27%	24%

The U.S. has adequate capacity in-place to supply this projected trade through 1996. A short-fall will be created if replacement costs (new mines and expansion of existing) cannot result in operations which yield favorable economic return.

Assuming stable markets and no significant new investment in new or replacement capacity, a short-fall in U.S. production of acid-grade phosphate rock as indicated in the following table is predicted.

## Million Tonnes of Rock

1997	-	1.8	2002	-	12.2	2007	-	21.8
1998	-	1.5	2003	-	13.2	2008	-	29.0
1999	-	2.4	2004	-	15.0	2009	-	30.3
2000	-	8.3	2005	-	15.0	2010	-	30.3
2001	-	12.2	2006	-	15.0			

This scenario would indicate, if present capacity is not replaced, that a market would be created in the year 2000 to support an alternative rock production scenario such as from offshore Georgia.

Acid-grade rock is that which is amenable to downstream chemical conversion, first to phosphoric acid and later to fertilizer products. Phosphate rock concentrates of grades 64-66 BPL  $(29-30\%\ P_2O_5)$  are routinely used by captive producers as feed stock for chemical conversion. This trend will increase as supplies of high grade rock world-wide are depleted.

Whether or not replacement capacity is realized will depend on economics. Replacement capacity will require new investment at the cost, in current dollars, of \$65 to \$90 per annual tonne of capacity, or a total of \$1.95-\$2.7 billion.

The lower required investment cost range applies where existing infrastructure can be utilized. The higher cost range includes some additional or new infrastructure. Higher costs will be incurred if totally new infrastructure is required.

Current and near-term future production costs of Florida producers operating existing mines and beneficiation plants provide one rational basis of comparison for any alternative domestic-sourced production. (See Table 5-21). This table shows direct cash cost of production and indirect costs for taxes, sales expense (Phosphate Rock Export Association) and insurance, plus items which account for the cost of money (interest), a minimum return on capital invested for physical improvements (amortization), and reserves (depletion).

To complete the comparison, the cost of handling, drying, transporting, and ship loading must be added to the FOB mine cost. These costs, common to both present and near-term future mines, consist of the following items.

## Dollars Per Short Ton (Dry Basis)

Freight to Port	\$3.40
Unload to Storage	.20
Drying (at port)	1.75
Port Storage	.65
(port charge)	
Vessel Loading	2.20
Total	\$8,20

Table 5-21

# Cost of Production

# Dollars Per Short Ton (dry basis)

		Current Mines		Near-Term Future Mines	
1.	Mining	\$2.45		\$ 4.24	
2.	Beneficiation	3.30		5.27	
3.	Waste Disposal, Land Reclamation and Water Re-use	2.44		4.53	
4.	Product Management	0.46		0.46	
5.	Admin., Clerical, Technical	1.30		1.30	
Cas	h Cost (Wet)		\$ 9.95		\$15.80
	Severance	1.35		1.35	
	Other taxes	0.50		0.50	
	Sales exp. (Phosrock)	0.50		0.50	
	Insurance	0.10		0.10	
	Sub-total		2.45		2.45
*	Interest on Working Capital	0.40		0.60	
**	Amortization of Investment (\$65/t)	9.75	(\$90/t)	13.50	
	Depletion	1.00		1.00	
	Sub-total		11.15		15.10
	Total Cost, Wet FOB Mine		\$23.55		\$33.35

<sup>\*</sup> Cash cost of 3 months production, 20 years @10%

<sup>\*\* 20</sup> years @ 15%

If all costs and expenses are allocated and a reasonable return on investment accounted for, as indicated in Table 5-21, Florida rock producers can put phosphate rock aboard vessels at Port Tampa for betwen \$31.75 and \$41.55 per ton (\$35.00 and \$45.81 per tonne), over the period 1988 through about 1992.

Current selling price of 68 BPL  $(31\% P_2O_5)$  phosphate rock loaded on vessels at Port Tampa is \$29.00 to \$30.00 per tonne. This pricing is in response to competitive pressure and is possible because most Florida producers have fully amortized the investments made when costs were lower, and/or are willing to sacrifice normally acceptable returns for sustained production and utilization of installed capacity.

Phosphate fertilizer producers will purchase and use 66 BPL  $(30.2\% P_2O_5)$  grade rock, if the quality makes it suitable for acidulation, etc., and if the selling price is attractive. Under certain market conditions a price penalty or premium is recognized when grade is much below or above about 68 BPL. The BPL grade point penalty, when market conditions warrant it, is generally on the order of \$0.70 to \$0.90, or \$1.40 to \$1.80 per tonne for 66 BPL rock.

Table 5-22 is constructed from these projections by adding current and estimated future freight, and port handling and ship loading costs. Return on invested capital at the rate of 15% is separately added to amortize the use of money. A 20% pre-tax profit based on cost is added for a total selling price which is the minimum considered necessary to attract investment in new or replacement facilities. Based on this analysis, a case can be made for predicting the selling price of 66 BPL wet rock in the year 1996 of \$34.00 to \$36.00 per tonne, and \$42.00-\$44.00 per tonne in the year 2000.

Economic analysis, therefore, is conducted on sales price of 66 BPL wet rock at \$35.00 per tonne, based on immediate implementation to achieve the first production in the year 1996. The most favorable scenario is to start production in 1999-2000 when it is more likely that a market will exist. Economic analysis is also conducted on a sales price of \$42.00 per tonne.

A charge for royalty or minerals severance tax estimated to be computed as 5% of the sales price is included, as indicated in operating cost Table 5-20, in the economic analysis.

An underlying premise of the economics and viability of the offshore configuration proposed is that implementation and subsequent production is based on having a market. The production from this enterprise needs to be committed on a long-term basis to chemical fertilizer producer customers. Limited storage of finished product is provided on the offshore island. The customer's production of phopshatic fertilizers must be linked to a continuous supply of phosphate rock feed stock from the offshore facilities. Storage of wet rock must be provided by the customer at his plant.

Table 5-22

Cash Cost per Annual Tonne Phosphate Wet Rock

Constant 1988 Dollars

	1988 - 1995	1996 - 2000
Average Wet Rock FOB Mine	\$13.25 - 14.35	\$14.77 - 15.10
Freight, Port Storage and Ship Loading	5.35 - 6.58	6.57 - 7.90
Total Cost Aboard Vessel	18.60 - 20.93	21.34 - 23.00
15% Charge on Invested Capital	9.75	13.50
20% Pre-tax Profit	6.00	7.00
Total Selling Price	\$34 <b>.</b> 35 <b>-</b> 36 <b>.</b> 68	\$41.84 - 43.50

## 5.7.2. Economic Analysis

The discounted cash flow rate of return on investment (DCFROR) method of economic analysis is used to evaluate the viability potential of exploiting offshore Georgia phosphate as proposed in this study. DCFROR is computed using computer-driven software programs adapted to this type enterprise. The computer software calculates to determine the rate of return at which the positive and negative cash flows, when discounted to the present, equal zero. The present value of cash outflow and inflow is computed to result in the lowest possible positive and negative net present values (NPV). This procedure is repeated for differing scenarios of investment, income (sales price) and operating cost to gain an understanding of sensitivity. All economic values are based on constant 1988 dollars.

Each scenario is represented by a separate computer run computation of DCFROR and net present value (NPV). A copy of each of the computer printouts for Case I and Case II is included at the end of this section.

Extraordinary costs associated with start-up are accounted for by taking into income 2.4 million tonnes of product sales, and taking as cost the production of 4.8 million tonnes. This procedure is used in each case.

Table 5-23 is a summary of DCFROR results for base case investment and operating costs, and for two sales price and revenue scenarios. The lower sales price is based on market penetration in the year 1996. The higher price is based on making market in 1999.

Table 5-23

	Sales Price	Construction Capital Millions	Production Cost	DCFROR
Case No.	\$/tonne	Dollars	\$/tonne	<del>%</del>
1	35	280	16.25	6.6%
II	42	280	16.60	12.2%

Table 5-24 is a summary of DCFROR results for two constant sales prices and revenue, constant production cost, and about 10% increments of change in investment.

Table 5-24

Case No.	Sales Price \$/tonne	Constructi Millions Dollars	on Capital Variance % +/-	Production Cost \$/tonne	DCFROR
I(a)	35	252	-10	16.25	8.4
I(b)	35	308	+10	16.25	5.0
II(a)	42	252	-10	16.60	14.1
II(b)	42	308	+10	16.60	10.6

Table 5-25 is a summary of DCFROR results for constant investment, two sales prices, and about 10% increments of change in production cost.

Table 5-25

6 1 6 1				
\$\frac{1}{5}\text{lonne}	Millions Dollars	Cost \$/tonne	Variance % +/-	DCFROR
35	280	14.80	-10%	8.0
35	280	17.70	+10%	5.1
42	280	15.15	-10%	13.3
42	280	18.05	+10%	11.1
	Sales Price \$/tonne 35 35 42	\$/tonne         Dollars           35         280           35         280           42         280	Sales Price \$/tonne         Capital Millions Dollars         Produc Cost \$/tonne           35         280         14.80           35         280         17.70           42         280         15.15	Sales Price \$/tonne         Capital Millions Dollars         Production Cost Variance \$/tonne           35         280         14.80         -10%           35         280         17.70         +10%           42         280         15.15         -10%

FILE: OPCOSTSE 29-A458 JWH 5/5/88

PAGE 1 OF 9 PHOSPHORITE SELECTED CASE OPERATING COSTS

MATRIE I	3.71	KNN	.045
TOTAL 1	9.78	OPERATING LABOR MM 17.14	H 17.14
TONS OF PRODUCT/YEAR	5.28	DIESEL FUEL GAL,	09.
OF SLINES IN MATRIX	24.30	A-FATTY ACID 0	.08
OF PEBBLE IN MATRIX	.00	D-FUEL OIL 0	.071
SAND TAILS IN NATRII	53,50	C-NADH/NH3 8	.075
OF FLOT. CON. IN NATRII	22.20	D-H2504 0	.025
MATRIX DRY DENSITY	1.22	E-ANINES D	.24
MATRII PURPING BISTANCE	2.84	F-KEROSENE 0	160.
SLINES PURPING DISTANCE	2.84		
TAILS PUNPING DISTANCE	2.84	36" PIPE KATRII	100
INICKNESS OF MATRIE	17.84	42" PIPE 0. B.	100
GALLONS/YR HYDR.STA.	21000	30 * PIPE MASTE	001
GALLONS/YR MAKE UP	3570		
CYD OVERBURDEN	32.09		
CYD MATRIX	19.59		
TORS MATRIE	23.80		
TONS SLINES	5.78385	9	
TONS SANDS	12.73399		
TONS PEBBLE			
IN TONS FLOT CON	5.28401		
DRE DENSITY WET	1.40		74
RATIO OF CONCENTRATION	3.4		48
FET OVERBURDEN	26.30		
ACRES/YEAR	756		
TONS/ACRE	4487		
ACRE FT SLINES/YEAR	14343		
FLOTATION RECOVERY 1	08		
MINE RECOVERY 1	90		
PROD. PEBBLE GRADE 18PL	63		
PROD.COM GRADE IBPL	65.92		
COMP.PROD. GRADE 19PL	99		
CLOT EFFO 1 RP!	24.2		

			***************************************				***************************************		京 日 日 日 日 日 日 日 日 日 日	
MODULE	CONSUMABLES	ELECTRICITY KMH/UNIT	OPERATING LADOR NH/UNIT	OPERATING SUPPLY 8/UNIT	MAINTENANCE LABOR NH/UNIT	MAINTENANCE LABOR NAINTENANCE SUPPLY RH/UNIT	FUEL GALLONS/UNTF	REAGENTS 0/UNIT	CONTRACT 6/UNIT	REPLACEMENT PIPE F1/UNIT
(a) OVERBURDEN DREDGE (b) NATRII DREDGE (d) SLURRY PUMPING NATRII	CY OVERBURDEN CY MATRII II MATRII TONS-MILE		.00489	.01245 .02028 .00197	.00153 .00248 .00046	.06100	.09798 .11286 .0866			.00030
BENEFICIATION (WORK AREA)	10 former consessed to A)						***************************************			HOLDS HOW AREA)
MODULE	CONSUMABLES	ELECTRICITY KWK/UNIT	OPERATING LADOR MH/UNIT	OPERATING SUPPLY \$/UNIT	MAINTENANCE LABOR TH/URIT	MAINTENANCE LABOR MAINTENANCE SUPPLY RH/UNIT	FUEL GALLONS/UNIT	REAGENTS U/UNIT (TOK FLT FD	CONTRACT 8/UNIT	REPLACEMENT PIPE Flunit
(e) WASHER	TOWS MATRIT	2.25	.00195	00100	.00199	.05114	-4	-		
(F) FLOTATION PREP	TONS FLOAT FEED	3.00	.00148	9.00076	15100.	.03861	-	1.25		
(g) FLOTATION	TONS FLOAT FEED	3,50	.00594	.00305	90900	.15577	. ٺ	₹.		
(h) IN PROCESS STORREE	TONS FLOAT FEED	700	10107	.00038	200075	. 01941	0			
						2	ىك م	<del>-</del> -		
MASTE DISPOSAL, LAND REC	WASTE DISPOSAL, LAND RECLAMATION AND WATER RE-USE (WORK AREA)	JE (NORK AREA)			2 2 2 2 2 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4					MASTE DISPOSAL, LAND RECLAMATION AND WATER RE-USE (MORK AREA)
MODULE	CONSURABLES	ELECTRICITY KWK/UNIT	OPERATING LABOR MH/UNIT	OPERATING SUPPLY 6/UNIT	RAINTENANCE LABOR MH/UNIT	RAINTENANCE LABOR NAINTENANCE SUPPLY #1/UNIT	FUEL GALLONS/UNIT	REAGENTS 0/UNIT	CONTRACT 8/UNIT	REPLACEMENT PIPE FT/UNIT
(j) SLURRY PUMPING TAILS TAILS TON MILE (t) SLURRY PUMPING SLINES SLINES TON MILE (i) Make up water 1,000,000 gallo	S TATIS TOW MILE ES SLIMES TOW MILE 1,000,000 GALLONS	.76 1.15 850	.00046	.00197 .00604185 .51591	.00046 .00142 .30401	.01194 .03841 7.82		**************************************		.00015 .00016
PRODUCT MANAGEMENT (WORK AREA)	**************************************					***************************************				PROUCT RANGERENT VOOR AREN
MODULE	CONSURABLES	ELECTRICITY KWH/UNIT	OPERATING LABOR NH/UNIT	OPERATING SUPPLY 9/UNIT	MAINTENANCE LABOR KH/UNIT	MAINTENANCE LABOR MAINTENANCE SUPPLY MA/UNIT 8/UNIT	FUEL GALLONS/UNIT	REAGENTS I/UNIT	CONTRACT 6/UNIT	REPLACENENT PIPE FT/UNIT
to) ChuufyOR	TOME PRODUCT NET	.05	1000.	1,000	00011	00284				
(o) \$108AGE	TOMS PRODUCT	.22	1500.	,02166	.00355	1160.				
(q) LOADOUT	TONS PRODUCT	.20	.00351	.01203	.00355	.09114				

MINING (VORK AREN) COST UNIT COST

	CONSUMABLES	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY NAIN. LABOR	MAIN. LABOR	MAIN. SUPPLIES	FUEL	REAGENTS	CONTRACT	REPLACEMENT PIPE	TOTAL
MODULE	UNITS	* PER UNIT	S PER UNIT	* PER UNIT	6 PER UNIT	8 PER UNIT	8 PER UNIT	S PER UNIT	1 NRI/8		8 PER UNIT
(a) OVERBURDEN DREDGE	CY OVERBURDEN	\$.000	6.084	\$.012	\$.026	1.061	\$.059			1.000	8.242
IN MATRIT DREDGE	CY MATRIE	£.000	6.136	8.020	8.043	\$.099	8.068			\$.000	\$.366
(d) SLURRY PUMPING NATRII NATRII TONS-HILE	T MATRIT TONS-HILE	000.9	\$.008	\$.002	1.008	\$.012	\$.052			6.030	1.112
BENEFICIATION (UDRK AREA) COST	) COST		141711111111111111111	041441494744444444	110211111111111111111111111111111111111	171711111111111111111111111111111111111					
***************	CONSUMABLES	ELECTRICITY	DPERATING LABOR	OPERATING SUPPLY	MAIN, LABOR	NAIN. SUPPLIES	FWEL	REAGENTS	CONTRACT	REPLACEMENT PIPE	TOTAL
NODULE	UNITS	S PER UNIT	\$ PER UNIT	S PER UNIT	6 PER UNIT	8 PER UNIT	6 PER UNIT	6 PER UNIT	\$/UNIT		s PER UNIT
(e) MASHER	TONS MATRIE	\$.101	f.033	1.001	6.034	\$.051					6.221
(f) FLOTATION PREP	TONS FLOAT FEED	6.135	\$.025	1001	\$.026	6.039					\$.226
IB) FLOTATION	TONS FLOAT FEED	\$,158	\$,102	£.003	£.104	4.156		187.3			\$.B03
(h) IN PROCESS STORAGE	TOWS FLOAT FEED	\$.008	8.013	\$.000	6.013	8.019					8.054
(i) HYDRAULIC STATION	1,006,000 GALLONS	631.50	\$5.17	1.15	\$5.27	67.90					645.99
ASTE DISPOSAL, LAND REC	MASTE DISPOSAL, LAND RECLANATION AND WATER RE-USE (MORK AREA)	ISTELLECT COLORS (E. LUCK AREA)	100404444444444444444444444444444444444		111111111111111111111111111111111111111						
	CONSUMBLES	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY	HAIM. LABOR	NAIN. SUPPLIES	FUEL	REAGENIS	CONTRACT	REPLACENENT PIPE	TOTAL
MODULE	UNITS	8 PER UNIT	s PER UNIT	s PER UNIT	\$ PER UNIT	S PER UNIT	S PER UNIT	8 PER UNIT	E/UNIT		s PER UNIT
(i) SLURRY PUMPING TAILS TAILS TON MILE	TAILS TON MILE	6.034	8.008	£.002	8.008	\$.012				\$.015	6.079
(I) SLUARY PUMPING SLIMES SLIMES TON MILE	S SLINES TON NILE	\$.052	\$.024	\$.006	\$.024	6.037				\$.016	\$.159
CITY MAKE HE WATER	1 000 000 CALLING	679 250	051.59	8.516	\$5.211	\$7.816					156.952

PRODUCT MANAGERIET (MORK AREA) COST

	***************************************	*************								Control of the Contro	
	5	CONSUMABLES ELECTRICITY	CONSUMABLES ELECTRICITY	OPERATING LABOR	OPERATINS LABOR OPERATING SUPPLY MAIN. LABOR	HAIN. LABOR	MAIN. SUPPLIES	S FUEL	REAGENTS	CONTRAC! RE	CONTRACT REPLACEMENT PIPE TOTAL
MODULE UNITS & PER UNIT & PER	UNITS		s PER UNIT S PER	8 PER UNIT	6 PER UNIT 6 PER UNIT	6 PER UNIT	# PER UNIT	\$ PER UNIT \$ PE	LUNIT 6 PER UNIT 6 PER UNIT 5 PER UNIT 5 PER UNIT 5 PER UNIT	\$/UNIT	UNIT 6 PER UNIT 6 PER UNIT 8 PER UNIT 8 PER UNIT 8 PER UNIT
(a) CONVEYOR TONS PRODUCT MET 6.002 8 (p) STORAGE TONS PRODUCT 6.010 8 (a) LOBBOUT TONS PRODUCT 6.009 6	TONS PRODUCT MET TONS PRODUCT TONS PRODUCT	13H 151	\$.002 \$.010 \$.009	\$.007 \$.060 6.060	\$.000 \$.027 \$.012 \$.012	00° 1.061	6.003 6.091				8.009 6.244 8.233

	VARIABLE	TONS OF PRODUCT	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY	MAIN, LABOR	MAÍN. SUPPLIES	FUEL	REAGENTS	CONTRACT	REPL. PIPE	TOTAL
		THE THE PARTY OF T	S PER TON PRODU	CT & PER TON PRODUCT	T & PER TON PRODUCT	T & PER TON PROD	S PER TON PROBUCT & PER TON PRODUCT	T & PER TON PROD	UCT & PER TON F	PRODUCT		
(4) OVERBURDEN DREDGE	CY OVERBURDEN	A. 67304	8 PM	6 CoB	4 674							
(b) MATRIX DREDGE	CY MATRIT	1 20741	900	90.00	0.070	VCI -0	5.3/0	1.32	\$.000	000.	1.000	61.470
(d) SLURRY PUMPING MATRIX MATRIX TONS-MILE	II RATALE TONS-KILE	10.52905	\$ 000	9.300	6.073	F. 138	9,368	1.251	000.9	000.1	1.000	\$1.358
TOTAL			8.000	181.097	6.021	8.084 8.084	5.126	8,547	000	0.000	4.318	\$1.178
ENEFICIATION COST	FEFE TO THE TOTAL	***************************************	100000000000000000000000000000000000000				7. 565	11.155	F. 000	8.000	f. 318	14.007
NODULE NAME	VARIABLE	TONS OF PRODUCT	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY	MAIN, LABOR	MAIN. SUPPLIES	FUEL	REAGENTS		REPL. PIPE	TOTAL
			S PER TON PRODUC	T S PER TON PRODUCT	* PER TON PRODUCT	S PER TOW PRODU	S PER TOM PRODUCT S PER TON PRODUCT S PER TON PRODUCT S PER TOM PRODUCT S PER TON PRODUCT S PER TON PRODUCT S PER TON PRODUCT	T & PER TON PRODU	ICT & PER TON P	ROBUCT		
MASHING	TONS MATRII	4.50450	8.656	8.151	£ 005	6.154	4 210					-
FLOTATION PREP	TONS FLOAT FEED	3.40991	6.460	6.086	6.603	8.08a	6.13					6.995
FLOTATION	TONS FLOAT FEED	3.40991	6.537	8.347	1.010	6.354	6.531		850 4			6.770
IN PROCESS STORAGE	TONS FLOAT FEED	3,40991	8.028	6.043	100.	6.044	\$.066					\$ 187
MTDMADLIC STALLON	1,000,000 BALLONS	.00397	t. 125	170.9	100.8	1.021	6.031					8.199
TOTAL ************************************	107AL 6.619 6.619 6.619 6.619 8.661 6.919 8.000 8.939 8.600 8.939 8.600 8.939 8.000 8.939 84.883 84.	72216468665500459500691	81.606 Betreetensters	8.648	f.019	1.661	\$.991 	\$.000	\$.959 101011111111111111111111111111111111		30 11111111111	\$4.885
MODULE NAME	VARIABLE	E	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY	MAIN. LABOR	MAIN. SUPPLIES	FUEL	REAGENTS	CONTRACT	REPL. PIPE	TOTAL
		בנע אשנישקוב	# PER TON PRODUC	T S PER TON PRODUCT	A PER TAN PRODUCT	S PER TAN BROKE	TOM PRODUCT S PER TOM PRODUCT & PER TRM PRODUCT & PER TAM PROMINT	A DCG TON BOOKE	FT & OCD TON DO	100 and 100 an		
	***************************************					The same of the sa	The state of the s	a ren son range	LI S FER 10R F.	KO PER IUN FRUDU		
SLURRY PUMPING TAILS	TAILS TOW MILE	6.84114	6.235	\$.054	\$.013	\$.055	6.082				<b>f.</b> 103	\$.542
MAKE HP NATER	1 DOD DOD CALLONE	3.10863	1.161	5.075	4.019	1.076	1.114				1.049	8,493
TOTAL	ויייייי מאנינות	Banno.	9.029	6,003	000'\$	\$.004	\$.005					1.038
PRODUCT MANAGEMENT COST	FRODUCT RANGEMENT COST		111111111111111111111111111111111111111	7.135 14110111111111111111111111111111111111	6.033	7.154 11101564D198884	6.201	\$,000	\$.000	\$.000	¢.152	\$1.074
MODULE NAME	VARTARIE	TOWE OF BOOMICE	Electorate	Some - Turing	20.2							***************************************
9			CECEINICIII	UTERMING LABOR	UPERRIING SUPPLY	MAIN. LABUR	NAIN. SUPPLIES	FUEL	REAGENTS		REPL. PIPE	TOTAL
		200	* PER TON PRODUCT	T & PER TON PRODUCT	S PER TON PRODUCT	S PER TON PRODUK	TON PRODUCT & PER TON PRODUCT & PER TON PRODUCT \$ PER TON PRODUCT \$ PER TON PRODUCT 5 PER TON PRODUCT & PER TON PRODUCT	# PER TON PRODUC	T S PER TON PR	ODUCT		TOTAL
CONVEYOR	TONS PRODUCT WET	1.17647058824	\$.003	\$.002	\$.000	\$.002	8.003		-			110 \$
STORAGE	TONS PRODUCT	_	\$.010	\$.060	\$.022	190.9	1.00					284
LUADOUI	TONS PRODUCT	_	\$.009	\$.060	6.012	190.8	6.091					8,233
10174			***									

PAGE 5 OF 9

	6 PER SHORT TOW OF PRODUCT	rkunner										
(MORK AREA)	ELECTRICITY	OPERATING LABOR OPERATING		SUPPLY KAIN LABOR	NAIN SUPPLY	FUEL	REAGENT	REPL. PIPE	CONTRACT	CONTRACT ADMIN,CLER,TECH CAP-AMORT		TOTAL
MINING	8.000	\$1.097	\$.172	\$.400	\$.865	11.155	6.000	6.319				64.007
BEWEFICIATION	\$1.606	\$.648	\$.019	1991	8.991	1.000	6.959	\$.000			000.9	64.885
MASTE, RECLAIM AND MATER	1.422	\$.133	6.033	8.134	8.201	000.	000.9	\$.152	\$.000			\$1.074
PROD MANAGEMENT	6.022	1.123	1.034	6.124	\$.186	\$.000	\$.000	000.8				6.488
ADRIN, CLER, TECH										61.300	2	81.300
TOTAL	\$2.050	\$2.000	6,250	11.319	62.243	41.155	6.959	8.470	1.000	81.300	8.000	\$11.753

2 OF LUDRIK AREA) COST BY MODULE

CONSUMABLES	ELECTRICSTY	OPERATING LABOR	OPERATING SUPPLY	MATNTENANCE LABOR	HAINTENANCE SUPPLY	r FUEL	REAGENTS	REPLACENENT PIPE	2	TOTAL
	1 NINE COSTS	I MINE COSTS	T KINE COSTS	I KINE COSTS	I NINE COSTS	I MINE COSTS	I NIME COSTS	I MINE COSTS	H	NINE COSTS
(4) DVERBURDEN DREDGE	.00	12.69	1.69	3.96	1.25	16.0	.00	.00	F	36.70
IN MATRIX DREDSE	00	12.62		3.94	4.19	6.27	90.	00.	n	13.09
I SLURRY PURPING NATRIT	00.	2.07	.52	2.09	3.14	13.65	00.	00.	2	29.41
TOTAL	00.	27.38	4.28	1.31	21.50	20.03	00.	7.94	-	100.00
BENEFICIATION INORK AREA) 2 OF 10TAL	2 OF 101AL	900000000000000000000000000000000000000		01001011100110011						DE REFIGIALION NOTA RARA Z OF 107A.
CONSUMABLES	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY	MAINTENANCE LABOR	MAINTENANCE LABOR MAINTENANCE SUPPLY	Y FUEL	REAGENIS	REPLACEMENT PIPE	01	101A.
MODULE	1 BENEF. COST	1 DENEF. COST	1 DENEF. COST	I DENEF. COST	I BENEF. COST	T DENEF. COST	I BENEF. COST	I BENEF. COST	н	I DENEF, COST
(a) WACUED	9.76	1.0R	60.	3.14	4.72	00.	80.	90.	~	10.37
ILL ELITATION PREP	9.42	1.77	15	=	2.71	8.	00.	00.	-	15.76
(a) FLOTATION	10.99	7.11	.21	7.25	10.87	00.	19.63	.00	νñ.	56.06
(h) IN PROCESS STORAGE	.87	-66	.03	.90	1.35	.00	00.	90.	•	3.74
(1) HYDRAULIC STATION	2.56	.42	10.	.63	.64	00.	00.	00.	•	4.07
TOTAL	12.88	13.27	04.	13.53	20.30	.00	19.63	00.	_	100.00
ANSTE DISPOSAL, LAND RECLAMATION AND WATER RE-USE (MORK AREA)	HALLOWER AND MATER RE-US	SECONDATIONS SERVICE (NORK AREA)				111111111111111111111111111111111111111	***************************************			HASTE DISPOSA, LAND RECLAMATION AND WATER RE-USE (MORK AREA)
CONSUMABLES	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY	MAINTENANCE LADOR	NAINTENANCE LADOR NAINTENANCE SUPPLY	Y FUEL	REAGENTS	REPLACENENT PIPE	CONTRACT TO	TOTAL
MODULE	1 M.D., M.R. COST	I M.B., W.R. COST	I W.D., W.R. COST	I W.D., W.R. COST	I W.D., M.R. COST	I W.D., W.R. COST	X M.B., W.R. COST	X N.D., N.R. COST 1	Z M.D., M.R. Z	1 M.D., W.R. COST
							90	6.13		60 60
(j) SLURRY PUMPING TAILS	21.91	2.02	1.26	7.0	10.40	00.	00.	4.54	. ~	45,92
(1) MAKE UP WATER		.32	.03	: n	.49	90.	00.	00.	3	3.50
19.29 12.34 3.04 Product makagenent (Work Area) I of Total CGST	39.29 ***********************************	12.34	3.04	12.47	18.70	90.		14.17	90.	12.47 18.70 .00 .00 .00 14.17 .00
CONSUMABLES	ELECTRICITY	OPERATING LABOR	OPERATING SUPPLY	NATWTENANCE LABOR	MAINTENANCE LABOR MAINTENANCE SUPPLY	Y FUEL	REAGENTS	REPLACENENT PIPE	2	TOTAL
MODULE	Z PRÔ.MAN. COST	I PRO.MAN. COST	I PRO.MAM. COST	1 PRD.MAM. COST	I PRO.NAN. COST	I PRO.MAN. COST	X PRD.MAN. COST	I PRD.MAN. COST	ы	PRO.MAN. COST
CA) CONUEVOR	85	.45	.06	.46	69.	.00	.00	.00	1	2.24
IN CONTESTOR	2.01	12.34	¥.9	12.46	18.69	00.	00.	00.	•	49.96
(4) LOABOUT	1.85	12.36	2.47	12.46	18.69	00.	00.	00.	-	47.80
	;	:		07.30	70 01	8	8	00		00.001

PAGE 7 OF 9

REDGE00 ING RATRIT .000000 3.88 4.57		SUPPLY MAINTENANCE LAI	MAINTENANCE LABOR MAINTENANCE SUPPLY	FUEL	REAGENTS	REPLACENENT PIPE	CONTRACT	CONTRACT ADMIN, CLEP, TECH	CAP-ANORT	TOTAL
NE DOE				1 64	90	90				
HE HATRII .00 .00 .00 SEP 3.42	19.	1.33	5.13	3.04	90.	00.				11 55
5 NATREE .00 .00 .08 3.88 3.42 4.57	-64	1.34	3.13	2.14	90.	00.				7.5
00 3.88 3.42 4.57	=	и.	1.07	4.65	00.	1.11				10.03
. 00 3.88 3.42 4.57			i						90	14.09
3.88	#:-	3.41	7.38	21.2	00.	11.7				
5.60 5.42 4.57	•		10 .	8	00	00.				8.47
1.92		-								6.55
4.57	.02	27.	2:1	00.	00.	00.				21 10
	60.	3.01	4.52	8.	===	8.				
TO DESCRIPTION OF THE PROPERTY	9	=	.56	8.	8.	8.				2 :
	=	=	.23	.00	00.	00.				1.64
10.1		5	9 44	90	1.16	00.			00.	41.58
SUBTOTAL BEMEFICIATION 13.67	-	3.15								
	:	;	•	*	6	6				4.61
11) SLURRY PURPING TAILS 2.00	=	=		۸۸٠						4.70
	71.	<b>5</b>	6.	8.	00.	76.				
	90	.03	5	8.	8.	90.				ç. ;
44.	-	1.14	1.11	90.	8.	1.29	00.			,
SUBTOTAL M.D., L.M. & W.M. J.DY										
;	•	8	10	90	00.	00.				60.
	90.	7 .			-	00				2.07
10. STORAGE		75.			. :					1 98
	91.	.52	=.	<b>8</b> .	00.	00.				
TOUR MAN.	.29	1.05	1.50	00.	86.	8.				4.13
								7		41 04054
ADATM, CLER. TECH								90.11		11.000.11
						:	•		00	00 001
101AL 17.00	2.19	11.22	17.08	1.03	9.16	6.00	90.	90.11		20.00

INPUS;										
MATERIAL CHARACTERISTICS:	UNITS:		CALCULATIONS:							
SEDINENT VOLUME TOMS SEDINEMIS	CV TOMS	394470000 479281050 90.00	PRODUCTION AND HORSEPONER	UNITS	PER DREDGE QUANITY:	ALL DREDGES QUANITE				
DEMISTURE (BY ME16HT) SEDIMENTS			Piloting Season and the	EN /111	45010	45010				
SOLIDSIDY WEIGHT! SEDINENTS	( <b>•</b> )	901	FLOW IN DREDGE CONTUR	CY/HOUR	13372	13372				
S. G. SEDIMENTS S. G. SOLIDS IN SEDIMENTS		<u> </u>	PRODUCTION OF SOLIDS	TOKS/HOUR	1972	3992 19726506				
			PER DREDGE	YEARS	20.00	00				
ONLUGING TARABELENSSTILES	9	7 7				,				
SINE OF DISCHARGE PIPE	FEET	200	VELOCITY NEAD	1111						
LENGTH OF PIPE MATIMUM	FEET	200	FRICTION NEAD	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	175	125				
DESIGN VELOCITY	FT/SEC	# # # #	SIMIL MEND TOTAL DYNAMIC MEND AVE	FEET	131	5				
1 OF SOLIDSIBY WEIGHT! PUMPED	•	140	TOTAL DINAHIC HEAD MAY.	FEET	=	131				
MATEM BILLIAMS MUMBER 170-1307 SER DIV FRICTION FACTOR MULTIPLER	(UATER-1)		PUNP HORSEPONER AVERAGE	<b>노</b> 노	P275	2259				
ELEVATION OF SEDIMENTS MATRIUM ELEVATION PIPE LINE HELECTAN MERCA		125	ANNUAL OPERATING COSTS	TIM	9/0817	OUANITT.	8/YEAR	DICY SEDIMENT		
DREDGE PUMP EFFICIENCY	•	₹	PER OREDEC			4000000	176321	1.048		
POWER IRRANSMISSION EPTICIENCY		7842	DETSEL FUEL	6A.	• •	076751	2690294	6.136		
DUASE DIES NOTICEMENT TO COLUMN			LABOR	T FADITAL COST	-	.01	2800000	1.142		
COS15:			MAINTENANCE SIPPLES	I CAPITAL COST		10.	400000	8.020		
		= = = =	rapital COST ALLONANCE	8/ YEAR CAPITAL		200030\$	2000305	101.4	•	
LABOR	#7HOUR #FM/CM	20.10	INTEREST	R CAPITAL COST		FORMULA	3150063	110.1		
NEW REGULKED	1/6AL		INSURANCE	T CAPITAL COST		FORMULA	210002	1.011		
DIESEL TOEL WUMBER OF DREDEES		4000000		LATIM LUST						
OREVOLT TO THE COLUMN		٠	1003				12796389	6,649	8.649	
VALUE AFTER JOB		. <u>s</u>				VITABILITY	8/VEAR	#/CY SEDIMENT		
T INTEREST ON LAPTING			AMNUAL OPERATING COSTS ALL DREDGES:	TWO.	1110/8					
BREDGE PRODUCTION FACTORS:			DEISEL FUEL	. E	17.19	1226274	1335764 2690294	8.088 1.136		
COURT OF DAYS I EAR	DAYS	123	MAINTENANCE	I CAPITAL COST		6 <sup>,</sup> 0.	000000	0.070		
SCHEDULES UMISTERN SCHEDULED SHIFTS/DAY	SHIFTS	mı	MISCELANEOUS SUPPLIES	S TEAR CAPITAL	_ =	2000305	2000305	101.01		
SCHEDULED HRISHIFT	HOURS	7848	INTEREST	I CAPITAL COST		FORMULA	3150023	\$.011		
10TEL MOUNS/TEAM SLMEDULED HOURS/SHIFT OFERATING	HOURS	3:	INSURANCE	I CAPITAL COST		FORMULA	210002	1.011		
I RECHANICAL AVAILABILITY	pat .	D	CHES							

3.14 7.48 27 62.4 60

PIE GALLOHS/CUBIC FEET EUBIC FEET/ CUBIC YAR MINITS/AR GAL/HP

PHOSPHAIE MINING Ilhousand 8 per Year) CASE I 28 \$ 4.8 \$ 4.2 \$ 2.2 \$ 5.3 17.175 1718 1888 1888 23550 67262 35 23577 43785 65288 12728 78608 3988 34358 17175 3435 1600 23550 55280 12728 78689 99998 2352**8** 60327 35 45558 51525 17175 5153 1009 21114 60006 55288 12728 78868 44441 4,8 35,00 168000 ម្នាស់ក្នុងស្នាស់ 90906 68769 17175 6870 1800 2352**0** 5861**0** 20514 38096 2812 55288 12728 18668 43325 4.8 35.80 85875 17175 8588 ម្មាល់ស្ទាល់ស្ន 65288 12728 78088 9996 23560 56832 35 19912 4254B 4.8 35.80 65288 12728 78888 90096 23520 55175 35 19311 41892 4.8 35.88 120225 17175 12023 23520 53457 96496 14 55588 12728 78608 39976 137468 23520 51740 90005 13 65280 12720 78089 154575 17175 15458 ម្មាល់ក្នុងស្នីស្ន 9000 23250 35 17508 32514 38853 65288 12728 78888 1099 12 17175<del>8</del> 17175 17175 37743 35 16907 31398 35.00 23528 71825 **- 38** E5280 12720 78660 1999 188325 17175 18893 36627 4.8 35.68 78187 23520 46587 35 16305 30682 65288 12728 78888 9000 2002 1000 4.8 35.66 20618 201175 15705 35510 9 65288 12728 78888 26.08 23528 888 93266-223275 17175 22328 1609 See 3 4.8 35.88 ម្មស្ដេញស្ដី 65288 12728 78886 90006 15320 23520 27832 9741 -36.736 - 72.736 - 1.38000 - 56.000 - 2.9150 - 3.65.62 - 49.116 - 356.78 - 3.85.79 - 1.35.50 - 27.7500 - 2.4.550 - 27.5500 - 2.4.550 - 27.5500 - 2.4.550 - 27.5500 - 2 7 5002 4.8 35.68 16889 248458 17175 24845 1888 35 5999 11141 38675 55280 12750 78680 64955 9000 4.6 35.00 16800 \$29765 \$7171 \$363 \$363 9 5002 3 4 8 8 8 8 5 5 5 5 5 2 2 2 2 3 2 3 3 55280 12720 18000 63237 30640 16293 16236 35 5784 10594 90006 4.8 35.00 168600 274896 17175 27489 1888 2999 61520 39675 15423 15422 35 35 \$ 4.00 \$ 55288 12728 78008 99098 18024 291975 17175 29198 4.8 35.00 168000 65280 12720 78880 90006 8458 35 2957 5492 ¥ 6661 1668 4.6 35.08 309150 17175 30915 1600 58985 65298 12750 7888 90096 3 1.8 35.00 16890 373650 17175 37365 1640 1880 2 2 55280 12720 78000 49835 84123 9000 -30150 2.4 ម្មស្នំក្នុងស្ន 1936 55280 12720 78660 3 28358 188 00039 00032 00034 - 1995 120000 --1994 -92758 -3 1993 85000 7758 92758 -4 1932 1750 -10%6 -5 1991 Indirect Production Cost, Wilenne Direct Production Costs #/Tonne Pre-construction Construction Capital Interest During Construction lotal Cash Cost, 9/yr lotal Indirect Cost, 9/yr lotal Production Cost, 9/yr Cash Flow (Revenue-Prod Cost) Investment Royalty @ 5% of sales price Cash Flow (After Investment) Super, Clerical, Tech Offshore Accommodations Preduction, Million IPY Sepreciation (7 yr ACRS) Total Indirect Cost Jotal Preduction Cost Handling and Storage Sales Price, Wionne Total Revenue Replacement Capital Hyrking Capital Principal Principal Payment Interest @ 10% Total Cash Cost lotal Investment Tam Rate, K Income Tam Net Income After F reduction Costs Mining Beneficiation Vessel Loading Administration Waste Disposal unnal Cash Fluid (misc) larable Income Sales Revenue Fioject Year Rinsing Deptetion Lash Flow 12 6 111 Javes pitRiff

50215	
Ē	
, PRODUCTION	
E-MOINTENI	
DKE USING	
	÷

Stationary   Control and Stationary   Control and sectionary   Control and Stationary   Contro				CALCULALIUMS:						
STATE   10.00   10.0	SENTHENT VOLUME	č	441600000						***************************************	
STATEMENT   107	TONE CEDIMENTS	-	000000114							
The property   U.S.	010111111111111111111111111111111111111	CHO.	866430000			PER DREDGE	ALL DREDGES			
STATE   STAT	PENSIST SCHOOLS	17/6	100.00	PRODUCTION AND HORSEPOWER	ENT.	QUANITY:	<b>QUANTTY</b>			
STRINGES  - 1	TUTSIONE OF BEIGHT SEDUNG		0	***************************************	:					
STATE   1.44	I SUCTOSTRA METRALIS SEGIMENTS	·	901	FLOW IN DREDGE OUTPUT	GAL/MIN	65068	65088			
STATES   1.44   PRINCETOR & SLALES   1.57   1.73	S. 6. SEDIMENTS	¥	1.602	PRODUCTION THROUGH PIPE	CY/HDUR	19337	19337			
FIFE   MANUAL PROMETION   CTYTING   TITLED   T	S. 6. SOLIDS IN SEDIMENTS	•	1.60	PRODUCTION OF SOLIDS	TOMS/HOTHR	7775	7775			
				ANNIAL PRODUCTION	LY/VEAD	1711011	13110141			
FIFE   THE PARTY    DREDGING PARAMETERSSTICS:		٠	PER DREGGE	YEARS	19.47	10 07				
FERT   1200   VILCIDIU MEND   FEET   14	***************************************									
FEET   17000   AUCTON READ   FEET   18   18   18   18   18   18   18   1	SIZE OF DISCHARGE PIPE	INCHES.	11.4							
	LENSTH OF PIPE AVERAGE	1999	12000	UEL DETTY MEAN	100	,	,			
The color   The	CACTURE OF DIDE WATHIN		90071	TELEVITY NEWS	111	-	-			
FIFE   15.4   STATE	LENGIN OF FIFE MALINUM	1	00021	FRICTION HEAD	FEET	146	146			
MARTINE NATION   MART	DESTRIK VELOCITY	F1/5EC	15.5	STATIC HEAD	FEET	35	35			
MALINER   1	I OF SOLIDS(BY WEIGHT) PUMPED		34.7	TOTAL DYNAMIC HEAD AVE	1333	101	101			
Mail Fig.   He   He   He   He   He   He   He   H	MAZEN WILLIAMS NURBER (70-150) SEE UIO		140	TOTAL BYNAMIC HEAD MAT	1222					
	EDICTION FACTOR MINITIOLES	ANATED-11		TOTAL PROPERTY NEW TIME.	131	200	184		5794	
THE   THE   TEE   15   TOWN MUSET WELL AND   TOWN MUSET WEER AND	ELEVATION OF REDIMENTS	Tanier-11		FURT HUMBEYUMEN MVENABE	ŧ	4814	4819			
CLEMENT   FEEL   3   ANNINAL OFFENTING COSTS   WIT   CLAWIT   DUANTIT   LYCER   LYCE	MATINIE CICIATION DIDE 1 INC	1221		FUNT HUNSEFUNEN MALINUM	÷	4814	4814			
CERT	THE THE CLEVILLE FIFE LINE		2						***************************************	
1	VELUCITY HEAD	FEET	<b>~</b>	ANNUAL OPERATING COSTS		\$/DNIT	DUANITY	\$ / YFAR	A/FY SERINENT	
Maritimestree   1.00   Maritimestree   1.00   Maritimestree   1.00   Maritimestree   1.00   Maritimestree   1.00   Maritimestree   1.00   1.	DREDGE PUMP EFFICIENCY		=	PER DREDGE						
Mail	POWER TRANSMISSION EFFICIENCY	٠	: _			B1000000000000000000000000000000000000				
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	HORSEPONER AUTHLIARY MOTORS		1043	ACTED THE		,				
PREDECT   PREDECT   PREDICT   PRED			710/	DEISEL FUEL	D.H.C.	•	3148211	1888977	F. 059	
DREDEE   FREEZING   1.14   COPTINE   T. CAPTINE   T. CA	erre.			LABOR	E	1.1	156960	2690294	# · 084	
NERGE   STATES   TAPIDIR    1000			MAINTENANCE	I CAPITAL COST		.01	2800000	8.087		
PREDEC   FATURA   17.14   CTRETION   FATURA   17.14   CTRETION   FATURA   17.14   CTRETION   FATURA   17.14   CTRETION   FATURA   17.14   17	•			MISCELANEOUS SUPPLIES	I CAPITAL COST		6.	400000	\$.012	
TABLES   T	LABOR	\$/HOUR	17.14	CAPITAL COST ALLOMANCE	S/ YEAR CAPITAL		2002514	2007514	£.047	
1	MEN REQUIRED PER DREDGE	MEN/SH	20	INTEREST	7 CAPITA! FACT		EDDMIR &	115010317	700.4	
COST FOR ROLES   1   INSEE   1   COST FOR ROLES	DIESEL FUEL	\$ /5AL			7 CADITAL COST		COMMIT A	2120183	0.070	
COURT PER DATE   1	NUMBER OF DREDGES	-	-	5141	T CAPITAL FOST		E ODMIN A	210017	.007	
1							4 70 10 1			
1. COST POR PARENE   1. COST										
1	DREDGE/PIPE/MISC. COST PER DREDGE	**	40000000							
FFTAL   1	VALUE AFTER JOS	-	•	TOTAL COST				0101711		. 411
STREE   1	I INTEREST ON CAPITAL	1	2		0770			i su lecci		4110
ACTURES   1   ALL DREDGES	1 INTEREST ON INCIDENTE		: -	AUNITED ADDITION AND ADDITION A						
ACTORS1	T INTEREST ON TATES	• •		ANNUAL DECEMBER CUSIS		S/DMC1	NOW IT	\$/TEAK	BACY SEDIMENT	
Maintenance		•	-	MLL WAEDUESS						
Company   Comp							***************************************		***************************************	***************************************
EAR         DAYS         327         HABORE         RH         17.14         156960         2670394         4.084           FAR         SHIFFS         3         HAINTERANCE         1 CAPTIAL COST         1.07         2800000         6.087           FF         HOURS         3         NATERIANCE         1 CAPTIAL COST         1.07         2800000         4.012           FT         HOURS         7848         INTEREST         1 CAPTIAL COST         1.07         2003514         3.05           ATING         AGE         INTEREST         1 CAPTIAL COST         1 CAPTIAL COST         6.003         6.02           ATING         HOURS         6.8         INTEREST         1 CAPTIAL COST         FORMULA         210013         4.06           PRODUCING         HOURS         6.03         1 AIES         1 CAPTIAL COST         FORMULA         210013         4.00           PRODUCING         HOURS         6.003.72         AIESTRANCE         1 CAPTIAL COST         FORMULA         210013         4.00           FET         7.48         1.35         1 AIESTRANCE         1 AIESTRANCE         1 AIESTRANCE         1 AIESTRANCE         1 AIESTRANCE           ET         7.48         1 AIESTRANCE         1	JAEUBE PRUDULITUM PACTURSI			DEIZEL FUEL	GAL	4.	3148211	1888927	8.059	
EN		!		LABOR	E	17.14	156960	2690294	1.084	
March   Marc	SCHEDOLES DAYS/YEAR	DAYS	327	MAINTENANCE	I CAPITAL COST		.03	2800000	18.087	
FT HOURS 8 CAPTRAL COST ALLOMANCE 8/ YEAR CAPTRAL 2002514 2002514 5.06.2 SCHEDULED HOURS 7848 INTEREST 1 CAPTRAL COST FORMULA 3150169 6.092 ATURE HOURS 6.0 INSTRANCE 1 CAPTRAL COST FORMULA 210013 6.007 ILABILITY T 90 INTES 1 CAPTRAL COST FORMULA 210013 6.007 FRODUCINE HOURS 6.043.77 INTES 1 CAPTRAL COST FORMULA 210013 6.007  3.14  ET 7.48  ET 7.49  ET 8.71  ET	SCHEDULED SHIFTS/DAY	SHIFTS	-	MISCELANEOUS SUPPLIES	I CAPITAL COST		10	400000	\$ 017	
SCHEDULE   HOURS   7848   INTEREST   1 CAPTAL COST   FORMULA   3150199   6.098     ATHIG HOURS   6.08   INSURANCE   1 CAPTAL COST   FORMULA   210013   6.007     ATHIG HOURS   6.003.72   ATTES   1 CAPTAL COST   FORMULA   210013   6.007     TABLE   1.14   1.15   1.15     TABLE   1.14   1.15   1.15     TABLE   1.14   1.15   1.15     TABLE   1.15	SCHEDULED HR/SHIFT	HOURS	•	CAPITAL COST ALLONANCE	S/ YEAR CAPITAL		2007514	2002514	£ 01.3	
ATTHE HOURS 6.0 INSTRANCE 1.CAPITAL COST FORMULA 210013 4.007  FRODUCING HOURS 6.003.72 IATES 1.CAPITAL COST FORMULA 210013 4.007  FRODUCING HOURS 6.003.72 FORMULA 210013 4.007  13351949 6.416  ET 7.48  ET 7.48  TWAIT 62.4  6.0	TOTAL HOURS/YEAR SCHEDINED	HUIRS	7948	INTEREST	T CABITAL FREE		4157007	4007034	700.6	
11   1   1   1   1   1   1   1   1	HOURS/SHIET OPERATING	THUID C		TACIOANCE	a Capital Cost		FUNDOL A	1810015	8.078	
		ENOUGH I		INSURANCE	I CAPITAL COST		FORMULA	210013	1.007	
FRUBULIND MUNKS 6003.72 13351949 6.416  5.416  1.14  1.48  1.48  1.48  1.48  1.48  1.48  1.48  1.48  1.48  1.48  1.48  1.48  1.48  1.48	A DECEMBER AVAILABLE TO THE TOTAL	-	0.4	INTES	I CAPITAL COST		FORMULA	210013		
13.14 1.14 1.14 1.14 1.19 1.14 1.19 1.19 1	IDIAL HUDA/TERN PRUDULING	MINUKS	27.5009							
ET C YAR	ONVERSION FALTORS							13351949		.416
ONS/CUBIC FEET IC FEET/ CUBIC YAR SHT CUBIC FOOT WAT	במשלבת שוני של וער וער מיי									
ONS/CUBIC FEET IC FEET/ CUBIC YAR SHT CUBIC FOOT WAT		:								
		=								
		87.								
		23								
/HR		2.4								
	MINUTES/MK	09								

2	Year)	
Z	ber	3
MINSMINE	1 Brousand \$	CASE

Year Year Year Seles Revenue P. Odortion, Million 189	-5	-4	-3	-2 1994	-1-		-	1998 IS	S 8.4 8.4 5.8 5.8	2000 Si 4.8 Si 4	5005 2002 5.00 4.8 5.00 75.00		1063 2884 4.8 4.8	9 16 14 2845 16 4.8 18 35.68	2.80£	1 12 2007 £ 2007		14 2003 4.8 4.8	2018 2018 4.8 35.08	31 2811 8.8 35.48	17 2012 4.8 35.00	18 2413 4.8 35.88	19 2014 4.8 35.60	2015 2015 4.8 35.80	
Sales Price, Vionne Total Revenue Production Costs					rn 60	35.00 35 64883 168	35.00 35.				_	99 15 999 99 99 99 99 99 99 99 99 99 99 99 9	_			-	_	-	_	158603	16969	16823	N-27331	16623	
Uniect Production Lests Wildham Natural Beneficiation						- 4,		5.48 5.	5.48 5	5.48 5.38	5. 48 5. 5. 38 5.	5.48 5.48	- 63	64.4 64.2 64.3 64.3		5.48	65.45 66.38		4. % 6. 6. 6.	5.48 5.48 5.48	5.48 5.48 5.50	5.48 5.48 3.38	5,48 5,48 5,50	3-3-3-3-3-3-3-3-3-3-3-3-3-3-3-3-3-3-3-	
Marding and Storage Vessel Loading													_		សស. សស.		_	ម្ចាស់ ម	ស់ ដូ ភ	ស្សក	អ្នក	ស ស ភ	श श <u>न</u>	25. 25. 25. 25.	
Waste Disposal Super, Clerical, Tach					i di															1. 1. S. I.	3.1	9.1	3.5	6.1	
Offehore Accommodations Fotal Cash Cost					_	3.69 13	.45 13.69 13	.45 13.60 13	3.68 13	3.69	.45 13.69 13.	. 65 13. 66 13.	C). C) 69 13.69	C. C. S. E. B. E.	5 . 45 6 13.68	. 43 8 13.68	13.68	13.68	13.60	13.60	13.68	13.60	1.69	13.60	
Indirect Production Cost, Wilomme Administration	QJ							si ki		S 10	ક્રાં ક્લ 			% श्र % श्र	\$ 65 \$ 75	85. 85.				45 €	≨. <del>.</del> .	\$ 3.	8.3	3.5	
Sales Royalty é SK of sales price Taxes (wisc)													_				_		-	1.75 65.	65.	27. 35.	1.75 .co	5. 3. 5. 3.	
Other Total Indirect Cost Total Production Cost					_	_	10 9	_	25.25 25.25 30.25	_	. 52.5 . 52.5 . 53.5	. 25 25	85. 85. 83.5 83.5 83.8 85.3	70 0	.0 9	25. 25. 25.5 25. 25.3 25.3	2	2. 23. 25. 25. 25.	85.5 85.3 85.3	23.2	25.65 26.65 26.65	8. 5. 5. 8. 5. 5.	2 2 3 3 2 2 2	8 8 7 8 8 8	
Total Cash Cost, Nyr Total Indirect Cost, Nyr Total Production Cost, Nyr						5280 65 12720 13	5250 65 12750 12 7860 78	52.00 ES 127.00 12 702.00 78	5280 C5 12760 12 78600 78	55.80 ES 12720 12 78000 78	55.80 65. 127.30 15. 78000 786	5280 655 121 62731 1830 763	65260 65260 12720 12720 76230 78433	69 £5280 59 £728	50 C5589 50 127c0 50 78020	10 E5280 10 12720 10 78220	8 ESc88 8 12728 8 78630	65588 12728 78008	65c88 12750 78638	E5ce0 15758 78660	65259 12759 78000	65588 18788 76883	65280 16733 76.03	E2250 167.3 76.00	
Cash Flow (Revenue-Prod Cost) Irvestuent	•	•	•	•	3	E000 94	N6 P0006	N6 88.W6	36 econs	96036 A	sould sa	୬୬୯୫ ବନ୍ଦର	93538 95358	88 900dd	80 Sv488	BLCUR WASH	8 53449	90338	95588	80226	92339	33339	26063	9000	
Pre-construction Construction Capital Interest During Construction Jotal Investment	ROSEI earchi	31528 1575 33875	9 91 66237 1 27488	0 166634 124246 124246	9 3£848 23488		••••				••••					3636	2006	9656	2000	***		35,55	2959	2032	
Principal Principal Paywert Interest & 184 Replacewert Captal Korking Captal	• • • • •					310159 33 1 0 15 25015 3 0	336965 279 15508 15 33697 67 1880 1	279135 261 15598 15 27914 26 1809 1	263628 246 15588 15 26363 24 1988 1	248124 232 15588 15 24812 23 1008 1	53513 517185 15508 15588 5351 51711 1854 1858	C)	9	6353 178563 5539 15588 8693 17358 1883 1848	53 155475 86 15588 58 15588 86 1559	75 139568 86 15548 86 13957 80 1848 9	8 155/8 7 154/8 7 154/8 8 1959	1,04553 1,5569 1,006 1,006	93542 15588 9359 1958	77536 15509 7754 1609	E2030 15548 E203 1600	46523 15508 4652 1868	31815 15505 3162 1000	6036 1038 1038 1038	
Cash Flow (After Investment)	-16009	-33075 -	-83475 -12428W		59468	-26815 5	53503 61	99819	19 (1929	53 88119	13 61/53	67289 686	£8848 70391	91 71942	13495	92 75843	3 76594	78145	79695	81∈+6	82797	84348	65598	91049	
Depreciation (1 yr ACKS) Uepletron Tarable Income Tarable ste, s Income Tar Tet Income Tet Income Tet Income			9 0 9 N 9 9	****	W	44320 7	3556 56	54245 38 3420 11 3420 11 35 1197 4 2223 3	38738 21 11958 16 11949 16 25 4162 1	27696 27 10246 15 10246 15 35 6386 6	27665 27 15037 19 15037 19 35 66.3 6 12374 12	27696 136 27979 23 28 311 28 28 311 6263 311 6263	235-8 235-8 31487 46871 35 35 11858 16495 20467 20466	49 A	13 63 63 63 63 63 63 63 63 63 63 63 63 63		255.0 253 53074 35 35 35 35 35 35 393 18576 390 34438	6.35c0 6.35c0 7.56c5 5.35 6.19119 8.3556	2550 56175 35 35 19681 30514	235.0 577.6 577.6 35 20.64 375.2	23520 55.77 35 20747 36530	235cd (0858 35 21250 33536	2.550 6.2578 5.578 3.5 2.16.32 4.05.40	0 6755 6755 35 5555 5555 43334	
Cash Flow Count Lash Flow	-1000 -33075 -63475 -124200 -10000 -43075 -126550 -250750	-33075 -	-33075 -63475 -124200 -43075 -126550 -250750		-55468	-335355 -29	37375 + -296978 -25	44381 4-254589 -211	42947 4,	4 - 46:24 	45.88 44 88-88/571-	44952 42- -60928 ==360	42312 38478 -36616 -138	18478 39486 -138 35348	36 40494 46 /3842	98 615124 98 61542	4.518 4. 163654	6 43516 6 c07372	44566	45534 c37432	46542	47558 391554	40228	EPs14 Sabste	
LCFRi] LLV è lòx	6.4.8														TE .										

ui US 23-8458-NV Phosphate Economics Project Number: 29 6458 NV File: FIGS233

PRUSPIRITE MINITIAS
(Throrsand & per Year)
(GSE 11b)

دما درون 1884 1885 2005 2005 62558 6719c 35 62519 63177 19 2014 65269 12750 76000 37665 16843 3769 1000 35 21599 40112 235c0 61711 E5280 12720 76023 56528 18843 5453 1040 43565 <1850 83347 235c0 53527 4.8 35.02 168029 55288 12758 76068 235c0 57943 **8008** 75374 16843 7537 1939 81463 35 24589 37663 175341 45340 4.8 35.63 IESA'3 160 55269 12729 76000 94c13 9481 235c**0** 5c059 155501 113955 55280 12720 78339 11386 1988 77694 63559 33898 11114 18% 65268 12728 78488 54000 38(65 518 6 18943 62151 1438 235c0 52690 35 18482 33788 13 2003 2003 65588 12750 78688 158748 1537 235cB 58486 35 1766 37441 13531 65588 12758 78688 169583 36216 19843 16959 1433 2328 48522 35 16983 115.39 55289 12729 78489 B0005 18843 18843 1884 35 16323 38314 34931 46637 4.8 35.00 10 2005 <u>चे शर्य राज्य के के</u> 65538 12738 7880 16843 20727 1998 9,1,100 33/16 23558 44753 9 4.8 35.30 168538 65288 12728 78033 226110 6/981 6/981 325/-235cb 4.8 35.63 16893 20A3 a: 15.12 20.12 20.13 2 244953 37200 65288 12728 78488 16888 2358 24177 16843 2895 1.8 35.60 1685/0 ម្មស់ស្ទីម្នាស់សំន E5288 12728 78388 263735 1983/25 26.393 33653 1093 4.8 35.44 169030 ន់ស់សំន នំសំសំន 65268 12728 78888 69263 18843 33615 13561 13560 5 4.8 35.80 381488 16843 30146 65280 12720 78660 -448-55 -148-25-5-151000 -7-2600 -33405 -57123 -36204 -36391 -347-04-59455 -574704 -594-55 152-55 -32-575-5-44004 -574704 4.8 35.68 1953 65288 12720 78000 324323 17869 1958 1949 F 85 4.8 35.80 HEBNOJ ទំព័ត្ធសំន័ន៍ 339165 65280 12720 78030 55983 203 418335 18843 55284 12728 78698 **46166** 2 <u>2</u> 3 31685 1995 44608 26608 72608 -5 1934 0 13c000 198i0 151800 -3 1993 93588 8555 106865 ş€61 -19699 -48425 -2-Indirect Production Cost, Milonne Direct Production Costs #/Terme Total Eash Cost, 8/yr Total Indirect Eost, 8/yr Botal Production Eost, 8/yr Royalty @ 5% of sales price Taxes (M15c) Construction Expital Interest During Construction Cash Flow (Revenue-Prod Cost) Investment Eash Flow (After Investuent) Offshore Accountations Depreciation (7 yr ACRS)
Lepletion
Lashle Income
Tax Rate, \$\$\$
Inc. we Tax
Pel Inc. we After Tax Preduction, Million 197 Sales Price, 1/Toune Waste Disposal Super, Clerical, Tech Handling and Storage Total Individet Cost Total Production Cost Interest # 18% Replacement Capital Total Cash Cost Principal Payment Total Investment Pre-construction Mining Eeneficiation Vessel toading Adamstration Preduction Easts **Halting Capital** tash Flyw Coavi Cash Flyw ales Revenue Project Year Rinsing Principal ECF FOT THE B TOX

9

MAISPHOLE MINING (Housand & per Year) CASE 1 (c.)

6661 6661 2661 9661 • E 2 1	2.4 4.8 4.8 4.8 4.8 35.00 35.00 35.00 35.00 35.00 35.00 80.00	3.96 3.96 3.96 3.96 4.66 4.66 4.66 4.66 4.66 4.66 4.66 4	11		••••	34354 26659 349150 291975 0 17175 17175 17175 21390 36659 34915 29190 0 1894 1694 1890 1804 1804 0	65045	9966 64123 CA478 42943 9 6 2484 11923 15 15 35 35 16 4175 17 1734	-21194 40316 47001 45112- -36859 -3683/4-219373 23396-
3 5	4.8 4.8 35.60 35.40 168640 168044	3.96 3.96 3.96 3.96 3.97 3.23 5.2 5.2 5.2 5.2 5.1 5.21 1.1 4.1 1.1 4.1 4.1 1.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1	1. 2. 1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	50752 50752 12:00 12:00 71040 71040 96:350 96:950	••••	27480 257625 17175 17175 27480 25763 1000 1000	68488	305.25 305.00 30	44689 46100 =1892/2 143172
2002	4.8 4.8 89 35.60 35.60 88 16888 168880	8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8	8. 8. 8. 8. 8. 8. 8. 1. 8. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	58752 12388 71848 96964		248458 17175 24845 1848	71915	38.28 28.20 28.50 35 76.7 11.003	47523 55C49 -
8 9	66 35.80	3.% 3.% 3.% 3.% 3.% 3.% 3.% 3.% 3.% 3.%		58152 58152 12589 16588 71040 71040	• • • •	22.12.75 26.6.160 17.175 17.175 22.328 26.6.18 16.78 16.88	135.12 15350	15324 0 23520 23520 34792 51630 35 35 12177 16141 22615 33589	44280 40034 5135 11335
5 5002	4.8 35.00	138 138 131 131 131 131 131 131 131 131	E 5. 1 5. 2 5. 3 5. 3 5. 3 5. 3 5. 3 5. 3 5. 3	50752 56 12260 13 71640 71		1069:5 1 17175 10693 160,8	1105.1	235c# 53547 35 18741 34845	41151 2981£
50.05 5005	4.8 4.8 35.00 35.00 16800 16800	3.% 3.% 4.6% 4.6% 4.6% 4.6% 4.6% 4.6% 4.6% 4.	81. 81. 53. 53. 17. 17.1 11. 61. 12. 53. 13. 68. 14. 68.	58755 58755 12289 12288 71840 71848 95960 96969	••••	171750 154575 17175 17175 17175 15458 1630 1648	78785 84582	2355@ 2355@ 55265 56982 35 35 19343 19344 19343 37838	42267 43383 72883 115466
13	35.88 1E968	3.86 4.86 5.23 1.23 1.24 1.25 1.25 1.25 1.25 1.25 1.25 1.25 1.25	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	56752 8 15c88 71640 9 5564	2000	5 137408 5 17175 8 13740 8 1654	95550	235.0 287.0 3 35 4 28545 8 38155	3 445kW E 159.HE
14	4.8 35.69 3	3.98 4.08 5.09 5.09 5.09 1.08 1.08 1.08 1.08	81. 81. 81. 81. 82.5 83.5 84.	58752 112588 11848 11848 11848		124225 10 17175 1863 1863	11619	235.0 69.17 35 211.96 39.71	45616 cebbst: 12
(all 8)	4.8 35.00 35.	3.3% 3.4% 3.4% 3.4% 3.4% 3.4% 3.4% 3.4%	<b>1</b>	28 25 88 21 8 22 8 3 1 8 3 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	••••	1295 821 17175 171 171 25171 1630 1631 1630 1631	85655 87	20 0800 20 0800 20 0800 20 0800 20 0800 20 0800	4733 473 Was 201535
7102 1182	4,8 35,84 35,84 16830	3.95 3.95	11. 81. 12. 12. 13. 13. 14. 15. 15. 15. 15. 15. 16.	58752 58752 15288 15288 11848 71848 71848 71848		85875 68788 17175 17175 8568 6678 1732 1732	67372 69878	6353 6358 6365 6358 35 35 5534 6358 61584 6568	47843 48.KS seele 543129
1 B	6 4.8	86. 88. 88. 88. 88. 88. 88. 88. 88. 88.	98.71 98.79 98.72 1.75 1.75 1.75 1.85 1.75 1.8	52 58752 58 12589 18 71849 18 9558		55 17175 76 5153 76 1808 8 1808	90807	60 2356 78 67287 35 35 36 2355 84 (3737	58,786
19 19	15.00 15.00 16844	3.96 4.06 5.02 5.03 5.03 5.03 5.03 5.03 5.03 5.03 5.03	81. 82. 81. 82. 83. 83.	59752 17569 71730 96.353	5 5 5 5	34359 27171 3435 1889	655	235:8 650/5 650/5 35 24152 443:3	87178 45559

91922 1, 8 35, NJ 185649 19 19 ## 55 71849 13155 84558 34558 17175 5455 1438 Pecits 4.8 35.80 16893 71608 13155 84964 51525 17175 5153 1050 76687 4.6 35.73 166003 68783 6873 6873 開発に 35 63 31.0 \$ 4.00 mm = 1.00 71848 13152 84958 85875 17175 8588 1638 1.8 25.00 166503 71868 13152 8496 8 384B 1135 15. eu 15. eu 1684 d £ 69 71608 33. 33. 33. 33. 54. 57. 57. 57. 830-18 1, 8 35, 88 13 71648 13152 84360 Byeku 137488 17175 EB 348 4.8 35.64 IEBUDA 18 6337 23. 23. 27.25 71888 13152 84368 154575 17175 15458 1648 83648 4.8 35.00 3005 71888 13152 84908 17.154 27.17.1 27.17.1 1,865 629 4.8 35.88 2645 188925 17175 18833 71888 13152 84968 1639 40.05 4.8 35.00 168030 206.189 17175 276.19 71896 33.55 30 4.8 35.80 16893 000 223275 17175 23328 1888 71668 13152 3580 83848 59712 PRASPIBILE MINING Ultrous and 4 per Year! CASE 140) - Sugar 4.6 25.48 169600 939CB 54455 57171 54655 54655 71666 57995 4.8 35.88 9 5 83848 257625 17171 25763 1888 25.25 26.25 26.25 27.25 71660 4.8 35.44 1686a 5005 55. 18. 18. 18. 18. 18. 18. 18. 18. 274876 17175 27488 1888 71888 13152 84968 54560 4.8 35.68 55. 55. 55. 55. 55. 55. 57. 57. 57. \$78165 \$7171 \$8185 \$186 71668 82848 3 936 4.6 35.03 1660/0 389150 17175 34915 1600 71888 13152 84968 8.3946 \$1165 4.8 35.00 2 1997 # 5.5 38-614 17175 36-8E1 180-8 180-8 71888 13152 84968 2. 4 35. 88 84828 1938 3152 -96 35310 1935 10000 26033 66039 5-1994 120658 18608 138690 -3 85000 7750 92750 ₹ 26 35000 1750 36750 -5 1991 10530 -1990 uh OFS 29 A-58-W Prosphate Economics Project Muher: c9 A+58 W File: PioSc37 Indirect Production Cost, Wilona Direct Production Costs Wlorne Total Cash Cost, Nyr Total Indirect Cost, Nyr Total Production Cost, Nyr Royalty @ 5% of sales price Taxes (misc) Construction Capital Interest During Construction Total Investment Cash Flow (Revenue-Prod Cost) Cash Flow (After: Investment) Super, Clerical, Tech Offshore Accoundations Peduction, Million IPY Handling and Storage Vessel Loading Waste Disposal Total Indirect Cost Total Production Cost Sales Price, 1/10mie Principal Paynent Interest & 10s Replacement Capital Working Capital fotal Cash Cost Pre-construction Preduction Easts Mining Beneficiation Administration Total Revenue Sales Revense Project Year Year hvestuent

15.63 15.63 165.63

22. 25. 27. 29. 29. 27.5 27.5

71560 1972 8989

60 2132

235c8 53357 35 18678 14689 41834 411534 5156 51659 35 16476 33572 6325.4 49932 1747E 3.5-E 35 16975 31348 235c0 025ES 23550 43852 35.8 4135 35 1471 36874 35/38 55c3 32103 235cə 37910 35 13469 24641 34.780 34768 15324 22156 22196 35 7763 14427 35.00 1366 1366 1366 35 4781 8879 36039 183968 38649 12819 12818 35 4486 8332 346.16 39675 11943 11942 35 4189 7762 33,05 65.93 49.70 49.70 49.70 49.71 17.33 17.34 33926 25304 3395# -35566 -321656 37110 -100/0 -36754 -3.754 -130/04 -660/0 -100/4 -46754 -139502 -277509 -343572 5.1 s =10315/ Deptectation (7 yr ACNS) Deptetion let Incore After In Takable Incode Tax Rate, 16 Procee Pax Crest Cash Flow ECFOR

64123

PHOSPHOTE MINING
(Thousand 4 per Year)
CASE 11

1808 1808 34578 35 33182 51476 8.8 14488 79680 17175 3435 1000 89251 35 31241 58620 1968 42.00 281689 5816 5.40 .36 .25 .25 .25 .15 .15 .146 .156 .156 .156 5. K. 5. K. 5. 5. 17175 5153 1600 66.836 42.08 42.08 201500 88.5 89.5 89.5 89.5 89.5 89.5 89.5 89.5 1860 1860 85826 35 14488 79688 42.68 593668 84188 35 8588 1888 %. %. %. %. %. %. %. %. %. %. 14488 79688 4.8 42.88 201680 527949 86331 35 42.08 42.08 201698 £3486 463346 17175 12023 1000 42.08 17175 13740 \$2855 \$2826 35 14488 79688 4.8 42.00 201508 961/EE 77238 2 88 14468 79688 £0138 276236 4.8 42.00 201698 75521 14488 79588 17175 16893 5989 14468 79688 42.89 201688 17175 22328 99172 42.00 201600 2 X = 2 X X 2 2 3 23234 55848 14489 79688 4.8 42.80 201500 240450 17175 24045 4.8 42.00 201600 17175 25763 36.293 -94665 4.8 17175 27488 1888 %. Xi = %. Xi € 3. 12883 22452 55,00 4.8 42.00 201600 5.46 .36 .25 .25 .15 1.15 1.48 1.48 17175 29198 -18000 -36750 -92750 -113074 -66800 -15930 66972 67593 66924 -18000 -46750 -139540 -277589 -343500 -259530 -295430 -224845 -158841 5528A 1448B 7968B 8543 15866 17175 30315 4.6 3 2001 2 2 2 2 2 2 3 5237 9726 4.8 42.88 20168 17175 35853 1688 1888 2 2 2 2 2 2 3 79680 2.4 42.68 00860 1-861 56898 66898 18696 138669 5-1997 7758 92758 566 1758 36758 2 PS 86-98 indirect Production Cost, Wionne Direct Production Costs #/Tonne Construction Capital Interest During Construction Royalty @ 5% of sales price Cash Flow (Revenue-Prod Cost) Cash Flow (After Investment) Total Inducet Cost, \$/yr Total Preduction Cest, \$/yr Super, Clerical, Tech Offshove Accomyodations Depreciation (7 yr ACRS) Preduction, Million IPY Handling and Storage Tetal Indirect Cost Total Production Cost letal Cash Cost, 1/yr Principal Payment Interest @ 18% Replacement Capital Sales Price, W/lonne Net Incree After law Tetal Cash Cost Total Investment Pre-construction Vessel Loading Administration Herking Capital Cash Floa Camul Cash Floa Production Cests Mining Reneficiation Maste Disposal Taxable income Tax Rate, 1 laves (misc) Sales Revenue Project Year Income las DECPOI Investment Principal Rinsing

to the common with speak Economics to be set and the set of aniest of male with the set of the set

5713788		4, 8 4, 44, 45, 46, 45, 46, 45, 46, 46, 46, 46, 46, 46, 46, 46, 46, 46	64.4 64.4 64.4 64.4 64.4 64.4 64.4 64.4	65. 65. 61.6 61.6 61.6 65. 65. 65. 65. 73. 64.6 64.6 64.6	65.80 65.80 146.0 144.0 796.0 73660	1219.4 1219su	3555	31015 (35.09 (15.09 0 3102 (35.1 (3.09 (35.1)	117816 Lec 3c3	8 58554 cbccs 89594 5475 35 35 33161 58 33161 58256 61594	70352 63503 860214 35.25.1	
	10	1,8 16,43 163165	4.00 4.40 4.40 4.40 4.40 4.40 4.40 4.40	\$2.5 \$2.5 \$3.5 \$3.5 \$3.5 \$3.5 \$3.5 \$3.5 \$3.5 \$3	65c60 14428 79c68	121950	9999	46523 15568 4652 1638	I I Eceb	88224 88844 35 38815 377.29	69945 8834cc b	
	= (2)	4.8 42.63 college	3 3 4 7 1 2 3 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	23. 24.5 25.5 35.0 3.00.8 16.60	65288 14480 79EE8	121324	<b>3666</b>	62038 15588 6283 1858	116717	65654 65493 35 30273 56220	6.8936	
		42.43 42.43 colles	64.68 53.55 53.55 53.55 11.55 13.58	2. 16 2. 16 6.5. 6.5. 6.5. 6.5. 8.8.8. 15. 16. 16. 16. 16. 16. 16. 16. 16. 16. 16	6558W 14408 79588	636154	5 9 9 6	77538 15588 7754 1400	113166	86942 86942 35 69738 69738	67779	
	4 岩	4.6 4c.eb coteco	6.46 6.56 6.55 6.55 6.55 6.55 1.15 1.16 1.16	9. 5. 83. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	65588 14488 79688	121980	9696	93045 15508 9305 1000	111615	83391 55 55 78187 54-284	66329 645283	
	2 5	9,8 44,08 colfos	04.4 08.5 08.5 08.1 08.1 08.1 1.1 09.1 1.1 1.3.50	9. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	65580 1448 79660	121930	7020	15508 15508 16355 1003	110065	81841 81841 35 28644 53197	55533	
	21 <del>2</del>	4.8 4c.68 calless	65.4 65. 65. 65. 65. 65. 65. 65. 65. 65. 65.	85. 85. 85. 85. 85. 83. 83. 83. 83. 83. 83.	65260 14480 79560	121924	2000	124764 15508 12406 1660	100514	28524 89298 35 28 28 35 52 168	64944	
	= 10	4.8 42.88 281623	64.4 68. 65. 65. 61.1 64.1 64.1 64.1	3. 10. ≥ 2. 10. 2. 2. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.	65288 14483 79688	1219.0	9 9 9 9	139568 15506 13957 1888	106.963	26254 78759 35 2753 51160	623% 48.516	
	≣ §	4.8 4c.88 cdle88	64.4 64.8 85. 85. 82. 82. 1.1 64. 1.0 63. 1.1 63. 1.1 63.	85. 85. 85. 85. 85. 80. 80. 80. 80. 80. 80.	65280 14480 79588	121920		155875 15588 15588 15588 8	182412	8 58c4 77189 35 57816 50172	62888	
	3 5	4.8 4c.88 ce1688	6.46 55.48 55. 55. 11.15 11.15 13.11 13.11	8. 25 . 25 . 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3	65568 14438 79688	121320	9999	170583 15588 17058 1600	103862	28254 75638 35 26.73 9165	61681	
	- T	4.5 42.88 201580	84.4 86.9 85.3 85.3 85.1 87.1 84.1 84.1 84.1	65. 81.2 83. 83. 85. 85. 85.	65260 14483 79688	121920	2520	166.338 155.28 186.33 183.8	102311	28254 74887 25 25 25938 48157	E0873 215851	
	* 5	4.8 42.88 231683	6.46 6.38 .38 .35 .25 .11 6.11 6.11 6.11 6.11 6.11 6.11	9. 10. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	88367 88381 88523	121920	9	15598 15598 20169 1888	100768	13833 28224 58793 35 28546 38157	6470E 154578	
Blallin F. F. Ve.		4.8 42.00 201603	5.5 5.5 5.5 5.5 5.5 1.15 1.15 1.16 1.16	3. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	65280 14400 79680	121920	••••	217105 15508 21711 1630	99209	27696 28654 43269 35 15151 28138	68558 94272	
Forstroff Mining Officerated Toylor Voin J Toyle Televic	- :	42.68 42.68 531603	3. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8.	<u> </u>	65280 14460 79580	121920	••••	232613 15589 2361 10801	97659	27665 28254 41778 35 14628 14628	67531 21722	
= =	* 4	4.8 42.88 2016.03	3.4 3.6 5.5 5.5 5.1 5.1 5.1 6.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	65288 11498 79688	121950		248120 15508 24812 1600	96196	276% 26224 44168 35 14646 26122	££534 458ay	
	* 4	4.8 42.88 201233	3.5 3.5 3.5 3.5 3.1 3.1 3.1 3.1 3.1	± 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	65288 14408 79688	121984		263628 15588 26363 1968	94557	38738 27919 27989 35 9768 18141	69281 112343	
	154	4.8 4c.00 201503	9.4. 9.6. 85. 25. 25. 1.15. 1.16. 1.	ន់ស្នំ នេះ នេះ នេះ នេះ នេះ នេះ នេះ នេះ នេះ នេះ នេះ	65288 14468 79680	121920	****	279135 15588 27914 1888	93306	56245 19281 19380 35 6783 12597	78715	
	* 3	4.8 42.00 201020	3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	65280 14400 79680	121950		321845 15588 32185 1608 1808	86935	75956 5498 5489 35 1921 3568	6950E -655339 -	
	1 12	2.4 42.88 102838	3 3 4 7 7 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7	≤. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	65280 14400 79680	21120		31015a 0 9695 0 1803	-11695	4432	-11695	
	= 2					•	23499 23499 59498		-59409	# <b>* * *</b> % * * *	-59480	
	- 5					•	665451 66581 66581	••••	124200		3 3	
	-					•	6 76508 168 6975 16 83475 124		-83475 -124200		-10000 -33075 -83475 -124200 -10000 -42075 -126550 -250750	
	· · · ·					•	9 31500 1575 33075		-33075	• • • လုံ • •	-33875	
6.0411.5	-					*	16030		-14039	999096	-1900) -19003	14.1 # 91803
of the 25 meta Whitespeak Economics in op. 4. diotest of meta W. Filler na. 18.	# # # # # # # # # # # # # # # # # # #	er datter, Billion Dr Sales Peres, Kalana Total Revens Production Cests	Direct Franction Casis Wilane Mining Emeticiation Riosing Hadding and Storage Vessel Loading and Storage Vessel Loading and Storage Vessel Loading and Storage Vessel Loading and Correction Total East Cost I'dial East Cost	Adunistration Sales Royalty & SS of sales price Taxes fusci Other Total Indirect Cost Iotal Production East	Total Cash Cost, Nyr Total Indirect Cost, Nyr Total Preduction Cost, Nyr	Cash Flow (Revenue-Prod Cost) Investment	P e-construction Construction Capital Interest During Construction Total Investment	Prizcipal Brincipal Paywent Interest ë 188 Replacement Lapital Kerbing Capital	Cash Flow Writer Investment)	Depreciation (7 yr ALMS) Depletor Tanble frome Tanble frome Tanble, x Income Tan Het income Miter Tan	Cash Flow Coaul Cash Flow	(CSRD) they is like

PHÖSPIGNE MINING (Thousand 6 per Year) CASE 1116)

bi 055 29-048e Norspale Economics Project froten: 39 하50 자 File: PuGS35

8 19 8	6 4.8 4.8 2 42.0 45.00 3 20100 20160	# # # # # # # # # # # # # # # # # # #	55. 55. 55. 69. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.	10 ESERO ESERO 10 14400 14430 10 79560 79660	w 12192w 12192w	2265	3 18843 18943 3 18843 8 3 3729 1884 6 1030 1033	7 117151 12.ce36	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	9 67184 83532 3 713837 EVECÉS	
7 18 5 2016	4.8 46.82 5.316.3	3.4.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3	92. 25. 83. 69. 5. 69.	65569 14483 79680	1219cu		55528 18843 5553 1808	115667	28224 87843 35 38462 56578	65339	
11	42.48 42.48 301603	3. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5	65288 14488 79588	121920	2000	15376 18843 7537 10001	113383	85128 85128 85128 85128 85128	64734 579354	
16 105	8.4 51.57	소 소	2 10 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	65268 14403 79688	121960	9999	94513 18843 9421 1969	111699	8224 63375 35 29146 54169	63514 515530	
2813	4.8 4ce 23 coleon	수 면. 는 등 등 기 : 1 : 1 : 1 : 1 : 1 : 1 : 1 : 1 : 1 :	55.5 51.5 52.5 52.5 53.5 53.5 53.5 53.5 53.5 53	65588 14580 79680	121924		526511 18843 1836 6031	1361	28254 81398 35 28467 52983	62284 451710	
2015	4.8 46.83 colfee	3. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	25.5 61.5 62.5 62.5 63.5 63.0 63.0 63.0 63.0 63.0 63.0 63.0 63.0	65588 14483 73688	121930	****	131838 18843 13198 1888	187738	28654 79586 35 27827 51673	61868 3894a6	
13	1,8 42.63 241633	ង្គិន និង្គស្លាសក្នុងក្នុង	95. 93.5 93. 83. 3.64 93.31	65288 14483 79680	121920		158748 15074 15074	348581	28224 77622 35 27168 5454	59835 3283EE	
12 2010	4.8 42.88 201600	64.4 64.5 53. 53. 51.1 64.1 64.1 64.1	¥ ¥ ¥ ¥ ¥ ¥ ¥ ¥ \$ \$ \$ \$ \$ \$	65558 14463 79688	121980	****	66583 16953 16953 16953	183562	28224 75738 35 26508 49230	56611	
11 2033	4.8 42.60 coltos	3.8 3.8 4.2 5.3 5.3 5.3 5.3 5.3 5.3 5.3 5.3 5.3 5.3	¥. ×. ×. ×. ×. ×. ×. ×. ×. ×. ×. ×. ×. ×.	65280 14480 79680	121980	9696	18843 18843 18843 1888	1105017	28224 73853 35 25849 48004	57365 201950	
10	4.8 42.88 2015/4	3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	ម្ចុស <u>់ ទី ទី ទី ទី ទី</u>	65588 14488 79588	12193	2636	607668 18843 20727 1033	189193	8 :8224 71969 35 :25189	56161	
9 2887	4.8 42.60 201603	\$ 3 8 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	ម្នាល់ <u>មា</u> ម្នាល់ មាន ខ្មា	65288 14488 79568	121920	3636	226114 18943 23611 1864	98303	28624 78885 35 24538 45.55	54936	
8 3005	6.8 42.80 coteoo	3. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8.	2.10 2.10 2.10 3.00 16.60	65288 14488 79668	121928		244953 18843 24435 1600	35455	16898 28224 51393 35 17968 33465	41438	
2005	4.8 42.89 201600	3. 4. 4. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	25. 2.18. 2.18. 3.08. 16.68.	65289 14488 79688	121920	••••	263795 14843 26388 1080	94246	33653 28624 32663 35 11432 21231	95181-	
6 (144)	4.8 42.88 201633	3. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5	65280 14480 79680	121920		282638 16843 28264 1600	95326	33615 28224 30817 35 10786 26831	630c7 82421	
5 5 603	4.8 42.83 201633	3.4.6 34.0 35.7. 35.1.1 3.1.1 3.1.1 3.1.1 3.1.1 3.1.1 3.1.1	± € € € € € € € € € € € € € € € € € € €	65250 14480 79680	121920	••••	381468 18843 38148 1808	90772	33653 28224 28695 35 19113 18782	61816	
2002	4.8 42.00 201603	3. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	25. 25. 25. 25. 25. 25. 25. 25. 25. 25.	65288 14408 79688	121920		320323 18843 32032 1000	86888	47869 20910 20909 35 7310 13591	62727 607564	
3 2031	4.8 42.00 201500	5.78 5.86 5.07 5.17 5.17 5.17 5.17 5.17 5.17 5.17 5.1	\$2.50 \$2.50	65280 14468 79680	121920	••••	339165 18843 33917 1858	87883	65911 18546 18546 35 3591 8695	- 1666 32-	
2840	4.8 42.83 201683	3. 3. 4. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5	65280 14400 79660	121920	• • • •	395215 18843 39522 1800 1800	79598	92291 6 53 55	- 334460 -	
1939	2.4 42.00 100E00	3.5 3.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5	5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5	65280 14480 79680	21120	••••	376858	-18365	53852 8 5 5 6	-18365	
1-1898					•	9 44888 28688 72688	••••	-726.00	စေ စေ မွှေ စေ	-72680 -376850 -	
-5					•	132608 19848 151648	***	9981	• • • • • • •	989 653	
3.61					•	93508 93508 8525 186025		R2825 -	@ <b>@</b> @ XX @ <b>@</b>	82428 - 52458 -	
1995					•	38508 1925 1985		-48425 -182825 -15		-48425 -192425 -15 -58425 -152459 -34	
-5					-	92991 9 9		10008		-10008 -40425 -102025 -15 -10008 -50425 -152458 -30	10.6 x 14227
Project Year Year Sales Revenue	Production, Million IPY Sales Price, Milonne Total Revenue Production Costs	Direct Production Costs Wilome Mining Reneficiation Mining Assing Handling and Storage Vessel Loading Waste Disposal Super, Clerical, Tech Offshore Accessodations Lital Cash Cost	Indirect Production Cost, \$/forme Administration Sales Royalty # 5% of sales price Taxes (misc) Other Total Indirect Cost Total Production Cost	Total Cash Cost, 8/yr Total Indirect Cost, 8/yr Total Production Cost, 8/yr	Cash Flow (Revenue-Prod Cost) Investment	A e-construction Construction Capital Interest During Construction Total Investment	Principal Principal Paywerk Interest @ 10% Replacement Capital Murking Capital	Cash Flow (After Investment)	Depreciation 17 yr ACRS) Depletion Tavable fricue	Cash Flow Cumul Cash Flow	DCFBUI RFV @ IRK

GA UFS 29 Ar54-00 for aphate Economics Project Musbers 29 Ar59 00 Files MuSc33

0.016

81 KG 25 G 5675c 133c8 767c3 81. 81. 81. 81. 81. 81. 81. 5875c 13968 7c7c4 2.63 2.16 2.16 1.18 2.21 15.15 58755 13909 767c0 Leach 81. 81.5 81. 81. 82.5 82.5 82.5 58752 13968 72738 legis, 58752 13968 72750 1,56883 - F 4 10 2 2 2 3 2 2 2 .18 .23 .2.18 .18 .18 .2.91 .15.15 .18 2.18 2.18 .18 .18 .23 .15.15 1,68883 56752 13568 72760 8.5 8.5 8.5 8.5 8.5 8.5 8.5 58752 13968 72758 128883 - \$ \overline{1} \ 22.00 2.00 2.00 3.00 2.00 2.00 2.00 128889 58752 13.68 72750 81. 82. 83. 83. 83. 83. 83. 83. 83. 126663 58752 13968 72768 128684 . 18 2. 18 2. 18 . 18 . 23 . 29 15. 15 58752 13968 72769 128830 81. 81. 81. 81. 82. 82. 81. 81. 81. 81. 81. 58752 13968 72758 128854 58755 13968 72758 58752 13968 76768 1,28864 . 18 81.5 81.5 81.5 82.5 82.5 83.55 58752 13968 72760 128894 12868 58752 13%6 72758 128881 58752 13968 72758 128689 58752 13968 72758 128983 56752 13968 72720 128889 **光端からがあるがまだった** = ¤. ₹ . 18 . 23 . 29 . 25 . 15 58752 13968 72764  $\mathbb{R}^{\frac{3}{2}} \mathbb{R}^{\frac{3}{2}} \mathbb{R}$ 38752 13968 72720 Indirect Production Cost, Wilonne Total Cash Cost, Wyr Total Indirect Cost, Wyr Total Preduction Cost, Wyr Royalty @ 5% of sales price Taves (wisc) Offshore Accountations :. elitiati.: Firstog Handling and Storage Super, Cherical, Jech Total Indurect Cost Total Preduction Cost 5 Total Cash Cost 40 0000 Vessel Leading Administration Giste Dispisal

66433 66433 66433 9 15853 1883 13593 6557 63758 92758 35808 1758 36758 e0001 18339 Construction Capital Interest During Construction Lash Flow (Revenue-Prod Cost) fotal Investment P. e-construction uvestment

17175 0 1718 1830 1860 1860

13.3 x BR485

5EF ROT 1107 @ 188

4.8 42.63 2015/3 616. 100 PE - 100 12,3 1 4,8 42.88 201683 19 5165 -1 315 715 53,96 88. 88. 52. 52. 53. 53. 53. 54. 54. 54. 54. 195 82301 35 4.8 71608 15432 85558 E3439 E38407 28 TB 523 E23 54543 166601 4.8 42.88 20169 66763 17175 1878 1868 £±31c 575479 2915 T-05 th to 19-19 71684 14835 54644 cbac4 73966 27643 51263 42.43 42.43 201523 23. 83. 83. 83. 83. 83. 83. 83. 83. 5.17 61135 513167 3 193 5 14 71E03 14832 81640 105.372 26cci 77158 4.8 42.88 201688 15 28 3 71649 14832 81648 17.15 13,45 #8.2 E.S. BS. 75.1 F.S. BS. 75.1 F.S. BS. 75.1 183655 451972 75+31 35 26431 49838 153 4.8 42.80 20163 17175 25. 05. 50. 55. 55. 83. 83. 84. 84. 84. 84. 84. 84. 11.00 14 88. 88. 88. 88. 88. 88. 71808 14932 Ecc. 50 101937 35 2-60 42.08 201599 13 %: 83.5 5 %: 85.8 88.8 88.8 71898 14832 86640 17175 5/8% 33:931 6-15 71936 35 25193 11:19 585.4 15/34 42.63 42.63 20169 1542/5 2918 Holes there then there there there there there there there 567 W 71648 1-632 8:540 15,59 3 282.4 70278 35 245.37 45081 4.8 42.60 201620 171753 52. 83. 53. 53. 33. 83. 83. 83. 71808 14635 EEE+4 35 23936 218355 = 5883 E883 171/5 1000 96.785 68561 cecch 4.8 42.80 2016.80 1837.5 71838 14938 86648 62333 35 2998 # 5.5 # 22. 28. 2. 23. 23. 23. 3. 63. 3. 63. 68. 68. 54497 1000 55067 u cBcc4 **EE843** 42.48 42.48 20169 53301 2997 25. 85. 57. 83. 83. 83. 83. 71638 14832 84630 Sec. 139 1/1/5 SE IN 35 227 34 PCM 93350 65166 ć85...**4** 2,706 4.8 42.88 201538 22. 68. 2.10 2.3. 3.03 3.03 18.65 71808 14832 84633 22.5275 17.175 22.32.8 1000 # 5.5 # 57636 31632 15350 16831 31257 4.8 42.68 201688 2895 71808 14832 8c.640 834842 24045 **美麗田斯斯斯斯斯斯** 5. 18. 5. 2. 2. 5. 2. 2. 5. 6. 6. 5. 6. 6. 17175 89915 38675 28224 31816 35 10856 20168 61884 -2763 42.60 42.60 201563 25/6.5 17175 25763 1888 2004 .22 .28 .2.5 .23 .23 .3.63 71808 14832 6c640 25.92 25.93 25.03 26.03 66197 30640 28224 29333 35 16267 19066 64647 42.80 42.80 201639 2033 71808 1-832 86640 17175 27453 1883 86468 30675 27983 27532 35 9766 18136 59539 274823 4.8 42.00 201630 68262 184341 -291975 27171 25133 85133 4.8 48.8 86. 86. 72.1 72.1 88.3 88.3 88.3 88.3 22. 83. 22. 23. 3.63 3.63 71888 14832 86653 2003 2003 2003 7355 13004 94762 4.8 42.00 201608 2001 38.154 17175 38315 1888 .28 .28 .2.18 .25 .28 .28 .3.09 71646 14832 86640 56978 11484 11483 35 4919 7464 42.00 201699 71688 14832 86648 365490 2.000 55. 54.5 54.5 56.5 58.6 58.6 58.6 58.6 36549 1844 1869 75611 -138000 -66000 -21990 5843E -277500 -343500 -365490 -307654 84123 71808 14832 6c640 1999 2.4 42.80 #8. 88. 88. 72.1 72.1 88. 20150 -21990 1893 60033 60033 60033 1-1 1 1,000,00 1,000,00 1,3880,00 -5 1997 5.5.5 7.5.5 92.75 1936 -18889 -36754 -92754 -1889 -46754 -139564 1753 36750 -4 1935 52558 -5 1934 60061 Total Cash Eost Individe Production Eost, Wienne Direct Production Costs #/Tenne i transportation of the control of t Royalty # 5% of sales price Tital Indirect Cost, Wyr Tatal Pognottion Cost, Wyr Cash Flow (After Investment) Super, Clerical, Tech Offsbare Accompdations Production, Million TPY Depreciation (7 yr ACRS) Ricetig Handling and Storage Tutal Indirect Cost Total Cash Cost, Wyr Frincipal Bajkent Interest 6 12% Replacement Capital Stal Production Cost Sales Price, W/Tonue ÷ Income law Net Income Aiter D Administration Sales ictal Ir estuent Pessel Loading Production Costs Waste Disposal **Harking Capital** Eereficial lon Count Cash Flow (351e) Total Revenue Texable Income Sales Revenue Project Year Tan Rate, " Fr Incipal beplet ron DOEROT NEV è 183 Cash Flow Mining 13485

14)						
		¥				
2						
(6)						
	ÿ					
					2)	
1 3						
rest ye						
**						

### **SECTION 6**

#### HEAVY MINERAL DEVELOPMENT FEASIBILITY

### 6.1 INTRODUCTION

Exploitation of heavy minerals occurring offshore the Atlantic coast of Georgia in OCS waters relies on data and information produced in previous reports. Publications of the Bureau of Mines and Minerals Management Service of the U.S. Department of Interior and of the Marine Mining Journal are the sources of most costs.

This section deals with the possible potential for commercial exploitation of these minerals by employing technology which has been tested in other offshore mineral mining ventures, and/or in offshore oil and gas exploration and production operations. The applicability of the technology to heavy minerals is reviewed in a comparison of alternative configuration schemes. The preferred scenario, which is the result of this comparison, is based on mining and partial on-board beneficiation by an ocean-going vessel. The suction-type hopper dredge commonly employed by United Kingdom and European operators is the obvious choice. These mining-processing platforms are not currently manufactured in the U.S. Final processing of the intermediate product is conducted offshore in a platform-mounted plant. Finished product is transported to port for sales and distribution. Capital and operating cost estimates are based on data gathered from researching previous publications, and from in-house experience with land-based heavy minerals operations. Economic viability is evaluated by discounted cash flow techniques based on the application of several variable cost scenarios.

### 6.2 MINING

## 6.2.1 Area Selection

Section 3 describes the processes that form heavy mineral deposits and how the mineral database was formed. The selected mining area is based on computer modeling techniques using the following sources:

- o discrete points from unpublished "sparker" seismic profiles received from Peter Popenoe, U.S.G.S.,
- o data file of sampling point on the continental margin off the Georgia

  Coast received from the USGS Woods Hole
  - percent sand fraction code line 210
  - percent of sand fraction consisting of heavy minerals, quartz, and feldspar - code line - 320
  - species of heavy minerals code line 560.

A distinct trend of heavy mineral concentration in ocean bottom grab samples is evident. This trend is supported by total percent mineral species as well as individual species information for rutile, monazite, zircon and staurolite. It should be emphasized that sampling points are widely spaced and have an average area of influence over 11,000 square kilometers. None of the actual sampling points were within the selected mining area. Figure 6.1 shows the selected mining area and geological trends. The selected area has a greater heavy mineral thickness and better data reliability than the trend located closer to shore.

The location and site characteristics are described in Tables 6-1 and 6-2.

Table 6-1

	AMS Cod	ordinates	Lat. and Long.
	_East_	North	
SW	543000	481400	80°32'39.14", 31°28'05.64"
NE	557600	495400	80°23'34.32", 31°35'38.11"

(Approximately 18.0 km by 1.5 km) (Area =  $28,134,100m^2$  or 6,952 acres)

Table 6-2
Site Characteristics of Mining Area

		Meters		Meters <sup>3</sup>
Item	Average	Min.	Max.	Volume
Water Depth	27.2	26.4	29.7	
Ore Thickness	10.4	9.8	11.8	292,200,000
Total Mining Depth	37.6	36.4	41.4	
Heavy Mineral Percent	3.6	2.6	4.0	

Since no adequate heavy mineral species data have been made available, for the purpose of this study only, it has been assumed that the contained heavy mineral content expressed in the model represents the total percent oxides of heavy minerals.

Site characteristics show that the total available tonnes of mineral-bearing sands within the study's orebody outline (520,100,000 tonnes) are more than sufficient to support a 15,300,000 tonne per year mining operation for a period of 20 years at minimum (306,000,000 tonnes).

# 6.2.2 Configuration and Production Rate Comparison

Although, at first, the topics of project configuration and production rate appear unrelated for Georgia offshore mining, the production rate depends upon project configuration. As such, they are included in the same discussion.

The annual production of any mineral beneficiation facility is dependent on the ability of the mine to supply ore. Normally, plant production is based on operational efficiency, largely independent of mining because of the ease in providing large stockpiles of plant feed. Most heavy mineral production is based on a linkage between mining, ore transportation, and the plant washer. High operating factors are realized and ore storage is not a requirement. Operating factors for most ocean mining equipment are low compared to onshore mining. This is due to climatic and other conditions beyond the control of the operator.

Production based on mining of ore at sea for beneficiation at a remotely located land-based facility is greatly dependent on the effective operating factors of the excavating and transporting equipment and systems.

As a basis for uniform comparison of alternative configuration schemes certain criteria were established. The criteria adopted for comparative evaluation given below in Table 6-3 are based on previous work and on reported experience with ocean-going dredges and transportation systems. These criteria were later modified to better fit the preferred mining equipment and systems configuration.

Ocean-going vessels equipped for mining are large, containing hoppers for collecting dredged material. These vessels also serve as transports and, therefore, their availability for mining is very limited. Investment is high and utilization for mining is low. This appears to be the norm as is experienced by operators who use these types of foreign-built dredges in the North Atlantic, Pacific Ocean and Sea of Japan. These systems are most effective where there is little or no overburden, where the ratio of ore to product is low, and where concentration takes place on board.

Table 6-3
Criteria Basis for Configuration Comparison

# Annual Mining Equipment Availability

Days lost:	
annual dry dock/repairs	30
adverse weather/sea conditions	36
	66
Days operational (1)	299
Hours/day operational	21
Mechanical availability	90%
Effective operating hours	5,651
(299 × 21 × .90)	,

<sup>(1)</sup> See Table 5-15, Climatic and Physical Oceanographic Data for basis used to determine days operational.

Table 6-3 (continued)

Item Description		Unit	Value
Average overburden thickness		meters	None
Average ore thickness		meters	9.80
Ore density		tonnes/m <sup>3</sup>	1.78
		lb/ft <sup>3</sup>	111
Mining recovery		percent	65
Suction head pipe or dredge pump discharge diameter		mm	900
inches		36	
Pipeline velocity		m/sec	4.92
		ft/sec	16.1
Dredge production dry solids	ú	m <sup>3</sup> /yr	10,300,000
	2	tonnes/hr	3,240
Average slurry solids		percent	26
Washer rejects		percent	50
Distance to land-based beneficiation plant		nautical miles	50
Average vessel speed		knots	12

Because sea-going suction head hopper type dredges have a long and successful history of operating under ocean conditions they are considered here in evaluating alternative configuration schemes.

The four major project configuration schemes considered for offshore heavy mineral production are:

- Sea-going hopper dredge for mining and transportation to an onshore plant.
- Sea-going hopper dredge mining and barge transportation of ore to an onshore plant.
- 3. Dredge mining, pipeline transportation of ore to onshore plant.
- 4. Dredge mining, pipeline transportation of ore to a nearby offshore island plant.

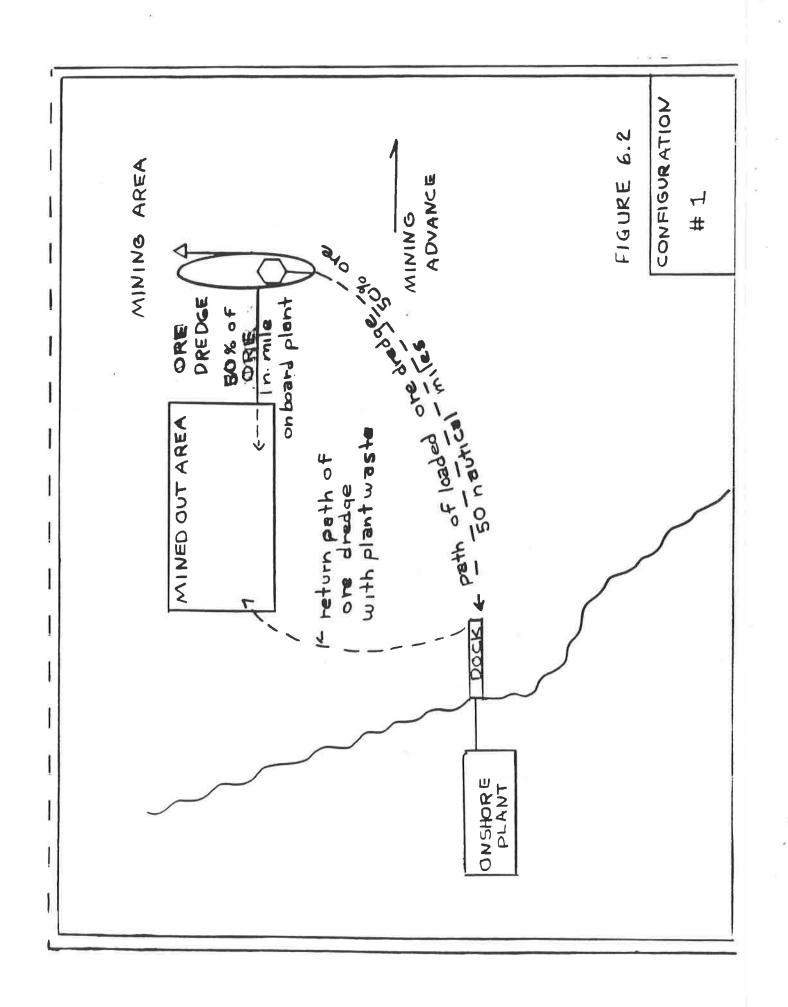
The mining dredge vessel or platform in each of the four major configurations is equipped with an onboard processing (washing) plant. Flowsheet data indicate that about 50% of the dredged material can be eliminated by washing. This reject material, a mixture of gravel oversize and sediments, would be disposed of in nearby mined-out areas. In Configurations 1, 2, and 3, matrix is transported, after washing, to a land-based plant for further processing. In configuration 4, matrix is transported by slurry pipeline from the dredge vessel to a nearby offshore plant for further processing. The physical dredge vessel size is determined by the necessity of making the vessel seaworthy, not by the dredging equipment. In Configuration 1 a large hopper is required for storage as the dredge is also the vessel used to transport ore, after washing, to shore.

Since dredge vessel size is larger than required for the dredging equipment alone, the addition of a washing plant costs only slightly more than if located onshore. Plant operating costs are identical. However, with onboard processing, material transported to shore decreases by 50%, resulting in a corresponding reduction in transportation costs of 50%. In addition, waste disposal of the 50% fraction rejected by washing at an onshore plant must be either re-transported from the plant and disposed of in the mined-out areas, or disposed of in tailing impoundments onshore. Either way, the on-vessel washing plant reduces costs considerably by wasting the 50% fraction rejected in nearby mine areas.

The cost comparisons indicate that an on-board washing plant is also favored for configuration 4, even though the cost savings are not as pronounced as for the other configurations.

# Sea-going hopper dredge for mining and transportation to an onshore plant.

Figure 6.2 shows this configuration. Since the mineral sands are on top of the ocean bottom, no overburden dredge is required. An anchored suction head dredge mines ore by removing the total ore horizon, then moves forward by mining the resulting bank. Mining recovery is limited to about 65% with this system. The anchored suction head dredge deposits the ore into a distribution box, from which it is screened, washed and desilted.



About 50 percent of the material is loaded into a hopper on board the vessel. Here, through a series of weirs, the washed matrix is dewatered to 75% solids. When the hopper is full, the suction head and pipes are raised from the bottom to the deck. The dredge now functions as a normal merchant ship and carries the material 50 nautical miles to the plant site. The plant site is located in an industrial area on or near Hutchinson Island, where permitting problems and land acquisition problems are minimized. It is felt that an onshore plant located closer on the barrier islands to the mining operation would be environmentally unacceptable.

Cost for hopper dredges were taken from the open file report "An Economic Reconnaissance of Selected Heavy Mineral Placer Deposits in the U.S. Exclusive Economic Zone" by the Bureau of Mines Washington Staff, released 4-87. Capital costs are based on U.S.-built hopper dredges constructed between 1977 and 1985. Operating costs are from actual operating conditions.

For a hopper dredge, cycle times consist of loading, travel, unloading and return travel. The hopper size increases capacity, but also increases capital. In an attempt to optimize hopper size, four loading capacities were analyzed. Table 6-3 shows the design criteria used to determine productivity and costs.

Loading and unloading is done by a 900 mm pump using the criteria in Table 6-3 at the hourly rate of 3,240 tonnes per hour

Table 6-4 shows the time required for each element in the cycle. The cycles per year are based upon 5,651 hours. The tonnes per cycle are based upon the loading time, which is different for each case. Table 6-4 also lists the tonnes per year of product produced for each capacity. As Table 6-4 shows, increases in loading times (hopper capacity) result in only a slight increase in tonnes per year of product.

Table 6-4
Cycle Time Configuration 1

Item	Hours	_Hours_	Hours	Hours
Load Ore	5.00	10.00	15.00	20.00
Travel to Plant	4.17	4.17	4.17	4.17
Unload Ore	5.00	10.00	15.00	20.00
Load Tails	5.00	10.00	15.00	20.00
Travel to Mine	4.17	4.17	4.17	4.17
Dump Tails	5.00	10.00	15.00	20.00
Total Cycle Time	28.34	48.34	68.34	88.34
Cycles per year	199.40	116.90	82.70	63.97
Tonnes per cycle	8,100	16,200	24,300	32,400
Tonnes hauled	1,615,000	1,893,000	2,009,000	2,072,000
Tonnes mined	3,230,000	3,786,000	4,018,000	4,144,000

The following USBM equations from Open File Report 4-87 were used:

(P) Hopper Capacity = 
$$\frac{\text{Daily Haul Capacity (DHC)}}{2.9607(\text{L})^2 \cdot 2923}$$

### Where

DHC = short tons hauled divided by operating days

L = one way haul distance in nautical miles

Operating Days = 299

Short tons hauled will be determined

Dredge capital cost = \$7,052 (P)-9421

Plant capital cost =

Onboard processing facilities =  $319.12(\times)0.960$ 

Onshore processing facilities =  $22,500(\times)0.68$ 

where X is plant feed in short tons per day.

Table 6-5 is a summary of calculated hopper sizes and the resulting capital required for each production rate from Table 6-4. The overburden dredge does not require a large hopper and its cost is estimated from other sources. Dollars per ton capital is based on 20 years of mine production for each production scenario.

Table 6-5
Capital Costs Configuration 1

			-	Mil	lions of	Dollars		
Million Pr	rod.Tonnes	Hopper	Mt.	Ob.	OS			\$*M
Annual	20 Years	Tons	Dredge	Plant	Plant	Misc.	Total	Ton
3.230	64.6	6,308	26	3	8	11	48	.75
3.786	75.7	7,394	31	3	9	13	56	.74
4.018	80.4	7,847	33	3	10	14	60	.75
4.144	82.9	8,093	34	3	10	14	61	.74

Operating costs for the suction head hopper type ore mining dredge are based on the following U.S.B.O.M. formula (from Open File Report 4-87).

Dredge operating cost (
$$\frac{s}{s.t.}$$
) =  $\frac{2.7534 (P) + 5,453}{Daily Dredge Capacity}$ 

where P = payload or hopper capacity in short tons daily dredge capacity = annual capacity in short tons + days.

Onboard processing facilities =  $25.5(\times)^{-0.520}$ Onshore processing facilities =  $59.4(\times)^{-0.345}$ 

where X is the plant feed throughput in short tons per day.

Table 6-6

Operating Cost - Configuration 1

Operating Cost \$/Metric Ton Product

Tonnes Mined	Dredge	O.B. <u>Plant</u>	O.S. Plant	Total
3,230,000	\$2.11	\$.21	\$1.63	\$3.95
3,790,000	2.04	.20	1.54	3.78
4,020,000	2.01	.19	1.51	3.71
4,140,000	2.00	.19	1.50	3.69

Table 6-7

Total Comparative Cost per Tonne, Configuration 1

Tonnes Mined	Capital		Operation	Total
3,230,000	\$	.75	\$ 3.95	\$ 4.70
3,786,000		.74	3.78	4.52
4,018,000		.75	3.71	4.46
4,144,000		.74	3.69	4.43

# 2. Sea-going Hopper Dredge Mining, Barge Transportation of Ore to an Onshore Plant

Figure 6.3 shows this configuration. The dredge pumps mined ore into a distribution box from which it is screened, washed, and desilted. About 50% of the ore is removed by onboard washing and disposed of in mined-out areas. The remaining 50% of the ore is dewatered to 75% solids aboard 26,000 tonne barges. These barges are towed to the onshore beneficiation plant by tug boats. After ore is unloaded by pumping it from the barge into live storage containment, the barge is towed back to the overburden dredge and another cycle begins. In order to avoid a large tailings area, an independent fleet of barges and tugs load, transport, and dump the plant tailings in the mined-out areas. By providing storage at the plant and a separate waste disposal sytem, the plant operation is not directly tied to the mine.

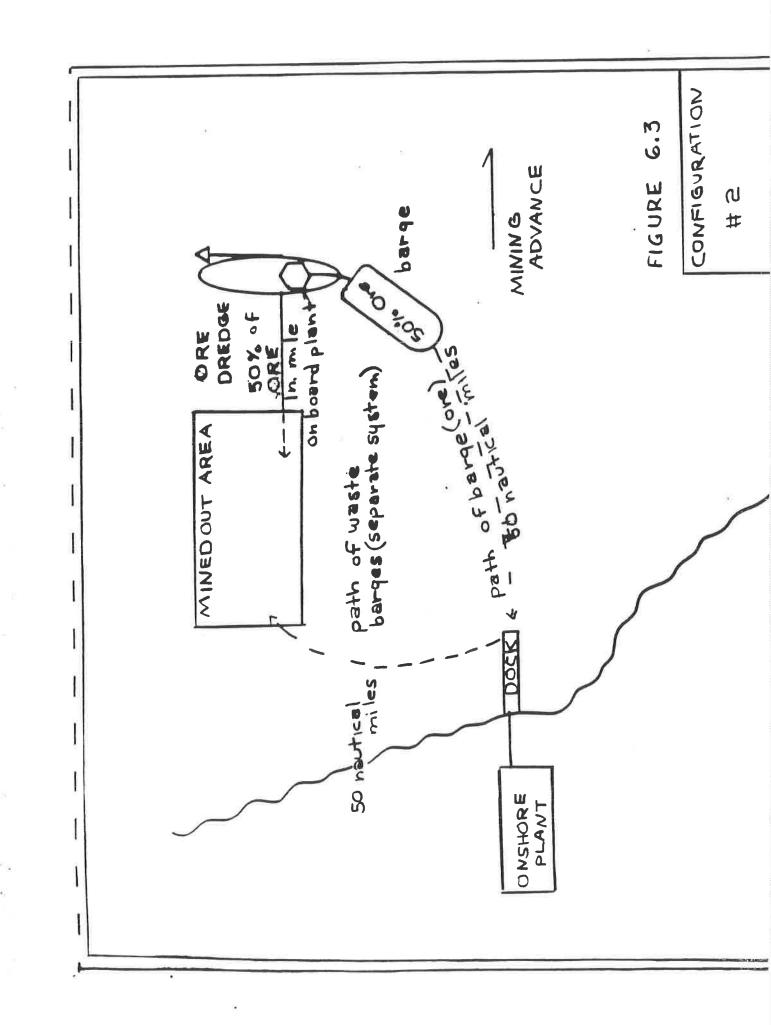


Table 6-8 shows the time required for each element in the cycle. Criteria from Configuration 1 apply here with the exception that barges move at 8 knots.

Table 6-8

Cycle Time Configuration 2

Item	Hours
Load barge	12.03
Barge to plant	6.25
Unload barge	12.03
Barge return	6.25
Total cycle time	36.56
Cycles per year	154.8
Tonnes per cycle	19,500
Tonnes hauled per year	3,019,000

Since the dredge mines 18,310,000 tonnes of ore annually, the number of dredges required is:

$$18,310,000 (.5) + 3,019,000 = 3.03 \text{ or } 3$$

The waste cycle is assumed to be similar to the ore handling cycle. Since the mineral concentration is only 6%, most of the waste from the onshore plant is barged back to the mined-out areas. In all, a total of seven barges and tugs are required, three for ore handling, three for waste disposal, and one for a spare.

Capital costs are calculated using the same methodology as Configuration 1.

Table 6-9 itemizes the capital required for comparison of Configuration 2.

Table 6-9
Capital Cost Configuration 2

Item	mm \$ Unit <u>Cost</u>	No.	Total Cost
Barges Tugs Ore dredge Beneficiation Plant Onboard Plant Infrastructure & Misc.	16.2 5.5 40.00 27.00 13.80 30% of above	7 7 1 1	\$113,400,000 38,500,000 40,000,000 27,000,000 13,800,000 69,800,000
Total			302,500,000
\$ per tonne annual mined	d		16.52
\$ per tonne mined mine	life (20 years)		.83

Operating costs for the plant are computed using the same methodology as for Configuration 2. Dredge costs are from ZW model explained in Section 5.7 (Operating Costs).

Table 6-10
Operating Costs Configuration 2

	Cost per tonne product
Mining Dredge	.42
Plant onshore	.90
Plant onboard	.09
Barge transportation	n .39
Waste disposal	39
Total	\$2.19

The total comparative cost for Configuration 2 is \$3.02 per tonne product.

# 3. Dredge mining, pipeline transportation of ore to onshore plant

Because the location of the plant is upstream on the river, a pipeline system is not feasible. A substantial part of the pipeline would lie across shipping channels and industrial installations. For this reason, as well as environmental considerations, the pipeline system was not considered in further detail for this report. This is the same conclusion reached by other investigators, i.e., Zellars-Williams, 1979, and Development Planning and Research Associates, Inc., 1987 North Carolina Offshore. Figure 6.4 illustrates the configuration.

# 4. Dredge mining, pipeline transportation to offshore plant

A sea-going dredge mines are and pumps it to the on-board washer. The partially beneficiated are is then pumped directly to a nearby offshore plant. This plant is built on an island formed by dredged material, located equi-distant an average of two nautical miles from the mining areas. The pipeline is flexible and most of it is submerged. Only the flexible portion near the dredge is floating. At the beneficiation plant, partly beneficiated are is processed, and a saleable product produced. Waste is pumped through a separate pipeline to mined-out areas and released. All processing is done at the island-based processing plant. Product from the beneficiation plant is barged to shore for sale. The dredge production is identical to Configuration 2. Figure 6.5 illustrates this configuration.

Barges or vessels are only needed to transport the product to the final destination. No extra cost was added since the final destination is not known.

Capital costs are summarized in Table 6-11. The only difference from Configuration 2 is the the island cost, and pipeline cost.

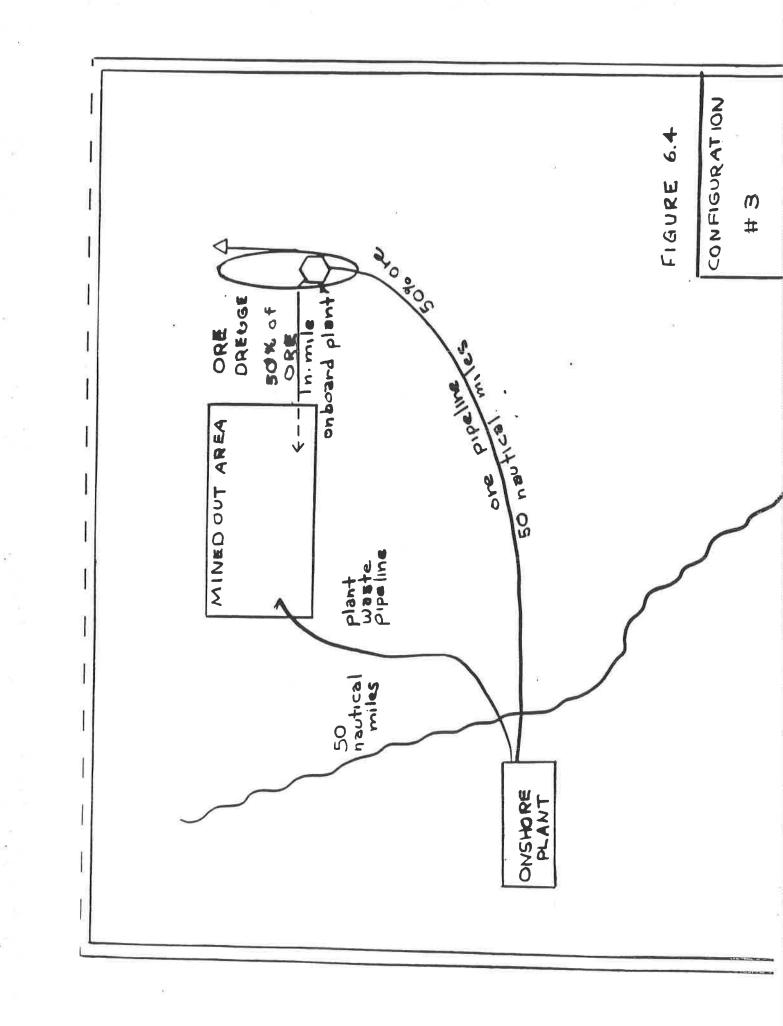


FIGURE 6.5

CONFIGURATION

**丁** #

Table 6-11
Capital Cost Configuration 4

Item	mm \$ Unit Cost	1	<u>vo.</u>	Total Cost
Ore dredge Beneficiation plant Onboard plant Island Pipelines Infrastructure & Misc.	40,000,000 27,000,000 13,800,000 60,000,000 2,500,000 30% of above		1 1 1 2	40,000,000 27,000,000 13,800,000 60,000,000 5,000,000 43,700,000
Total Capital				189,500,000
Tonnes mined				18,300,000
\$ per tonne annual production (mined)		:00		10.36
\$ per tonne (mined) mine life (20 years)				.52

Operating costs for dredge costs and waste disposal were computed using Zellars-Williams operating cost model. Plant costs are from the U.S.B.M. model. Table 6-12 summarizes the operating costs.

Table 6-12
Operating Cost Configuration 4

<u>Item</u>	\$ Cost per tonne
Mining	.42
Plant (onshore)	.90
Plant (offshore)	.09
Waste/water	51
Total	1.92

The total cost for comparison of Configuration 4 is \$2.44 per tonne of product.

# 6.2.3 Selection of Configuration

It is evident that from a material handling standpoint, the offshore plant should be more efficient. Material is processed near the plant and wasted near the plant in mined-out areas. With onshore plants, washed matrix is hauled 50 nautical miles by barge and tug, processed, and the waste hauled 50 nautical miles back to the mined-out pits for disposal. Table 6-13 outlines comparative capital and operating costs for each configuration. Based upon this trade-off study, Configuration 4, utilizing an offshore plant, was selected as the basis for examining the economic feasibility of exploiting offshore heavy minerals. This configuration is developed in further detail in the following parts of this section.

Table 6-13
Configuration Selection
\$ per tonne concentrate

# Annual Production

Configuration	Tonnes	Ca	pital	Operating	Total
1	851,000	\$	.74	\$3.69	\$ 4.43
2	18,300,000		.83	2.19	3.02
3	Not feasibl	e (n	o econo	mics done)	
4	18,300,000		.52	1.92	2.44

Configuration 1)	Sea-going hopper dredge for mining and transportation to
	an onshore plant.
Configuration 2)	Seagoing hopper dredge mining and barge transportation
	of ore to an onshore plant.
Configuration 3)	Dredge mining, pipeline transportation of ore to onshore
	plant.
Configuration 4)	Dredge mining, pipeline transportation of ore to nearby
	offshore island plant.

# 6.2.4 Design Criteria

Table 6-14 lists the design criteria used for determining production limits, operating costs, equipment needs, and capital requirements of the selected configuration. As with any mining project, the physical and chemical geologic parameters are site-specific, having been determined by nature. These characteristics were based upon the initial mine site selected in Section 5.1.1.

Operating factors were determined by past experience, as well as consideration of the unique mining environment. In the case of offshore dredging, it is necessary to consider the size and design of the dredge from a seaworthy standpoint. A large vessel is necessary to accommodate the mining depths; therefore, required size is somewhat independent of production. The largest dredge pumps operating in ocean mining today have a suction head pipe diameter of 1200 mm (48"). For the conditions of offshore Georgia, a 900 mm diameter (36") suction head pipe was used to determine productivity. The design philosophy is to use the largest practical dredge pump, mounted on a seaworthy vessel. For example, a dredge pump producing half the capacity of a 900 mm dredge pump gives only a small reduction in capital and operating costs. Therefore, the design philosophy maximizes production while minimizing the costs.

Table 6-14
Design Criteria

0	Grade Criteria:			
	Feed Grade: Ilmenite Rutile Leucoxene Zircon		5.31% .35% .87% .62%	
	Monazite		.17%	
0	Recoveries:		Wet	Dry
	Ilmenite	Mine	Mill	Mill
	Rutile	92%	83%	97%
		92%	85%	97%
	Leucoxene	92%	70%	95%
	Zircon	92%	92%	90%
	Monazite	92%	70%	90%

Table 6-14 (continued)

## o Operating Factors

Average Ore Thickness

Ore Density, tonnes/cm

	Dredge and Washer Beneficiation Plant	4,700 4,700
0	Mining Data	
	Average Water Depth Maximum Mining Depth (below MSL) Average Mining Depth Maximum Ore Thickness	27.2 41.4 37.6 11.8

Note: Oceanographic information is contained in Table 5-15.

Section 4 lists the available state-of-the-art technologies. Anchored hopper dredges have been used successfully in the Pacific Ocean for commercial sand and gravel mining. The heavy mineral sands are not consolidated, so a system utilizing this dredge is reasonable.

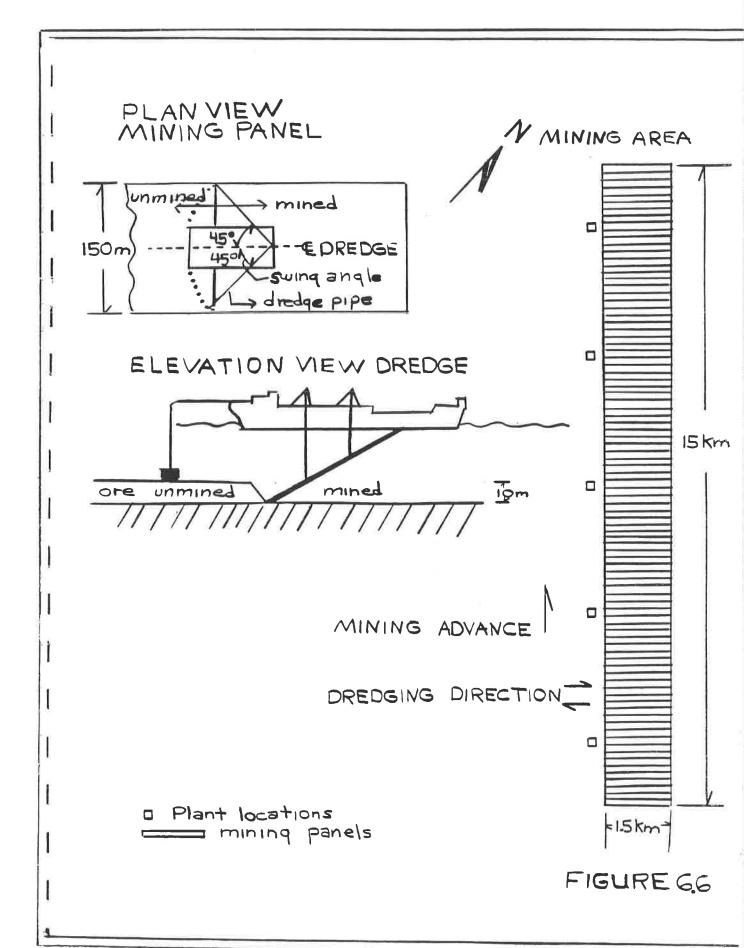
10.4

1.78

### 6.2.5 Mining System

The heavy mineral mining area shown in Figure 6.6 is 15 km long and 1.5 km wide. This is a simplified depiction of the strand identified and selected for mining. The anchor suction dredge will start mining at the south end of the mining area. By moving forward slowly through winches operating against anchors, the dredge is able to mine the full 10 meter face. Movement side-to-side is controlled by winches which swing the dredge about 45° each side of the center line. With the anchor pivot point 100 meters from the dredge intake, the dredge can mine about 150 meters wide. This "150-meter width" is called a panel.

The anchor dredge starts mining at the south end of the mining area. Movement across the narrow orebody is accomplished by mining panels 150 meters wide. Within these panels a cut face, about 10 meters deep by 150 meters wide, is developed. After the dredge finishes mining the first panel, it reverses direction and mines the adjacent northern panel. Dredge movement is alternately east to west, then west to east, in panel increments. Mine advance is south to north.



On-board the dredge is a wet mill designed to eliminate 50% of the ore which is without heavy minerals. This wet mill is fed directly from the dredge. Waste material from the washer plant is placed in a collection hopper, dewatered to 40% solids, and pumped to mined-out panels. For the first 1000 meters of mining, waste must be disposed of outside the mining area. From this point, a steady-state operation is reached, with disposal 1000 meters from mining. Any closer than 1000 meters could result in some waste being carried into the present mining operations. If necessary, preventive measures, such as turbidity curtains could be maintained between the mining area and the disposal site. However, with 1000 meters between the disposal areas and current mining, it is not anticipated that disposal in mined-out areas will drift into and dilute currently mined ore.

The waste disposal pipe is 24"-30" in diameter and is attached to the dredge with flexible pipe. The pipeline is attached to flotation devices every 50 meters. A small tug will be required to move the pipe into position for waste disposal.

Concentrate from the wet mill is placed in a distribution hopper, dewatered to 40% solids and pumped to the floating dry mill. A 20" pipeline is required to pump 1600 tonnes per hour. When distance exceeds 2.1 km, the dry mill is moved 3 km north and continues to operate at that location until pumping distance again exceeds 2.1 km. Again, the dry mill moves 3 km north. Over 20 years of mine life, the dry mill is moved four times. More mill detail is given in Section 6.3

#### 6.3 PROCESSING

#### 6.3.1 Design Basis

The processing facilities are designed to recover rutile, ilmenite, leucoxene, monazite, and zircon from heavy mineral sand deposits typical of those found off the coast of Georgia. Processing facilities include an initial concentration plant (wet mill) located onboard the dredge, and a platform-mounted recovery plant (dry mill) located 1 to 3 miles from the wet mill. Sea water will be used for processing at both the wet and dry mills.

Because of probable periods of unscheduled maintenance and unfavorable sea conditions, the dredge wet mill and dry mill are scheduled to operate 250 days per year, 21 hours per day with a 90% availability. This results in 4,725 operating hours per year.

The mineral distribution in the mineral sand deposit is calculated from Open File Report, USBOM 87-04, using annual production estimates for mean grades of the minerals. The in-situ mineral distribution is summarized in Table 6-15.

Table 6-15

Percent Distribution of Individual Minerals

(in-situ)

Mineral	Mineral Classification	Ore Per	cent of Mineral
Ilmenite Rutile Leucoxene Zircon Monazite	Heavy Heavy Heavy Heavy Rare Earth	5.31 0.35 0.87 0.62 0.17	72.54 4.78 11.89 8.47 2.32
Totals		7.37	100.00

Overall recovery for the orebody for the individual minerals is presented in Table 6-16. The overall recovery of 72.42% was based on a mining recovery of 92%, an average wet mill recovery of  $82\%^{(1)}$ , and an average dry mill recovery of  $96\%^{(1)}$ . Product tonnages are based on 15,300,000 tonnes/year of ore to the dredge.

# 6.3.2 Initial Concentration Plant (Wet Mill)

The initial concentration plant or wet mill is located onboard the dredge. The onboard processing facilities include trommel screens to eliminate

<sup>(1)</sup> Based on "in-house" information of recoveries at heavy mineral operations and are considered a realistic representation of the products which could be recovered.

Table 6-16

Percent Distribution of Heavy Minerals to Final Product

	duct	Tonnes	601,750	40,600	81,460	72,250	15,040	811,100 (2)
	Product	Wt %	53.73	75.85 3.63	7.27	6.45	57.96 1.34	72.42
	Overall	Rec.	74.07	75.85	61.18 7.27	76.18	57.96	72.42
ls	Mili	8	97 53.73	97 3.63	95 7.27	90 6.45	90 1.34	96 72.42
Minera	Dry Mill	Rec.	16	6	95	90	90	96
Weighted % Distribution of Minerals	Wet Mill	8	55.39	3.74	7.66	7.17	1.49	75.45
6 Distri	Wet	Rec.	83	85	70	92	70	82
eighted 9	Mining	%	41.99	4.40	10.94	7.79	2.13	92.00
*	Σ	Rec.	92	92	92	92	92	92
U	Toppe		812,419	53,534	133,163	94,861	25,983	1,119,960 (1)
Distribution	Mineral	in-situ in-situ	72.54	0.35 4.78	11.89	8.47	2.32	100.00
	Ore	% in-situ	5.31	0.35	0.87	0.62	0.17	7.32
		Mineral	Ilmenite	Rutile	Leucoxene	Zircon	Monazite	

Notes:

(1) (15,300,000 tonne/year ore)(.0732) = 1,119,960 tonne/year in-situ minerals in ore.

<sup>(1,119,960</sup> tonne/year minerals)(.7242) = 811,100 tonne/year recoverable minerals. (2)

oversize material (+10 mesh), cyclones to reduce fines (-200 mesh), and spirals to concentrate the heavy minerals and reject the lighter fractions. Spirals were chosen because they are least affected by ship motion production by wave action.

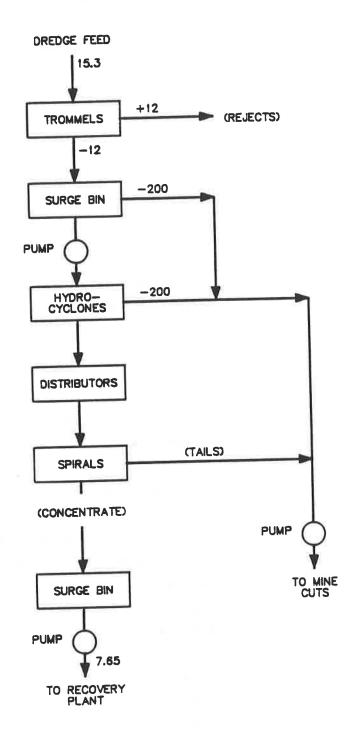
Approximately 50% of the ore consisting of +10 mesh rejects, -200 mesh fines (sediments) and spiral tails is eliminated at the wet mill. This reject material is combined and pumped to the mined-out areas for disposal. Typically, the discharge point would be well below sea level in order to minimize dispersion.

Spiral (rough) concentrate is collected in a surge bin (4 hour capacity) and is then pumped to the platform-mounted recovery plant or dry mill. A flowsheet/material balance for the initial concentration plant is given in Figure 6.7

## 6.3.3 Recovery Plant (Dry Mill)

Rough concentrate from the wet mill reports to a feed surge bin. The bin is designed to provide about 8 hours of live feed storage, smooths out upstream process surges, and helps to maintain a constant rate of feed to the recovery plant. When the bin overflows, it also removes fines. Feed is reclaimed from the storage bin as a slurry and is pumped to the primary vibrating screens where +48 mesh material is removed and sent to the rod milling circuit. The rod mill discharge is treated by hydrocyclones to remove -200 mesh fines and then returned to the primary vibrating screens.

Minus 48-mesh sand from the primary vibrating screens is passed through rougher cone concentrators (Reichert cones), and then concentrating tables, to produce a material containing 70 to 80 percent heavy minerals. Tailings from the cones and tables are sent to scavenger cones to recover additional heavy minerals. The scavenger concentrate is recycled to the rougher cones, while the scavenger tails are discarded.



XXX - DENOTES RATE IN MILLION DRY TONNE/YR.

GEORGIA OFFSHORE
MINERALS ASSESSMENT
DATE: 5-17-88 BY: MEK

ZW

INITIAL CONCENTRATION PLANT FIGURE 6.7

Most of the ilmenite contained in the heavy mineral concentrate is removed using high-intensity wet magnetic separators. The remaining material is dewatered using classifiers, then dried and heated prior to electrostatic separation. A high tension electrostatic separator is used to separate the conductors (ilmenite, rutile and leucoxene) from the non-conductors (monazite and zircon). A middling fraction is returned to the high tension electrostatic separator feed.

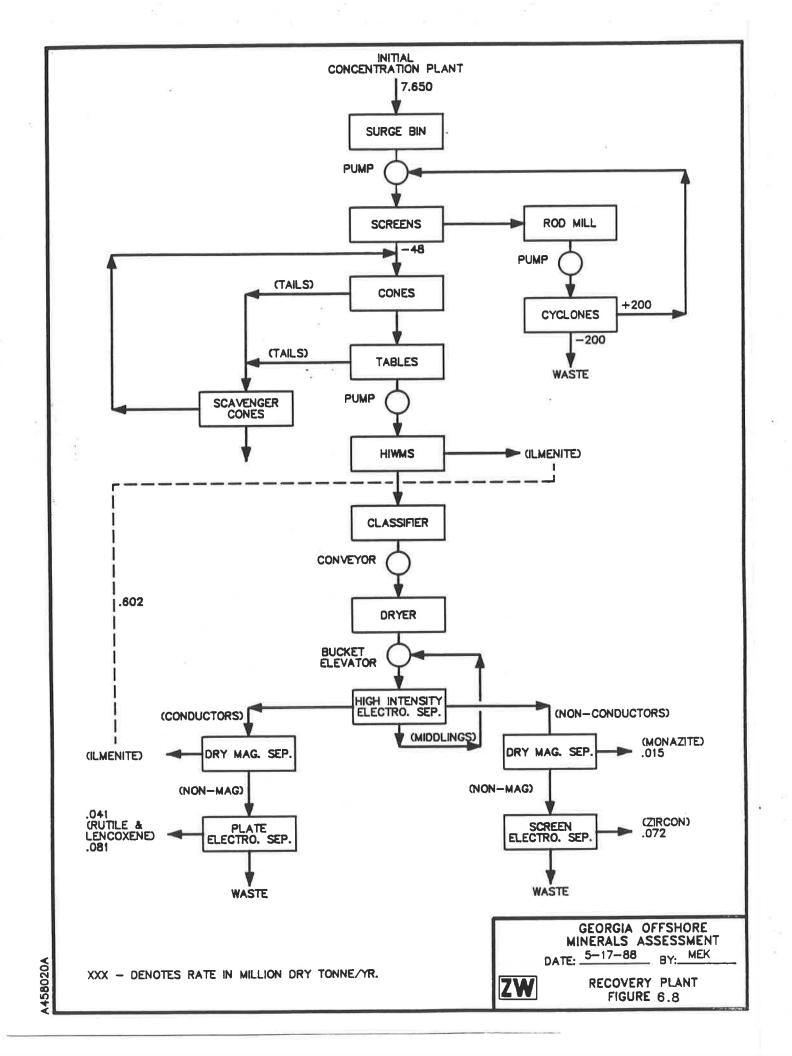
Conductors first report to a dry magnetic separator to recover ilmenite not removed by the high-intensity wet magnetic separators. The non-magnetic conductors are then concentrated into a rutile-leucoxene fraction using plate electrostatic separators. A middling fraction is returned to the plate electrostatic separator feed.

Non-conductors from the high tension electrostatic separators are fed to dry magnetic separators where the monazite fraction is recovered. The non-magnetic non-conducting material then flows to screen electrostatic separators which recover the zircon fraction.

A flowsheet/material balance for the recovery plant is given in Figure 6.8.

In practice, the waste streams from the plate and screen electrostatic separators usually contain other minerals such as sillimanite, kyanite and staurolite, which can be recovered as byproducts. "Zircor" is a product made by heating sillimanite, kyanite and zircon, and marketed as a foundry sand substitute for zircon.

The -200 mesh fines (sediment) and most of the tailings from the dry mill will be combined and pumped to the mined-out areas. Typically, the discharge point would be well below sea level in order to minimize dispersion. The discharge line would require periodic tending to move the effluent point for even distribution of the mined area backfill.



### 6.3.4 Water Requirements

Water is used extensively in mining and beneficiation as a processing medium and as a means of transporting solids in the form of aqueous slurries. The source of water for the initial concentration plant (wet mill) and the recovery plant (dry mill) is sea water.

It is assumed that the recovery plant efficiency and/or product quality is not affected by the presence of chlorides (sea salt) and that a fresh water wash is not required.

## 6.3.5 Product Storage and Loading

Products from the recovery plant will be stored in bins and transferred to vessels/barges alongside the platform, via a shiploader.

## 6.4 CONFIGURATION AND INFRASTRUCTURE

The most favorable configuration for the exploitation of heavy minerals offshore Georgia requires the use of state-of-the-art ocean mining equipment. Seabed mining world-wide is dominated by pump-type ocean-going vessels having hoppers to contain and transport dredged materials. These dredges are known as suction hopper dredges. They may be of the trailing suction head type, or they may be of the leading suction head type. The latter type, which operates at anchor, is preferred for heavy minerals because it permits excavation of the entire mineral-bearing sand horizon. Since no overburden sediments occur in the area targeted for mining, this type dredger will remove all of the mineral-bearing sand within the scope of its anchor chain and suction pipe arm before moving forward. These dredges are essentially ocean-going seaworthy vessels equipped with the specialized apparatus required, and are built in European, Taiwanese, Korean and Japanese shipyards. United Stated shipyards are not able to compete in this market.

The preferred dredge is a vessel with a hopper capacity of about 5000 m<sup>3</sup>. The hydraulic mining system consists of a suction head, suction pipe arm, a submerged slurry pump, and on-board booster pumps.

This dredge must be capable of mining to about Elevation -140, or 160 to 170 feet below sea level. Depending on specific design, the suction arm will be as much as 300 feet long. The lower end of the arm is hinged to permit raising and stowing within the length of the vessel.

Mineral sands mined from sea bottom are pumped as a solids-water mixture by the submerged pump to an on-board wet processing mill. The wet mill rejects oversize, barren light weight particles and tailings which are wasted overboard. About 50% of the mined materials are rejected from the shipboard plant, and directed to previously mined cuts at sea bottom. The concentrated mineral-laden sands are collected in the hopper. This hopper acts as a live storage sump feeding the suction side of the booster pump(s) which transfer the concentrate slurry to a nearby dry mill via semi-submerged surface buoyed pipeline.

The dry mill completes beneficiation of the mineral sands through a series of unit process steps, each of which produce five or more minerals having value. The complete dry mill is located on a square-hull type semi-submersible platform anchored nearby. Rejects from the dry mill, consisting of sand tailings and sediments, are combined and discharged by pipeline to the mined-out cuts. Products comprising the four heavy minerals and rare earths are separately stored in bins to provide several day's storage. Bins are unloaded by conveyors which transfer material to a ship loader.

The platform envisaged is similar to one designed by Marcon Engineering of the Netherlands (Norring 4). This is a four-column, square-hull, semi-submersible production platform having two 246-foot square main decks. The upper deck is the platform on which the dry mill and ancillary facilities are located. The lower deck contains crew quarters, and all the facilities required to sustain life in a comfortable fashion. The lower deck also contains storage and maintenance facilities. Cantilevered sections extend the effective area of each deck to accommodate shiploading and unloading, heliport, and other features required.

The dredger and floating production platform (FPS) are self-contained and, to a great extent, are self-sustaining. They require no direct service link to the mainland, or to land-side facilities, other than for re-supply and to transport workers. One ocean-going tugboat is assigned to service the mining operation. This tug is equipped with a rotating lift crane suited to at-sea maintenance and repair work. The tug moves and positions pipelines as mining progresses.

All offshore operations will be based on work crew cycles of two weeks duty and one week off. This requires three completely staffed crews of operating, maintenance and supervisory personnel. While on duty, offshore personnel work 14 twelve-hour shifts, for a total of 168 hours each three week cycle. The wages for this work schedule is based on 40 hours per week, three weeks, 120 hours at regular time, and 48 hours at premium time. All meals and sleeping accommodations are provided by the enterprise at no cost to employees.

A motor launch will be provided to transport personnel and supplies from the island to the location of the turning basin in Port of Savannah. The launch will be seaworthy in all but severe weather conditions and capable of making  $\pm 30$  knots so that a one-way trip takes no longer than one hour.

Accommodations, consisting of two-bed cabins, each complete with lavatory and shower, clothes lockers and desks are provided. Each offshore operating location contains its own accommodations. A fully-equipped kitchen, provisioned commissary and staff will prepare and serve three meals each day in a dining room. Library, television, and indoor activity rooms will be provided. Physical exercise and conditioning facilities, both indoor and outdoor, will also be provided.

The FPS facilities will include a first-aid station, with a nurse, to attend to minor maladies and injuries. A heliport will enable the rapid evacuation of seriously sick, or injured, persons to mainland hospitals.

Diesel engine electric generators supply power for the marine/vessel systems, the beneficiation plant, living quarters, and to meet other demands as required to make the semi-submersible floating production system totally self-sustaining.

Finished heavy mineral and rare earth products of about 810,000 tonnes per year are loaded aboard bulk cargo vessels on barges for transport to destination. This configuration proposes shipping to Port Savannah by enterprise operated barges, and offloading, warehousing, and distribution by other commercial operators. The point of sale is FOB, Port Savannah.

The configuration selected, using currently available technology and equipment, makes possible the early implementation of the programs required to exploit heavy minerals offshore Georgia. The dredger and FPS have the flexibility to recover mineral-bearing sands at whatever location on the OCS their occurrence warrants it, at the least economic and technical risk.

## 6.5 ESTIMATED CAPITAL COST

This section deals with the expenditures required to implement a heavy minerals mining-beneficiation operation having the configuration and features previously described. Estimated cost is based on conceptual and schematic designs, and is order-of-magnitude having an accuracy of plus or minus 30%.

### 6.5.1 Capital Cost

Estimated capital cost has been prepared by combining techniques developed by the U.S. Bureau of Mines, together with generally accepted methods by factoring in-house or researched information. Dredges, wet mill, and dry mill cost estimates are based on formulas contained in Bureau of Mines Open File Report 4-87. Cost of the semi-submersible production platform is based on data published in Ocean Industry, April 1988.

Table 6-17, Heavy Minerals Mining Enterprise Total Facility Capital Cost Estimate, is a summary of the total capital cost required to construct the offshore phosphate mining facilities described in this section. Twenty percent is included as an allowance for costs which will be incurred for items not now predicted. Total capital costs include design, engineering, procurement, and construction management services as are applicable to each item.

## 6.5.2 Pre-production Cost

Pre-production cost in the amount of 10 million dollars is included as a part of the total investment required to implement the proposed enterprise mining scheme. This cost is intended to include the extensive drilling, sampling, and testing programs required to accurately identify the areal extent and gradequality characteristics of the Middle Miocene targeted for exploitation. This cost is also intended to include the cost of limited studies required to obtain This program would include exploratory drilling to the extent required to describe and define economically mineable reserves, based on the most effective beneficiation process flowsheet developed by the test work. This program includes the cost of bulk sample collection and a pilot plant test program to verify and refine the process flowsheet, material balances, reagent and water consumption, and recovery efficiencies such as are required to provide criteria and parameters for design and detail engineering. No interest is charged for the use of this money because it is assumed that these expenditures are in the nature of the regular research and development costs incurred by enterprises engaged in commercial minerals exploitation. Payback of pre-production/development cost is, however, included as a part of the total investment required by the enterprise.

This program will be conducted over a period of 24-30 months and will be followed by a comprehensive economic analysis based on the latest market supply-demand price scenarios. A list of the tasks/objectives to be accomplished during this pre-production period before design and detailed engineering is undertaken is listed below.

Table 6-17

Heavy Minerals Mining Enterprise - Total Facility

Capital Cost Estimate

* 4	Cost \$X1000
Floating Production Platform	\$ 66,100
Suction Hopper Dredge	45,800
Trailing Pipelines	3.800
Waste Disposal at Sea System	1,100
Tugboat	2,500
Wet Mill (aboard dredge)	12,800
Dry Mill (abord platform)	26,300
Product Storage	4,400
Shiploader	9,200
Product Transport (tug-barge)	22,800
Sub-total	\$194,800
Contingency, 20%	39,000
TOTAL	\$233,800
Round-out and use	\$235,000

# Capacity Basis

Mineral sands mined	15,300,000 tonnes/year
Intermediate product	7,650,000 tonnes/year
Final heavy mineral product	811,000 tonnes/year

- o drilling
- o sampling
- o geologic database update
- o bench scale test work
- o economic cutoffs applied
- o reserves estimates
- o bulk sampling
- o pilot scale test program
- o fresh water rinse tests
- o acidulation test work to determine amenability of concentrate to acidulation of fertilizer manufacture
- o preliminary mine plan
- o preliminary design of dredges and ancillaries
- o island construction engineering alternatives evaluated
- o environmental issues identified
- o cost and likelihood of permitting estimated
- o lease and royalty fees/costs established
- o capital cost estimates
- o implementation plan and schedule
- o supply-demand and market scenarios
- o identify potential market
- o current product selling price
- o bankable document report.

The decision to move forward to implementation by contracting for detailed engineering, procurement, and construction can be taken with a high degree of confidence in the reliability of the economic analysis. Technological and economic risks will have been reduced to an acceptable level. If the economics are favorable and the market supports sales price and demand premises, the final phase of implementation can be initiated.

### 6.5.3 Replacement Capital

The employment of capital to replace equipment when its useful life has expired is replacement capital. Useful life is based on the concept that the level of maintenance is as required to keep the equipment (facilities)

operational at an acceptable level of production. Useful or economic life is the period (time in years) until the failure rate increases to such an extent that it is no longer economical to operate.

The proposed mine-mill complex operation and production is based on certain mechanical availability. This level of mechanical availability is the result of regular and scheduled shut-down maintenance. Maintenance expense for parts, supplies, and labor is included in operating cost.

The severe service and adverse climatic environment requires a high level of regular and preventive maintenance. During scheduled periods when all facilities are shut down while the dredger and floating production system are in dry-dock, certain capital will be employed to sustain the equipment and facilities at design production capability. The additional sum of 3 million dollars per year is allowed as replacement capital. It is anticipated that this will maintain facilities at design level for a period of 30 years, without requiring the employment of additional replacement capital. The only exception is in the event technologically superior replacement equipment is warranted as justified by the economics of increased production.

#### 6.5.4 Working Capital

- o Ordinary operation of a business involves a circulation of <u>capital</u> within the current asset (capital cost) group. <u>Cash</u> is expended for materials (parts, supplies, expendibles), labor and services (electric energy, rental, fees, royalty, ...) and these expenditures are accumulated as costs. These costs are converted (concentrate inventories) into receivables and ultimately (back out by shipment) into cash again.
- o The average time intervening between the acquisition of materials or services and expenditure for labor, entering this process and final cash realization constitutes an operating cycle.
- o The amount of capital committed (taken out of current funds or borrowed) to this cycle is working capital.
- o Cost of working capital (interest) is added.

The working capital requirement for this enterprise is estimated to be equal to about 20 days total cash production cost. To simplify economic analysis, working capital of \$3,300,000 is used throughout and recovered in the last year.

### 6.6 ESTIMATED OPERATING COST

Operating costs for dredging were taken from the ZW dredge module. Operating costs for transportation, ore pumping, and waste disposal were also taken from ZW cost modules.

All plant operating costs were taken from formulas in the U.S.B.M. report for heavy minerals. A description of these formulas is given in Section 5.2.2. A complete discussion of ZW modules is given in Section 5.7

Operating costs are listed in Table 6-18.

Table 6-18
Operating Costs

	\$ per tonne mined	\$ per tonne product
Dredge	.41	7.73
Onboard plant (washing)	.09	1.70
Offboard plant (concentration)	.90	16.98
Ore pumping	.16	3.02
Waste disposal	.08	1.51
Barge transportation	.02	.38
Administration, clerical	.16	3.02
Island Accommodations	05	94
TOTAL COST	\$1.87	\$35.28

# 6.7 ECONOMICS AND VIABILITY

## 6.7.1 Market Potential

The United States relies, to a large extent, on the import of certain heavy minerals and rare earths to supply domestic needs. Production and supply is for the most part dominated by Australia, which establishes quality standards and sets market price.

The heavy mineral-bearing sands also contain a host of other not readily identified rare earths for which the U.S. depends totally upon imports for supply. Many of these relate to strategic minerals required to sustain production of vital manufactured goods needed by the U.S. in the event of emergency. There is good reason to believe that the selling price of these minerals will continue to increase as demand grows. Recovery of the minor quantities of high-value rare earth minerals will add significantly to the revenue. These two factors will serve to improve viability and hasten the time when offshore recovery of these minerals is realized. The commitment, if made, by the private sector with the support of responsible agencies of the U.S. Government to pursue the programs necessary can achieve this objective. Some of what is required is described in Section 5.5.2 of this report, and is included as part of enterprise investment in the economic analysis which follows herein for heavy minerals.

### 6.7.2. Sales Price

Total annual revenue from sales is based on an average price for the suite of heavy minerals produced. The price is in dollars per tonne for bulk concentrates, FOB Port Savannah. The average selling price is obtained by computing the total annual sales revenue by summating the annual revenue generated by each of the five minerals. The sales price of each mineral was obtained by converting or otherwise adjusting current bulk quantity market prices quoted by Metal Bulletin and published in Industrial Minerals, April 1988.

It is important to recognize that the average sales price resulting from this computation is a totally hypothetical value based on a theoretical product mix and on recent quoted market prices for each product. No recognition can be made for grade or quality as these are unknown. The average sales price, computed as per the following table, is simply a convenient way to estimate annual sales revenue.

_Mineral	Annual Tonnes	Sale Price \$/tonne	Sal	Annual es Revenue
Ilmenite Rutile Leucoxene Zircon Monazite	601,750 40,600 81,460 72,250 15,040	46.00 430.00 385.00 248.00 570.00	\$	27,680,500 17,458,000 31,362,100 17,918,000 8,572,800
TOTAL	811,100		\$ 2	102,991,400
Average Sell	ing Price, FO	B Savannah	\$	126.98

# 6.7.3 Economic Analysis

The discounted cash flow rate of return on investment (DCFROR) method of economic analysis is used to evaluate the viability potential of exploiting offshore Georgia heavy minerals as proposed in this study. DCFROR is computed in the same manner described for phosphates in Section 5.7.2. This procedure is repeated for scenarios of investment, income (sales price) and operating cost to gain an understanding of sensitivity. All economic values are based on constant 1988 dollars. A charge computed at 5% of the average product-tonne sales price is included to cover the estimated cost of royalty or severance tax.

Each scenario is represented by a separate computer run computation of DCFROI and net present value (NPV). A copy of the computer printouts is included at the end of this section.

Extraordinary costs associated with start-up are accounted for by taking into income 410,000 tonnes of product sales, and taking as cost the production of 811,100 tonnes. This procedure is used in each case.

Table 6-19 is a summary of DCFROR results for base case investment and operating costs, and for one sales price and revenue scenario.

Table 6-19
Base Case

Average Sales Price \$/tonne	Construction Capital Millions Dollars	Product Cost \$/tonne	DCFROR
\$127.00	235	42.53	4.2

# 6.7.4 Sales Price Sensitivity

Sensitivity to sales price is indicated by the results of economic analyses at increased sales price, in increments of 10%, with all other costs remaining constant. Table 6-20 illustrates sensitivity to sales price.

Table 6-20
Sales Price Sensitivity

Avg. Sales Price \$/tonne	Increase	DCFROR %
130.70	+10%	6.8%
152.40	+20%	9.0%
165.10	+30%	11.7%

6A OFS 29-A-58-60 Heavy Minerals Economics Fillyeot Number: 29-6458-00

2313 .81 62.751 078501 1759 5873 3443 EB433 1454 3852 3853 3853 19462 46:64 ENEEE 16132 3035 .81 66.751 675561 5165 5185 3. 2. 4. 3. 2. 2. 3. ម្មសំអ៊ 684:10 5/13/88 5873 48118 35 16839 58577 29075 14538 8882 3888 14402 .81 127.63 102678 B1 53 5473 3450 .89 .23 7.65 62.53 E8423 43613 436. 61059 46657 16333 .81 127.84 182878 1000 28577 5873 7.73 1.78 3.62 16.98 8. 12.1 3.8.5 82.28 £8428 2 8 8 8 8 34458 58159 5815 2525 596.45 14482 15821 3362 .81 127.60 182670 66.63 69459 5873 72668 7269 3080 15312 59151 14482 .81 627.68 182878 ន់លើងទំលើជំ 50 88 88 5877 5873 68429 87225 14538 8723 3888 56697 (2255 14492 14893 .81.64 60.751 102678 7.73 1.78 3.62 16.98 1.51 3.62 3.62 3.62 14 63420 5 xi xi xi 28577 5873 34458 101763 14538 13176 BOSE 14402 42842 14295 26547 .81 63.751 185a78 25.00 \$\frac{1}{2} \text{ } \frac{1}{2} \text{ } \text{ } \frac{1}{2} \text{ } \text{ } \frac{1}{2} \text{ } \text{ } \frac{1}{2} \text{ } \t 5673 68420 116300 53798 28577 11633 14538 3608 14402 39388 13786 .81 60.751 105678 ន់ដង់ ស្ន ស្ន 7.73 1.70 1.70 1.51 1.51 3.62 3.63 3.63 50% 20% 5873 63459 28577 130338 3033 13277 14538 14482 37934 .81 60.751 678501 ទំពង់ទំពង់ ខំពង់ 7.73 1.74 3.65 16.98 1.51 3.62 3.62 3.63 = % 6.842.0 145375 5873 14538 14538 598B2 36480 35 127£8 23712 200 14402 .81 127.03 182870 10 68429 82.7 27.85 42.53 5873 35 12259 22768 28577 14538 3959 63469 14402 35,027 15391 .81 127.68 182678 9 68423 52.7 59.8 59.8 59.8 5.3 5.3 5.6 5.8 5.8 5.8 174450 35 11751 21822 28577 5873 34420 17445 14538 3639 14402 33573 .81 63.751 678501 7.72 7.73 1.73 16.78 1.51 1.51 1.62 3.62 3.62 3.63 الالاغ زدلاغ *នំសំ*ងីន់ស់សំង 68423 5873 188588 28577 34450 14538 18639 20551 13821 (Thousand Oper Year) BASE CASE .81 66.751 105.878 র রে ম র র র র র জন্ম র র র র র 2009 68430 HEAVY MINERALS 3.62 16.98 . 38 1.51 3.62 35.28 5873 2035.55 28577 14538 20353 5364 9552 9551 .81 63.751 678501 9.9 ន់សង់នំសំ**ង**ង 68450 34450 28577 5873 218063 14538 8840 31606 . 81 127. 83 102878 5 28 28577 5873 34450 6.8420 કાં તે જે છે. કાં તે જે છે 232600 25364 8038 8098 14538 83368 3000 . 81 127. 64 102874 68420 1997 7.73 1.78 1.6.98 1.6.98 1.5.19 1.5.11 5.9.25 85.25 28577 5873 34458 247138 14538 36315 2196 2195 35 768 1427 24714 361 .81 127.63 182878 7.73 1.73 1.82 1.82 1.83 1.83 1.51 1.51 1.51 1.53 3.62 85.83 ម្មាស់ មាន ក្រសួ 28577 5873 34458 68459 261675 14538 3020 . 81 127. 88 18838 E8459 5873 34450 304281 14538 38428 3888 1658 33342 71205 24 KH 26 KH 27 KH 1994 28938 5946 34876 17194 -13531 41548 11891 659 -I 1993 8 35969 21759 56759 -56750 9 99339 15599 105589 -87ec3 -185530 505363 7038 87038 9-189 36368 1588 31588 -31588 -5 -16339 9959 Indirect Production Cost, \$/Tonne Direct Production Costs \$/Torine On board 3-scessing (Net Mill) Platform Processing (Dry Mill) Royalty # 5% of sales price Cash Flow (Revenue-Prod Cost) Construction Capital Interest During Construction lotal Production Cost, \$/yr Cash Flow (After Investment) Total Indirect Cost, \$/yr Offshore Accomodations Freduction, Million TPY Slurry Transport (One) Sufer, Clerical, Tech Depreciation (7 yr ACRS) Total Indirect Cost otal Production Cost Ictal Cash Cost, \$/yr Sales Price, 1/Tonne Replacement Capital Tax Vessel Transport Total Cash Cost Frincipal Payment Total Investment Pre-construction Production Costs Adamstration Net Income After Interest è 10x **Horking Capital** Total Revenue (3518) Sakel Sales Revenue Javable Income Project Year Tax Rate, # Income Tax westrent Principal Depletion

23576 -64233 -67643 -14000 -41500 -126000 -234000 -290750 -344281 -285477 -200/63 -235363 -214575 -184593 15407 -135127 -110441 27186 55480 18884 -56750 -13531 -87339 -195508

16063 -31583

Court Cash Flow

Cash Flow

2JUSE B

31135 158394

30191 127259

2924£

23301 67622

27256 39521

254.1 12165

-14246

-39712

1355

Economics	
SA OFS 29-R458-00 Heavy Minerals Economics	8
Heavy	29-8458-8
1458-BB	# ₹
1-62 S	ect Numb
占活	Project

HERVY MINERALS (Thousand & per Year) BASE CASE

17262 E6338 35 22056 3 2 2 3 3 3 3 3 3 6901 35478 1454 3880 3380 30212 .81 152.48 12344 3.62 16.90 .38 1.51 3.62 .94 (S) (S) 44848 17682 64776 35 22672 7.73 1.78 3.02 16.98 .38 1.51 3.02 3.62 6991 5981 35478 25975 14538 2908 3898 32058 87966 .81 152.40 15344 19 43984 17282 879EE HOLES .81 152.48 12344 57.7 56.1 3.05 86.31 88. 12.1 3.05 49. 59577 5901 35478 14538 4361 3800 168 2011 42959 .81 17282 61869 35 21654 40215 87966 58159 14538 5815 3038 7.73 1.70 3.62 16.98 .38 1.51 3.62 3.62 35.28 58577 6981 35478 19151 . 81 . . 81 152.40 152.40 11 123444 123444 11 42814 17282 60415 35 21145 39270 726.88 145.38 726.9 380.0 16317 7.73 1.70 3.62 3.62 16.98 1.51 1.51 3.02 3.02 6961 6961 35478 87966 91 41869 67225 14538 8723 3008 17262 58961 35 20636 30325 7.73 1.70 3.62 16.98 1.51 1.51 3.62 35.28 E501 5478 87966 15 2888 40124 .81 74790 17282 20128 7.73 1.70 1.70 1.70 1.51 1.51 3.62 3.62 87966 101763 3898 8 2 3 8 5 8 8 8 28577 6901 14538 14 2887 39179 179158 17282 56054 15619 .81 152.4**8** 123444 116300 7,73 1,70 3,02 16,98 . .38 1,51 3,02 .94 28577 £981 93678 14538 11630 2400 13 2836 38234 139979 17282 19110 13484 .81 87966 71882 7.73 1.70 3.62 16.98 1.51 1.51 3.62 35.28 E991 E991 35478 14538 12 2005 37289 145375 17262 53146 35 78428 93628 14538 14538 3000 18631 .B1 152.4**8** 12344 5.7.7 5.1.7 5.8.3 5.8.3 3.8.3 1.12.1 1.12.1 3.62.3 3.63.3 3.63.3 £901 = % 36344 58975 172B2 51693 35 18093 33£00 87966 14538 E901 E901 35478 3948 . 81 152. 48 12344 15831 0 F 35399 281182 174450 58233 28577 6981 35478 93678 3899 1551 17262 뛼 17584 .81 152.40 12344 5905 38993 188988 14538 18899 12967 17262 35818 35 12536 23382 .81 152.40 12344 7.73 1.78 3.82 16.98 .38 1.51 3.62 .94 87966 6991 55478 E B 25964 17282 21367 42597 203525 14538 20353 3030 .81 152.40 123444 28577 6901 35478 (+20x SALES PRICE) 87966 ម្មាល់ខ្លាំ ខ្លាំ ខ្នាំ ខ្លាំ ខ្នាំ ខ្លាំ ខ្នាំ ខ្លាំ ខ 200 41642 218963 14538 21806 3008 25935 17282 19943 .81 152.40 123444 63160 7.73 1.78 13.02 16.98 1.51 1.51 3.62 3.62 3.63 28577 E901 35478 9362 9 1999 -31500 -67000 -105500 -56750 -4157 39287 42869 415.5 44007 -41500 -126500 -234000 -230750 -2990907 -255620 -212751 -171226 -130519 25964 17282 18468 64E1 87966 14538 23568 3880 7.73 1.76 3.02 16.98 ..38 1.51 1.51 3.02 35.28 .81 152.40 12344 £991 £981 35478 1998 247138 36315 11969 35 4189 7779 11968 7.73 1.70 3.82 16.98 .38 .38 1.51 3.62 3.62 87966 3090 .81 152.40 12344 E8577 E901 35478 24714 1997 59852 3973 3973 261675 14538 26168 3838 35 1331 2582 .81 152.4**0** 123444 87966 7.73 1.70 3.02 16.98 1.51 1.51 3.62 35.28 2. 2. 2. 2. 2. 2. 2. 2. 1969 361 28577 53825 97%6 294997 14538 29491 3003 1650 71205 .81 152.40 12344 ម្មាល់ខ្លួស់ខ្លួ 35478 935 3.0% 16.98 3.62 3.62 3.63 3.63 3.63 28577 581 1 6986 6986 5916 26568 299750 2597 659 -4157 .41 2 2 2 2 2 2 3 3 3 3 3.62 6.38 .38 1.51 3.62 3.62 35.28 -56750 35848 21758 56759 -1 1993 -182299 96084 15560 185580 2 og 1 86698 7638 87698 1991 -10000 -31500 38848 1588 31588 1986 -16449 -18000 9699 Indirect Production Cost, \$/Torme Mining On board Processing (Net Mill) Direct Production Costs #/Tonne Platform Processing (Dry Mill) Construction Capital Interest During Construction Cash Flow (Revenue-Prod Cost) Royalty @ 5% of sales price Cash Flow (After Investment) Ictal Production Cost, Wyr Total Cash Cost, 9/yr Total Indirect Cost, 9/yr Offshore Accommodations Depreciation (7 yr ACRS) Slurry Transport (Bre) Production, Million TPY Super, Clerical, Tech Total Indirect Cost Total Production Cost Interest @ 10% Replacement Capital Working Capital Sales Price, 1/Tonne Total Investment Principal Paywent Vessel Transport Total Cash Cost Pre-construction Net Income After Adamistration Cuttyl Cash Flow Waste Disposal Production Costs Faxable Income (axes (misc) Total Revenue iax Rate, ≱ Sales Revenue Income Tax Project Year DCFROI NSV ë 10% Investment Principal Cash Flow Depletion Sales

GA DFS 29-8458-80 Heavy Minerals Economics

2413 .81 165.18 133731 3.62 16.50 .38 1.51 3.62 .94 35.28 7416 35993 71262 35 24942 3368 3368 658154 . 61 165. 10 133731 14538 2988 3000 7416 35933 . 61 165. 10 133731 3.66. 16.98 1.51 3.66. 35.28 14538 4361 3008 . 81 165. 10 133731 2418 3.62 16.98 .36 1.51 3.62 .94 9. KN 99. KN 9. KN 7416 35993 14538 5815 3888 24578 45631 .81 165.18 133731 31 6865 741E 35993 634/8 14538 7269 3888 2008 . 81 165. 10 133731 7.73 9.13 9.85 1.38 1.51 1.51 1.51 3.65 3.68 7416 35993 14536 6723 3868 23553 43748 2883 .81 165.10 133731 7.73 1.70 3.62 16.98 1.51 1.51 3.62 3.62 3.62 7416 35993 35 23844 42796 .81 165.10 133731 741E 35993 22535 41851 18722 64386 .81 165.10 133731 2005 741E 35993 816.54 62932 35 22026 40906 . 81 165. 10 133731 (30%) 7.73 1.70 1.70 1.86 16.98 1.51 1.51 1.51 3.02 3.02 ន់ស្នងស្ន ន c45934 . 81 165. 10 133731 2883 741E 35993 . **61** 165. 1**9** 133731 52. 53. 63. 53. 53. 54. 44. 9 2003 7.73 1.70 3.62 16.98 .38 1.51 3.62 .94 118589 .81 B Cool 7.73 1.30 1.30 1.30 1.31 1.51 1.51 3.05 3.05 3.05 HERVY MINERALS (Thousand % per Year) BASE CASE (+30x SALES PRICE) .81 18395 19384 3048E 9 9 . 81 165. 10 133731 7,73 1,78 3,02 16,98 1,51 1,51 3,62 ,94 2. Ki 8. Ki 21886 3008 18722 28275 18966 .81 7.73 1.70 1.70 16.98 16.98 1.51 1.51 3.62 5.85 5.85 **0** 3969 18722 26792 26792 35 9377 .81 7416 35953 24714 3888 35 35 5899 6955 -115027 <u>ड</u>. श. श्र. घ. श. च. दे .81 3.62 16.38 1.51 1.51 3.62 35.28 26168 3888 -31500 -128500 -108500 -56750 528 74677 50931 -41500 -128500 -234060 -290750 -290262 -215545 -164614 6859 .81 2 5 7.73 1.28 16.98 16.98 1.59 1.50 2.66 3.66 4538 3030 1650 0915 35 3820 7095 7.73 1.70 1.70 1.6.98 1.51 1.51 3.62 3.62 5.28 7548 36438 -1 . 21758 56758 -2 1992 15588 185588 -3 1991 -31588 -5 -10000 -16330 -18609 Indirect Production Cost, \$/Torme Direct Production Costs #/Torme Un board Processing (Net Mill) Platform Processing (Gry Mill) Total Cash Cost, 8/yr Total Indirect Cost, 8/yr Total Production Cost, 8/yr Royalty & 5% of sales price Construction Capital Interest During Construction Cash Flow (Revenue-Prod Cost) Project Number: 29-8458-00 File: HERVKINI Cash Flow (After Investment) Super, Clerical, Tech Difshare Accommodations ΤPY Slurry Transport (Gre) Depreciation (7 yr ACRS) Total Indirect Cost Total Production Cost Production, Million Sales Price, \$/Tonne Total Revenue Principal Payment Interest & 10% Replacement Capital Working Capital Ţ Vessel Transport Total Cash Cost Pre-construction Total Investment Production Costs Waste Disposal Adwiristration Net Income After Cash Flow Cumul Cash Flow (axes (misc) Sales Revenue Taxable Income Project Year Tax Rate, # Investment Principal Income Tax Depletion Sales DCFR01

#### **SECTION 7**

#### **ENVIRONMENTAL**

### 7.1 ENVIRONMENTAL SETTING

In the present study, two areas are under consideration for potential exploitation of mineral occurrences. The phosphorite occurrence is located 5 nautical miles offshore Savannah, and the heavy minerals location under consideration is 35 nautical miles offshore Savannah. Both of these suspected occurrences lie within that broad portion of the southwestern Atlantic Ocean known as the Georgia Bight. This region is bound by Cape Fear, North Carolina to the north, and by Cape Canaveral, Florida to the south. The Georgia Bight extends seaward from the coast to the Florida-Hatteras Slope which represents the edge of the Contintental Shelf. The coastal margin of the Bight in the vicinity of the mineral resources is characterized mostly by undeveloped sea islands and extensive coastal marshes and tributaries.

The scope of work and assignment described for this resource assessment study includes economic feasibility without the requirement to evaluate environmental considerations. This section presents a very brief overview and describes the kinds of things which would require comprehensive study in an EA or EIS. No attempt is made to describe the scope or content, nor to definitively estimate the cost of such studies.

#### Coastal/Estuarine Environment

Coastal Georgia is typified by a barrier island salt marsh regime. Sand beaches of mild relief face the open waters of the southeast Atlantic. Beaches give way to parallel dune lines placed by deposition of sediments transported through wave action. The dune areas generally protect a stand of coastal vegetation that grades from sea oats to salt-tolerant grasses, into oak and pine forests. Behind the islands lie protected salt marshes replete with tidal creeks, streams, and bays.

Salt marshes serve as a mixing zone for fresh water from coastal rivers with saltwater pushed into the marsh during tidal maximums. The dynamics of

tidal bore and streamflow drive an ecological mechanism fueled on nutrients and sunlight. Productivity in the salt marsh and estuaries forms the foundation of the marine food chain.

Resort and recreational developments are numerous and notable on the barrier islands. Jekyll, St. Simons, Sea Islands, and Tybee Islands, have commercially important resort areas, along with public access recreational areas. The status of these highly acclaimed vacation destinations gives credence to the value of Georgia's coastal natural resources. Interspersed with commercial developments are large areas of undeveloped lands in the form of parks, reserves, and wildlife management areas.

Jekyll Island State Park, the islands within the Savannah Wildlife Refuge, and Wolf Island National Wildlife Refuge and Wilderness Area are representative of areas that remain as undeveloped, or natural coastline. These sanctuaries of preserved natural ecosystems and geographic microcosms currently protect many coastal resources. Strict coastal zone management practices are now controlling further degradation of barrier islands, while allowing compatible development to continue.

Impacts to the beaches on the barrier islands, or to salt marshes and wetlands in the coastal zone, are a concern for the feasibility of any onshore or offshore activity. Review of the impacts should consider methods to improve the existing natural resource when possible, without defeating the mission of utilization of the discovered mineral.

### Savannah River

The Savannah River has its headwaters in the Blue Ridge Province in northern Georgia. A significant freshwater river, it transverses a hundred or more kilometers and has a 27,392 km<sup>2</sup> drainage basin. Discharge of the lower river has been estimated at over 300 m<sup>3</sup>/s. Control structures, dams, and maintenance dredging have altered the natural hydraulics of the system and impacted the associated ecosystems.

Deepwater port facilities located on the Savannah River handle a variety of cargoes. Bulk shipments of dry and liquid products, along with increasing

numbers of container vessels from other U.S. and foreign locations, now utilize the historic port of Savannah. Continued use of the maintained channel by the river's many industrial facilities further emphasizes the nature of this busy port area. Forest products, petroleum, and basic chemicals are produced and shipped from the Savannah area. Georgia Port Authority reports cargo levels near seven million tons for the 1987 year at the deepwater facilities.

Development of the river frontage began in 1733 with the founding of the city by General James Edward Oglethorpe. General Oglethorpe's planned development of the city has matured into a major east coast port. Commercial and industrial developments along the river and on islands in the river are extensive, above and the below the originally planned community.

At present, concern over the impact of developments on the river and in adjacent coastal marshlands has led to the promulgation of regulations governing future impacts. Due to the importance of the coastal marshlands and riverine wetlands on the river's ecological status, future developments are likely to occur only at suitable non-marsh or non-wetland locations.

### Offshore

The width of the Continental Shelf in the Georgia offshore area is approximately 130 km. The depth of the shelf break off Georgia averages 56 m. The average depth of water at the location of the occurrences (heavy minerals) is 27.2 m, and at the location of the phosphorite occurrences in the Middle Miocene is 15 m.

The shelf is a marine extension of the Atlantic Coastal Plain which is relatively flat and slopes seaward an average of 36 cm/km.

The south Atlantic seafloor is over 80% sand bottom (Hollister, 1973; George & Staiger, 1979). Two major sedimentary regimes occur: an inshore area approximately 10 to 30 km wide characterized by fine to very fine-grained sand, and an offshore expanse stretching to the shelf-slope break covered by coarse-grained sediments (Gorsline, 1963; Henry & Hoyt, 1968). Off the

coast of Georgia this boundary is distinct and occurs quite consistently at a depth of 11 meters (Pilkey & Frankenberg, 1964). The near-shore shelf zone acts as an effective sediment trap, beyond which little sediment deposition occurs (Neiheisel & Weaver, 1967; Pilkey, 1963; Bigham, 1973). Distribution of minerals in Continental Shelf waters and sediments off Georgia indicates a long-shore transport from north to south within the near-shore zone. Lateral transport of sediments across the shelf is not extensive.

The shelf surface is generally smooth with rare and intermittent outcrops of hardground; hardgrounds in the South Atlantic are "reefs" and express relief above the surrounding sedimentary regime or are buried under superficial sediments of varying thicknesses. One such "reef" is within the Gray's Reef National Marine Sanctuary. The location of Gray's Reef is 17.5 nautical miles off the coast of Sapelo Island, Georgia, with corner coordinates of: 31°21.45'N, 80°55.17'W; 31°25.25'N, 80°55.17W; 31°25.15N, 80°49.42'W; and 31°21.45'N, 80°49.42'W.

Natural hardground and artificial reefs support a wide variety of marine life. Such hardground is known as a live bottom reef and is defined as: those areas which contain biological assemblages consisting of such sessile invertebrates as sea fans, sea whips, hydroids, anemones, ascidians, sponges, bryozoans, or corals living upon and attached to naturally occurring hard or rocky formations with rough, broken, or smooth topography, or whose lithotope favors the accumulation of turtles, fish, and other fauna.

Reef areas support invertebrates, recreational target fish, migratory pelagic fish, small seasonal tropic reef fish, common indigenous fish, small schooling bait fish, mid-water fish, and marine turtles. Pelagic birds are seen in the vicinity of these reef areas. Sport fish such as snapper or grouper tend to be long-lived and do not stray far from the reef areas. Long-lived fish are usually secondary or tertiary consumers, at the top of a reasonably large and diverse food web.

Twenty-five species of cetaceans (whales, dolphins, and porpoises) have been reported in offshore waters within the Georgia Bight. Twelve of these species have been found stranded along the Georgia coastline, and one, the spotted dolphin, has been identified by numerous offshore sightings.

Surface water temperatures follow seasonal air temperatures, with a slight lag. Near-shore in the south Atlantic, surface temperatures often show wide seasonal variation in response to varying climatic and run-off patterns and commonly range from 10 to 25°C. In the offshore zone, surface temperatures also respond to climatic changes, but are moderated by the consistently warm (25°C) Gulf Stream and thereby show only minor seasonal variations. In mid-shelf areas, surface water temperatures are relatively constant (19-27°C) year-round. Offshore at deeper depths, bottom temperatures are not readily influenced by weather or wind and are more stable.

Circulation in the Georgia Bight is affected primarily by freshwater runoff, wind, or the northerly flowing Gulf Stream, and to a minor extent by tidal currents, which proceed in a clockwise fashion, and the Coriolis effect. Surface circulation is northeasterly off the Carolinas and intermittent off Georgia and Florida, with a northerly drift in the autumn and winter. A southerly flowing coastal current prevails nearly year-round, inshore of a predominant northeasterly drift offshore, except during winter when runoff is low and when northeasterlies blow for several days at a time. Circulation off Georgia is strongly influenced by the prevailing winds which are most often northeasterly or southwesterly.

Bottom currents off Georgia show no consistent pattern and it is speculated that these currents are influenced by in-drafts from the northerly flowing Gulf Stream. Reefs often provide areas of calm bottom water or favorable bottom currents by damping or deflecting currents, and it has been noted that vertical relief of natural patch reefs or live-bottoms causes an upwelling effect.

In the offshore area of interest, waves come, on an annual basis, from all directions about the same percentage of the time. Seas of less than 4 feet occur most of the time, while wave heights greater than 12 feet are rare. Wave conditions are more severe during fall and winter in response to weather conditions. During the winter months, the area is subjected to extra-tropical storms, locally known as Hatteras lows, and during the summer and fall, to tropical storms and hurricanes originating in the Caribbean and the Gulf of Mexico.

The primary commercial interest in the Georgia offshore area is shrimping (GMFMC & SAFMC, 1980). Shrimp are harvested offshore of Georgia in amounts of 3,000 to 4,000 tpy, compared to 50 tpy of harvested fin fish. Historically, Georgia's commercial fishery has been based upon a six-month coastal shrimping cycle, commencing in the spring, usually late May or early June, when over-wintering and migratory white shrimp move toward offshore waters. During late August a new crop of white shrimp enters the fishery and provides a major portion of Georgia's catch. Georgia's sounds have not been opened since 1977, but prior to that year they were opened during the fall white shrimp period.

Shrimp are most abundant within 4-5 nautical miles of the Georgia shoreline. This location seems to be associated with depth. White shrimp are concentrated in waters of 27 m or less. The commercially less important brown shrimp and pink shrimp can be found in water depths of 55 m and 11-37 m, respectively.

In Georgia, most spawning of shrimp occurs more than 1.2 nautical miles from the shore; some spawning may occur inshore. Spawning seems to correlate with bottom water temperatures of 17-29°C. The spring spawn occurs with the rapid rise in water temperatures and the fall spawn ends with temperature decline. Shrimp may spawn up to four times within the spawning season. Spawning season ranges April - September.

After emerging from their demersal eggs, shrimp go through eleven stages of larval development. The larval stage of shrimp lasts approximately 12 days. Near shore tidal currents transport the post-larvae from the spawning areas into the estuarine shrimp nurseries. While in the nurseries, the shrimp grow quickly and, as juveniles, migrate toward the commercial fishing areas offshore, in late spring and summer. The adult shrimp move from near-shore spawning areas to commercial fishing areas from August through December. Starting in fall to early winter, the adult shrimp migrate south to Florida offshore waters and return to Georgia waters during late winter and early spring. Some portion of the shrimp will over-winter in Georgia waters. The shrimp spawning area and estuarine nurseries are the most important and sensitive habitats of shrimp, with regard to shrimp development.

### 7.2 PHOSPHATE MINING

The proposed methodology to mine and process the offshore phosphorite occurrence will utilize dredge-type mining equipment, followed by offshore processing. This proposed method will reduce possible onshore impacts associated with site development and plant operations in coastal areas. Infrastructure needs such as power supply, transportation, and operating supplies, would be available from existing on-shore facilities.

Long-term impacts from the mining operations are associated with the condition and characteristics of the mined bottom. Large-scale changes in bottom topography could seriously affect species composition in the mined area waters. If mining operations drastically change the characeristics of the bottom sediments, future biologic development of the bottom and surrounding waters may be severely altered, though it should not be inferred that this represents an adverse impact. The proposed operation would create deep, wide, and long excavations which may cause wave pattern modification. These excavations may never naturally fill due to wave action, since sediment transport is unlikely at water depths greater than 45 feet (Drinnan & Bliss, 1986).

Another area of the proposed mining operation with potential for negative impact on the marine environment concerns the various process effluent streams. The different effluent streams are generated at sea on the mining dredge and artificial island that supports the product beneficiation operations. The effluents can be placed in three categories: sized/inert rejects, process waste clays, and sand tailings.

The mining/beneficiation operations will have a potential impact in three domains within the marine environment. The first region is the upper portion of the euphotic zone. One short-term impact is an influence on phytoplankton. Surface plumes created by effluents from mining or processing can reduce the available sunlight in and beneath the plume. This reduction in sunlight can adversely affect development of phytoplankton by limiting photosynthesis. On the other hand, effluent plumes may concentrate dissolved or suspended nutrients within the euphotic zone, and the presence of these substances may stimulate phytoplankton productivity.

The second area of potential environmental impact due to effluent streams is the water column. Effluent plume turbidity can create a stressful environment for marine organisms. Fin fish and other highly mobile animals can, and usually do, avoid a high particulate area, but eggs and larvae cannot escape. Thus, high concentrations of particulate may create changes in seasonal and spatial patterns of organisms. In addition to particulates, effluent streams may also add dissolved substances to the water column. At significant concentrations these may be toxic to certain organisms, leading to biomass reduction, or they may represent nutrients and lead to inordinate localized rise in biomass.

Shrimp populations are sensitive to conditions that can develop from openocean dredging and dumping of dredge spoil. The resulting silt and turbidity from operations could result in shrimp gill erosion. To avoid adverse impacts it is ordinarily necessary to curtail such operations in shrimp trawling grounds when shrimp are abundant. Another adverse effect of dredging on the shrimp fishery is the smothering and destruction of the demersal eggs by the dredge spoil. In addition, severe alteration of bottom contours and substrata composition by dredge spoil can make trawling hazardous, if not impossible, in spoil areas.

Finally, benthic impacts may represent another important receptor of effluent streams. Impacts of effluent streams on the bottom are similar to, but not as severe as, the mining operation itself. If sedimentation is heavy, then benthic communities will be smothered. The characteristics of the sedimentation and type of benthic community will determine whether benthic impacts are severe.

Potential environmental impacts of airborne emissions from the dredging and beneficiation operations are expected to be very light. The only emission from the mining and processing operations will be exhaust from diesel power generation equipment or vessel operation.

## Floridan Aquifer

In the vicinity of the hypothetical mine, the Middle Miocene phosphorite source bed overlies the principal artesion aquifer of the region. Because of the importance of the Floridan Aquifer as a water supply, particularly to Savannah, there are concerns about the potential for aquifer contamination from mining activities.

Research will be necessary to define aquifer and aquiclude characteristics in the vicinity of the mine. Items that need to be addressed include the following:

- o thickness and effectivenss of the aquiclude after mining,
- o potential for breaching the aquifer during mining,
- o aquifer water quality and the position of the salt-water/fresh-water interface; if the water quality is poor and the interface is landward of the mining area, then contamination by mining is not an issue.

### 7.3 HEAVY MINERALS MINING

Potential commercial development of the offshore heavy mineral occurrences has been based on the use of a suction-type hopper dredge with support facilities at an offshore platform-mounted processing plant. As in the case of the proposed phosphorite occurrence, all processing will occur offshore, thereby eliminating onshore impacts that would be associated with onshore processing of the heavy minerals.

Because of the nature of heavy mineral occurrences, mining of heavy minerals will differ from the mining of the phosphorite. Where phosphorite mining will require two dredges, one dredge to remove overburden and one dredge to mine phosphorite matrix, heavy mineral mining will require only one dredge since there is not expected to be any overburden needing removal.

Impacts of heavy mineral mining will be similar to those of phosphorite mining, but substantially reduced. The proposed mining of heavy minerals will excavate to a depth of 7 meters into the ocean bottom. Beneficiation,

both onboard the dredge and the offshore plant, will generate sand tailings which will be placed into the 7 meter deep mine cuts. There will not be any waste-clay effluents to be dealt with as in the phosphorite mining; therefore, increased turbidity due to very small particle waste-clays will not be an expected problem.

## Coastal/Estuarine Impacts

Coastal or estuarine ecosystems should not receive direct impacts from offshore mining operations. Current movements of turbidity plumes are generally north or south in the offshore mine locations. Should mine operations occur in waters less than 20 meters in depth, a potential for affecting the sediment budgets of coastal shoreline is possible.

Identification of the mining locations and rate of bottom deepening will play an important role in assessing effects to coastal shorelines. Processes of deposition and removal on coastal shorelines have been shown to result from modification of natural bottom conditions at depths less than 20 meters. The dynamics of current movements, wave action, will need identification, along with bottom and shoreline characterization, prior to confirming specific impacts.

The generation of clean well-sorted sands in the mining and processing operations does present an opportunity to mitigate impacts from mining. Production of beach quality sands from mining beyond the 20 meter depth could provide valuable reconstruction materials for shorelines undergoing erosion caused by other forces. As with all activities in natural environments, investigations into habitat biota relationships prior to the actions would be required, but mitigative and restorative practices are possible.

Impacts on estuarine systems should be minimal as no disturbance of natural conditions are projected. Siting of onshore plant facilities in an area of existing suitable locations is likely. Construction of infrastructure such as docks or canals may be needed, but do not represent perturbances to the natural setting that are unacceptable.

### Potential Benefits of Mining

Mining of minerals in the Exclusive Economic Zone (EEZ) is anticipated to generate much interest and debate on the environmental effects associated with resource utilization. While detrimental consequences are discussed at length in many of the available references on the subject, little information has been located that documents positive effects from resource utilization. Lack of information on the environmental benefits may be due to the lack of citable evidence, or lack of directed research on post-utilization conditions. Studies are needed to define methods of reaping potential benefits from mining activities, and to formulate guidelines for making evaluations of what constitutes acceptable impacts versus benefits.

In coastal or deepwater zones of low biologic diversity, mineral resource utilization offers the opportunity to use mining technology to increase habitat diversity and thereby induce biologic diversity with associated benefits. Areas of monotonous bottom conditions, when modified and reclaimed to increase habitat via niche development, offer the potential for increased diversity of species and associated recreational or economic benefits. To effect such measures, actions designed to save potential construction materials are needed. Construction of rock piles, or reef-like areas, when suitable reject materials are encountered, is one technique. Areas excavated to leave behind overhanging ledges or bluffs may be feasible as well, and should be considered.

Similarly, the construction of islands, or the installation of permanent work platforms, offer the potential to incorporate habitat for a variety of species. Artificial habitat in otherwise barren areas will quickly attract a full range of sessile and motile forms of both vertebrates and invertebrates. Clear evidence of this form of pioneer colonization is found at oil platforms and artificial reefs throughout the oceans of the world.

Another potential benefit from mining of offshore bottoms is the generation of materials suitable for beach renourishment. Overburden sands of suitable quality for beach renourishment are expected to occur in mining zones within practical pumping, or barge transportation distances. Use of these materials from deeper waters has the potential to minimize impacts from dredging

operations in the near-shore zones. This trade-off of impacts should be considered as a form of mitigation of environmental consequences due to mining.

Emphasis on habitat enhancement or restoration techniques needs to be considered in the planning stages of all projects. Hence, as mining or exploitation technology evolves with the mining experience, so should mitigation technology evolve. Methods to mitigate impacts, restore bottoms, or create new habitats, will improve the overall acceptability of mineral resource utilization in the public's perception of offshore projects.

# Mitigation of Potential Adverse Impacts

Mitigation of potential environmental impacts depends on detailed analysis of mining procedures and plans. While the initial damage to benthic communities may be unavoidable in the short term, measures to re-establish communities may be possible. Careful consideration of waste materials placement may provide an avenue to enhance or reclaim mined-over areas. Methods to re-introduce native flora and faunal components have evolved for land-based mining and need consideration for ocean applications. Similarly, careful consideration of non-benthic components and mining plans may identify measures to alleviate any adverse impacts to those components.

Damage to benthic communities can occur in a variety of forms, includings total removal, substrate removal, smothering of resident sessile forms, reduction of oxygen levels, decreased photoperiod, and loss of food source. These impacts are due to direct and indirect perturbation of the benthic environment. Impacts due to smothering, decreased photoperiod, and decreased oxygen levels from particulates or plume migration may be reduced by careful placement of these materials back into open waters.

Removal of the substrate during mining and elimination of food sources represent more difficult challenges in the reclamation of the seafloor. However, with careful identification of materials handling techniques, and mine planning, the movement of unusable substrate, i.e. overburden, to suitable new locations may be possible. With saved or reclaimed substrate in place, the re-introduction of species appears feasible if similar pre-mine

conditions such as depth, lighting, and food source, prevail. Recolonization by pioneer species brought to barren sites by drift in currents may supply adequate innoculation of sites, when nearby undisturbed areas are upgradient.

Avoidance of areas during periods of sensitive activities may be possible as well and should be considered during mine planning. Seasonally utilized areas for spawning, migration, and breeding, can be identified in advance and operations altered to minimize intrusion. Monitoring of currents and prevailing weather patterns also would allow for the shifting of mining or disposal activities away from sensitive areas downgradient to prevailing conditions.

Another valuable technique applicable to highly motile or pelagic species is hazing. By creating annoying or nuisance conditions in areas to be impacted, it may be possible to cause voluntary abandonment by certain sensitive species. This form of activity, along with removal techniques, while not completely effective, does have merit when less favorable circumstances may prevail.

In summary, further development of mitigation procedures need to be explored. Restoration, reclamation, or enhancement of conditions should receive attention at an early stage of planning to allow for consideration of alternatives prior to initiation of operations. Attempts to mitigate impacts from active operations also need to be considered when sensitive or economically important resources are at risk.

### 7.4 PERMITTING

#### 7.4.1 Permit Acquisition Procedures

Federal environmental regulations affecting the operation of offshore mining/processing activities are based on two major legislative provisions at the federal level. The Marine Protection Research and Sanctuaries Act (MPRSA), along with the Clean Water Act (CWA), have sections governing the disposal of dredged materials and non-dredged materials in estuarine,

coastal, and open ocean waters. Various other secondary acts also have the potential to be cited as being relevant, as well. These secondary acts which may affect both the heavy minerals site and phosphorite sites include:

- o Endangered Species Act (ESA)
- o National Environmental Policy Act (NEPA)
- Port and Tanker Safety Act (PTSA).

MPRSA - Provisions of MPRSA require permits issued from EPA for the transportation and dumping of waste materials into the contiguous zone and beyond with restrictions as specified by EPA for non-dredged materials. MPRSA tasks Corps of Engineers with issuing permits for dumping dredged materials while applying EPA criteria for evaluating the impact on the marine environment. MPRSA further delegates Coast Guard with conducting appropriate enforcement activities for unlawful dumping or transportation for dumping of materials.

Basic to the tasks of EPA and Corps of Engineers under MPRSA, is the determination of whether permitted activities will "unreasonably degrade" public health or the marine environment. In making this determination, EPA and Corps of Engineers use criteria specified by statute or established by the EPA Administrator. MPRSA is generally not applicable in estuarine waters.

CWA - The Clean Water Act contains provisions for the establishment of water quality criteria, treatment standards, issuance of discharge permits, and issuance of permits for land-based pollution sources, or stationary pollution sources discharging into territorial waters. Further, the discharge of dredged materials into navigable waters is regulated under the CWA; however, MPRSA usually preempts this provision in coastal or the open ocean.

The CWA will affect any discharges from processing operations associated with the beneficiation of ores. The National Pollutant Discharge Elimination System (NPDES) is the operative format for the execution of CWA provisions as administered by EPA at facilities with pollutant discharges. CWA Section 404 directs Corps of Engineers to issue permits for dredge and fill activities in navigable waters, using criteria promulgated by EPA for disposal sites.

Permitting requirements for the emission of non-dredged material effluents from the offshore processing facilities will be according to NPDES criteria. Application of regulations formulated for the NPDES program have particular relevance to the phosphorite operations. Disposal of spent reagents with tailings or waste clays are anticipated to represent a minor impact due to the bio-degradable nature of the materials utilized. The absorptive capacity of phosphorite matrix clays should immobilize reagents allowing degradation to occur. This form of treatment is common to on-shore operations of a similar nature.

Air - Provisions of the Clean Air Act (CAA) will govern air emissions associated with any of the mining/processing facilities. Should heating systems for reagents or drying facilities for product become necessary, applicable CAA emission restrictions would be applicable, particularly for the stationary facilities. Industry standards for mineral processing operations are routinely met by operations at on-shore facilities of a similar nature should air emission sources be defined.

Georgia environmental regulations will affect only the onshore activities associated with ore shipment. The Environmental Protection Division (EPD) of the Georgia Department of Natural Resources administers programs governing:

- o Water quality control discharge (NPDES),
- o Air quality,
- o Groundwater withdrawal,
- o Surface water withdrawal,
- Solid waste management,

Georgia has a consolidated environmental program with authority delegated from the U.S. Environmental Protection Agency for issuance and enforcement of federal permits.

## Coastal Marshlands

Issues concerning the construction of a storage facility or appurtenant devices in coastal marshlands, are regulated under the Coastal Marshlands Protection Act. Provisions of the Coastal Marshlands Protection Act are administered by a three-member committee, consisting of the EPD Director, Coastal Resources Division Director, and a Natural Resources Commissioner.

Construction and operation of storage or shipping facilities at hypothetical locations on-shore will likely require review and permitting under the Coastal Marshlands Protection Act. Review of dock construction, discharge/intake structures, and other infrastructure, are likely to have temporary impacts on estuarine wetlands. Mitigative measures and procedures would be employed to lessen or alleviate impacts.

## SECTION 8

# **BIBLIOGRAPHY**

Zellars-Williams Company key professional contributors, in addition to J. M. Williams, P.E., as a principal investigator, are recognized as follows.

SECTION	TITLE	AUTHOR
1	Executive Summary	J.G. Tavrides
2	Scope of Study	T.D. Abel
3	Resources	J.S. Spalding T.D.Abel
4	Offshore Mining Technology	J.W. Hughes J.G. Tavrides
5/6	Phosphate and Heavy Minerals Feasibility Mining Area and Alternative Configuration	J.W. Hughes
	Configuration and Infrastructure	J.G. Tavrides
	Estimated Capital and Operating Cost	J.W. Hughes J.G. Tavrides
	Economics and Viability	J.G. Tavrides
7	Environmental Impacts	T.P. Oxford F.I. Nance J.W. Whittington

Credit is due the computer programmers, operators, and particularly Shirley B. Nicks, secretary and word processor, who put it all in print, and others in Jacobs reproduction department who compile and assemble report documents.

#### BIBLIOGRAPHY

- Ariathuvia, R., MacArthur, R.C., and Krone, R.B., 1977, Mathematical Model of Estuarial Sediment Transport: prepared for Army Engineers Waterways Experiment Station, DMRP-TR D-77-12, available from NTIS AD A047 202, Springfield, VA.
- Attanasi, E.D., and DeYoung, J.H., Jr., 1987, Economics and the Search for Offshore Heavy Mineral Deposits: Marine Mining, Vol. 6, p. 323-337.
- Attanasi, E.D., DeYoung, J.H., Jr., Force, E.R., and Grosz, A.E., Resource Assessments, Geologic Deposit Models and Offshore Minerals with an Example of Heavy-Mineral Sands, in: (Teleki, P.G., Dobson, M.R., Moore, J.R., and von Stackelberg, U., eds.), Advances in Marine Minerals Research and Assessment NATO Advanced Research Institute Series; Dordrecht, Netherlands, Reidel Publishing Co, p. 485-515.
- Ayers, M., Blackwelder, B.W., Howard, J.D., Keer, F., Knebel, H.J., and Pilkey, O.H., 1977, Vibracore Studies, Georgia Embayment Shelf, in Popenoe, P., ed., Environmental Studies, Southeastern United States Atlantic Continental Shelf: U.S. Geological Survey Open-File Report 80-146, p. 6-1 to 6-88.
- Barnard, W.D., 1978, Prediction & Control of Dredged Material Dispersion Around Dredging & Open-Water Pipeline Disposal Operations: prepared for U.S. Army Engineers Waterways Experiment Station, DMRP-DS-78-13, available from NTIS AD A059 573, Springfield, VA.
- Bastian, D.F., 1974, Effects of Open-Water Disposal of Dredged Material on Bottom Topography Along Texas Gulf Coast: prepared for U.S. Army Engineers Waterways Experiment Station, DMRP-Misc. Paper, D-74-13, available from NTIS AD A002 659, Springfield, VA.
- Bigham, G.A., 1973, Zone of Influence Inner Continental Shelf off Georgia: J. Sediment Petrol. 43(4), p. 207-215.
- Bureau of National Affairs, 1986, <u>U.S. Environmental Laws</u>: Bureau of National Affairs, Inc., Washington D.C., 665 p.
- Cathcart, J.B., 1968, Phosphate in the Atlantic and Gulf Coastal Plains: Proceedings from Fourth Forum on Geology of Industrial Minerals, University of Texas.
- Cruickshank, M.J., 1988, Marine Sand and Gravel Mining and Processing Technologies: Marine Mining, Vol. 7, No. 2, p. 149-163.

- Curray, J.R., 1969, History of Continental Shelves: In <u>The New Concepts of Continental Margin Sedimentation</u> (D.J. Stanley, ed.), p. JC-VI-1 to JC-VI-18.
- Dehais, J.A., and Wallace, W.A., 1988, Economic Aspects of Offshore Sand and Gravel Mining: Marine Mining Vol 7, No. 1, p. 35-48.
- DPRA, Inc., 1987, The Economic Feasibility of Mining Phosphorite Deposits of the Continental Shelf Adjacent to North Carolina: Report to Office of Planning and Assessment North Carolina Department of Natural Resources and Community Development, Raleigh, North Carolina.
- Drinnan, R.W., and Bliss, D.G., 1986, The U.K. Experience on the Effects of Offshore Sand and Gravel Extraction on Coastal Erosion and the Rishing Industry: Nova Scotia Depaartment of Mines and Energy, Open File Report 86-054.
- Duane, D.B., Field, M.E., Meisburger, E.P., Swift, D.J.P. and Williams, S.J., 1972, Linear Shoals on The Atlantic Continental Shelf, Florida to Long Island: in, Shelf Sediment Transport-Process and Patterns (D.J.P. Swift, D.B. Duane and O.H. Pilkey, eds.) Dowden, Hutchinson, and Ross, Inc., Stroudsburg, PA, p. 447-498.
- George, R.Y., and Staiger, J.C., 1979, Epifauna Benthic Invertebrates and Demersal Fish Populations of South Atlantic/Georgia Bight in: South Atlantic Benchmark Program, Volume 3 (Final Report). A Bureau of Land Management Report to U.S. Department of Interior, Washington D.C. by Texas Instruments, Inc., Dallas, TX, p. 211-254.
- Gorsline, D.S., 1963, Bottom Sediments of the Atlantic Shelf and Slope off the Southern United States: J. Geol. 71, p. 422-440.
- Griffin, M.M., and Henry, V.J., 1984, Historical Changes in the Mean High-Water Shoreline of Georgia, 1857-1982: Georgia Geologic Survey Bulletin 98, 96 p.
- Grosz, A.E., Nature and Distribution of Potential Heavy Mineral Resources Offshore of the Atlantic Coast of the United States: Marine Mining, Vol. 6, p. 339-357.
- Grosz, A.E., and Escowitz, E.C., 1983, Economic Heavy Minerals of the United States Atlantic Continental Shelf: in, (Tanner, W.F., ed.), Nearshore Sedimentology, Proceedings of The Sixth Symposium on Coastal Sedimentology, Florida State University, p. 231-242.
- Grosz, A.E., Hathaway, J.C., and Escowitz, E.C., 1986, Placer Deposits of Heavy Minerals in Atlantic Continental Shelf Sediments: Proceedings of the Eighteenth Annual Offshore Technology Conference, Houston, TX, p. 387-394.

- Gulf of Mexico and South Atlantic Fishery Management Councils, 1980, Draft Environmental Impact Statement and Fishery Management Plan for Coastal Pelagic Migratory Resources (mackerel).
- Hathaway, J.C., ed., Data File Continental Margin Program, Atlantic Coast of the United States, Sample Collection and Analytical Data: Woods Hole Oceanographic Institute Unpublished Report 71-15, Vol. 2, 491 p.
- Henry, V.J., and Kellam, J.A., 1987, Seismic Investigation of the Phosphate-Bearing, Miocene Age Strata of the Continental Shelf off of Georgia: Georgia Geologic Survey Bulletin 109 (preliminary draft), 41 p.
- Henry, V.J., Jr., and Hoyt, J.H., 1968, Quaternary Paralic and Shelf Sediments of Georgia, Southeastern Geol. No. 9, p. 195-214.
- Hurme, A.K., and Pullen, E.J., 1988, Biological Effects of Marine Sand Mining and Fill Replacement for Beach Replenishment, Lessons for Other Uses: Marine Mining, Vol. 7, No. 2, p. 123-136.
- Huston, J.W., and Huston, W.C., 1976, Techniques for Reducing Turbidity Associated with Present Dredging Procedures and Operations: prepared for U.S. Army Engineers Waterways Experiment Station, DMRP-TR-D-76-4, available from NTIS AD A025-623, Springfield, VA.
- Johanson, E.E., Bowen, S.P., and Henry, G., 1976, State-of-the-Art Survey and Evaluation of Open-Water Dredged Material Placement Methodology: prepared for Army Engineers Waterways Experiment Station, DMRP-AD-AO27-O24, available from NTIS AD AO27 O24, Springfield, VA.
- Keeley, J.W., and Engler, R.M., 1974, Discussion of Regulatory Citeria for Ocean Disposal of Dredged Materials: prepared for Army Engineers Waterways Experiment Station, DMRP-MP-D-74-14, available from Elutriate Test Rationale and Implementation Guidelines: NTIS AD 755 826, Springfield, VA.
- Kellam, J.A., 1981, Neogene Seismic Stratigraphy and Depositional History of the Tybee Trough Area, Georgia/South Carolina: Unpublished Master's Degree Thesis, University of Georgia, Athens.
- Marvasti, A. and Riggs, S., 1987, Potential for Marine Mining of Phosphate Within the U.S. Exclusive Economic Zone (EEZ): Marine Mining, Vol. 6, p. 291-300.
- Mertie, J.B., Jr., 1975, Monazite Placers in the Southeastern Atlantic States: U.S. Geological Survey Bulletin 1390, 40 p.

- Milliman, J.D., 1972, Atlantic Continental Shelf and Slope of the United States, petrology and sand fraction northern New Jersey to Southern Florida: U.S.G.S. Professional Paper 529-J.
- Milliman, J.D., O.H. Pilkey, and D.A. Ross, 1972, Sediments of The Continental Margin of the Eastern United States: Geological Society America Bulletin 83-5, p. 1315-1333.
- National Ocean Service, 1986, Soundings in Feet Map, St. Helena Sound to Savannah River, Nautical Chart 11513, Scale 1:40,000: U.S. Department of Commerce, NOAA, Washington D.C.
- National Ocean Service, 1986, Sounding in Feet Map, Savannah River and Wassaw Sound, Nautical Chart 11512, Scale 1:40,000: U.S. Department of Commerce, NOAA, Washington D.C.
- National Ocean Survey, 1978, Bathymetric Map, Hoy & Hills Quadrangle, NOS NH 17-3, Scale 1:250,000: U.S. Department of Commerce, NOAA, Washington D.C.
- National Ocean Survey, 1976, Bathymetric Map, Jacksonville Quadrangle, NH 17-5 (OCS), Scale 1:250,000: U.S. Department of Commerce, NOAA, Washington D.C.
- National Ocean Survey, 1978, Bathymetric Map, Stetson Mesa Quadrangle, NOS NH 17-6, Scale 1:250,000: U.S. Department of Commerce, NOAA, Washington D.C.
- Neal, R.W., Henry, G., and Green, S.H., 1978, Evaluation of the Submerged Discharge of Dredged Material Slurry During Pipeline Dredge Operations: prepared for U.S. Army Engineers Waterways Experiment Station, DMRP-TR D-78-44, available from NTIS AD A062 616, Springsfield, VA.
- Neiheisel, J., and Weavey, C.E., 1967, Transport and Deposition of Clay Materials in Southeastern United States: J. Sediment, Petrol. 37, p. 1084-1116.
- Oertel, G.F., II, and Howard, J.D., 1972, Water Circulation and Sedimentation at Estuary Entrances on The Georgia Coast: in, Shelf Sediment Transport: Process and Pattern (D.J.P. Swift, D.B. Duane, and O.H. Pilkey, eds.) Dowden, Hutchinson & Ross, Inc., Stroudsburg, PA, p. 411-427.
- Office of Technology Assessment, Congress of the United States, 1987, Wastes in Marine Environment: OTA 0-334, Washington D.C.
- Owen, R.M., 1977, An Assessment of the Environmental Impact of Mining on the Continental Shelf: Marine Mine Mining, Vol. 1, No. 1/2, p. 85-102.

- Pequegnat, W.E., Smith, D.D., Presley, B.J., Darnell, R.M., and Reid, R.O., 1978, An Assessment of the Potential Impact of Dredged Material Disposal in the Open Ocean: prepared for Army Engineers Waterways Experiment Station, DMRP-TR-D-78-2, available from NTIS AD AO53 183, Springfield, VA.
- Pilkey, J.H., and Frankenberg, D., 1964, The Relict Recent Sediment Boundary on the Georgia Continental Shelf: Bul. Ga. Acad. Sci. 22C1, p. 37-40.
- Pilkey, O.H., 1963, Heavy Minerals Investigations of Pleistocene Terraces of Lower Coastal Plain Georgia: Soc. Am. Bull. 73, p. 365-374.
- Pirkle, E.C., Pirkle, W.A., and Yoho, W.H., 1974, The Green Cove Springs and Boulougne Heavy-Mineral Sand Deposits of Florida: Economic Geology, Vol. 69, p. 1129-1137.
- Pirkle, E.C., and Yoho, W.H., The Heavy Mineral Ore Body of Trail Ridge, Florida: Economic Geology, Vol. 65, p. 17-30.
- Popence, P., 1986, Paleogeography and Paleoceanography of the Miocene of the Southeastern United States, In Burnett, W.C., and Riggs, S.R., eds., World Phosphate Deposits, V. 3, Neogene Phosphorites of the Southeastern United States: Cambridge University Press (in press).
- Popence, P., and Spalding, J.S., 1988, Isopach and Structure Contour Maps of the Miocene and Post Miocene Sediments in the Southeast Georgia Embayment, Florida Hatteras Shelf: U.S. Geological Survey Open-File Report 88-397, 12 p.
- Richardson, M.J., 1986, Technologies for Dredge Mining Minerals of the Exclusive Economic Zone (EEZ): Revised Draft of Report prepared for Office of Technology Assessment, Congress of the United States, 70 p.
- Sheng, P.Y., 1984, Preliminary User's Manual 3-D Mathematical Model of Coastal, Estuarine and Lake Currents (CELC3D): prepared for U.S. Army Engineers Waterways Experiment Station, DMRP-IR-D-84-1, available from NTIS AD A142 070, Springfield, VA.
- Schubel, J.R., Carter, H.H., Wilson, W.E., Wise, W.M., and Heaton, M.G., 1978, Field Investigations of the Nature, Degree & Extent of Turbidity Generated by Open-Water Pipeline Disposal Operations: prepared for U.S. Army Engineers Waterways Experiment Station, DMRP-TR-78-30, available from NTIS AD A058 507, Springfield, VA.
- Shuba, J.L., Tatem, H.E., and Carroll, J.H., 1978, Biological Assessment Method, to Predict the Impact of Open-Water Disposal to Dredged Material: prepared for U.S. Army Engineers Waterways Experiment Station, TR-D-78-50, available from NTIS AD A060 502, Springfield, VA.

- Smith, J.B., and MacGillvray, T.J., 1988, Developing a Regulatory Framework for Leasing Minerals on Submerged Federal Lands: Marine Mining, Vol. 7, No. 2, p. 137-148.
- South Atlantic Fishery Management Council, 1981, Profile of the Penaeid Shrimp Fishery in the South Atlantic: South Atlantic Fishery Management Council, Charleston, South Carolina.
- Stubblefield, W.L., and Duane, D.B., 1988, Processes Producing North Americas' East Coast Sand and Gravel Resources, A Review: Marine Mining Vol. 7, No. 2, p. 89-122.
- Swift D.J.P., Kofed, J.W., Saulsbury, F.P., and Sears, P.,1972, Holocene Evolution of the Shelf Surface, Central and Southern Atlantic Shelf of North America: In <u>Shelf Sediment Transport: Process and Pattern</u> (D.J.P. Swift, D.B. Duane, and O.H. Plikey, eds.) Dowden, Hutchinson & Ross, Inc., Stroudsburg, PA, p.449-574.
- Tixeront, M., Lelann, R., Horn, R., and Scolari, G., 1978, Illmenite prospecting on the Outer Continental Shelf of Senegal methods and results: Marine Mining Vol. 1, p. 171-187.
- U.S. Bureau of Mines, 1987, An Economic Reconnaissance of Selected Heavy Mineral Placer Deposits in the U.S. Exclusive Economic Zone: U.S. Bureau of Mines Open File Report 4-87, 112 p.
- U.S. Congress, Office of Technology Assessment, 1987, Marine Minerals Exploring our New Ocean Frontier: OTA-0-342, Washington D.C., 349 p.
- U.S. Congress, Office of Technology Assessment, 1987, Wastes in Marine Environments: OTA-0-334, U.S. Government Printing Office, Washington D.C., 313 p.
- U.S. Department of Commerce, 1980, Final Environmental Impact Statement on the Proposed Gray's Reef Marine Sanctuary: National Oceanic and Atmospheric Administration, Washington D.C.
- U.S. Department of Commerce, 1983, Gray's Reef National Marine Sanctuary Management Plan: National Oceanic and Atmospheric Administration, Washington D.C.
- U.S. Geological Survey and National Ocean Survey, 1978, Topographic - Bathymetric Map, Brunswick Quadrangle, NI 17-2, Scale 1:250,000: U.S. Geological Survey, Reston, VA.
- U.S. Geological Survey and National Ocean Survey, 1978, Topographic Bathymetric Map, James Island, NI 17-12, Scale 1:250,000: U.S. Geological Survey, Reston, VA

- U.S. Geological Survey and National Ocean Survey, 1978, Topographic - Bathymetric map, Savannah Quadrangle, NI 17-11, Scale 1:250,000: U.S. Geological Survey, Reston, VA.
- van den Kroonenberg, H.H., 1977, A New Approach to the Design of Offshore Mining Equipment: Marine Mining, Vol. 1, No. 4, p. 327-347.
- Wise, W.M., and Duane, D.B., 1988, An Introduction to the Sand and Gravel Workshop Proceedings: Marine Mining Vol. 7, No. 1, p. 1-6.
- Woolsey, J.R., 1977, Neogene Stratigraphy of the Georgia Coast and Inner Continental Shelf: Unpublished Ph.D. dissertation, University of Georgia, Athens.
- Wynn, J.C., and Grosz, A.E., 1986, Application of the Induced Polarization Method to Offshore Placer Resource Exploration: Proceedings of the Eighteenth Annual Offshore Technology Conference, Houston, TX, p. 395-402.
- Zellars-Williams, Inc., 1978, Evaluation of the Phosphate Deposits of Georgia, North Carolina and South Carolina using the Minerals Availability System: U.S. Department of Interior contract J0377000, 65 p.
- Zellars-Williams, Inc., 1979, Phosphates-Offshore Georgia and South Carolina: Prepared for U.S. Geological Survey under contract number 14-08-001-17501, 161 p.

## **SECTION 9**

# APPENDIX

- 9.1 MODELLED DATA

  Averaged and listed by OCS Block Number (NH21000).
- 9.2 RAW DATA
  Sea floor Characterization, listed by U.S.G.S. sample point number.
- 9.3 RAW DATA
  Grab sample mineralogy, listed by U.S.G.S. sample point number.

is .				
i.t				
				4.5
		q		
ä				
, ž				
· ·				
2				
		(£)		
			a l	
54			W 5	
5.	*			
X				
54				
B				
3				
5				
E				
			90	

# SECTION 9.1

BEDREIA OFFSFORE NINERALS ASSESSIENT MODEL. PAGE 1

nt Scount	•	6 _		=	=	==	<b>8</b> ;		2 2				9.79	<b>8</b>	1. B		= :	= :	<b>3</b> :	2 :		1.10	=	<b>7</b> 3 :	<b>3</b> 3	2 M	3.20	8	=	6.6	£ 38	3:	<b>3</b> :				=	8:		1.20	7.	
of Acount	16.68	16.4	15.40	12.70	6.98			d i	<b>3</b> 8	1 -	- 2		9.6	10, 90	11.70	<b>8</b> :	8.	8 :	99:		2 Z	£.2	7	e :	- F	7.70	8.6	37 ;	ಔ 2 ನು <		19,78	93:	<b>8</b> :	2		4	5.80	3.78	2.98	2.7	2.38	900
f Xcount	8 0	3	2.7	2.3	1.60	<b>8</b>	<b>3</b> 3		8 8	1 8		8	8	8	3	3	2		2 2			33.	2:	3	8 8	8	8:	2 :	3 3		=	8	3 3		8	9.6	E	<b>1.</b> 3	1.80	8.	8:	500
t Acount	E		0.10	<b>.</b> 45	2.9	<b>3</b>	<b>8</b>						=	3	8	3	8 3		2 2			8	8 3			9.10	9	3 1		8	=	2 :				8	8	8	8	3	= :	-
* Acount	3	8	9. 10	4	2 3	3 :					3	8	=	=	3	2	<b>3</b> 2					8	3 :			9	2			8	3	2 : 0 :			8	8		3	2	3 :	2 :	- 100
Scount Scount	3	3	3	3	3 3					8	8	8	3	2	2 :	2	3 1				3	2	3 3			=	3	3 5		3	2 :	2 2		E	8	=	8	2	2 :	3 :	<b>8</b> 1	
Mcoun		3.10		2.80	គឺ	3	۳ <b>۶</b>	3	3 6	1		5.70	5.4	<b>4</b> .8	3 3	8 : d :	= 8 ri =	R		2 2	8 3	M	3.0	# # 1 n	2. IS	저신	36.5	8 8 d u	R R		4.6	2 2	R 8	8	7	4.10	3.60	3.10	8 8	87 ;	<b>2</b> 2	,
Scount Scount Scount Scount Scou	3.20	3.48	3.70	3.80	5. Z	9 8	R R		8	8	<b>3</b>	2.80	<b>8</b>	<b>8</b>	两片	2 5	R 2	3 3		2	<b>8</b>	2.40	2. % %		8 8	4.78	3 8	Ra	8 8 i mi	£.2	2 ;		3 3	7	4.28	3,90	3.60	3, 10		<b>7</b> :	= 3	
Acount	 8.:	1.2		8 :	8 3			8		1.7			<b>₹</b>		<b>≘</b> :	7	= 8	3					<b>2</b> 8				2. 2.1		2 2								=	<b>3</b> 7	两月	<b>3</b> 5	2 E	_
(a) Acount	99.60		91.38	2.4 2.4				87.98		86.88	87.10	8	87.48	2 .	87.88			1 2	1.3				R 7				\$ 5 \$ 5		87.78		<b>8</b> 8	3 5	: 3	8	3	馬	2	8	<b>8</b> 5	<b>R</b> 8	8 7	
(a) thk (a)	8			<b>2</b> 1	8 9		1	49.80	3	_		3	<b>3</b> :	8 8	R 2		R S			14.60 9									_	_	14.36 27.50 27.50	8 8	:	2	3.40 89.	¥. 25	8:	<b>3</b> 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	5 6 5 8	B :		
thk (m)	8.3		-188, 68	# 15 E	e s	8		M		_	3	3			= R	3							8 8		12		-24.00				25.55 25.55 25.55				3	- -	- ·		::: 7:8	7 8		
thk (e)	_	8	8		2 8	1	2	8					8 :	7 2				=					# # # # # # # # # # # # # # # # # # #	-			31.66 -71 11.84 -21				5. 6. A. A.				•	1.28 -38.	8 1	R 1			3 3	
thk (a)	3.4	ក គ	- ` 80 8			25.46			8		2.10			8 5				3																		3	8 8	•	3		i 18	
S E	3.86	_	_		8	-	_			8	8	8 :	3 8					8	8	8	8 :	 B 8	° =	51 8	2	# : # :	£ -	8	8			3		=	: 2 :	~ :		i -		;		
(a) thk (a) thk (a) thk (a) thk (b) thk	13.70			2 2 7	8	21.80	8	95.6		M	8	3 :	3 8		3		8	=	1.38	<b>A</b>	4.10	2 2		7.98	8:			3	2.30 0.	حة د 18 ع	5 a	3	3	=	2	<b>3</b> 2						
	14.60	<b>?</b> 8	7 :			用	3	肃	7	<b>5</b> .	គ្ន	<b>.</b>	8 =	,		12,28	11.60	12.00				8 1	12	8	8 :	7 :								_	<b>-</b>	<b>∹</b>	ų 4	fu	ف اه	i ~	. ~	
4 9	8 :			_	.30 16.	-		#. *6	_	ਹ ਵ	र्त : #:	≃ : B 8			=	12	=	51	12.	.21	= : = :		: °	26	81	ri o B 1	* z	22.38	18.		11.70	12.10	_	3.6	2	2	20.51			9		
.	= :			N N	2	37	87	248	8	=	8:	8 3		3	R		3	=	=	2	e :			=======================================	2:	88	: d	3	3			<b>1</b>	•	2						•	-	
	<b>3</b> 2	Ŗ	R	3	8	97.70	8	_		_					. <del></del> .	3	<del>-</del>	=	=======================================	- -	e . 2 :			3								_	9.11						_	•	3	
	<b>3</b> 8		i s	8	.es	_			9 i	\$ i	3 S	7 % G	7.6		46 99.28	10 99.78	28.	3	3			8	89.28	25.55 25.52	20 A	9		97.78	_		36					8	\$ 55 \$ 55			_	<b>8</b>	
1	2			39.5	39.8	_	_	_			6 6 6 7			_	18.8 0.	19.4	e:	<u>-</u>	4.	e i	ر ا	4	6	-	9 6		•	1			-	•	4 × 0.10	9				9,10		•	_	
	330400.0 J				-		_	•	•		- 4		•	•	•	•	•	•	•	•			•	•	0.0 18.6 0.0 77.7		•	•		0.0 IA.2		•	-	•	8 8			_	•	.e. 25.5	_	
- 41 - 4		1		•		•	•		•		6.8 31/2006.			L. 8 531286.			•				. B 5696.88			•	. 0 588888. . 0 5935.88				. 0 516800.			•	•	•		2,000		•			-	Second &
.   }	72 425 M	72 429589							24 4236 <b>8</b> 0.		A SOCIAL			18 52568E.	9 325688.	9 525688.	A 525600		6 32568.	. Second	Service.	4 525588	16.3 S25640.	200		12560	520600	M. 873 T2860.	520000	22988	520000.	1228686.	528886.	M. 318 328088.	22888	22000	528888	520000.	528888.			Connect
. 8	A 472	88.372	127.00	16.88.271	_	_	_				_	_	_	7 89.678		_		_		_	88.264	_	-	•		-	-	-			_	-	26.269	A6 467	86.417	88.366	88.315	88.265	00.214	80, 163	80.112	679
٦	÷ =	16 31.0	18 31.0	16 31.0	<b>7</b>	_			24, 350 14, 350 14, 350										31.06/						# # # # # # # # # # # # # # # # # # #				21.E2				31.824	70.15			31.823	31.822	31.822	31.62	31.82	27 14.24
.   8		র								17 498	. n	23.040	23.040	23.040	23.046	<b>1</b>	# C	20.00	2 2		3.5	23.04	20 E	j	<b>3</b> 3	23.040	11.42			£ 5	23.64	23. EX	3 2	22 646	23.	23.0	23.040	23.84	23.040	23.0	# 7 E	1400
0101	H21001	5015	H21883	H2184	F0105	HK I Day	M 4	101000	10.0	2	<b>E</b> E E	FE114	<b>FP115</b>	년 9 1 1 9	1112	F 18	F 13	10101	2 2 2	12	HE124	F123	HP126	MCIE/	F 123	F2138	HEIST ST	2 2	15158 H2158	H2159	<b>15158</b>	H2161	7 G	2	E I E	H2166	H2167	F2168	H2169	F13	1713	

ZIRCON	Acount	2	2		3	85	8 :				8	=	8	<b>8</b> 8	3	; ¿	M 58	7 :		2	=	2	7 3	8.	8	7 E				=	<b>3</b> 8	8.	3.2	# 5 6	3 <b>3</b>	8	<b>8</b>	<b>3</b> :	3	3	8
1	3 1	 	9:	<b>8</b> 8		8 4	<b>第</b> :二:	2 ×		2.5	9.5	8	200	用: ni n	3 8		5.70	2. W	R 2		3.	# :	3 6	10.98	19.00		8	9 9	3 8	2.10	2.10	R J mi	<b>8</b>	20 S	9 4	90	10. BB	8 ;	2 2	3	1.1
STALRO TITRA	Scount	=	2				= :	= =	2	3 3	1.10	3	8:	<b>8</b> 8	R 8	2 3	1.6	37	? :		8	= :	# S		87 F	3	3	<b>3</b> 3		2.	<b>8</b> %	R 85	1.68	3 3		1.3	8	8 :	8 8	3	3
RUTILE ST	Scount	8	=	<b>8</b> 1			=	= :			3	=	=	<b>3</b> :		2 2	3	27 S	3 8		8	= :	2 2		= :		3	<b>3</b> 8			<b>8</b> 8		3	3 5	2 2	3	2	8	2 2	8	3
1	Acount	=	2	3 1			=	2 2		2 8		8	=	2 ;		8	7	35	3 1		3	= :	2 2	=	= :			<b>3</b> 1			<b>3</b> 5		3		2 2	8	8	3	3 1	8 8	8
SPART AC	Acount	9.00	=	2 :		3	=	2 2				8	2	2 :			=	2				= :	2 2		3 :	= 1		8 2			2 2		8			3	3	2	<b>3</b> 9	1 S	3
WING PH	Count	8 4	5.2	<b>3</b>	2 2	2	4.68	<b>3</b> 5	R		2	W 88	3.9	8 : mi	3 2	4 Z	<b>87.7</b>	# ? ?	2 1 N -		3	4.28	= 7 	2	8	8 I	8 4	4.68	2 7	3	33.5	2 20 m	23.	<b>8</b> 8	2 A	<b>8</b>	3.76	8	8 4 m 4	8 M	4.38
WH dSG H	Count					2 5		3 7	9 8							3					3	33	2	2	<b>8.</b> 4	= =	2 2	86%	R 2	8 8 1 m	<b>8</b> 8		4.28	<b>8</b> :		<b>7</b>	10 M		<b>2</b> 4	<b>3 3</b>	8
Leg P.	<b>Acount</b>	= :				3															7		= 8			ਲ ਹ -	: :	<b>M</b> :	<b>9</b>	1.20	87:	2 25	1.10	<u>ء</u> د	7 7 -	7	3.38	. 28 	<b>9</b> 3	2	8
INC. BOTTS FLASSON GLOST? * K. FLISS P. FLISS HAYRING PASSART HONG	Count 1	**				8.99												91.10					<b>8</b> :			27.00		99.19	\$ 5 5 5			2 2 2	23.50	2 S	# <b>7</b>	200	2	M. 20	38.70	9 9	88.46
GROW DLAD	hk (m) %	8	8	2 :	2 :	: 3									_				8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	•	_		27.46	_	_	2 2 2 2	1 2		25 × 25 × 25 × 25 × 25 × 25 × 25 × 25 ×			19.20		2 :		_	B. 70	8	<b>.</b>	2 =	2.0
BOTTS OVE	(a)	=	8		3 1	=======================================			2 :	8 2				-49.50 17							# # F		14.18				-		2 8 8 F F			5. 19. 19. 19. 19. 19. 19. 19. 19. 19. 19	3	33 :	R 1		_	8	•		-51.20
ADC 100	k (s) t		병			9.28 -37.		•																	10.56 -37				7 1 2 3 4 5	8 2	33 :			18.58 -2	' '		8			? ?	-
TUL 187	k (a) ti	11 B	_	_		* 6* * 4*		_	# 12 m							2 2	2 2		_				2:						3 %							R =		8	28.8	3 2	33
N GH JU	(e)	8	4			:						: =		2	2 :	4 a	` =	=======================================	열 : 목 :	2 1	: =	=	2 2		8	m 4 8 t			2 2		8:	3 2	=	8	2 : 2 :			3	= :	3 8	8
																								-					<b>~</b> 4												
N OIL NO	(a) th	<b>5</b>	3	=		8 2	•	•	<b>-</b>	<b>.</b>	6 .	<b>.</b>	•	8	3 :	3 5	2 2	8	<b>3</b> :	<b>3</b> 3	i di F M	8	用包	R	8	8 :	2		2 1		87		2	8		e =		8	8 6	2 8	3 =
IN OIL FOREN JID IN	(a) thk (a) th	•	_				3.10 6.	2.00	1.28	3 3			6.30			97.0				# # # # # # # # # # # # # # # # # # #	_		10 12.30			<b>d</b> (	<u>ا</u> ا		# 1	E 89	2	27	-	•	== 0 3 8	ri <u>s</u>		8	8 :		3 3
COLOR DE TOPEN AND MEDE NO MEDE I IL MEDE		8	25,55				3.10 6.	2.00	1.28	<b>.</b>			6.30	用		20 10:10 7:50 00 10:10 7:50 00								12.45 6.78		<b>d</b> (	12.70 1.60		2 1		2	~	_	<b></b>	<b>-</b>	R		8	8 :	7. 10.	3 3
IN OIL MOTOR OF LOCATION OF VO. C.		8	3				3.10 6.	2.00	1.28	3 3			6.30	0.00 10.30	0.00		A 10 10 10 10 10 10 10 10 10 10 10 10 10	6.00 11.10	6.00 12.20	2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3						<b>d</b> (	<u>ا</u> ا			E 89	2	~		•	== 0 3 8	_		2.40 0.00 0.	40 0.00 B.00		30 6.60 18.60
VA T III		3.10 6.00 25.30 6.	20.00	1.50 0.00 22.00	1.00 0.00 19.00		6.20 6.00 12.50 3.10 G.	0.10 0.00 12.10 2.00 0.	1.28	3 3			6.30	0.00 10.30	0.00		A 10 10 10 10 10 10 10 10 10 10 10 10 10	6.00 11.10	70 C.10 C.00 12.20			56 6.46 6.88 17.58				<b>d</b> (	<u>ا</u> ا			E 89	0 6.00 6.00 10.70	~		•	== 0 3 8	_	L71 LM 8.60	2.48 2.48 8.88 8.	70 6.40 0.00 6.00		50 1.36 0.00 18.60
VAN THE NAV	AN AN AN	3.10 6.00 25.30 6.	20.00	1.50 0.00 22.00	1.00 0.00 19.00		6.20 6.00 12.50 3.10 G.	0.10 0.00 12.10 2.00 0.	1.28				36 0.06 0.08 10.50 6.30 0.	99 6.00 6.00 10.30	70 6.00 6.00 10.50			6.00 11.10	70 C.10 C.00 12.20			56 6.46 6.88 17.58	00 0.10 0.00 15.10		98 6.00 6.00 12.10	<b>d</b> (	<u>ا</u> ا			E 89	2	~	99.60 0.00 0.00 10.70	79.50 8.60 8.00 13.78 8.		_		2.48 2.48 8.88 8.	70 6.40 0.00 6.00		30 6.60 18.60
70 E 113 Gross Classes	MAN AND SALI LLAN MAN	3.10 6.00 25.30 6.	20.00	8.78 97.88 1.58 8.88 22.88	6, 45 99, 56 1, 86 0, 88 19, 88		6,46 99.30 6,20 6.00 12.50 3.10 G.	8.39 99.68 8.10 8.00 12.10 2.00 B.	0.10 99.96 0.06 0.00 12.40 1.20 0.				0.00 99:30 0.00 0.00 16.50 6.30 0.	6.16 99.39 6.80 6.80 18.38	6.26 99.70 6.60 6.00 10.50			4.10 99.70 6.00 6.00 11.10	6.16 99.70 6.10 6.00 12.20			0.10 99.56 0.40 0.80 17.59	0.00 99.00 0.10 0.00 15.10	F.10 25.76 6.20 5.30 15.30	8,16 99.30 6.80 6.80 12.10	2.69 97.40 0.00 0.00 15.70 0.		1.00 100.00 0.00 0.00 13.20	0.00 100.00 0.00 13.10		6.00 99.90 6.00 6.00 10.70		0.20 99.60 0.00 0.00 10.70	19.90 79.50 0.60 0.00 13.70 0.	9.16 99.86 0.00 0.00 11.50 B.		1.84 97.50 p.76 p.86 p.50	8,38 94,28 2,48 2,48 8,00 B.	0.80 96.70 0.40 0.00 8.86	6, 15 93, 15 6, 45 6, 15	8.10 98.50 1.30 9.00 18.50
VAR THE RANGE COMPANY	(a) at 5 at 5 at 5 at 5 at 5	A A 9 A 20 95.70 3.10 A.00 25.30 4.	A 16.3 6.45 97.65 2.88 6.88 25.65	.0 14.4 E.70 97.80 1.50 E.00 22.00	.0 15.9 0.40 90.50 1.00 0.00 19.00	. 6 17.3 6.20 99.30 6.30 6.00 15.00	19.5 0.46 99.30 0.20 0.00 12.50 3.10 0.	.0 19.5 0.30 99.60 0.10 0.00 12.10 2.00 0.	0 19.8 0.10 99.98 0.08 0.00 12.40 1.20 0.				0 24.2 0.00 99.30 0.00 0.00 10.50 6.30 0.	8 30.0 6.10 99.99 6.00 6.00 10.34	31.6 6.26 99.70 6.60 6.00 10.56			.0 46.5 6.10 99.70 6.00 6.00 11.10	0 41.7 6.10 59.70 6.10 6.00 12.20			.0 16.9 0.10 99.56 0.40 0.00 17.50	17.9 6.60 99.50 6.10 6.86 15.18	8 19.2	.6 20.2 4.16 99.90 6.00 6.00 12.10	1.0 10.4 2.60 97.40 0.00 0.00 15.70 0.	1,0 201.7 0,00 100.00 0.00 0.00 12.40 CA	0 23.7 0.00 100.00 0.00 0.00 13.20	18 28.9 8.88 180.88 0.88 0.88 13.18		6 29.9 6.86 99.96 6.86 6.86 18.78		0 39.2 0.20 99.60 0.00 0.00 10.70	.0 10.4 19.90 79.50 0.60 0.00 13.78 0.	.0 40.3 0.10 99.80 0.00 0.00 11.60 B.		A 15 A 150 47.75 B.70 B.70 B.60	0 1.5 0.30 94.20 2.40 2.40 0.00 0.	0 17.9 0.80 98.70 0.40 0.00 8.80	0 7.4 0.10 93.50 6.40 0.00 20.50 0 13 0 4 10 07 74 0 90 4 10 02 90 0	13.5 0.10 30.50 1.30 0.00 18.60 18.60
VARIATION TO COMPANY STATES		3.10 6.00 25.30 6.	A 16.3 6.45 97.65 2.88 6.88 25.65	.0 14.4 E.70 97.80 1.50 E.00 22.00	.0 15.9 0.40 90.50 1.00 0.00 19.00		19.5 0.46 99.30 0.20 0.00 12.50 3.10 0.	.0 19.5 0.30 99.60 0.10 0.00 12.10 2.00 0.	0 19.8 0.10 99.98 0.08 0.00 12.40 1.20 0.				.0 25.2 0.00 99.30 0.00 0.00 10.50 6.30 0.	8 30.0 0.10 99.90 0.00 0.00 10.30	.0 31.6 0.28 99.70 0.00 0.00 10.50			0 44.5 6.10 99.70 0.00 0.00 11.10	.8 598480.0 41.7 6.16 99.70 6.10 6.60 12.20	. B. Sec. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10		0.516000.0 16.9 0.10 99.50 0.40 0.00 17.50	.0 TELEBO.8 17.9 0.00 99.00 0.10 0.00 15.10	18.50446.6 15.2 11.10 75.70 11.00 11.30 11.30 11.30 11.30 11.30 11.30 11.30 11.30 11.30 11.30 11.30 11.30 11.30	0.53600.0 20.2 0.16 99.90 0.00 0.00 12.10	.0 516800.0 10.4 2.68 97.40 0.00 0.00 15.70 0.		0 350464 0 23.7 4.00 104.00 4.00 4.00 13.20	0.332200.0 26.9 0.00 100.00 0.00 0.00 13.10	0.550000.0 29.0 0.00 100.00 0.00 0.00 12.00 0.00 0.00	0.55560.0 29.9 0.00 29.90 0.00 0.00 10.70		364000.0 39.2 0.20 99.60 0.00 0.00 10.70	\$21600.0 10.4 19.90 79.50 0.60 0.00 13.70 0.	588880.0 48.3 0.10 99.80 0.00 0.00 11.60 B.	8 293686.8 41.7 6.68 25.38 8.68 6.68 16.38 6.58 6.58 16.38 1	0.525.000.0 15.7 0.00 25.75 0.75 0.00 0.55 0.55	0 468890.0 1.5 0.30 94.20 2.40 2.40 0.00 0.	0.531280.0 17.9 0.80 90.70 0.40 0.00 8.80	18 497588.8 7.4 8.18 93.58 6.4 0.58 20.58	8 30/200.0 14.8 0.10 98.50 1.30 0.00 18.60
NAME THE PARTY CONTRACTOR OF THE PARTY CONTRACTOR	MICHAEL CAND SALI CLAY MAN (B) (B) (B) MAY	5, 25, 25, 21, 5, 26, 26, 26, 26, 26, 26, 26, 26, 26, 26	SIGNAL B S27200 0 10.3 0.49 97.69 2.00 0.00 25.60	516000.0 512000.0 14.4 B.78 97.80 1.50 B.00 22.00	Sidema, 8 Sidama, 6 15.9 6.48 98.50 1.88 0.80 19.80	516886.0 \$21686.0 17.3 0.20 99.30 0.30 0.30 0.30 15.00	SIGNADA SSIZNA 19.5 0.44 99.30 0.20 0.00 12.50 3.10 0.	SIGGOD. 8 536000.0 19.5 8.30 99.60 0.10 0.00 12.10 2.00 0.	S16000.0 SABBOO.0 19.6 0.10 99.90 0.00 0.00 12.40 1.20 0.	216080.8 SASSBLG 20.1 0.00 100.00 0.00 0.00 12.00 0.00 0		216.0000.0 223.2500.0 24,3 4,00 100.00 6,00 6,00 13,3 6,00 6,10 6,10 6,10 6,10 6,10 6,10 6,10	516880, 854880, 254.2 0.00 59.30 0.00 0.00 10.50 6.30 0.	516898.8 569588.8 38.8 8.18 99.99 8.80 8.00 18.30	516888.8 574488.8 31.8 8.28 99.70 6.68 8.88 10.58	SIGNAC 079200.0 34.6 0.46 99.30 0.00 0.00 10.10	SIGNATURE STANDARD STATE OF STANDARD ST	516000.0 593600.0 40.5 0.10 99.70 0.00 0.00 11.10	SIGNOR, 8 598400, 0 41.7 0.10 59.70 0.10 0.00 12.20	S11298.0 S22.48.0 6.3 9.10 99.50 5.30 0.40 52.12	511279.0.507290.0.13.7 41.30 55.0.10 1.50 11.00 52.50 53.12.10 53.00 13.5 5.40 59.50 11.10 6.00 50.00 13	511200.0 516600.0 16.9 0.10 99.50 0.40 0.00 17.50	511200.0 521500.0 17.9 0.00 99.00 0.10 0.00 15.10	511290.0 325400.0 15.2 0.10 25.70 0.20 0.00 15.30 51.00 0.10 0.10 0.10 0.10 15.30	511296.0 536906.0 29.2 6.16 99.39 6.00 6.00 12.10	SYSSM 0 516800.0 10.4 2.69 97.40 0.00 0.00 15.70 0.		511280.0 550400.0 23.7 0.00 100.00 0.00 0.00 13.20	511204.0 5552504.0 26.9 0.00 100.00 0.00 0.00 13.10	511200.0 560000.0 25.0 0.00 100.00 1.00 1.00 1.00 12.00	511204.0 359600.0 29.9 6.00 99.90 6.00 6.00 10.70	511296.0 574486.0 12.0 0 0.10 99.00 0.00 0.00 10.30 7.	511280.0 554280.0 39.2 0.20 99.50 0.00 0.00 10.70	535286.0 521586.0 10.4 19.90 79.50 0.60 0.00 13.70 0.	5112mg. 6 55650mg. 0 44.3 0.10 99.80 0.00 0.00 11.60 8.	511290.0 593600.0 41.7	311200.6 330900.0 43.7 0,00 32.10 0.10 0.00 11.10 0.00 11.10 0.50	566400.0 468800.0 1.5 0.30 94.20 2.40 2.40 0.00 0.	535200.0 531200.0 17.9 0.80 90.70 0.40 0.00 8.00	506400,0 497600,0 7.4 0.10 93.50 6.40 0.00 25.50 control of the co	506490.0 507200.0 14.8 0.10 98.50 1.30 0.00 18.60
NAME THE PARTY CONTRACTOR OF THE PARTY CONTRACTOR	MICHAEL CAND SALI CLAY BANGE (B) (B) (B) AND	A A 9 A 20 95.70 3.10 A.00 25.30 4.	CO. S. (AMAG. B. S. 27.50 2.00 0.00 25.50	86.673 516886.8 512886.8 14.4 8.78 97.88 1.59 8.00 22.00	89. R23 S16888.8 S16888.8 15.9 6.48 98.68 1.88 0.80 19.80	88,772 516880.0 521680.0 17.3 6.28 99.38 6.38 6.58 15.00 a.m. lb.00	Ma. 678 SIGARA, B. SSIZHA, B. 19, S. B. 46 99, 30 G. 20 G. 10 12, 50 3.10 G.	80.629 516880.8 536880.0 19.5 8.39 99.68 0.10 0.00 12.10 2.00 0.	88,569 516888.8 548888.0 19.8 0.10 99.98 0.88 0.00 12.40 1.29 0.	BM.518 515000.0 515500.0 20.1 0.00 100.00 0.00 0.00 12.00 0.55 0.50		26.417 315.000.0 333200.0 24.3 4.00 100.00 0.00 0.00 13.3 6.10 0.00 0.00 0.00 0.00 0.00 0.00 0.00	60.316.516.000,0 SA4000,0 SA.2 0.00 99.30 0.00 0.00 10.30 6.30 0.00	56. 265 516000.0 269500.0 30.0 0.10 99.90 0.00 0.00 10.30	86.214 516986.0 574486.0 31.0 6.28 59.70 6.00 6.00 16.50	28.164.516.884.0.579284.0.34.6.0.45.99.38 0.48 0.48 10.10	SECTION STATEMENT STATEMEN	89,011 516800.0 593600.0 44.5 0.10 59.70 0.00 0.00 11.10	79, 961 516888.8 598488.0 41.7 6.18 99.78 6.18 6.68 12.28	26.975 511298.6 51248.6 6.3 6.10 95.66 51.30 0.00 25.70	28.29 51129 0 5179 0 14.7 4 3 3 5 6 6 7 1 10 4 5 5 6 6 6 7 1 10 4 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	84.423 511204.6 516506.0 16.9 0.10 99.56 0.40 0.00 17.50	84.772 511280.0 \$21680.0 17.9 0.00 99.00 0.10 0.80 15.10	28,721 511284,0 525440.0 15.2 0.10 55.70 0.20 0.00 15.30 15.40 as 531500 0.50 0.00 0.00 0.00 0.00 15.40	84.620 511290.0 536904.0 29.2 4.16 99.39 0.00 0.00 12.10	86, 622 535290.0 516800.0 10.4 2.69 97.40 0.00 0.00 15.70 0.	88,559 511280.0 548680.0 28.7	56.468 511200.0 330440.0 23.7 8.00 100.00 6.00 8.00 13.20	04.417 511200.0 555200.0 26.9 0.00 100.00 0.00 0.00 13.10	60,367 511280.0 560000.0 28.0 0.00 100.00 0.00 0.00 12.00 12.00 14.00 14.00 17.00 18	M. 255 511200. 0 559500. 0 29. 9 0.00 99. 90 0.00 0.00 10.70	58,215 511286.0 574486.0 12.0 0.10 59.00 0.00 0.00 0.00 18.30 7.	BA, 113 511280, 0.54880, 0.39.2 0.20 99.60 0.00 0.00 10.70	86.771 535286.0 521686.0 18.4 19.90 79.50 8.66 8.00 13.78 8.	89,863 511290,8 588880,8 44,3 8,18 99,89 8,69 8,69 11,69 8,	25.012 511200.0 593640.0 41.7 0.00 35.30 0.00 0.00 16.30	73, 301 311000.0 320100.0 13.7 0.00 22.10 0.10 0.20 0.10 0.10 0.10 0.1	81,329 586400 468600 1.5 0.30 94.20 2.40 2.40 0.00 0.	84,670 535200.0 531200.0 17.9 0.80 90.70 0.40 0.00 5.00	81.025.506400.0 497600.0 7.4 0.10 93.50 6.40 0.00 25.50	88,973 386488.8 387288.8 13.16 98.58 1.38 8.88 18.58
NAME THE PARTY CONTRACTOR OF THE PARTY CONTRACTOR	ATTILLE LIMBITUDE MUNITH EAST URPHY BANNEL SHOW SILL LLANT AND (deg) (deg) (a) (a) (a) while we'll not it in the sill limbitude (deg) (deg) (a) (a) (a) (b) while the sill limbitude (deg)	475 Sidema a september 8.9 8.78 3.18 8.88 25.38 6.	31.701 Ma Que Signata 1972ma 1 m. 3 m. 40 97,50 2.00 0.00 25,50	31.781 80.873 516800.8 512800.8 14.4 8.78 97.86 1.59 8.00 22.80	31,781 80,623 516000,0 516000,0 15,9 0,40 90,60 1,00 0,00 19,00	516886.0 \$21686.0 17.3 0.20 99.30 0.30 0.30 0.30 15.00	Ma. 678 SIGARA, B. SSIZHA, B. 19, S. B. 46 99, 30 G. 20 G. 10 12, 50 3.10 G.	31,781 00.620 516000.8 536000.8 19.5 0.30 99.60 0.10 0.00 12.10 2.00 0.	31.789 88.569 51698.8 54888.0 19.8 8.18 99.98 6.88 8.00 12.40 1.28 6.	31,789 BB.S18 515086.8 545586.8 20.1 8.00 100.00 6.00 6.00 12.00 0.60 8.		31,789 58,417 515890,0 535290,0 24,3 4,00 100,00 6,00 6,00 13,30 6,70 6,31 13,30 6,30 10,00 13,30 6,30 13,30 6,30 13,30 6,30 13,30 6,30 13,30 6,30 13,30 6,30 13,3	31,779 de,316 516apa, 6154apa, 25,2 6.00 59.90 de,00 de,00 18.50 6.30 ft.	31,779 04,265 516004.0 565600.0 34.0 0.10 99.90 0.00 0.00 18.30	31.779 80.214 516000.0 574400.0 31.8 0.20 99.70 0.00 0.00 10.50	31,778 del.164 516886.0 579286.0 34.6 6.46 99.36 6.80 6.80 10.10	31.7/6 EM. 113 316000.0 324000.0 374	31,777 86.011 516000.0 593600.0 46.5 6.10 99.70 0.00 0.00 11.10	31.777 79.961 516000.0 598400.0 41.7 0.10 99.70 0.10 0.00 12.20	31,736 56,975 511296,6 562466,6 6.3 6.16 54.66 51.36 6.46 52.78	31,736 58,294 51120 6 34720 6 13,7 41,39 78,50 14 6 14 6 15,50 14	31,738 86.623 511286.6 516586.0 16.9 6.18 99.56 6.40 6.80 17.58	31,738 84,772 511280.0 521580.0 17.9 6.00 99.00 6.10 0.00 15.10	31,736 08.721 511200,0 525400.0 19.2 0.10 55.70 0.20 0.00 15.30	31,737 86,620 511200,0 536000,0 20.2 8,10 99.90 0,00 0,00 12.10	31,954 88,822 552280.0 516800.6 10.4 2,69 97,40 8,00 0.00 15,70 8.	31,737 BB,569 511200.8 548600.0 58.7 6.40 100.00 0.00 0.00 0.00 16.40 6.	31,737 66,466 511200.0 330400.0 23.7 0.00 100.00 0.00 0.30	31,737 88,417 511298.0 555298.8 26.9 8.00 106.00 0.00 0.00 13.10	31,735 60,367 511200,0 560000,0 23,0 0,00 100,00 0,00 0,00 12,00 1	31,736 80,265 511280,8 55560,8 29.9 6.00 99.90 6.00 6.00 16.70	31,725 50,215 51200.0 574400.0 22.0 '0.10 99.00 5.00 0.00 0.00 10.30 7.	31,725 BB.113 511280, 8 54480, 0 39.2 6.20 99.50 6.00 0.00 10.70	31,954 86.771 535286.0 521686.0 10.4 19.90 79.50 0.60 0.00 13.70 0.	31,734 B0.063 511200.0 556500.0 40.3 0.10 99.80 0.00 0.00 11.60 8.	31,734 BB.012 511200.0 593500.0 41.7 0.00 25.30 0.00 0.00 15.30	31.734 73.301 311200.0 33000.0 43.7 0.00 32.10 51.0 51.0 31.0 31.0 31.0 51.0 51.0 51.0 51.0 51.0 51.0 51.0 5	31,694 81,329 586490.0 468890.0 1.5 0.30 94.20 2.40 2.40 0.00 0.	31,954 60,670 535200.0 531200.0 17.9 0.00 90.70 0.40 0.00 8.00	31,655 81,825 586488.8 497688.8 7.4 8.18 93.58 6.48 8.89 25.38	31,655 88,972 306480,0 306480,0 13.5 8.10 98.50 1.30 8.00 18.60 31,695 88,924 306480,0 307200,0 14.8 8.10 98.50 1.30 8.00
NA TIES AND PROPERTY PROPERTY OF THE PARTY O	LATITUE LUBSITUE NUKTH EAST DEPTH BANNEL SWAD SALL LLANT MA. (deg) (deg) (a) (a) (a) whi with the standard control of the stan	4. 25. 25. 31.0 at 17. 17. 17. 17. 17. 17. 17. 17. 17. 17.	31.701 Ma Que Signata 1972ma 1 m. 3 m. 40 97,50 2.00 0.00 25,50	31.781 80.673 516800.8 512800.8 14.4 0.78 97.80 1.50 0.00 22.00	31,781 80,623 516000,0 516000,0 15,9 0,40 90,60 1,00 0,00 19,00	88,772 516880.0 521680.0 17.3 6.28 99.38 6.38 6.58 15.00 a.m. lb.00	31.751 ON.751 310000.0 LEGIONO. 16.7 6.20 0.30 0.20 0.30 0.30 0.30 0.30 0.30 0	31,781 80.629 516000.8 536000.8 19.5 8.39 99.60 0.10 0.00 12.10 2.00 0.	31.789 88.569 51698.8 54888.0 19.8 8.18 99.98 6.88 8.00 12.40 1.28 6.	31,789 BB.S18 515086.8 545586.8 20.1 8.00 100.00 6.00 6.00 12.00 0.50 8.		28.417 315.800.0 333.200.0 24.3 4.00 100.0 0.00 0.00 0.00 13.3 6.10 0.00 0.00 0.00 0.00 0.00 0.00 0.00	31,779 de,316 516apa, 6154apa, 25,2 6.00 59.90 de,00 de,00 18.50 6.30 ft.	31,779 04,265 516004.0 565600.0 34.0 0.10 99.90 0.00 0.00 18.30	31.779 80.214 516000.0 574400.0 31.8 0.20 99.70 0.00 0.00 10.50	31,778 del.164 516886.0 579286.0 34.6 6.46 99.36 6.80 6.80 10.10	31.7/6 EM. 113 316000.0 324000.0 374	31,777 86.011 516000.0 593600.0 46.5 6.10 99.70 0.00 0.00 11.10	31.777 79.961 516000.0 598400.0 41.7 0.10 99.70 0.10 0.00 12.20	31,736 56,975 511296,6 562466,6 6.3 6.16 54.66 51.36 6.46 52.78	31,736 58,294 51120 6 34720 6 13,7 41,39 78,50 14 6 14 6 15,50 14	31,738 86.623 511286.6 516586.0 16.9 6.18 99.56 6.40 6.80 17.58	31,738 84,772 511280.0 521580.0 17.9 6.00 99.00 6.10 0.00 15.10	31,736 08.721 511200,0 525400.0 19.2 0.10 55.70 0.20 0.00 15.30	31,737 86,620 511200,0 536000,0 20.2 8,10 99.90 0,00 0,00 12.10	31,954 88,822 552280.0 516800.6 10.4 2,69 97,40 8,00 0.00 15,70 8.	31,737 BB,569 511200.8 548600.0 58.7 6.40 100.00 0.00 0.00 0.00 16.40 6.	56.468 511200.0 330440.0 23.7 8.00 100.00 6.00 8.00 13.20	31,737 88,417 511298.0 555298.8 26.9 8.00 106.00 0.00 0.00 13.10	31,735 60,367 511200,0 560000,0 23,0 0,00 100,00 0,00 0,00 12,00 1	31,736 80,265 511280,8 55560,8 29.9 6.00 99.90 6.00 6.00 16.70	31,725 50,215 51200.0 574400.0 22.0 '0.10 99.00 5.00 0.00 0.00 10.30 7.	31,725 BB.113 511280, 8 54480, 0 39.2 6.20 99.50 6.00 0.00 10.70	31,954 86.771 535286.0 521686.0 10.4 19.90 79.50 0.60 0.00 13.70 0.	31,734 B0.063 511200.0 556500.0 40.3 0.10 99.80 0.00 0.00 11.60 8.	31,734 BB.012 511200.0 593500.0 41.7 0.00 25.30 0.00 0.00 15.30	31.734 73.301 311200.0 33000.0 43.7 0.00 32.10 51.0 51.0 31.0 31.0 31.0 51.0 51.0 51.0 51.0 51.0 51.0 51.0 5	31,694 81,329 586490.0 468890.0 1.5 0.30 94.20 2.40 2.40 0.00 0.	31,954 60,670 535200.0 531200.0 17.9 0.00 90.70 0.40 0.00 8.00	31,655 81,825 586488.8 497688.8 7.4 8.18 93.58 6.48 8.89 25.38	88,973 386488.8 387288.8 13.16 98.58 1.38 8.88 18.58
NA TIES AND PROPERTY PROPERTY OF THE PARTY O	ATTILLE LIMBITUDE MUNITH EAST URPHY BANNEL SHOW SILL LLANT AND (deg) (deg) (a) (a) (a) while we'll not it in the sill limbitude (deg) (deg) (a) (a) (a) (b) while the sill limbitude (deg)	6.35 81.3 81.2 81.2 82.3 92.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8	31.701 Ma Que Signata 1972ma 1 m. 3 m. 40 97,50 2.00 0.00 25,50	23.044 31.781 00.873 516000.0 512000.0 14.4 0.78 97.00 1.50 0.00 22.00	23,046 31,781 80,623 516000,0 516000,0 15,9 6,40 90,60 1,00 0,00 19,00	23,040 31,781 86,772 516860,0 521680,0 17,3 6,28 59,38 6,58 6,58 6,58 6,58 6,58 6,58 6,58 6,5	31.751 ON.751 310000.0 LEGIONO. 16.7 6.20 0.30 0.20 0.30 0.30 0.30 0.30 0.30 0	23.040 31.781 80.620 516000.0 536000.0 19.5 0.30 99.60 0.10 0.00 12.10 2.00 0.	23.044 31.786 88.569 516000.0 548800.0 19.8 0.10 99.98 0.00 0.00 12.40 1.20 0.	23,040 31,780 80,516 516,000,0 515,000,0 20,1 0,00 100,00 0,00 0,00 12,00 0,100 0,00 0,		23,040,31,780,08,417,315,000,10,333,000,00,233,000,00,00,00,00,00,00,00,00,00,00,00,	31,779 de,316 516apa, 6154apa, 25,2 6.00 59.90 de,00 de,00 18.50 6.30 ft.	23,648 31.779 56.265 516860.8 569580.8 30.0 6.10 99.90 6.00 6.00 18.30	23,040 31,779 50,214 516000.0 574400.0 31.0 0,20 99.70 0.00 0.00 10.50	31,778 del.164 516886.0 579286.0 34.6 6.46 99.36 6.80 6.80 10.10	23.044 31.76 00.113 315000.6 374900.0 37.4 0.35 22.10 0.40 0.40 10.50	31,777 86.011 516000.0 593600.0 46.5 6.10 99.70 0.00 0.00 11.10	23,040 31,777 79,361 516000.0 599400.0 41.7 0.10 99.70 0.10 0.00 12.20	11,392 31,738 36,975 511298,6 51246,6 6.3 0.10 54.66 5.38 0.00 25.78	31,736 58,294 51120 6 34720 6 13,7 41,39 78,50 14 6 14 6 15,50 14	23,046 31,738 84,823 511284,0 516586,0 16.9 0.18 99.56 0.40 0.00 17.58	23,646 31,738 86,772 511260.6 521660.8 17.9 6.00 99.50 6.10 6.80 15.10	31,736 08.721 511200,0 525400.0 19.2 0.10 55.70 0.20 0.00 15.30	23,040 31,737 00.620 51/200.0 536000.0 20.2 0.10 99.90 0.00 0.00 12.10	2,721 31,954 68,822 535280,0 516880,0 10,4 2,69 97,40 0,00 0,00 15,70 0.	23,046 31,737 86,569 51,280,0 546660,0 28.7 6.45 190,00 6.45 6.45 5.45 5.45 5.45 5.45 5.45 5.45	23,040 31,737 00,468 51120a.0 55040a.0 23.7 0.00 100.00 0.00 0.00 13.20	23,040 31,737 80,417 511200.0 55520.0 26.9 0.00 100.00 0.00 0.00 13.10	31,735 60,367 511200,0 560000,0 23,0 0,00 100,00 0,00 0,00 12,00 1	23.040 31,736 00,265 511204.0 55560.0 29.9 6.00 59.90 6.00 10.70	23,646 31,735 68,215 51/200,0 574460,6 22.0 '0,10 99,00 0,00 0,00 0,00 18,30 7.	31,725 BB.113 511280, 8 54480, 0 39.2 6.20 99.50 6.00 0.00 10.70	21, 341 31, 954 86.771 535286.0 521686.0 18.4 19.90 79.50 8.60 8.60 13.70 8.	23.040 31.734 00.063 511200.8 588800.0 40.3 0.10 99.80 0.00 0.00 11.60 8.	23,046 31,734 66.012 511280.0 393566.0 41.7 6.00 35.30 6.00 6.00 15.30	31.734 73.301 311200.0 33000.0 43.7 0.00 32.10 51.0 51.0 31.0 31.0 31.0 51.0 51.0 51.0 51.0 51.0 51.0 51.0 5	23,040 31,654 81,329 36400,0 468800,0 1,5 0,30 94,20 2,40 2,40 0,00 0,	23.046 31.554 84,670 535286.0 531286.0 17.9 0.86 98.70 6.40 0.00 8.86	22,784 31,655 81,825 56468,8 497686,8 7.4 6,18 93,56 6,48 6,48 25,58	31,655 88,972 306480,0 306480,0 13.5 8.10 98.50 1.30 8.00 18.60 31,695 88,924 306480,0 307200,0 14.8 8.10 98.50 1.30 8.00

ZINCON:				25	<b>3</b> 5	R 2	8			8		8	8	= :	1.64	2.88	4.4	5.70	6.30	6.48	8.	2 2			2	1.20	1.50	8 8	R	2 <b>2</b>	8	=	=:	= :	= :	6	R 7	3 8	3	6.50	6.70	8	5. <b>68</b>	8	9
7 #		=	8	6.28			8 5		2.10	\$ ri		5.10	8.	82.3	2.80	7.	6.60	6.38	9.68	9.30	8.	8.5		3 8	3	8	20.5	97.0	2 1	3	8.9	8	2	8:	3	<b>*</b> :	8 5		3	3	997	95.	99.	. 2	8
STRUMO TITUM		Į	-	_	2 ×		27.7		3	8	85	2	8	2	8.	1.70	2	82.	91	•	8	<b>3</b> 8		3	3	=	=======================================	m s	3		<b>7</b>	200	3	3 1	<b>R</b> 2	Ŗ 8	R	9		1.10	8	87	8	8	8
AUTILE ST				2	<b>3</b> 1				8	8	=	8	3	3		馬	3	_	8	8	=	3 8			3	3	=	2 2		: 2	8	=	= =	= : 8 :	- ·	:	2 8		3 2		35	8	- -	3	1
* #			3	2	<b>.</b> .			8	: = : 8	3	3	2	2	8	10 0.	- R	33		<b>3</b>	<b>≕</b> 88 :	- 2	e :			=	2	• •	- -	i .		•	=	•	ei ( 2 :						=	*	•	<b>.</b>	•	
R. FLUSP P. FLUSP HYTHING PRESPIRIT MANUAL SCOUNT S				- 2	e . 2 :				: = : 22	2	2	2	2	<u> </u>	•	-	2	•	=	2	•	2 1			-	-	<u>.</u>	-			•	3	-	= ;						9.9	9.9	9.0	9.9		-
Acount to			<b>8</b>	- R				4		3	-	•	1	-	3	-	-	-	3	3	3	3 :			-	3	3	33		3	3	3	3	3;				ŀ		-	•	-	3	9	9.0
unt Yea	1_	•	i iri	<b>-</b>	<del>-</del> -	<i>i</i>	-	4.8	7	4.5	4.6	4.8	6.2	4.4	3.7	3.1	2.68	2.4	8.7	e i	# d		6 = 6 =		4.1	_	7			-	4.0	in mi	₹.	ਲ -		7 8	4 3 4 mi	7			3.76	3,00	ਲ. <del>*</del>	2.7	2.4
int Acount	8.5	ri R	eri -	ri	# #	÷ -4	-	mi mi		eri eri	3.9	4.0	5.7	+	4.10	4.1	4.10	4.	4.1	M i	<b>两</b> :	4 4			5.2	4	ਹ ਜ	2 7		, M	3.5	4.	3	<b>3</b> :		2 4		8	7	4. 10	4.10	 3.98	4. W	3, 38	2.9
		L.	1.6	= :		1.3	1.28	1.5		1.60	<b>M</b> :	1.10	9.8	 87.1	7.	1.10	9.	9.3	3	3 3	8 3	<b>8</b> 5	3		<b>6</b> . 28	3	8	g =	7		3.4	## 	<b>3</b>	<b>8</b> :			7		0.7	9.50	9.60	<b>9</b> 7	9.0	7:	2.20
) thk (s) thk (s) Xcoun		88.18					89		56.7	89.80	89.10	69.10	86.38	89.20	89.60	96.18	<b>38</b> '85	91.38	<b>35</b> .28	2 2 3 3 1	27.78	2 S		# # £	86.78		89.59	2 Z		1 2	88.18	æ::6	<b>8</b>	3 8	R		89.28	89.30	89.38	89.50	86.88	8 8	88.38	91.30	91.60
(a) this (a) Acount		34.78		31.80	2 K					14.86	14.38	15, 10	10.80	16.38	19.50	19.90	20.60	સ સ	24.50	= : रा	2.2	7 2		1 3	<b>2.3</b>	8 9	8 2	R R	8	14	16.10	3.5	5. 10			2 8	A	3	21.30	23.10	26. 48	14.60	31.60	14.80	15.20
(a) thk (a		27.00		2.5		3	23.58	-39.20	1.23	43.78	4.10	-46.88	55.10	56.98	-5c	£5.28	-73.28	-89.00	8. S	3.5	<b>9</b> 7	<b>1</b> 2	1 5	57.78	-39. PR	57.38		명 R 위 약	¥ 4	8	3.7	-50.88	\$ .	47.10 1.7.10	R		61.20	-71.20	-78.98	-67.78	-97.70	53.30	107.98	33.55	57.60
thk (m		20.6	=	= :	2 T	8	19.28	8.6	3	P 28	S. 33	187. '9	10.11	=	, M vi	5.88	7:	=	2	3 :			3 8		6.88	3 :	8 :	1 1 3 A 4 E	,		_	19.60	7.50	9 5	B 5		2.78	2.10	851	8	8	3	5.68 -1	3	200
(a) thk (a) thk	8		8	<b>3</b> 3	5 F	7	3	用:	8.3	0.70	2.0	9.6	2.43	1.20	3. <b>4</b>	6.56		5. 50 5. 50 50 5. 50 5.	<b>3</b>	23.52		7 7	2 2		\$	A :	<b>用</b> :	R 8	3	3		3	<b>8</b> :	= 5	3 3	8		2.80	18.10	24. 86	<b>38</b>	14.40 2	8,	 35	8
thk (a)		=	=	2 :		3	8	8	8	8	8	8	8	8	8	8	=======================================	= :	2	<b>3</b> 3					3	8	<b>3</b> 1		1		8	3	8:	<b>2</b> 1	1	1		8	8	28	₹ 8	2	₩ 8	<b>3</b>	3
(a) thk (a) thk		8			64.6	2.7	39	8.	<b>两</b>	3.	8	8	1 12:	8	=	9.78	Pi.	=	2			9.4	15	2	3	用:	3 /		8	8	8	3 :	2	8 8					R	93	•	8	<b>-</b>	<b>3</b>	85
thk (s) t	8	10 19	8	# :	= 5	2	8	2 8	8	<b>4</b> 2.	2 #7	78 3.	- T	<b>8</b> 8	# #	8	ei M	<b>3</b>	8	- 8 #		ન ક જ ક	; <del>-</del>	* ₹	2	33 :	3 S	z z			÷	: 8: :	eri i	~i ^	•			=======================================	6	36 6.	9.	તાં જી	25.	rri Se	*
14	16.	15.	=	# : <b>#</b> :		=	5.	12.	51	.2i	51	=======================================	6	6	6	<u>=</u>	=======================================		± :	≃ °	ri o	* 4		9		21:				11.11		실 :					6		12.1	14.0	17.6	12.	19.	=	=
¥	9		•			-	-	•	•	-	-	-	-	3	-	-	-	3	3	3 3					3	3			<b>!</b> -	3	3	3:					3		9.6	•	-	-	-	-	
*		=	-			3	=	3	3	3		3	9.6	3	-	3	-	3		3 6			-	-	9.3	9				3	3	3					-		-		3	<b>3</b>	<b>3</b>	3	9
M M M	98.2	99.00	38.5		8	100	188	100.0	180.0	186.	18.0	100	38 38	86	39. B	8; 8;	20. 20.	<b>8</b>	8 i	F 8	6 8	r s	8	88.58	99.5	<b>8</b> 8	F 8	8 8			E	8				8	86	98.38	99.38	<b>32</b> .38	99.80	3	<b>3</b> 7	26 37	98.56
¥	3	-	<b>a</b>			=	=		=	-	9	-	<b>₩</b>	4		=	-	3		8 8			-	3	=	2 2			8	=	3	3 3				3	8	9. 10	3	3	3	3	3	3	33
3	16.5	=======================================	_	19.2		-	-	-	-					•		. X	39.0	46.3	j.	2 0			_		_	19.2			25.6	23.8	32.6	នូវ	<b>d</b> 8	e e	2	33.1	25.3	37.7	39.5	40.6	45.5	24.2	¥ ;	Si Si	27.5
3	512888.	516888.	536000	200	53/200	536808.	54888	545680.	258488	25528	25,0000	264888	548686.	269688.	574486.	5792BB.	564999.	2888 <b>8</b>	1976	2455 BB	250.00	492948	35528	587298.8	512000.0	516888.0	Total Control	3312B.	33600E.	540000.0	545686.	56000		.K.0000	564.000	569600.	574488.8	579288.8	584888.8	588899.	593600.0	564888.	298488	26.9680.	574488.8
3	585488.8	586488.8	535200.0	Section .	585486	586498.8	586488.8	586488.8	586488.8	506400.0	586488.8	586499.8	•		•	•			-	75200 A								501680.0	-		•	-		Salkan a	2017			501600.0	581688.8		_	-			535280.0
(gab)	80.873 5	M. R23 S	66.619 5	20. //C 20			36.569 50	M. 519 St	<b>6.</b> 468 51	36.418 50	367 54	98.316.51	<b>16.</b> 568 50	30.266 50			7				20.01	81.076 58	88.416 53	F. 924 58	96. 673 58			M. 671 50	98.628 58	90.578 58	Se. 519 Se	365 53	28. 406 JB	26. 410 J	217 50	BB. 256 58	88.215 58	86, 165 58	88, 114, 58	88. 863 58	86.913 56	88.314 53		88.264 5X	88.213.53
_				464 15	_	_	_	_	_	_	_	_	~	_	_		_			31.634	_			_	_	-			-	_	_		_	31.650.00				_							31.952 88
(ded)	-	~	m i	ñ =																					_		_																		
		3	3 3	3	3	3	3	3	3	3	3	3	₹.	₹ :	₫ :	<b>3</b> (	•	-			•		•	•	•	•	è	2	<u>a</u>	3	<b>a</b> :	3 2		-		- 2	-	3	3	₹.	₹ :	₹ :	₹ 3	≰.	<b>æ</b>
(sq. km) (deg	23,646	_		10291 C3. MA		_						_						15.24 23.148 15.30 23 23.048		163 C3.076		_				H2333 23.648	FESSY CO.			H2338 23.040	H2339 23.04	H234 23.048							H2347 23.848		H2349 23. 848		H2538 25.848	<b>\$</b>	23.040

100012	Scount					8	3	8	7:	1.38	=	=	8	=:	8.	1.38	3	주 신	8 M	<b>3</b>	3	7 S	R 8	R S	2 2	1 0	i a				9	M.	<b>8</b> 7	3	3 6	R 8	8	=	8	= :	用: 二:	3 8	7	<b>:</b> :	: <b>3</b>	6.3	7.88	<b>3</b>
TITON	Acount		8 :				8	#	5.68	9.10	A. 70	7.88	24	87 vs	4.10	74	# #	<b>4</b> . 10	<b>8</b>	<b>8</b>	9	<b>3</b> 3	R S	<b>R</b> :	<b>2</b> 6	R	9 <b>8</b>	3	7	3	2	8	2.70	4.68	8 8	R M	9.10	A. 68	7.98	8	g vi	# 1 # 1	8 8	RE	1 To		5	
STALIND I	Acount		2 :				8	9.6	3	6.00	8	=	*	25.1	1.70	8:	2.	1.78	1.5	8	<b>2</b>	= :	2 2		3 8	R	8 8					2.8	<b>6</b> .28	3	3 :		8	1.15	1.2	7 :	3	3 5	2 2		! =	=	=======================================	=
BUTILE ST	Acount		2 :					=	2	8		8	2		2	3	9	<b>1</b> .28	20	=	3	<b>8</b>	2									3	8	2	2 3			8	3	2	3	2 2		7 5	! <b>#</b>		=	=
	¥		2 :	2 :				8	8	2		8		3	3	9.10	0.10	123	25.	=	3	8	8	2	E :						Į	3	=	<b>8</b>	2 :			=	3	8	=======================================	= ;			: 5	8	=	<u>.</u>
SPHET NO	Moount		3	2				8		8				8	8	8	2	= 1	=	=	=	2	=		2 2		8 1					3	=	2	8 2		Į	8	8	2	8	<b>3</b> 1					2	=
K, FLDSP P. FLDSP HYMING PREPART NOW?	Scount 1		<b>8</b>	3 1	R :		3	3	2.5	3	¥ 7	2 2	8	2	3		3.60	3.56	3.30	82.5	3.20	<b>8</b> %	7	7	3 :	7 : N	3 3 ~	8 3	8 = 4 ~	2 10		2 E	4.20	4.78	2	7.5	2.4	8.4	4.8	7	8.4	<b>3</b> 5	9 7	# 5 # 6	8 =	3	<b>8</b>	4.78
WH dSQT	Scount 1		3.60	2 :	<b>,</b>	8 1	8 8	1 3			8		2	i in	8	M.	39.	25.4	7.	3.00	4.2	<b>9</b> .	= -	4· 10	8		3 i	7 :	2 E	8 5	3 5	3	4.60	4.9	8 :	7		3. 28 3.	3.28	3.78	2 ·	3 3	<b>₹</b>	2 2	R =	2	8	÷.
LIGP P.F	Scount 1		8	_		3 3		_	3	: #F	3		2 2	3		8		2.1	1.50		9:1	8.	8	8	3	# :	<b>8</b> 5	3 3	3 :		3	2 S.	9	<b>8</b> .28	0.2	8 2		3,60	3.60	2.3	2.30	8 2	<b>3</b> 3	8 3	7 T	<u> </u>	8.3	<b>.</b>
			=	8	= :	2 2		8	3	_				_	1 3		8	8	=	3	99.10	25	27.40	27.38	2.38	2	<b>用</b> :	R :	2 1		2 4		19.70	19.20	13.28 13.28	R S		87.38	87.30	87.8	99.68	86.98	8 3			8 2	B. 45	37.88
CHEER IS THEN ID WITE IN MITE I'M MITE HE WITE HE LINE GARGEON GLIBETT	the (a) found		8		<b>8</b>		3 1	3 5	1	_		<b>.</b> .	, F	2 8	12	8	3	3	3	S 87	_	_	_		2	_	_	_	<b>3</b> :			17.10	_	35.20 8	_	3 3				_	2	用:	# 1		2 8	8.8	3	3
OTS OVE	# (E)		用票	2	<b>R</b> :	# X	3	•			1	-		_	2 3					_									3 1	B	2 1	1 2					2 1						3		10 1		1 38	2
10C 10C.	(E)		1				8 1	8 8		_						77		2.10 -68.70					本 第三	.80 -185.28	•		25 PE 26		• 9	<b>8</b> 2			_		8	_				_	_	5.28 -5	神神	_	2- 2-		.89-18	
INC 18LB	3		M 3			•		-				8 8	Ŗ #	2 3	3 8	3 5	A. 10			15.4 W		_			_		20					5. 48. 31 5. 48. 31						1	3	8	3	8	3	3 :	2 1	B #		8
10 E	3		0.60	-		8:					1 ·	4 4 R 1	, . R 1	1 4 2 2	d v	1 <			=	27	16.	<b>ದ</b>	# =	# =	Ki Ri	<b>3</b>	<b>2</b>	2	<b>3</b> :		8 1			=	2	a) :	2 5	3 2	1	3	=	8	8	전 전 :	<b>3</b>	3 M	X  	38
EN 10 M	3		3	3	3	-														3	3	2	3	3	3	<u>-</u>	4	<b>3</b>	<b>3</b> :	3 i	e e			2	20 00					2 8	8	2	2	m 用:	<b>3</b> :		1 3	S S
OUT B M			-		用だる		4	3 8			7.1.	7 0	, , , , , , , , , , , , , , , , , , ,					_		7.38	-	7.80		_	_		B B.10		18.68				-			19.45					76 3.	រក - 3	_	<b>*</b>	si	å ~	;	10 12
OIGH	d		15.1	15.46	14.38	12.70	E 10.			6 0										4	10.6	13.70	17.1	16.9	8 21.38	9.6	9.60	14.	17.98	7.7	# 2 2 4	2		3.6	6	9.0	6 6 8 9				16.78	19.69	=======================================	10.	= : = :		: :: : ::	ම
20 6		1	-		7	3								1					ŀ	F	2	3	3	3	-	3	3	3	7	3	3	3 :			3	-	3			3		3	•	•	2 :	2 1		; <del>=</del>
110		•	9.0	97.0	3	7	7 :										1	1	ŧ	ŧ		3	3		_	3	_	2.30								•	-					3	-	9.0	2	2 1	;	3
Sept.		- 1	3.6	3.5	33.	8.38	<b>3</b>	87 8 87 8				2	2					Ì	8	8	8	95	8	85.18	39.4	23.12	99. R	25.35	97.78	2 S	33 2	2	i s	8	100	100.0	=					3	100.0	180.0				85
- 1	T TO THE		3	3	3	=	3	2	2		=	3	3	2 3	2						ŧ	ł		-	-	3	<b>™</b>	M -	17	3	3			ŧ	3	-	3				3	2	5		-	<b>.</b>		1.0
100	1		12.5			_	_		•	•	_	ි ස්	-	•	<b>1</b>			7 7	X	į p	5	8	4	13			•	6.7	_		_	_	4 =			-	•		d a			A P	•	1.0 36.	37.	e :	* 4	<b>2</b>
- 1	3		497/6#B	2.5	507200.	512000.	516.000	PIGE.	25.48	27308	Salam.	53688B.	7,460 E	54564	SA PARE	200		TO AGE			7.00		I	20.5	29648	38888	593640	46666	49288L	497686.	382488.	587288.	, 120 PM	316.00	221640	1 525 ABB.	Salan.	135.000	7,525,00		200				8 574488.		584888.	593600.
			ASSAM.		1.924 496888.B	96.088. 0	49688.8	49688.	495888.8	, ite sasen.	671 4968BL	49688.	578 496888. I	1.519 496888. I	1. 469 4968 <b>48.</b> (	418 496800.	12/ 13/20 E	31/4950	LCbb 4350m.	1. Clb 42000.	165 496.04	115 495.000	KA 496.940	A4564	495.888	1.664 535298.	33528	1, 126 492000.	45288B.	492888.	4923000.	. 924 492 <b>888.</b>	2. 509 D.C.	23 400	772 492	1.722 492000.	. 671 49200B.	. 621 492000.	27 45Km	A69 A89	A18 49288	. 364 492000.	.317 492889.0	1.267 492000.	6.216 492000.	90.165 492000.0	96, 115 492006.0	58. 814 452866.
			A	88. 975 49588B.	126	<b>88.873 496888.</b>		DB. 772 4	<b>20.</b> 725 4	23 .	11.671	100 TES	ST. 578	<b>86.</b> 519	89.469	80.418	197	200		1	1	1			79, 963, 496.88	9	90.00	81.126	81.876 49280	81. 825 49280	88.975 4928	8		P 823	A 772	221.725	179.00	<b>88.</b> 621	76.37	A A69	1	18.36	317	<b>88.</b> 267	88.216	99. 165	CII .98	86.9
	LATINDE LOGINDE	(dead)	21.688	3	31.686	31.686	31.688	31.600	31.600	31.85	31.686	31.607	31.607	31.607	31.607	31.607	999	31.546	4 3	25. P. S.	2 2	20.12	3	3	31.64	31.951	30	31.565	31.565	31.565	31.565	31.565			7	31.564	31.564	31.564	# S		2 2 2	31,563	31.563	31.563	31.562	31.562		31.361
	5	SQ. KE	A44 50	_	_	23.040	_	23.040	<b>84</b> %	23.040	23.52	23.04	23.040	23.040	23. PM	23. PE	23.	77	7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.			ja	200	22	7	23.	3	4	28, 973	23.040	23.040	23.040	<b>1</b> 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3			23.0	23.040	23.04	# S	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3 2			23.	23.84	23. 84	# # # #	<b>3</b>
	BLDCXID AREA	٥	ניייייייייייייייייייייייייייייייייייייי						_		_									_	2000								H2416	H2417	HE418	H2419	24.2	HOACE CO.C.	12421	12423	15454	200	12436	12421	HEAEB LOAD	10 PA	15431	H2432	F633	H2434	H2435	H2437
1	<b>7</b>		1 3	2 3	±	. <u>भ</u>	보	뽀	보	보	뽀	꺞	Í	뽀	포	of .	*	<b>z</b> :	<b>z</b> :	= :	= 1	6 3	= 3	= 3	- 2	. 3	. =	2	. =	-	æ	<u></u>		_ =		=	_	-					-	_	_	_		_

Scount	3	2	25	7.	1.38	2	23	88	8.	8	8	=	3	=	*	8	80.7	M	27	39 1	6.38	8,	23	=	3 8	ļ	8 8	2	2	8,	8	<b>3</b> 2	<b>.</b>		8	=	2	3	8	3 1	<b>5</b> (	<b>3</b> 1	e e	2 19	1	: 2	Ą
¥	2		20	3	A	2	8	3	8	2	79.6	2	=	3			88	3	27	9.68	8	9 8	8	<b>9</b>	- ·		7 8	3	3	# # # # # # # # # # # # # # # # # # #	3	<b>.</b>	 R 1		3	3	=	# .	m =	# 1 g :	n .	2 Z	, c	ات ک	1 Wi	5 0	,
	6	2	M	~ ~	M	4	4	4	-6	6	6	oi	6	8.64	7	7.	9	7.		9	.9	<u>6</u>	<u>م</u>	6	. E	4	e d	1	4	4	6	of (	ri e		-	9.6	<u>.</u>	-i	-d	<b>a</b>	, i	× 6	<i>i</i> =	6 0	9	å a	,
	1	ŀ	ਲ ਵ	M 4	3	9	9	6.9	4		1.0	=	=======================================	1.2 1.2	₩.	7:	₹.	<b>™</b> :	1.2	-	=	=	=	=	= :				=	===	-	= :			=	=======================================	==	2	<b>7</b>	₹ :	- 1	P 8		] <b>3</b>			,
Krount	85	8	=	8	=	2	8	3	8	3	8	=	3	3	=	0, 10	7	77	-	<b>8</b>	8	=======================================	=	8	3 3	Ļ		3	3	4	3	3 3			3	=	2	= 1	用 : di :	3 8		R B		, S	£ 78		ĺ
7	8.4		=	2	=	=	8	2	2		3	8	3	8	=======================================	<b>6.</b> 10	7	2	3	8.4	=======================================	8	= ;	R :				3	=	=	2	3 1			3	=	3		<b>司</b> :	3 4		R SI		8	2	1	
this (a) this (a) this (a) this (a) this (a) this (a) Younk Scounk Scounk Scounk Scounk Scounk Scounk	3	3	=	2	8	=	=	2	2	=	2	2	=	=	=	8	=	=	=	8	8	8	8 :	3	2 :			=	8	8	<b>3</b> 3	3 :	3	3	8	3	2	3 3	3 1	<b>.</b>	B 8	ļ <b>1</b>		3	2	1	
Acount	8	3	=	7	8,	7	2	<b>7</b>	8	8	8	2	3	8	37	8	3.20	8	8	8	2	2		<b>3</b> (	7 1	2 2	(A)	3.80	:	3.80	= :	8 3	3 2	: 8	2	3	<b>一</b>	<b>.</b> .	7 /	2 1	8 1		3	: A	<b>一</b>	7	
Acount 14	8	<b>3</b>	m m	M	m R	3	*	<b>₹</b>	8	*	3	<del>-</del>	. <del>*</del>	۳ ا	بر ج	ri B	~	~i	~ =	<i>-</i> ;	÷	<del>-</del>	<del>-</del>	<b>.</b>	M ~	_				~	e i	ન તે •			<u>س</u>	M	M •	mi 1	4	w -	;   .			. 4	-	-	
- 1	4	*	<del>ام</del>	M	÷	÷	7	*	4.0	7	3.4	M	۳. س	3	7	4.1	7.7	<b>3</b>	7	7	7	7	7	-	7 7		1 M		4.4	£.3		R S		-	*	÷	7	3 :	# 6	4, 4	3 ~	3 65 3 mi	-	7	<b>*</b>	R.	
A Acount	6.9	2.4		3	₹ .	بت ح	9.5	편 <b>6</b>	<b>8</b>	-	~	ਲ ਅ	뻔	۳. در	<b>≈</b>	7	<u>=</u>	1.	7	2. 2.	-	35	3		7 F		3 3	9.68	7	<b>6</b> .2	3 3	8 8	2 S	3	2	2.	=	8 2	R :		3 7	! =	0.70	3	2	4	
thk (m) thk (m) thk (m) thk (m) thk (m) thk (m) Xcount		91.38	91.60	9.18	77 27	Z Z	<b>3</b>	<b>5</b> 9. <b>6</b> 8	<b>8</b> 3.5	<b>89.10</b>	8.48	67.58	8	86.78	<b>3</b>	<b>8</b> 3.8	<b>8</b>	<b>8</b>	3	<b>8</b> 7.88	8	8. 8	8.7	3 3	7 8 5 9	*	<b>3</b>	25.25	<b>R</b>	2,2	<u>5</u>			<b>19.68</b>	8	<b>8</b> 3. 4	F 6	त्र : इं. :			3 8 6 3	87.78	8.7	89	88.78	90	
th C		38.66	45 13 13 13 13 13 13 13 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15	4.2	20.50	27	33, 10	23 23 23	27.60	æ Æ	23.28	17.88	14.10	13.80	12.80	14.70	16.98	19.10	<b>3</b>	21.78	21.98	2.3	<b>3</b> ;	9 9	2 2 2 2 2 4		3	33.38	8. 8.	<b>2</b>	<b>男</b> :	<b>3 3</b>	3 2	8.5	12.50	8:	3	S :		1 to 10	- To	3 3	35.58	5.5	28.98	8	
节		19.E		<b>3</b>	<b>7</b>	7. 7.	8.5	3	3	51.70	-21.60	12. St	£.28	57.80	39.78	開き	80			2				2 S	3 8 2 4 7	3	8	8	3	Ħ				R	8				8	7 7		3 23			8	8	
9 2	8	8	8	_	8 :	8	8	=	8	8	8		8	2	8	# # # # # # # # # # # # # # # # # # #	<b>4 3</b>	7 8	7	ም =	=	8	8 3	•	7 Y		7	8	3	8	R :	7 3	2	. 3	3	8	3						3.46 -121.90		38 -135.		
9	_	*	3	8		2	<b>1</b>	<b>3</b>	<b>8</b>	.61	19.	8 IA	25.	12.	e; =	<b>2</b>	<u>د</u>	ri Se	mi i	را ج	-i 9	_	તો ત જીવ	é s R 1	d ~			21	±	76	를 : • :	≓ g	j <u>e</u>		.55	<u>~</u>	oi .	o :		, .		5 <del>-</del>	r i	i M	15.30		
3	37.	-	~				 -	7	7	=	2	-	=======================================	- -	4	15.0	=	17.	2.2	ซี่ ซี	×	33	₩.		4 2	4	M	2	7	ત	H .	J -		12.6	16.4	18.4	13.6	6.5		£ K	; =	×	4	43.3	99, 8	92. 4	
	9.0	9	3	<u>.</u>	3	-	-	-	=	=	3	3	3	3	3	3	3	3	3	=	3	3	3 3				7	3	3	3				3	3	8		3 :					8	3	8	4	
th		21.98	ह्र स	27.78	27.16	đ	<b>ಾ</b>	19. S	16.38	16.38	13.38	7.38	3	37	2.6	7	<b>8</b> 7 4	<b>8</b>	3	2	8	70 eri		1		1	8. 8.	27.9	<b>3</b>	정 :	3 5	# 8 4 ±		3	<b>3</b>	3	2	<b>3</b> 5		4 5	1 5	8	19.00	KI KI		200	
	22.38	16.78		17.48	8 :		3	8	80 6	9.6	9. <b>8</b>	8.6	10.10	M •	10 S	2 4	19.61	<b>8</b> :	2	16.	19. 10	6 :		3 3	4 4	3 B	M 1	11.68	2	2 :	R :	2 2 ri	3	8.3	9.60	<b>7</b> 1	<b>R</b> :	8 3		2 8		8 6	9.70	92	£.78	91	
× ×	6.28	<b>9</b> . W	=	-	= :		2	3	2	=	=	=	3	=	3	8	3	3	8 :		3	=	3 8	8	8 9	8	=	3	=	3 :		1		3	=	- 8 :		3 3			1 2	1 2	= -		7 PT	7	
100 M	0.66	1.55	<b>3</b> :	3	<b>a</b> :	= :	2	2	8	8	=	8	8	8	8	8	=	8 :	<b>8</b> :	E :	2	= :	<b>7</b> 8	RS	2 3	A	8	8	8:	8 :				=	8	8 :		8 8	8 8		2 =		0.30	8	8:1	9	֡
M			3	7	ه ا	<b>R</b> :	2 :	<b>:</b>	3	=	-i 2	=	=	2	3	2	=	2 :	2 :	R :	<b>3</b>	- 	8 1			8	_	2	न्तं । ऋ :	4 :				=	<u>.</u>	ei :					; ed t 91		6.0	_		200	
*	98.38	<u>s</u>	86 : 12 :	gi E	gi s me s		<u>.</u>		<u> </u>	<u>=</u>		<u>=</u>	<b>≅</b>	<b>.</b>	<u>.</u>	• ਵ	= = =			ei i	<b>S</b>	8 8	F 8		i si	8	99.78	39.1	<b>S</b> i	<b>S</b> :				<u>=</u>	<u>=</u>					8	8	8	85	85	8	7	
*	3	3	3	3	3 3	3	3	-	3	3	3	3	3	3	3	3	3	3 :	3		3	3 :				3	2	3	3	3 :			3	3	3				1			-	-	-	<u>.</u>		
3	Ĭ	9.0	-		•				•	-	_	_	_	•	•	#	•			_			* 4		12.4	15.0	17.2	19.2	20.2	<b>T</b>	3 8	1 1	27.0	7	8.5	3.3	31	d a	2	2 2	3	7	42.6	44.6	46.6	9	
3	396488.	45288B. (	497688				216.000	2		Sizan.	S35.000.	54888.	545688.	12010E	TESTE .		25.488B.	269686	3/4	7/2		2000m.	73.55 MB.	480	1888 1888	497648.	<b>382488.</b> [	3872B.	512000.0	216.00	200	2312B	335.000	54888.4	545680.		TO COMP		200,000	57448	179	<b>58</b> 4 <b>88</b> .	58888.0	593600.0	598486.0	483200.0	
9	492000.0	487288.0	487200.0	48/200	40/200.	40/08.	4872	48/CM.				•	•	-									447200		424											-					-	-		_	482466.0 5	477688.8 4	
(Beg)	963 49	81.076 48	8. 625 8. 625 8. 625			DF 6/8				_	-		<b>3</b>	4.469 48		20 AS	90.318 48	26.267	M. 216 48		M. 115 4872M.	7	20 CCA AB	1 1 X 4 K		BI. 625 48	30.975 4&	젌	8.874 4&		# 722 AE2AM	m. 672 445	9 (55) 48:	578 462	528 482488.	30, 469 482480.0	204 414	8. 355 452486. 8 318 462486	A SK7 ARPAN	0.217 482486.	98 166 482	BB. 116 482	88.865 482	BB. 015 482	79.964 482	81.177 477	
				_	-		_	_ `	_	-	_	<b>15</b>	_	_		_		_	~ -	•	~ .	_		_	_	_	8	Ħ	~	<b>5</b> 3	8 3	_		Ħ			•	<b>a</b>		, 40	90						
										_		_				_						51.316									21.478					31.477		31.477								31.435	
9	ส	성	<b>3</b> 3	3	25.5	3			<b>1</b>	23.040	2. 2.	<b>₹</b>	₹ 7.	23. E	<b>3</b>	3	<b>3</b>	i a	1	3 7	1 2	1 3	3 %	15 4	3	23.04	2, 18	23.5	ತ : ನ :		1 7	1 a	23.04	<b>₹</b>	23. W	a a		i z	7	1 2	23, 84	23.	23.040	23. <b>S</b>	23. PM	5, 152	
	F643H	1246	15461	Ž.	245	10,00	TO ST	HC400	H2467	H2468	F2469	F478	12471	12472	H2473	¥44	1247	124/6	11647	56.47	247	10,00	H2482	2	<b>1</b>	7852H	HE586	<b>120</b>	1558 1558 1558 1558 1558 1558 1558 1558		2	200	E2513	H2214	125	90	100			125	22	253	H2524	22	F258	H2546	

South	ĺ	3	8		8	8	8	<b>=</b>	<b>.</b>	<b>:</b>	<b>3</b>	8	s.	<b>3</b> :		2	R :	8 8	R	<b>2</b> 2	8 8	<b>3</b> 2	<b>4</b> 5	2 2	2 1	3 3		3 =	2 8	8	8	8	2	2 2		=	=	1.10	3 :	8 S		3 3	8		3.78	8.3	2.88	8	
at Menual		-			•	-	•	_	_	_	_	_	_				-														=	2	<b>#</b> :	2 1	1 1		=	8	3 1	<b>8</b> :	: 5	3 3	! =	3	3	7	3	8	
4	(a) this (a) this (a) this (a) Scount	7.80	7.30	7.10	7.38	P.	85	9.6	8	16.	9.	100	5	86		<b>7</b>		_				7 .		?		,		_	_	25.4		-	ei ;			=	10.1	9.0	of 1	of 0	n 0					-di	_	28 9.	
	ACOUNT.	3	1.2	7.	3.	2.1	用:	1.10	=	=	8		8.	=	=	==	- 1						-	-	3		-			2	3	2.	=	3 :		=	=	=								=	-	1.1	
	MCOUNT.	E		3			2	8	2	3	8	3	8	3	3	<b>6</b> 10	7	3	3	R 8	R 1	8	3	3	3 3						3	3	4	3 3	ł	-	=	3	-	<b>明</b> 5	3 4				•	m	3	•	
	XCOUNG	:	ŀ	3	2	=	2	3	2	=	=	=	3	8	3	2	<b>8</b>	9	8	# :	<b>R</b>	8	3	3	2 1						3	3	3	3 3			3	3	<b>6.</b> 10	# S	3 8	8 8			9.0	# · ·	-	8	
	ACOUNT.		ŀ	3	3	3	2	=	2	3	8	2	2	=	=	=	2	3	2	2	2	2	3	3	3					Į	3	3	3	3 3		3	3	3	3	2 2						3	8		
	COMING		1 2		3.2	200	2.28	2.00	88.2	8	3	3.38	3.28	===	3.28	8F 16	3.50	8	2	4.18	80 -	<b>8</b>	<b>4.</b> 28	Ħ	۳ ا	8 3	# 2 시 4	R A	2 7		7	3.	2.10	3 2	, i	8 5 ml	8	3.10	# #	<b>8</b> 8	<b>7</b> 6	8 8 4 r	R 8			7		28	
AL LON	Count	8	8	3		8					85 %		- 10				3.00	##	*	3.68	28	2	<b>.</b> .	 20.	2	用: ri	2 : 2 :		8 S	2 p	3 = M	200	20	20 H		2 2	3	<b>4.</b> IS	3.78	育: mi.	2 t	9 5	8 8	R 8		· 两	8. M	13 N	
	Sound N				2		_			_		_		3	2	8.					8	3	138	8	2	3	<b>3</b> !	R :	8 5	2 2		7	8 4	<b>8</b> :	<b>3</b> 8		3	2	8.	8:	8 i	2 2	97.1			8	1.28	1.70	
CHATERN PLICES UP.NICE NO.NICE LINICE MA.BUIS CONSIGN LINELS PARTICE PARTICE PARTIES PARTIES FOR THE	Durat M	1 8	: - : :			2	_		3	2	3	2	8	8	2	3	3	_	=	=	2	8	=	_	_				F 18			8	25.78	91.30	<b>?</b> :			9. 10	8	=	2	<b>3</b> :	2 5			87. 18	=	8	}
	9	ā	i			<u> </u>	28 93,10	_	_		.69		. B.	_	_	_	10 49.		_	_	_	 59			49.30 91		-								_		-	1 2	3	E 27.11	<b>*</b>	8 :	R 2	8 8	2 2		3	2.12	:
S CANDE	3	1	į :	4 4	7	3	Ø	Ħ	i xe	8	<u>4</u>	2	5		=	2:1	13.10					43.10		_			-			-				•				_	'					= :	2 ¥	2 9	R 3		}
		1		į q		į	8	Ģ				_			Ė	_		-73.64			0 -112.50	1.25-1	0 -133.30			_	_							•					\$ .69 \$	2					3 :	- 1- 25 - 1- 25 - 1- 25	,	- 14- - 14-	Ŗ
					2	1	Į.	17.3				4	2	7.6		_	_		_	12.10	10.68	9.10	_	_	_				_				16.3	_	_	14.28		é =	16.	6	Ħ	켮	_	₫ :	<b>R</b>	i s			
<b>6</b>	the (	1	7 E		1 .	. ·	7	7	i ~	4 4	1	4	9	2	2	8	5	8	K K	<b>87.78</b>	E M	39.10	河河	31.4	7.98	11.0	11.28	e e	3		3 2					27.50	_		39.65	_	21.78	24.10	Zi Zi		7. A		ė =		4
JP. MICE	thk (a)	10.		9 3							7							3	3	3	3	4	3	3	3	=		8	2		10 1 Ni o	1 ~	2	1.2	3	# 2	8 5	\$ 6 •		3	-	3	-	-				4	
	thi (a) thi (a)		<b>≘</b> ;			R S	1 1			4 9	16.18	‡ 1		3	8	R 2	<b>M</b>	1	F. 10	10.45	21 21	21.30	8	27	25	N S	<b>8</b> .4	阿斯	18 18 18	R I	<b>3</b> 3	# <b>#</b>	1	3	in in	2	3 3	2 2		33	\$ ·\$	9.5	1.9	15,98	8	른 3 원 2	i X	g k	
INTERN C	thk (e)		2	2 1	# T				8 2	7 A	2 5	<b>3</b> :			t g	1 7	2 5		13.70	16.70	19.70	2	8	7	15.28	15.00	16.10	15.28	13.58	12.2	= ; = :	R 2			=======================================	3			3	8	10.50	12.60	16.10	28.88	Xi Xi	R :	# F		15. C
D.AY D	×		<b>8</b>	2 :														Ę		3	=			F	7.7	3	6.10	£ 10	3	3	3				3	3	3 3				3	3	8	-	. :	<b>8</b>	8 2	7 :	
SILT	14		7		8	2 2														F	P				2.3	3	8	914	=	=	3				=	=	3				3	3	=	82.4		3	R 5	3 t	7
5 965	_			2	8	<b>8</b> 1			8 3	8 :	8 :	8 3		2 2 2 3					8	8	3	3 3			3		93.66	28.68	33.53	20.50	8	2 1 2 1		1 2	8.8	8.8	8	8 1		1 2	8.8	89.80	99.88 89.88	99.68	99.70	99.38	% S	97.80	<b>3</b>
GROWEL SK		- 1	<b>8</b>	8	8 8	8 ; 8 ;			2 :	2	2 :	2		2:														3	33	8.6	. 88	21			2	8	3	2	B 1		8	8	8	8.8	8.8	8	2 :	8	8
DEPTH GS		- 1	13.3	14.9	16.6	16.3	6.61	•	ි ස්	24.5		27.7	7 7	-		5.5	7.5	9 64			7 67			2 5	9 4	4 4	13.7	9	16.2	17.5	18.8	مر جو ج	i a	: ×	1 187	23.0	8.8	9.6	d :	e o	1 9	41.6	42.6	43.6	4.6	1.9	48.5		12.6
ı			•		•	•	_	•	•	•	•	-	•	•		•	•	•				•							-					221288 B			545580.0	55848B.8	200208.0	SCARGO B	54.96.88 B	27448	579286.0	584898.0	588589.8	593688.8	596488.8	483280.0	488999.0
TH EAST			1.0 492800		•	•	•	•	•				•	•	•	•		20.00		•			8. 8. 3000m				•		-			-													-				
INF MIRTH		- 1	5 47768B.	5 477688.8	\$ 477600.							1 477648.			47768	9 477688	9 477688.	4//bm.	47.75 PM	AND AND AND	ADLIA I	10 4//pag	4/Ver	13 4//ban	7. 55. 47/6	4/20m	81. 125 4/28	A 775	975 472800		M. 674 472568	R23 472888	DB. 773 4725000.	22 472888 22 472888	21 472940	571 472808	528 172888	78 472968.	80.419 472560.0	369 4/2868.8	X 8 472988 8	217 472688	67 472888.	88.117 472888.	166 4728	88.816 4728	79.965 4728		126 468888.
SOUTHWELLINGSTON	(den)	- 1		_	20.97	~	-	Ź	20	3	ź	-	-5	3	2	40	<b>3</b> :			_				_		_				É	1				0//60	28		E.		<b>z</b> i 1	g a		2						
STITUTE	) (des)	- 1	31.435	31.435	31.435	31.433	31.435	31.435	31.435	31.434	31.434	31.434	31.434	31. 434	31.434	31.433	31.433	31.455									100							31.391							21.53							Ħ	
			23.040	23.04	23.04	₩.i	23.04	<b>₹</b>	23.040	<b>ま</b> だ	23.64	23.040	23.040	23.040	<b>34</b> f2	<b>₹</b>	23.0	₹ 7	3 7 7	25.5	1	2	<b>₹</b>	7	# S	12.636		ja	27 848	23.848	23.040	23. <b>BM</b>	E E	2 S	2 2	23.648	23.048	23. BM	23.88	23.84	2 2	200	22.00	3 2	23.0	33.	23.64	18.85	23.2
THE DESCRIPTION AND ADDED			NSW.						H2554	F255	H2556	F2557	F250	653	E256	1952	12562	250	Š	3	900	1200	K2564	50	F22	C.	E S	X S	200	9	£036	H2597	200 200 200 200 200 200 200 200 200 200	H2599	10 E	2	H26A3	H2684	12685	12686	9		LOX 1		19615	H2613	<b>₩</b>	H2634	H2635
1º	4	1	- 2	. #	Ŧ	Ŧ	×	÷	=	=	_	-		_	_	_	_	_					-	_		- 1	•																						

1.52   1.53   1.53   1.54   1.54   1.54   1.54   1.54   1.54   1.55	THE CHEST THROUGH IN THE THROUGH THE THROUGH THE THROUGH THE THROUGH T		100501UP.1	in (a) this	CANTERN PLICISIN UP.NICC TO.NICC LENICO WE BOTH DAY OF THE DAY P. FLICS HANNING PASHET NOWS THE (a) the (b) th			LINETZ L	(RUBD)	FLDGP H	VMINE	HESPET.	1 1	BUTILE ST	STAURD T	TITON 2	MCDII 2
6.25         1.32         1.44         1.45 <th< th=""><th>21 348 Mt #70 Areas a second a second as a second</th><th>1</th><th></th><th></th><th></th><th></th><th></th><th>ACOUR.</th><th>KORN</th><th>NCOMME.</th><th>Mount</th><th>*Count</th><th>Scount</th><th>Acount</th><th>Acount</th><th>Scount</th><th>Acount</th></th<>	21 348 Mt #70 Areas a second a second as a second	1						ACOUR.	KORN	NCOMME.	Mount	*Count	Scount	Acount	Acount	Scount	Acount
A.	ALLES ACADEM A ATTACAGE STATE OF THE PASS OF THE STATE OF	- W B	of d 用 g	선 (	3:	8		91.28	1.88	3.10	2.00	3	2	_	1.60	P.40	<b>8</b>
1.39	31.348 50.975 460000.0 382400.0 16.2 0.00 59.50 p.10 p.m. 12.	a 4	i d	ri -	3 5		# X	2 : S	<b>?</b> !	9 5 m	8 d	3	2	_	8:	A. 28	1:10
7.56   2.39   2.40   1.53   -7.43   4.50   5.10   5.10   1.50   1.50   4.50   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   5.10   4.50   1.50   4.50   1.50   4.50   1.50   4.50   1.50   4.50	86.924 46888.8 33728.8 17.4 6.88 99.98 6.88 6.88	*		M	! =		_	1 m	9	8 8				_	<b>5</b> 5		= :
2.77 5.50 5.50 1.50 1.60 -7.20 6.50 5.50 6.70 1.50 1.50 1.50 6.50 6.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1	21.340 dat. 0/4 45000.0 31200.0 18.5 0.00 100.0 0.00		d	M 8	8			¥. 16	*	A 10			3		2	9	
15.39	THE SHIP OF DESCRIPTION OF THE SHIP OF THE		ed i	男:	10.00	-	8	3, 5	<b>8</b> 7	3.10	1. W	=	=	3	8	100	8
1.28	AND SILVER AND THE PROPERTY OF THE PARTY OF	_	rå .	8	3	-	8	<b>8</b>	2		8:	8	=	8	10.	2.6	8.3
1, 20   1, 20   1, 1, 20   -6, 20   1, 20   -7		R 8	4 6	B :	<b>M</b>	<b>8</b> :	8	8	-:		2.10	=	=	2			8.4
3.73 1.20 1.20 1.20 1.20 -6.60 1.20 9.20 1.30 4.30 2.00 6.00 6.00 6.00 1.00 1.00 1.00 1.20 1.20 1.20 1.20 1	PARTITION OF THE PROPERTY OF THE PARTITION OF THE PARTITI					8 :		3 :	<b>7</b>	<b>8</b>	ار 14	=	=	2	2	8.0	8:
1.38   4.78   2.13   1.124   -6.75   1.139   2.14   1.39   2.29   2.29   2.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29   1.29   2.29	P40 31.347 00.571 45000.0 54000.0 M.S. 0.00 10.00 0.00				2 2	R 1	R /	8 S	<b>7</b>	用	3	3	8	8	8.	5.8	= :
18   18   18   18   18   18   18   18	We 31.347 BR.121 468686.0 545586.0 32.1 8.80 186.80 8.80 8.80					R 1	Red				2	2	2		8	8	==
1.00   6.00   6.00   7.00	31.347 JB. 470 453000.0 350400.0 34.0 0.00 100.00 0.00 0.00				1 2	-			# # -: -:		3 /			_	2 :	2	=
1.13 6.23 22.39 22.39 12.39 12.39 23.41 12	31.347 Mt.428 458886.8 TTZ98.8 JS.9 8.88 186.88 8.88 8.88 8.								2 2		2 2				- R :		3
4.39 6.29 6.33 6.20 6.32 9.11 1.39 3.10 3.10 3.10 1.39 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.30	31.347 86.369 46888.8 55888.8 37.8 6.48 186.88 6.80 6.80					1			8 8		R 2			_	8 :	R	=
1.50   1.60   1.50	31.346 80.319 464000.0 254800.0 39.6 0.00 100.00 0.00 p.m.				3	1 8	_		R S		R :				8	<b>3</b>	3.
14.00   4.00   12.00	31.346 80.258 460000.0 355500.0 40.7 0.00 100.00 0.00 0.00			ā	3 8	R 8			R S		R /			_	2	9. Z	25
11.39	H4 31.346 BG.218 468000.0 574480.0 41.9 0.08 99.90 0.10 0.00	_		8	1	t g					2 :			_	2	3	2
17.50   1.00   2.30   2.30   1.00   2.30	31.345 86.167 468000.0 579200.0 43.0 0.00 59.70 0.20 0.10	. –			3 8	. 5					<b>3</b> 1		2		2	<b>8</b>	8
17.00   4.00   33.00   27.44 - 122.00   33.00   4	31.345 80.117 468000.0 584000.0 44.2 0.00 99.60 0.30 0.10 20				2 2	2 1	_				<b>3</b>	2	8		2	8	7:0
25.56	31.345 Mt. 666 458884.0 588884.0 45.2 0.00 49.64 0.34 0.10	-	4			R S	_				8	2	2			<b>8</b> 4	4.6
25.96 6.89 25.33 3.40 -17.24 35.53 35.53 45.30 45.30 45.30 45.30 1.30 4.30 4.30 4.30 4.30 4.30 4.30 4.30 4	50.016 4500m.0 5350m.0 45.2 4.24 52.00 - 12 4.24	- •			ZI- 8-12	R :	_				8.	3	<b>1</b> .68		_	7.38	82
35.50	31.34 75.96 464mm.0 594mm.0 44.2 m.m. q. q. m. z.	_	6 4			R :	_				<b>8</b>	2	2			200	2.3
3.5.9	31.365 81.177 462394.0 442394.0 16.5 A.10 96.10 1.60 A.20	-	4								2:	2	6.28				1.8
4.5.3 6.00 6.10 11.39 -71.20 11.30 11.70 11.30 2.10 6.70 6.00 6.00 6.00 6.00 1.50 11.50 71.30 11.70 11.30 2.10 2.30 6.00 6.00 6.00 6.00 11.50 71.30 11.70 71.30 2.10 2.30 6.00 6.00 6.00 6.00 1.50 11.50 71.30 11.70 71.30 2.10 2.30 6.00 6.00 6.00 1.50 11.50 6.10 11.50 71.30 11.70 71.30 2.10 2.30 6.00 6.00 6.00 1.50 6.10 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 11.50 6.10 6.10 11.50 6.10 11.50 6.10 6.10 11.50 6.10 11.50 6.10 6.10 11.50 6.10 6.10 6.10 11.50 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.1	31.305 81.105 4529a.8 488aa.8 13.2 a.m. 99.9s a.m. s.m.	5 X										2	2	_			2.3
4.50	31.911 86.873 539480.8 512980.8 A. S. 2.68 92.78 A. 78 A. M.	7	R	_			•				3	2	2				#:
4.50 6.30 6.30 6.30 6.30 75.30 55.40 92.30 1.20 3.30 1.70 6.30 6.30 6.30 1.30 6.30 6.30 1.30 6.30 1.30 6.30 1.30 6.30 1.30 6.30 6.30 1.30 6.30 6.30 6.30 6.30 6.30 6.30 6.30 6	31.365 81.676 45294.0 49294.0 14.5 8.89 99.70 8.30 A.M.	,									3	7	=	_			=======================================
4.08 6.49 1.08 1.40 1.40 1.72 5.50 5.50 5.50 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.7	46234.0 497644.0 15.9 4.00 99.00 4.30 4.00		1 8			_					用 i	8 :	3 :				1.16
96         42.38         2.16         2.16         2.16         2.16         2.16         2.17         3.26         3.26         3.26         1.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26         3.26	31.385 88.975 462388.8 542488.8 17.2 8.40 59.98 8.18 8.80												2				# #
37.38 6.39 3.70 6.00 10.	948 31.365 86.924 462396.8 307396.0 18.4 8.80 186.80 8.80 8.80										2			2			=
37.73	31.365 88.874 452398.0 512898.0 19.4 B.M. IM. M. B.M. B.M.				2.5						7		=				8
24.46 5.69 13.90 13.10 14.70 31.10 13.10 1	31.365 86.623 46228.0 316888.0	2 9									<b>7</b>	2 :	3				28
24.46 6.60 3.00 13.10 10.70 -71.30 31.20 11.40 3.30 2.30 0.00 0.00 0.00 1.10 10.00 3.00 1.40 11.20 0.00 0.0	31.345 M.773 452M.0 1216M.0 22.6 0.00 100.00 0.00 0.00					_					7					_	3
16.46   3.20   13.40   14.40   -71.20   31.40   91.50   14.40   2.30   2.30   2.40   4.60   4.60   1.40	H4 31.385 86.723 45258.0 32548.0 24.8 4.00 100.00 6.00	-			1 1											_	3
	31.384 66.672 45296.0 531286.0 27.1 6.00 100.00 6.00 6.00																3
6.88         6.89         2.39         11.69         -23.64         15.39         2.22         4.33         4.39         6.89         1.69         6.89	H4 31.344 80.622 452384.0 536884.0 29.1 6.80 180.80 6.80 6.80 1					-	_										
16 5.59 2.50 16.34 11.16 -66.44 15.79 51.66 1.66 3.50 2.50 6.50 6.50 6.50 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.6	181 31.911 80.822 539490.0 516390.0 10.1 7.20 89.60 3.20 0.00		_												R		
73 3.39 2.29 20.31 11.69 -68.10 16.20 91.70 1.60 3.30 2.30 6.00 6.00 6.00 1.00 1.00 1.00 1.00 2.30 1.70 21.32 14.10 -68.10 12.00 12.00 39.20 1.00 3.30 2.30 6.00 6.00 6.00 1.00 1.00 1.00 1.00 2.30 1.10 21.23 14.10 -68.10 12.00 99.30 1.20 3.30 2.30 6.00 6.10 6.10 1.00 1.00 1.00 1.00 1.0	31.384 80.571 462301.0 546801.0 36.2 \(\times\) 4.00 100.00 0.00 0.00														8 1		2
2.33 1.77 21.23 14.10 -68.00 14.44 91.44 1.00 3.50 2.33 0.00 0.00 0.00 1.00 1.00 1.00 2.33 1.10 21.20 18.20 -68.00 15.00 1.00 3.44 2.00 0.00 0.00 0.00 1.00 1.00 1.00 1.00	31.304 80.521 452300.0 545500.0 31.3 0.00 100.00 0.00 0.00						_								R		
2.33 1.11 21.23 16.29 -66.80 12.00 31.00 1.30 3.30 3.30 6.00 0.00 0.00 1.00 1.00 1.00 1.00 1.0	848 31.384 88.478 452286.8 558486.8 33.1 8.88 198.88 8.88 8.88														B :		<b>.</b>
3.99 0.70 21.10 21.40 -71.70 14.00 34.50 1.59 3.30 3.30 0.00 0.10 0.10 0.10 0.10 0.10	23.040 31.304 06.420 45294.0 SEE206.0 34.9 A.M. IM. M. R.M. A.M. 9.44					1									2		ä
7.59 8.70 21.18 21.40 -71.70 14.80 596.66 1.59 3.30 3.30 8.00 6.10 6.10 1.60 9.59 7.59 8.70 21.40 -71.70 14.80 596.66 1.59 3.30 3.30 8.00 6.30 6.30 1.60 9.50 1.60 9.50 9.60 9.60 9.60 9.60 9.60 9.60 9.60 9.6	11 20 An					R		*			3	3	2		2		=
9.66 7.99 6.44 20.23 25.99 -76.69 17.99 99.69 1.99 3.29 3.39 6.99 6.39 6.39 1.99 9.99 1.99 3.29 3.39 6.99 6.39 6.39 1.99 9.99 1.99 1.20 1.20 3.29 3.39 6.99 6.39 6.39 1.99 9.99 1.89 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20	31 363 66 310 453500 0 055500 0 35.7 0.00 E		_			2	2	3			<b>河</b>	8	0,10		•		3
78 9.60 0.10 19.78 28.40 -79.60 19.78 98.90 1.00 3.20 3.00 0.00 0.30 0.30 1.00 2.40 0.70 0.10 0.30 1.00 0.40 0.70 0.10 0.30 1.00 0.70 0.10 0.30 1.00 0.30 1.00 0.30 0.10 0.30 0.3	SILVER OF SIT PERCENT TENERS. B. SELS. B. CO.	3	_		8	3	8	3			10						3
18.78         6.16         24.78         25.66         -55.46         25.16         91.46         1.56         3.46         2.70         4.78         1.66         2.78         1.66         2.78         1.66         2.79         2.76         1.66         2.79         2.76	51.383 BB. 259 46.238.0 35568.0 40.1 0.00 1	2	9.10	19.70	9	9						E			1	B :	₽ :
11.73 6.89 38.40 23.30 196.20 25.66 95.40 1.80 3.50 2.00 6.00 6.70 6.70 1.80 7.59 1.80 1.70 1.70 1.80 1.70 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.8	23.040 31.382 86.218 463206.8 574486.8 41.7 6.80 99.90 6.18 6.60	38 18.	2	2		•	•	1		3 3						2 :	7
13.40 0.00 33.40 24.70 -1104.10 22.00 025.30 0.65 3.50 3.50 0.00 0.70 0.70 1.00 7.50 1.00 7.50 1.00 7.50 1.00 7.50 1.00 7.50 1.00 0.70 0.70 1.00 7.50 1.00 0.70 0.70 1.00 7.50 1.00 0.70 0.70 1.00 7.50 1.00 0.70 0.70 0.70 1.00 7.50 1.00 0.70 0.70 0.70 1.00 7.50 1.00 0.70 0.70 0.70 0.70 0.70 0.70 0.7	23.848 31.382 88.163 462388.8 579288,8 43.2 6.18 99.78 8.28 8.18				8 8		2 5	1		<b>P</b> :	2	3	2	-		_	=
24 12.50	4 SA4000 0 44 7 A 10	R 5			8 8		3 :	7		3	=	8	2	 			8.
74 5-74 0-100 0-121 0-120 -30-10 12-30 07-40 3.50 2-70 5.40 0-10 0-10 0-10 0-10 0-10 0-10 0-10 0-	THE STATE OF THE PROPERTY OF THE PARTY OF TH	2 :		35.4	2	•	8	- 		8	3	8	17	1.2			=
11.120 N. 00 35.00 25.10 -125.20 43.30 85.50 6.40 4.20 4.00 6.00 6.30 6.30 1.00 6.40 6.20 1.20 1.00 6.40 6.20 1.20 6.40 6.20 1.20 6.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1	21 281 PA MC ACTORN & SERBER A MS O A DA CO CA A CA		<b>-</b>	ni	7	=	<b>.</b>	2	8	2		8	=		8	_	2
6 21.78 0.00 33.40 36.20 -136.20 55.10 56.76 0.60 4.50 4.50 0.00 0.30 0.30 1.00 5.00	Market 10-10-10-10-10-10-10-10-10-10-10-10-10-1	e :	<b>=</b>	ģ	=	S.	馬	3. 3.	7 7.	_		8	97.70	_	8	3	8
	STATE OF THE PROPERTY OF THE STATE OF THE ST	2	<b>.</b>	Z,	R	2	=	. W	¥ 89.	<b>3</b>	,	2	- M.	_	8	8	

Mount Mount	-	8.0	<b>-</b>	Ai -	-	-	•	÷																																						
STALKO TITAN			£8 II.	200		2.88	1	B	8 8	882	88888	888888	888888		****			******																												
Keount Keount			_	_	_	_	_																																							
	2		_	_		. –	_	_																																						
Acount Acount	8		4	<u>.</u>	4	4	4	ď	4	6	<b>.</b>	4 4 4	4 4 4 4								,	,	,			,					******	44444444444444	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		4444444444444	44444444444444	1	444444444444444	1	44444444444444	44444444444444	1	444444444444444	44444444444444	44444444444444	**************************************
Acount N																																														· · · · · · · · · · · · · · · · · · ·
	5		3	8																																										
	1		8 .8		# # # 8							3 2		8 16 18 18 18 18 18 18 18 18 18 18 18 18 18	2 2 2 2 2 2 9 5 9 9 9 9 9 6 9 9 9 9	2 5 5 2 5 6 2 8 6 8 8 6 3 8	3 5 7 2 8 7 3 3 9 4 6 6 6 6 6 3 9	8	3 5 7 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	3 5 7 2 8 7 3 7 3 8 8 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		3 5 5 5 5 6 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7	3 5 7 2 8 7 3 7 8 7 2 7 8 7 3 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8	3 5 7 2 8 7 3 7 8 7 5 7 5 7 5 7 5 7 8 7 8 7 8 7 8 7 8	3 K A 2 B A 3 A 3 A 5 A 5 A 5 A 5 A 5 A 5 A 5 A 5	3 K A 3 B 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	3 K	3 5 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	3 K 3 S 3 S 3 S 3 S 5 K 5 K 5 K 5 K 5 K 5 K 5 K 5 K 5 K 5	3 K 3 S 3 S 3 S 3 S 5 K 5 K 5 K 6 K 6 K 6 K 6 K 6 K 6 K 8 8 8 8 8 8 8	3 K 3 S 3 S 3 S 3 S 3 S 5 S 5 S 5 S 5 S 5 S	3 K 3 S 3 S 3 S 3 S 3 K 5 K 5 K 5 K 5 K 5 K 5 K 5 K 5 K 5 K	3 C S S S S S S S S S S S S S S S S S S	3 K 3 S 3 S 3 S 3 S 5 S 5 S 5 S 5 S 5 S 5 S	3 K 3 S 3 S 3 S 3 S 5 S 5 S 5 S 6 S 5 S 5 S 5 S 5 S 5 S 5	3 K 3 S 8 S 8 S 8 S 8 S 8 S 8 S 8 S 8 S 8 S	3 K 3 S 3 S 3 S 3 S 5 S 5 S 5 S 5 S 5 S 5 S	3 K	3 K 3 S 3 S 3 S 3 S 5 S 5 S 5 S 5 S 5 S 5 S	3 K 3 S 3 S 3 S 3 S 3 S 5 S 5 S 5 S 5 S 5 S	3 K S S S S S S S S S S S S S S S S S S	3 K 3 S 3 S 3 S 3 S 5 S 5 S 5 S 5 S 5 S 5 S	3 K	3 K N N N N N N N N N N N N N N N N N N	3 K 3 S 3 S 3 S 3 S 3 S 5 S 5 S 5 S 5 S 5 S	3 K N N N N N N N N N N N N N N N N N N
	8 5	2 4	82	8	3 3		57.38	2	61.10	-	A S	# # # #	4 5 3 1 4 5 3 1	4 4 3 4 4 4 8 2 8 4	# # # # # # # # # # # # # # # # # # #	<b>海外部位置</b>	កានធនភាកាក្ន ស្នាស់ ជាកាស់ កា	医阴极性医原性性	医阴极性医疗抗抗抗抗抗	医阴极性医阴炎 化二氯甲基	កានធន្លាក់ក្នុងភាពនេះ ឬជាស្ថាក់ស្តាធ់ប្រជាព																				2 · H x w w w w z z z z w w w w w w w w w w w					
		100	8	-73.60	4	×	-77.28	# #	3.4	90 74	Ř	# # # #	F = 2 2 5	* * * * * * * * * * * * * * * * * * *	R \$ \$ \$ \$ \$ \$ \$ \$ \$	<b>以其情况还以记录的证明</b>	· 真情况在礼记引	我 我 我 况 我 我 我 我 我 引 引		お 真 典 作 本 れ で 引 引 引 引 引 引			\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	# # # # # # # # # # # # # # # # # # #	44 44 44 44 44 44 44 44 44 44 44 44 44		24.24 24.24 24.24 24.25 25 26.	######################################	######################################	######################################	######################################	######################################		**************************************	**************************************	######################################				***************************************	**************************************					**************************************
E the s	1	4	7.00	11.78	15. 15.	1 7	±	10.8	<b>8</b>	7.		E E	333			_						# 2 # 2 # 2 # 2 # 2 # 2 # 2 # 2 # 2 # 2	<b>网络罗朗斯拉斯斯拉耳耳拉斯拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉</b>	#@####################################	# 3 # 8 8 7 # 8 7 # 7 # 7 # 7 # 7 # 7 # 7 #			# W # # # # # # # # # # # # # # # # # #	គឺ ១គឺ ខេត្ត គឺ គឺ ១ ១ ១ ១ ១ គឺ គឺ ១ ១ ១ ១ ១ ១ ១ ១ ១	# 3 # 8 8 7 # 5 7 = 7 = 7 5 6 6 6 7 5 6 6 6 6 6 6 6 6 6 6 6 6 6	# 3 # 8 8 7 # 5 7 = 7 7 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7	# 3 # 8 # 5 # 5 # 5 # 5 # 5 # 5 # 6 # 5 # 6 # 5 # 6 # 5 # 6 # 6	# 3 # 8 # 5 # 5 # 5   5   5   5   5   5   5   5	# 3 # 8 8 7 # 8 7 2 7 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	# 3 # 8 # 5 # 5 # 5 # 5 # 5 # 5 # 6 # 5 # 6 # 5 # 6 # 5 # 6 # 6	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	ਫ਼ੑੑਫ਼ਫ਼ਫ਼ਫ਼ੑਫ਼ਫ਼ਫ਼ੑਫ਼ਫ਼ਫ਼ੑਫ਼	ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਸ਼ਫ਼ਫ਼ਸ਼ਫ਼ਸ਼ਫ਼ਸ਼ਫ਼ਸ਼ਫ਼	# 3 # 8 8 7 # 8 7 1 2 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	# W # # # # # # # # # # # # # # # # # #	ਫ਼	ਫ਼ੑੑਫ਼ਫ਼ਫ਼ਫ਼ੑਫ਼ਫ਼ਫ਼ੑਫ਼	ਫ਼ੑੑੑਫ਼ਫ਼ਫ਼ਫ਼ੑਸ਼ਫ਼ਫ਼ੑਸ਼ਫ਼ਸ਼ੑਖ਼ਖ਼ਫ਼ਲ਼ਫ਼ਫ਼ਫ਼ਫ਼ਲ਼ਫ਼ਫ਼ਲ਼ਜ਼ਲ਼ਸ਼ਜ਼ਲ਼ਲ਼ਫ਼ਲ਼ਲ਼ਲ਼ਲ਼ਫ਼ਫ਼ਫ਼ਖ਼੶ਫ਼ ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਲ਼ਫ਼ਜ਼ਖ਼ਲ਼ਫ਼ਜ਼ਖ਼ਲ਼ਜ਼ਖ਼ਲ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼	ਫ਼ੑੑੑਫ਼ਫ਼ਫ਼ਫ਼ਸ਼ਫ਼ਫ਼ਸ਼ੑੑਫ਼ਜ਼ਸ਼ਫ਼ਫ਼ਸ਼ਫ਼ਫ਼ਲ਼ਫ਼ਲ਼ਲ਼ਖ਼ਖ਼ਖ਼ਖ਼ ਖ਼ਖ਼ਫ਼ਲ਼ਲ਼ਫ਼ਜ਼ਖ਼ਜ਼ਖ਼ਲ਼ਖ਼ਲ਼ਖ਼ਸ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਜ਼ਖ਼ਜ਼ਜ਼ਸ਼ਫ਼ਲ਼ਸ਼ਲ਼ਲ਼ਲ਼ਲ਼ਫ਼ਫ਼ਫ਼ਫ਼ਖ਼ਫ਼ਲ਼ਲ਼ਫ਼	ਫ਼ੑੑਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ੑਫ਼ਫ਼ਲ਼ਖ਼ਫ਼ਲ਼ਖ਼ਖ਼ਖ਼ਖ਼ਲ਼ਖ਼ਫ਼ਖ਼ਖ਼ਖ਼ਖ਼ਜ਼ਜ਼ਫ਼ਲ਼ਲ਼ਲ਼ਲ਼ਫ਼ਫ਼ਫ਼ਖ਼ਖ਼ਖ਼ਲ਼ਫ਼ਖ਼ ਖ਼ਖ਼ਫ਼ਖ਼ਖ਼ਖ਼ਜ਼ਖ਼ਲ਼ਫ਼ਫ਼ਫ਼ਲ਼ਫ਼ਲ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼ਖ਼	ਫ਼ੑੑਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼ਖ਼ਫ਼ਫ਼ਲ਼ਖ਼ਖ਼ਲ਼ਲ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ੑਖ਼ਜ਼ਜ਼ਫ਼ਲ਼ਲ਼ਲ਼ਫ਼ਫ਼ਫ਼ਖ਼ਫ਼ਖ਼ਲ਼ਲ਼ਫ਼ਖ਼ਖ਼ ਫ਼
m) this (m) this (m) this (m) this	1		7	12.00	= = =	3 7	3 3	200	4.10																																					
				2	2 2	3	7	4	9.68	10.60	3	# N	4 6																																	
(a) thk (a) thk		7 F		# ·#	37.10	9 2	3	41.8	41.10			3 H										·-	-																		Ma					
ユ		2 :	į of	_	7:		12	_	3	=	ď	2	ri :		₹ 2	즉 건 건	즉 전 전 전																				机心心心 计连续编译 计计算数数数 化偏偏 医自己尼亚氏征	机 记 记 记 计	章 진진진 : · · · · · · · · · · · · · · · · ·	机 記 記 计 电 电 电 计 计 计 更 经 环 化 电 机 页 记 记 记 计 计 电 电 年 5 5 6 6 7 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 2 2 2 2 1 4 4 4 4 4 1 1 1 1 1 1 1 1 1		机尼尼尼比亚 化硫酸钠 计计算数据 化性原性 医克尼尼氏征 化二二甲烷 电电流线	机尼尼尼比亚 化硫酸钠 计计算数数 化铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁铁	# 2 2 2 2 1 1 4 4 4 4 4 1 1 1 1 1 1 1 1 1	机尼尼尼比 化硫酸钠 化红红色 经未代债 医耳巴巴尼比氏征 电电子线点记记记
¥		? !		-					3	3																																				
¥		<b>3</b> :	2 5	8	3			E	3	=	8	3		3			333																	**************************************	**************************************				44444444444444444444444444							
¥		# S	. 5	2.2	<b>78</b>	e s	R SI É SI		8	18.8	8	1			3																															
¥	1	3 :		3	=======================================	2 2		F		=	9.6	4	3	3	4	3 3																														
3	1	49.0		.01	•	•	4 5			.0 19.9	.0 18.5	•	នា	ad T	4	•	25 SZ																													
3 3	- 1	0 35848B.	12.28	44.20	8 45268.	49288	49/04	47.5	312	9 51688A.	0 535.000.	Selest.			-	23,500	375.00 34.00 34.55.00	33500 34500 34500 34500 34500	20 M	3358 3458 3458 3458 3458 3458 3458 3458																										
3		<b>16</b> 238									STREET,	45048										1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	25 (5)44.			2018 2018 2018 2018 2018 2018 2018 2018	2040. 2040. 2040. 2040. 2040. 2040. 2040. 2040. 2040.	1, 522 (554) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (534) (1, 527) (1	22 (5048, 75048,	257 (2544) 251 (2544) (27 (2	150 to 15	130 mm (130 mm	43948. 43948. 43948. 43948. 43948. 43948. 43948. 43948. 43368. 43588.	13040. 13040.	2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2358. 2358.	2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2358. 2358.	2514 2514 2514 2514 2514 2514 2514 2514	1. 52 (3548) 1. 571 (3548) 1. 571 (3548) 1. 571 (3548) 1. 572 (3548) 1. 573 (3548) 1. 573 (3548) 1. 573 (3548) 1. 573 (3548) 1. 573 (3548) 1. 574 (3558) 1.	2344. 2344. 2344. 2344. 2344. 2344. 2344. 2344. 2344. 2344. 2344. 2344. 2344. 2354. 2354. 2354. 2354.	2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2358. 2358. 2358. 2358.	23-44. 23-44.	2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2348. 2358. 2358. 2358. 2358. 2358. 2358. 2358. 2358. 2358. 2358.				
9			1/2									54.773		50,672								# # # # # # # # # # # # # # # # # # #				4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	19 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	19 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	99, 521 99, 521 99, 471 99, 472 99, 531 99, 531 99, 531 99, 531 99, 531 99, 531 99, 531 99, 531 99, 531	99 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	99, 521 99, 531 99, 531 99, 531 99, 531 99, 531 99, 163 99,	99 95 75 75 75 75 75 75 75 75 75 75 75 75 75	99 95 75 75 75 75 75 75 75 75 75 75 75 75 75	99 95 15 15 15 15 15 15 15 15 15 15 15 15 15	99 9 1 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	99 15 25 25 25 25 25 25 25 25 25 25 25 25 25	299999999999999	299999999999999	999999999999999	99 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	99 15 15 15 15 15 15 15 15 15 15 15 15 15	9.9 P. C.	9.9 P. C.	99 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	99 15 15 15 15 15 15 15 15 15 15 15 15 15	99 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
9	1	31.301	31.911	3.8	31.261	31.06	2 S	K K		31.08	31.911	31.261	31.261	3. B		i 7	# # # # # #	8 78 78 8 75 75 75 8 75 75 75	8																											
(deg) (deg) (deg)		23.040	<b>1</b> 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	15.163	23.046	23, 940		1 2	1 7	22.0	2	23,046	<b>8</b> %	25 PE	j	93 646	## ## ## ## ## ## ## ## ## ## ## ## ##	# # # # # # #	3333 ជន់ ជន់	# # # # # # # # # # # # #	##### ################################	3333333 333333	33333333 33533335	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	######################################	######################################	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	* * * * * * * * * * * * * * * * * * *	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************	**************************************		**************************************
FIRM		HE7NE	15. 15. 15. 15. 15. 15. 15. 15. 15. 15.	HP722	F723	<b>₩</b> 25	15 TO 15	9 20	1070	82728	1673	F2738	F2731	H2722	7	AFFOR	HE734	HE734 HE735	HE734 HE735 HE735	HE 733	HETS HETS HETS HETS HETS HETS	######################################	#2735 #2735 #2735 #2736 #274	######################################	######################################	E E E E E E E E E E E E E E E E E E E	######################################	HE133 HE143 HE144 HE145 HE145 HE145 HE145 HE145 HE145 HE145 HE145	HE133 HE133 HE133 HE143	HE73 HE73 HE73 HE73 HE74 HE74 HE74 HE75 HE75	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HE73 HE73 HE73 HE73 HE73 HE74 HE74 HE74 HE75 HE75 HE75 HE75 HE75 HE75 HE75 HE75	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HETS HETS HETS HETS HETS HETS HETS HETS	HE133 HE133 HE133 HE133 HE133 HE133 HE133 HE134 HE133 HE134 HE133 HE134 HE134 HE135	HE133 HE133 HE133 HE133 HE133 HE134 HE135 HE135 HE135 HE135 HE135 HE135 HE135 HE135 HE135 HE135 HE135 HE135	HETS HETS HETS HETS HETS HETS HETS HETS
	51																																													

GEORGIA OFFSHORE MINERALS ASSESSEDIT MODEL. page 9

ZIRCON	8.4		<b>7</b>	2	2	R :	<b>3</b> :	= :	2	=	191	=	2,4	8	1.10	=								13	20	F. 7	R	3	10	23	2	5 S			1.1	=	8:	<u>.</u>	<b>8</b> .3	8	8	2°	2	<b>8</b>			=	F 38	8
TITION t Acount	10,60	19.23	<b>3</b> ;	7	4 1	R /	<b>8</b> 8	3	4	8	\$ 10	8.4	14.10	25	2.4	A.18				7	2	9		2	19.00	<b>8</b>	10.30	=	11.20	7:	2:3	<b>8</b> 8	7		9	37	S. 28	2 :	2 S	2	2	2	3	R :		9 1		<b>8</b> 1	2 4
STALED 1	2.3	1.2	7		B :				3	8	*:	1.28	33	8	7	8	2	8	1	8	2	3	8	=	=:	1.70	1.10				_	3 5			8	3	:	8	==	8	=	8:	8:	8 8	RI	B 1	8	8 :	8
MUTILE S Kount	===	0.10	3 :	3 3					3	2	25		8	2	8	F	Ļ				Ę			8	8.0	8 4	=	8	2	3	2	2 2	8 9	2 2	8	=	8	8	8	8	8	8 :	8 :			B 1	8	<b>3</b> 1	B
MDR2 R	=	91	3 :	3 3				2	3	8	2	=	8	8	8	L	Ļ	ļ		Į	Į	Į			81	8 1	8	8		=	8			2	8	3	8,	8,	8,	2	8	= :		, i		Ŗį	= :	<b>3</b> 1	ļ
<b>=</b> 1	=	= = :	<b>=</b> :						8 :	2	8	2	8	=	=					L	I	l		=	*	=		=	=	=	8 :				8		:	=	•	=	8	2 :				 	<b>.</b>	<b>3</b> {	B
CLANEIN PLICICAL UP. NICE IN. NICE LIA. NICE WAS BOUNG BOOTT IN FILES P. FLESS HAVING PASHET THE (a) that (b) that (b) that (b) that (b) that (c) t	238	用:	R :	<b>9</b> 2		2 5		2	2	200	37	2.50	3.10	280	2.30	2.10		1.28	3	1.66		3		8.1	1.00	2.30	1.60	97.7		R	<b>:</b>		3	3	8	T R	8	R	a R	\$	8	<b>a</b>			2 2		3	= : = :	ř
Acount ,	8	<b>8</b> 8	<b>.</b>	2 8		2 2		2 2					4.50	_	2.4						3.64				3.60	_					_	7		3.10		.2	8	M M	÷ R	<b>*</b>	۳ : ۲ :	2	2 2	7 c	3 8	: . 8		 <b>-</b> - :	: R
Kount S		ار ار		r r		21		R 8	<b>S</b> R 1			_	8		2													1.78 3.		_	_	4 ^		ام ا	3	÷	ri R	÷ =	*	- <del>-</del>	er.	4 . 8 :	e :	d -	;	* *	# :	# : <b>#</b> :	ė
New K.	3			3 5	<b>3</b> 2	8 8			e :	3 :	8	*	3													-			_			 R 8		3	3	٠	=	3	- E	<u>.</u>	2	m ,	7					= =	-
6 6	28 91.		<b>3</b> K	8 14					el a	# I		•	7.68	91.4	66 91.78		-	_			-		-	•		•	-	•	-	•	<b>ਜ਼</b> ਂ ਹ	ž .	8	i si	91.6	35	69.7			2	2	S S	Ġ		Ka		, i	91.18	į
LNICC LILMICC DOLDING CARRIED GLANTZ K the (a) thk (a) thk (a) thk (a) Xcourt	2	_		d a						2	_	6.21	16.1	44.0	4	43.88	_	49.0	51.38	23	35.18	, K	3	2	42.9	15.0				27.53		é s	8	18.0	33.0	16.1	a M	45.3	* # # # # # # # # # # # # # # # # # # #	7.0	3i	16.0		2 3	2 4	4	ġ!	47.74	12:11
	-73.6		4	4 9		120 20			2 Table 1	7	# H - P	422	4	1-76.8	おおり	-73.64	-73.3	-76.6	-78.8	4	7	7	39 4	-78.8				-72.23		-X-	_	2 9	100	-101-	•	7 19	-123.8	-137.0	7:4	왕	-172.4	1	į	77		4 4/2	9	F- 2	
1	15.1		g a	-	d	d 8	3 8		ज़ : यं त	# 1 # 1	E E	•-•	12.3	12.4		11.0	9	91	1	4	er!	4	4	K.7	F	<b>19</b>		2				7 2	4	21.40	81 TO	¥. 8	S Ki	<b>8</b>	*	\$ \$	2	2 2	R 8			1 2	5	8 8	å
	24.68	er :	8 7. 8		i x	1 1			3 2		었	36.38	7.4	17.38	11.30	17.30	14.66	11.78	9,10	7.7	7.8	7.10	2 5	100	E ::	12.28	15.10	17.60	19.20	2.4 2.4		2 2	31.0	33.66	3	17.30	<b>3</b>	4	47	2	4 :	# : # : : :		R 3	15.8			ਨ 1 =	
thk (a) thk (a)	4.7	= 8 M -	R 8								3	3	3	3	-	4	8	85	2	7	7.7	3.5	9.10	200	1	3	9	3	<b>1</b> 3	3		4 4	8	3	3	2	8	=	3	2	2					1 2		<b>8</b> 5	1
(a) this	24		2 2	2	2 2	4 4					8	<b>8</b>	#	3	6.8		¥.10	3	8	37.38	37.38	18° 58	31.38	27.68	S.	£.3	17.38	37 14	8	8 a			=	200	13.40	7.10	2	17.8	15.30	Z	24. 8 24. 8		8 8 4 9		2	2		2 2	
1 to	= 3		1			i K	1 7		2 1	2 :	= %	3. 2.	## 	12.48	9. 38	16.38	12.10	12.68	12.50	12.8		10,60	=======================================	£	2	7	174	16.3	15.60	2	2 5	# # # # # # # # # # # # # # # # # # #	=	17.10	15.38	<b>8</b>	র র	R N	<b>8</b>	R F	8 3 5 9	<b>3</b>			2	2 2	R :	17 E	
* E	=										3	2	3	Ħ	8	9	3	=	3	=	8	3	8	3	3	8	=	2	2	3			3	3	8	=	=	=	= ;							2 2	2 2		ì
¥ 2	3				8	1		2 %			3	2	۳ ا	2.	2	<b>#</b>	3	<b>9</b> . 10	2	<b>6</b> . 10	=	8	3	3	=	3	=	2	=	3			8	8	6.15	=	# :	=	3 1	2	8 1 N			2 =	3	3 5		= 1	
2 % 3 %	8			8	1 2	3 <b>3</b>	3		8 1 d 1		97.18	2	調点	97.28	85 '58 20' 28	# #	35. LE	8.3	<b>8</b> .38	<b>3</b> 2	8.8	8.8	2 4	8 4	2	33.55	2	8	2	# :			8	2 1	<b>3</b> %	3. 3.	<b>3</b>	<b>3</b>	2		R :	Ro	2 A		3	2	8 8	7 S	ĺ
*	3	3 3			8	1		2 8		B 7	2	=	8	7	=	23	91.0	3	8	3	=======================================	= = =	- 81	=======================================	2	<b>8</b>	=======================================		2	3 3			200	-	9.19		70	8	2 :		7 2								
E 3	2	d z	1 3		7 7 7	5 7	2	7 67		d	4	œ K	4.9	<b>9.6</b>	<b>SF 3</b>	12.4	14.1	15.4	17.6	19.2	19.9	20.2	21.1	7.2	24.4	23.7	b b	27.7	ત્યું :	au c	3.5	id	34.3	46.3	12.3	31.6	1.4	9	9 :		7	7 K		13.3	14.7	16.1	1 2 2	9.6	P :-
- 1	SEC. 0		¥0.5	2777	S. A.			0.77.00		DAORE.	250 VBC	2696a. a	473588.8	476488.8	574488.0	48.228. B	48200.0	49288. B	4976at. 0	382488. 8	507200.0	S12888.8	516,000.0	\$21688.0	525 AB. 0	57238.0	•	•	3400B. 0	34.55 B. B	1		564beg. 8	569688.0	•	•		264em. 0		13.00		•				492840.0		49/ben.	
E	-	ASTRONO A SE						•				•	•	•	•		•		•	•	3	•	•	•	•	•	3	3	•	•				9	3	9	9 9	2	2:	9 .	9 9	•			9		•		•
											75.567 45.66E.		81.277 448848.	81.227 44884B.		81.176 448888.			11.625 44888	M. 975 446648.	924 44888				L 723 4488	1. 152 S30480.	8. 673 448881				77 44888	378 44888			219 448384	DE 112 53844									35 444			973	
(del) (del)	217 88.		1		8			1				3							_	_	\$	鬈	8	8	•	-	•	8	8	<b>25</b> 4	8 8		35	8	_	_	_	_	<b>E</b> :	8 8	<b>E</b> 1		į		. IO	2 Al. 076		<b>3</b>	İ
3 1	71.217																	* 31.17						# M.17						4 31.17 4 21.17								_							31.15	31.12		31.15	
9	<b>स</b>							2	i	3 8	3	ส	ซีร	14.6		ដ								<b>3</b>		ส่	ส่			<b>X</b> 5	1 2	1 1	<b>3</b> 5	<b>₹</b>	ສ	75 E	7	รู้	<b>1</b> 3	3	<b>1</b> 3	1 2	7	7	2	23.	22 62	ร์ ส	ĺ
4	HE781	F783	H278A	19	1	18787	P2788	1 2	3 ,	2070	<b>R</b> ,			200	2	200	3	길	<b>F2813</b>	<b>19</b>	<b>F2855</b>	916	917	100	5		200	<u> </u>	27	1000	280	1 30	H2827	H2828	25 25 25 25 25 25 25 25 25 25 25 25 25 2	2			3	3		2 2	2	VGE	1283	285	Į,	H2858	

Month.	1	3	<b>8</b> 2	R :			2 :		<b>3</b>	3	3	3	<b>8</b>	<b>8</b>	= :	<b>8</b> :						2.2		1.10		=======================================	8	2 3	3 2			8				2 4	8	<b>8</b>	=	8 :				<del>-</del> -	<u>-</u>		š -	•
5	1	A of	3			8	= = =																										11.10	# :									21	# <b>8</b>	H S	id		
Signed Item		3	8; 8	7	=======================================	=	=	=	 81	<u></u>	2.	8.	2 19																					2 :				2. S	7.	2.6	<b>3</b>	= :	-				-	:
Xcount I		3	2	3	2	3	3	3	3	3	3	3	9	<b>6</b> .28	3	8	<b>⊸</b> ·	- •	•				•			•	•	•	_	•		_	8	_	-	_		- 10	20	6.50	3 3	<b>3</b>						i
3		3	8	3	3	3	=	3	3	2	3	=	1	<b>6</b> .28	3	2																	-						6.28	3	8 3	<b>F</b> 3						i
Menter a		2	2	3	2	3	8	3	3	3	2	3	3	=																			3						3	8	3	8	-		5 .			
K.F.LIGS P.F.LIGS HAMING MENHAT MINKA I Scount Scount Scount Scount Sco		8:		1. 8																													<b>3</b>															
P. F. Dep		4.10	4.7	24	3.78	*	#	2	 4.	33	3.10	3.10	3.28	3,38	# #																		3									85 m	17	月5	7 4			5
K.F.LBSP		H .1	2.8	7	<b>87.</b>	=	8	1.3	7:	7.		1.3	3.	7	7																		3						7			1	0.00	33 7	<b>5</b> 2		1 2	5
		91.30	8.3	91.00	8 8	8 8	80	8 kg	9	9.3	8	25.55	91.28		9i																		9		25 . E													
MELECTS CARBICON CLIPICTY i) that (a) that (a) Acoun		49.80	17.20	4.5	45,28	45. <b>8</b>	<b>8</b>	39 15													2 2		1 2		41.2								2									_	H.6	49.9			_	
DE TENE		8	-76.58	2. C.	-76.30	-77.60	2 C	-72.10	-72,10	- 10 B	-77.98	3	19.20	18	-191.38	-111.30	-128.28	-136.38	-140.70	-147.20	-13.5	7 5	R	2	-7.4	-74	12	8 E	-76.68	-76.00	123	i K	7.6	-72.00	<b>第元</b>	- 10	j	180	-104.2	-110.00	-115.3	-127.	-136.0	146.0	<u> </u>	用"药"——		9
		8	33.88	2	3	7.78	3	84	8	2	A 20		11.2	4	17.78	19.3	19.7	성	£ ₹	\$													8															
MO. MICE.		10,40	12.28		11.00	2		7	5	8																							2 2 2											48.50	H-2	25.2	28.7	17.64
UP. MIDC		8		4	7.68	7.9	7.10	7			7	F	7.10																				4 4															
ATERN PLICIES UP.NICC NO.NICC LL.NIC the (a) the (a) the (a) the (a) the		2	43		8	23.78	17.60	7.78	8	7				15	12.6	14.3	16.60	17.98	16.28	14.48	用式	21.78	<b>4</b> 5		e s								13.98														28.48	β
CANTERN C		10 10		7	10.7	-	2				-	10					21.40			_	••		7 2										13.5											38.00				
N THE		1					ŀ																																									
SILT		1															13	3	2	4	8	2	<b>只</b> i	# S	3		3 6		8	8	3			ŀ	3	-	8 1	+	ŧ		_			1.1	_	_	8.0	
985	6	1	8					ŀ								8	2 2	86	3	8	**	開発	# :	# :	# 8 # 8	i s	r s	8	3	3	10.00	8				100	8 3		İ	8	; S	95	_	_	8.4	_	7.98	
GHONE	r W	1												1 1				ř	3	4	3	<b>–</b>	3	2	3 3			ł		3	3	3				-							6.28	. <b>.</b>	10 m	<b>-</b>	0.30	4
EPH 1	3	١,	_	37.8		3			-												_	-		-	•	•	15.2					•	2			-	•	•	4 6							•	•	
1982	3		2017		Sicher.	316000			7	9		34.75		100		20,00	2 44 6							0 4735.00.	-		1000		•		. 51200E.	. S16.000.	2016	12128			. 0 SASSAB.	•	STATE OF		10 AC		5799B	SAABB.				
1 = 1	3																				9. 018 44400.0	9.968 444888.	43558F	1.277 4392ML	11.226 439288.	11.176 439200.	1000	1.873 4.39E	475 470	4.792	674 439280.0	EN 43558.8	774 439288.	1/25 4350E.	623 4398.	572 439200.0	522 4392M.0	1, 472 439200.0	6. 421 43998.	771 43500.0	276 43528.	4 224 4 3228	M. CC 435CM.	A 119 439286.	M. M69 439200.	4.019 439200.	79,968 439288.	
DESTINE THE					20.07					2	3/5	2	2	24.2	16.37		200	8 1	A 119	M. 069	_	-	-	81.27	72. 13.	11.176	100			1	26.674	1 88.824	120.74		8 8	8	3	8	8 :	8 1	8 1						, , -	
ATTUDE	<b>E</b>		24 H										M. 1.	M.1.W	H	31.15	31.13	21.167					31.000	31.008		_	31.068	4		, F	31.60	31.008	31.004	31.00						# ;				2 5 E				
BLOCKID AGEN LATITUDE LONGITUDE	(sq.km)		<b>3</b>	ສ. ສ.	₹ 1	<b>3</b>	2	₹ 7	<b>₹</b>	<b>3</b> ສ່	<b>₹</b>	Z; ₩	<b>₹</b>	23.040	2 2 2	Z :	<b>1</b> 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	3 3		1 2	22	22.69	8.862	17.723	<b>1</b> 5	<b>₹</b>	23.04	<b>1</b> 3	1 6	1 2		2,00	20.00	1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1 7	12	23.040	<b>₹</b>	23. 04	<b>3</b> 5	<b>3</b> 3		<b>3</b> 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	2 2	3 %	3	18	01
BLOCKID			H2659	285 285	2867	1286 1286 1386 1386	2982	3	H2864	HEB63	12856 1886	H2867	F2868	15969	282	1287	F8972	2/8/2	HC0/4	7,000	1287	H2878	12895	H2898	F2857	<b>12836</b>	H2899			70001	12984	<b>2862</b>	12986	1864		1831	1231	H2915	£2913	¥23	536	1531g	1631	2000	C COCH	000	1000	HC3C

MCON12	Scount	1		8	8	A. 60	3	===	8	2	2	=	<b>P</b> . 10	<b>M</b>	9.68	8	8.3	8.4	==	===	<b>8</b>		<b>3</b>	<b>8</b> 1				8	8.4	25	2	2	7 Z		8		3 3		2	6.00	<b>8</b> . 9	 8	2 7	R 2	3 1	2.60	2.10
- 1	3	2		7	P 50	9, 10	<b>8</b> 6	10.60	10.30	=======================================	8	1.2	2.11	13.00	14.50	15, 50	6.8	25.98	14.00	8:3	<b>4</b> 8	8 .	8		B 8		35	9. 19	A.50	# 4	8 :	<b>37</b> :		8	8		2 9	3	用士	15,78	16.40	= :	<b>2</b> 8	R 2	3	3	2
STALRO TITON	Acount	8	8	8	8.1	1.68	<b>?</b> :	1.10	8.1	8:	=	=					2.78	_	_			<b>8</b> :	2 :	B :			8 8	2	8	*	3 :	2 3	7 2	=	8:	ļ	1 2		=	2.60	8	_		3 7		2	#.1
AUTILE SI	Acount	1			8	8 4	8	8	= 1	=	8	2	8	8	8	8	8			2			= = :					8	8	=	8 :			=	8:				8	2 8	8	_	- ·	_		8	8
- 1	*				8	8 1	=	8	=	8	8	=	=	=	=		=	=======================================	_	3	2	<b>*</b>	B :		3 8		3	8	8	8	= :			8	<b>3</b> 1	8 8	: 8		3	- -	<b>3</b> :	e :		. <del>.</del>		3	•
	Account 5				=	=	3	=	=	3	=	8	=	3	=	=	=	=	2	<b>3</b> :	2 :	e . 8 :		- 			3	=	4	<b>1</b>	11:11	3 4 R 1		=	<b>.</b>				=	•	2					-	-
K.FLISP P.FLISP MAMING REPHET MINAZ	Scount Se			3	10	=	ڪ ھ	- E	10	3	=	9	2	70 E.	33	3	•	3	<b>=</b>	<b>a</b>	2 ·	3 1					2	3	3	3				3	3			3	3	3	3			; ;	3	3	3
DSP HAM	Acount fo	١_		2		N 2.10			-									9 7 8										22		2.2		3 .		2	<u>.</u>		5	2.7	70	*	<b>4</b> 1	<b>3</b>	4 ~	7 37 4 mi	4	mi	mi.
89 P.FL	Acount Aco	45	-			24 8										3.00				8 ; m			_			_			_	_	_	2 %	1 4	<b>₽</b>	ਭ ਹ ਵੱ		-	4	<b>8</b> 2 m			d ·	7 R	7 7	Wi Wi	4.68	4.
K.P.	and Moo	-	٥	4	<b>=</b>	4	_	_			_	200	9.0		= -	::			= :				3 3				_	_	<b>-</b>	3 .			3	3	# # -		2 2	8.	===	-:	87 5	2 .			1.3	1.7	7.
HAL BOTS OVERADIK BLIGHTZ	(a) this (a) this (a) Scount	•	69,68	\$	59.20	_	•	91.10	91.00	9i	8i 8i	_	91	8	対象	•	-	-	-				_			_	_		_	<b>3</b> 3		8		91.28	2 i 2 i			91.8	8.3	<b>77</b>	用言			69.10	87.68	89.80	73.20
S DARBOO	(e) thk		39.68		42. B	42.8	41.10	S M	# .X	# #	<b>1</b> 2	S X	<b>3</b>	27.00	27.10	<b>3</b>	T)	Si Si	2 ×	<b>字</b> / 字 /		4	3 8		51.2	3	<b>8</b> 7	<b>3</b>	e R	<b>3</b> 5			2	# #	3 :		17	8	S S	27.68	3		2 2	2 3	3	3.	3
191 193	e) thk		-74.78		-76.18	-76.78	-76.98	10°	12 K	8 K-	-76.00	8. IC	-76.4	-78.28	8 7	9	=	-101.80	-107.88				2 2 1	7 95	-164.88	-151.38	-69.38	-71.00	-7.4	2 i		1 ×	37	-7. S	# 5 K	7	-7.3	-78.28	<b>≘</b>	43.78	70 S	-/2.4	7		3	=	8
	ž		7.38			# :		<b>8</b>	<b>8</b>	4	7	<b>8</b>	3	19.68	<b>5</b>	= :	F :		9 1							47.38		7.50	2	3 5	8 8	3 1	18		8 S				8 2	25.5			_	3	3	=	2
D. MICC	) thk (m)	28.88	3,42	19.30	16.48	7. 2	# :	17.4	19.60	16.78	16.98	13. <b>B</b>	S S	8	24.42	27.8				3 1			R 2		49.98	3	16.30	19.38	<b>7</b>	# :	2 S		17.10	3:	<b>3</b> 1	8	2.3	<b>3</b> .23	33 77	A :	<b>3</b> 3	8 9			8	8	2
P. MIDC	thk G	3	=	=======================================	<b>7</b>	3	# i	3	<b>2</b>	<b>3</b>	<b>8</b>	2	8	80 4	7	8 ;	8	<b>3</b> ;	# 8 -i e	8 8					8	3	3	3	2	3 3			3	3	2 A	3		3.10		3					8	=	8
QUATERN PLICISM UP.NICC	thk (s) thk (s) thk (s)	20.43	27.38	27.50	27.28	<b>3</b>	d :	# #:	9. 10	IA 10	16. ±	80 m	<b>3</b>	3.	2	2 :	7 1	<b>19</b> 1	<b>8</b> 5	8 9	2 2	1 3		8	A. 28	16.00	27	R :			2 5		92 10	2	9 S	9	8.5	# ::	2	<b>7</b>	R 2	R 2	3 2		8	=	8
ATEM P	tht (e)	11.38		2	3	8 :	0	8	8	유 신	23	2.3	<b>8</b>	7	91 1	12,78	3 2	R 3	3 3		19 44 61			25.25			_		_				-			_	_	12.48	_	_		R	2		8	8	8
	u u	1.28		3	3	2 :		2	2	2	2	= :	2	2	8	8 1					3 7			7	7 87	87	_	8					8	= : 8 :		8	=	25	<b>8</b> :	21 :	2 ·			=	8	=	=
=	w.	85	8	8	2	8 1		8	2	8:	8:		8 :	2 :	3	8 1	<b>3</b> 1		ļ	; =	1			8	8	2	2	2 :	3 2	3 3			=	<b>.</b> .		3	=	2	8 :	8 :			· ·	3	2	<b>2</b>	<del>=</del> <del>2</del> 7
1	-	8	=	<u>ज</u> ़	<b>.</b>			8 :			<b>.</b>					8 2					1	3		8	2	3	7	= :	2 (		8	8	2	<b>3</b> :		3	3	٠ 3	= :	ه 2 :	í.				=======================================	<b>.</b>	<b>≕</b> ≅
1 .	, w	# #	_	8 :	R						2 2									§ 8	i		20.00	3	3	si m	න් න	र्ज र <b>अ</b> १	e s R 1	r s	i gi	8	3 3			3	8		<b>3</b> :		8			28	 8.		2
1	3	13.1	14.7 B.	16.2	17.7	13.2		2.2			<b>-</b>	<b>1</b>			<b>-</b>	<b>.</b>							- m	6	7 1	اري ا	<b>.</b>				•	7	9		- ~	13 (1	5 6.1	9.6	9		# # # # # # # # # # # # # # # # # # #		9.6	-	1 0.6	2 <b>0.</b> 6	~ •
1		_	_	_	_						•		•			22.2					•			•	•		•	-				_	_	8		-	1.0 27.	•	20 S		y s		1.0	1.0 45.			
-		-				-	9									24.20m						-					•	-	4 2 2 2		-	8 49768B.		38728		•	8 S26488.	<b>4 331286.</b>	536888.	7	CATCOM.	642		612888	6 617688.	•	6272
	(800)										1						7	¥2448	7		4344	43448	43448	38.869 43448E.	43448	7.969 43448	12.00 m	100 M	3000			429688.	42964	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	12.00 10.00	429648.	42964	429688.			200	2000	120000	528688.		178888 1888	
11907	- 1						_		_				_		4 535		A A23		2	<b>8</b> . 27	22.00	3	4	88.869	86.019	73,969	12.5	12.19		1 1 2		81. ES	<b>16.97</b>		8 . 62	88.774	88, 723	68.673		2/2/2		79.91	79.859	79, 888		79.70	3.636
ATTION	9	31.045	31. M3	31. 043	31.045	21.050	7	31.015	7	21.00	25.00	21.0				7	1	7	31.043	31.043	31.043	31.042	31.042	31.042	31.041	3. W				3	31.002	31.002	31.00		3 5	31.001	31.001	31.80	# F		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	31.820	31.819	31.819	31.616	31.818	31.81/
PRES.	9	23.040	7	<b>1</b> 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		3	3		3 2	1 3	i		i	ja		1 2	22	iz	23.0	2	23.04	± 5.	3.€¥	23.040	23.04	7.200	3.13		27 27	<b>3</b> 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	23.040	23.040	23.04	77.77	<b>:</b> 3	2,046	3. <b>E</b>	S S	i a							22.39	
BLOCKED PARA LATITUDE LONGITUDE		H2948	E A	H2943	37001	7604	1001	USQ10																				1000					_	2000						00000		~					86
1	1	:		- 3	. 3	- 1	= 1	- 5	- 3	= 5	2 3	= 3	6 3	= 5	c 3	= 1	: 14	: 1	<b>.</b> 4	Ή	뽀	뽀	뽀	뽀	뽀	逆!	# S	# 3	3	선 및	및	坐	말 :	# J	i 37	및	뽀	9 :	¥ 3	F 3	2 2	3	끞	뀦	¥ 9	<b>2</b>	2

ITON ZIRCON Scount Scount		97.	-6 c	37.		<b>8</b> 5		6.30											R \$4			2 4 5 4 5 8 6 8 7		8 3 √ √		_	2.8		84 S			20 · 1 · 20		i «
D TETAN		0.7	4			3	6 ~	_	~ `	R		5.0		_		7 33 1 11 2 3			3 55 14 14 2 15				B 6.28	3 4 8 8	8.6	# 25 5' 5' 2 #						E .3	2 :	n 4
JTILE STRUND T Acount Acount		E.1	N .		7.1	2.0		<b>-</b>	-i «	<b>.</b>		-	7 7	-		نے ک		<b>d</b>		3 8				ک کے	2.0	2 3 2 6 2 6 2 7			971		1.5	_	= :	:
- g		<b>a</b>	3 6		3	<b>-</b>		<b>-</b>	•	<b>.</b>		<b>-</b>	: :	<b>-</b>	•	4	<b>=</b>	<b>-</b>	•	<b>.</b>	<b>d</b> (		_	<u>.</u>	•	]	₫.	<b>.</b>	• •		<b>.</b>	<b>3</b>		
IT HOW?		6.50	# 8 # 6			3		3	6.3			3	3 3	5	2	3 3	5	6.7		3	9 6		5	* °	3	::	33	6.2			<b>-</b>	9	_	
S PEPHIT I					3		+	3	9			3		3	3		3	3			3		3	33		] ] 	33		33	3 3	4	3	3 3	
K.FLDSP P.FLDSP HYMING RESPIRT NOW?	- 1	=	줘 .	4 4	-	M I	7 4	-	<b>4</b>	ન . -	; ;	÷	2 Z	<b>+</b>	-	4 4	4						7			로 R 사 사			8 7 7		3.6			-
P P. F. DSP Int Xcount	- 1	# T	7 /	e e		eń -	7 7	-	4.70	<b>.</b>		4	# #		4.7			5.5						2 7		足別する								÷ <
	- 1	= :	<u>-</u>	3 3	7	25 C		<b>.</b> →	<b>-</b>	# :	# R]	<b>-</b>	70 F	_			_	0.0		3	97		28			전 <b>조</b> 시 시	6.1		_			_	200	
N GLIPRTZ (a) Scoul		3				79.			26.00	_		Ź	2 2 2	=	_			8 3			69.6	2. 2. 4. 5. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	3	2 2 2	=	* 10 * 10 * 10 * 10 * 10	-		86.98		_	87.	# 12 m	
CHRIEFIN PLICIEN UP.NICE NO.NICE LIK.NICE INL BOTS CARSAGN CLIERT? THE (a) the (a) the (a) the (a) Source the (a) the (a) the (a) the (a) Source the (a) the (a) the (a) the (a) Source the (a) the (a) the (a) the (a) the (b) Source the (b)		8.3				17.50	3 2	_	25 25	# ;	의 의 의	\$	2 E S	37.		* *		45.78	7 4	49.8			N.	8 18		2 15	3		-			65.20		
(a) thk		-67.50	7			-74.80				-	-117.8		M 411-			-127.5			5 X	4 2	-136.44	-123	7	-142.28		# × ×	3	-147.8						-147.4
LIL NIO		41 8	12.5		3	33.8	10 10 4 0	8 6	1.3	2 :	2 S	12.50	3 3	3	17 th	7 7 2 1	12.3	75	2 4	9 4	27.00	<u> </u>	8	# K	22.22	의 의	3	G ₩				•		y s
a) thk		21.98	M Ki	# S	3	17.30	₹ <b>1</b>		3	3		<b>37</b>	워 =	22 22	25. 25.	<b>8</b> 3	2 <b>2</b>	23	2 2	2 <b>3</b>	87 · 58	3 E	12	27.28	21 22	15.8	8	2 2				<b>8</b> %	83 8	i k
UP. MTOC		=	8	3 :		=				3		3	3 3		=	3 :		=	3 1		=	3 :		3			3		8		3 4	8.	3 3	3 4
RIERN P. IOCEN LP. NICC AD. NICC LALNICC WA. ACT the (a) the (a) the (a) the (a) the (a) the	100	9.30		2 2 3 4	3	1.2	15.2		12.28	8	라 <u>로</u>		2 t	15.2		16.28	1 4	8	7 1 7 :	1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8	8. 4	7	នា ន	7	A. 70	-		3			24.50	<b>8</b>	27.18
CANTERN CANTERN		12.98	13.70	<b>7</b> 1		2	4 4 5	19.38	17.28		2 7 2 7	ន ដ	19.28	8		## ## ## ## ## ## ## ## ## ## ## ## ##	1 2	₹ a	# X	3 E	72.78	<b>3</b> 3	M	A B B	5 = :	# 5 6 6	=	4 4	=	2 1	1 2 1 3	40.60	43.80	\$5.58 8.88
F 20	6	97.0	<b>6</b> .10	<b>₹</b>	8	=	= 5		8	E.28	2 2	=	3 3	100	<b>8</b> 7	# S		7	3 2		# =	A :		2 2			=	3 8	**	<b>8</b> 5	8 M	=	87.7 7.7	Ni e
51LT	É	3	3	9:			7 S	R 8		1.2		3	2 5	2 3	=	2	3 8	1.6	त्य है त्ये -		39.1	7 7	3 4 -	3 5	3	3 5	3	# E	1.60	3 5	# <b>=</b>	2.8	<b>8</b> :	d o
68 # 68 #	É	99.40	<b>3</b> 6	<b>3</b> 5		<b>3</b> 6.	<b>3</b>	g g	2 3	81.98	#	83	<b>2</b> 2		25.28	8.78		8	2. S		35	<b>≘</b> 5	13 E	2 S	i si	8. 8 8. 8	8	F 15	99	<b>3</b> 5	F 5.	<b>8</b> .8	91.5	37 S
ENONE!	ê	9	=	3		=	2 1			3		3	3 3		=	3 3		=	3 3		=	3 3		2 2	1 7 N	33	-	2 2		3 :		9.19	=	
E 3	9	43.3	45.6	48.9	2 2	33.4	45.7	2 5	46.2	_	45.6			\$ .5 5.2	_	-	47.6		_	44.6			46.7	24.55 50.55		39.8		4 74 4 74 6 74		-	4 7 P	•	_	51.3
E851	9	683288.	600000.	612988.	5224m	50000	603200	612988	617686.	6224 <b>00.</b> (	CARAMA.			66.29	50000	612808.1	64 C BB	5808B.	612988.	61768.	98999	612888.		5.00000	64286.8	6.00000	617600.	642280.	622488.	622488.	K. 2000.	683208		683288.
震 二	3	516000.0	516888.8	516000.0	Sibon.	335.00	511200.0	311cm.	511200.0	511200.0	585488.8 Secure	3648.	506400.0	30168L	501688.0	501600.0	A96.00	49688.	496800.0	ASS 84	4%2000.0	492804. B	4972	487288.	539 to	530480.	539468	482486. 482486.	530	535280.	13016	477600.	477500.	472800.0
1-	- 1							7.00		79. 706	79.911			79.912	79.061		20.00	73.16.2	79.01	79. 76. 436.000	79.062	79.812	5 5	73.863	79.98	73.658 74		5. S. S. S. S. S. S. S. S. S. S. S. S. S.	75.786	79.765		79.914	79.864	79.915
	- 1	79.910	73.659	73.889	2 2	e	-						_			99	7 3	3	31.68	3. S. S. S. S. S. S. S. S. S. S. S. S. S.	31.56	S	31.517	31.516	31.96	31,986	31.985	31.473	31.965	31.946	M. 18	31.438	3	. W
	- 1	8			2. K. K. K. K. K. K. K. K. K. K. K. K. K.			21.15	31.72	31.731	31.690	31.689	31.689	2	31.646	31.646	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	31.663	ਲਂ :	₩ ₩	ניין נ	~ .	A) W)	(4)	7 M	143 14		L. (L.	L (m)	ਲ ;	<b>5</b> F	8	31.430	31.307
OMETITE (deg)	(Bap)	31.777 79.910	31.776		e 12	31.949	31.733				23.0M0 31.690						22 646 31.6		_	17.288 31 17.288 31			23.040		23,040 3	_		23.040			2.52 2.73 2.73 2.73			23.040 31.

GEONGIA OFFSFORE MINERALS ASSESSMENT MODEL. page 13

ZINCOM!	2.8		27.0	6.78	3.20	3.10	2.90	2.60	8:3	2	8		<b>6</b> .10	<b>6.2</b>	<b>3</b> 3	2 A		2 2	9.10	9.10	0.20	7.	27	P. 38	=	<b>8</b> :	2 2			= -	# ·	= :		8		8 4	9. 10		87	3 ;	<b>8</b> 5	2	3 8			=
	8.8		4. W	4.70	3.6	3 %	9.30	B. 68	6.8	9	E	97:1	8.3	<b>8</b> 5		2 2	3	16.38	M. II	11.70	12.30	13.40	15.80	16.20	16.88	8:2		8 8	R R	2	=	3 2	R p	3 8 5 vi	80 %	1.28	9.00		20 i	2 :				8	3 5	3
DRIZ MUTILE STAIND TITAN 2 Acount Acount Acount Acount	8	8	3	. 38	8.	8.	1.88	1.70	# ·	2.1	2.90	_	_			7.8	_							2	- S	= .	2 1			33.3	8	<b>3</b> 2	ģ			2.70	1.58	_	_ ਗ਼	_ `	= 1	8 8	1	3 2		
MUTILE ST			=	_	=======================================	8	8	=	8	8	8		110			9 9		8	2	8	8	8	8	8	2	3 :	2 1	ļ <b>8</b>	1 8	2 2	<b>3</b>	<b>3</b> 8	Ŗ	8	=	8		=		_		7 8		: T		
RZ MEU		A	=	_	_	=	*	=	=	=	=	=	=	= :	2 :				3	=		=		8	=	8 :						3 2	r s		8	:	•	=	<b>.</b>					1	1	8
R.F.L.DAY P.F.L.DAY HAVINING MESHATI MURIS.  1 Acount Acount Acount Acount Acount Acount		8		2	=	2	2	=	8	2	8	=	8	2 :				2	=	2	=	=	=	2	= = :	2 :	6 4 8 2		;	3	<b>3</b> :	- ·	5 - 6 8	: -: : 8	=	2	2:	- 2	e :	#	e e R S		i ei L S	;	1	ľ
Acount &		9	A P	=	<b>3</b>		10	3	2	8	=	3	10	<b>.</b>	e .			3	8	=	**	<b>3</b>	<del>-</del>	<b>3</b>	2				3	8	8:3	3 :	* 8		3	3	3	3	<b>.</b>				2 91	;		į
Acount Ac		-	<b>+</b>		rri	ri R	ᆏ	٣i	7	m	_	3.0	તાં	ai r	ન -	1 1		· ~i		33 1.0	•	•	-	-	ر م	ਜ ;	4 6	1 4	-	1.0	-	<u> </u>		=	=	2.6	പ്	م <b>ن</b> _	~f ·	F .	3	ř	ŕm	6	- ن	-
, i	6.1	9			<del>-</del>	<b>-</b>		÷	<u>در</u>	wi	_	<u>ئە</u>	-	<u>ب</u> ،	ಗ - _	# M	5 1	i ~i		~				F .	_	۳. م				3.0	<b>3</b>	mi -	5 ~	m	33	7.0	7.4	7.4	П	7 F	4	7	. M	F 1	; ~	'n
	-	9.6		-	તાં _	-	_	<b>∹</b>	7:	-	=		3	3			ŧ	- RI	25	<b>=</b>	8.4	1.8	==	F .	2	<b>8</b> 8	# P		3	1	3	M 1		8	-	-	-	-					. =	9		5
) thk (a) thk (a) Arount	3	2.2	<b>87</b>	_					<b>8</b> 5.	89.78	89. 18	<b>8</b> 3. E	<b>8</b>	<b>用 3</b> 第 3	i a	2 2		8		3.4	2.3	2.3	93.8	주 : Si		80 8 87 8		8	2	8.3	<b>8</b> :	9i 8		2.5	23.	<b>89.</b> 38	8	<b>3</b>	89.40		R 8	91.12	. Si	3	7	17.
(e)	3	3	69.68	일 르	17.68	17.90	16.30		3		3	\$	<b>3</b> 2.	<b>3</b> 5	7		3	7	<b>8</b>	100	27.20			නි : ස්	¥d :		2 E 2 €	3		39.38	7	3.5	1 3 2 4	27	47.50		#	<b>‡</b>	3 3		7 2	1 1	1 35 1 35	2	2	P.
(a) thk (	3	3	-118.78	-148.68	-73.30	-74.70	200	=	8		3	-69.30	-72.10	27 T			7	-74.40	-75.10	-76.10	-77.10	-77.98	-77.70	-78.38	3	2 :		8	10.49	-116.58	-117.40	-127.98	10.1	-176.98	-151.30	3		-73.20	27.50		ار بر 10 ا	2 17	-7.20		. F	
(a) thk (a	8	3	_	21.6	31.4	M	) 구	3	3	=	2	7.30	\$	3 5	A S	3	M	8	<b>3</b>	9.78	12.70	14.2		2.5	16.28	15. 2 5. 3 5. 3	3 3		8	8	8	= #	2 E		33.58 -	=	<b>3</b>	<b>8</b>	<b>3</b> !	<b>3</b> (	7	3 8	i vi	8	8 8	ó
(a) thk (a) thk (a		=	15.98			16.68	17.4	=	3		=	19.70	19. 10	3 2		3	36	21.50	22.38	22.78	<b>8</b> 1	E 17	<b>8</b> 7	<b>8</b> :	7		d K	1 N	25.10	8 .K	의 :		3 3	8	34.68				<b>9</b> 7 9 9					21.50	8	
(a) thk (a)	3	3	=	2	3	2	=	3	8	=	8	3	2	2 2				=		9 19	8 4	<b>6.</b> 10	<b>8</b> 3 :	= :	明 ; 5 ·	<b>M</b> 8		2	2	3	3 3			8	2	=	2 :	3	<b>3</b> 1		8 8	3 8	8	8	1	B
(a) thk (a)		8.4	35 n	전 전	P. 10	7	2	2	=	=		_	33	-	d a	2	9,40	7.8	16.23	I6.48	6. 58					# 15 C	n a	17.88	2.38			3 1 d a	4	9.30	1.50	_		<b>3</b>	e s xis		e e	#1 rd	: M	9.6		
thk (a) thi (a) thk (a		9.80	_	2	<b>2</b> 7	3	3	3	=	8	=	2	R	8 :			18	8	2	1.32	1.78	_	2	12.58	4 2	8 8	R		3	Ħ	8	2 5	3	8	8	8	 8 i	7	<b>37</b> 8	_	2 8		8	2	2	B
W.	_	8	_	3 7	3	8	8	=	7	82.	8	_	_		1		8	8	1 8	=	=	=	2	2 : 2 :	3 :	B 8			=	.61	의 : 유 :		2	83	xi B	_	_	_	<u> </u>		i	_		15.		
*	2	<b>A</b>	2 2	<b>*</b>	=	=	2	2	- -	82	8	一 用	3	n :			2		=	:	:	=	8:	<b>3</b> :	8 :		3 2		8	8	<b>2</b> :	^ 8 1	i wi	20	10 3		元:	• •	#	* :		8	; <del>-</del>	3	1	j
* * *	9	3	15 13	 	<b>.</b>	<b>3</b>	<b>3</b>	2	ري 13	5.	Si Si	<b>1</b>	2 :	<b>.</b>			2	4	=	<u>د</u> 1	<u>.</u>	- 2	ei :					· ·	2	4 2			12.3		9.	_	_	_	e :	ri e			_	9		i
	86	<b>*</b>	元	<b>s</b> i	si st	gi :	8 :	gi R	 	g 2	si =	<b>x</b>	<b>%</b>		8 8			9 10		8	100		=	<b>3</b> 9				8	F. 98. A	1.65	8 t	gi gi	=			8 % <b>4</b>			86					_	100	7
	9	9	ان در	9	<b>م</b>	e .	7	-i	2	2 0.0	3 6.0	- E	<b>a</b>			-	9	3 0.1	9	•	9.6	3		3 ;		-			3	2	= :			_	7	_	_	_	<b>8</b> 9				•	•		•
3	9.0 49.	•	3	<b>.</b>	•	•	•	•	•	-	•	•	•	L. 14.8				_	_	_	_	_	_	_	_	5. % 5. %			_	_		, K		_	•	-	_		. b. lb. l			-		_	_	j
3	63288	66298		•		•	-	617648	62248	62728	# 46488	46888	47368	467200	1	4928	497688.	542400	597288.(	1 51288B.	516888.	12216an.	25488	33128	1000	2452	1			364888.	569686.	2/44	26488			_			4/648	40000						
3	535286.	453688.	44888B.	111000			256 <b>8</b>		2268	22568	415288.	415288.	41528	120		<b>1</b> 25	415200	415200.	415288.	415200.	415288.	415286	15.00	150		A SOME	415200	415280.0	415286.	415200.	1500	A September 1	152	4152BB.	415288.0	41040E	41040	-		444000	4 104.00	410400	4:0400.0	110400.1	410400	TO TAKE
(dea)	3	79.917	79.917	79.918	75.58	2		2	73.786	3.63	81.377	32.326	91.276	9 2	A1 13	61.075	81.825	88.975	86.255	88.874	<b>80.</b> R24	26.77	724	67.674 10.674		5/2		88.423	80.372	22 명	<b>317.72</b>	3 2	121 7	179.00	88. EEL	91.376	92.13	81.276	9	77.10	2 2	41.075	81.825	88.975 410466.8	55	5
(deg)	31.947	31.214	31.178	31.127	31.863	31.063	28.5	31.052	31.061	31.861	30, 671	30.871	30.07	38.872	28 A72	30.872	30, 672	38.872	38, 872	30.872	30.872	30.075	120.671	10.87	38.07	20 071	30, 871	36. 670	38.878	30.678	20 m	18. (B)	38.869	39.668	39.668			_						_	_	
(sq. ke)	1		2.973		7		23. <b>24</b>				-		_								-		-		•				-						-			<b>3</b> 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		4.308 3		23,040				
(sq.ka) (deg) (deg) (m)																																														
1	5	모	7	2	2		E .	2	H593	H39	Q	9	2		1919	ĝ	H5169	1010	100	Ø	<b>9</b>	101	SIG	91104			1019	HSIZI	2153	200	12121	0 X	15127	H212B	H2129	10146	16147		FIG.	C101	1	H5152	15153	H5154	H5155	3

JTILE STALED TITM ZIRCON Scount Scount Scount Scount		<b>\$</b> 5		2	R 2		<b>3</b> 5			2 2	1.8	3 8 4 -		2 2	6.7	2 2	-	8 8 3 3	3 5	8	<b>8 6</b>	<b>8</b> 5 €	4 6	2 8	8.	2 2	2 2		R 8		2 2	2
TITON Acoun		R :	15.7	9.69	4 4 8 8	17.0	2.5	16.9	16.50	# # # # # # # # # # # # # # # # # # #	2	8 \$ 4 d	4	2 A	6.66	9 9	80.65	# S	12.45	13.80	12.30	5 8 8	13.30	15.30	16.78	17.8	17.8	-	16.8	15.4	12.7	98.3
STALIND TITAN . Acount Acou		3 2	3 3	2	<b>2</b> 2	<b>8</b>	<b>8</b> 8	4 4	2.38	2 2	1.6	<b>8</b> 8	=	=======================================	8	- Z	=	2 2	8.8	8.	1.8	÷ 5.	2.18	4 5	8	8 8 4 M	W W	<b>8</b>	# 5 C	27	2. S	A
		3 3		=	= =	3	8 3		=	8 3	2	3 5	=	2 2	3		=	2 A	37	3		<b>3 2</b>	2 2 3 3	2 2	3	2 2		3			3 3	2
3		3			3 3	3	3 3		=	8 7	. 7	3 5		2 2		2 2	3	8 8 -	37	3				33	3	2 2					3 3	4
CHATERN PLICESN UP, NICC 10, NICC LIL, NICC NA. BOTS CHABRON CLART? K. FLISS P. FLISS HAVING PASPHRT NOW? this (a) this (a) this (a) this (a) this (a) this (a) this (b) this (b) this (b) this (c) this		3		2	3 1		3 3			3 3							3	::	33			= =	33					3	3 3	3 3	2 2	3
VOLING P	200	<b>8</b>	7 7		<b>3</b> 8	<b>8</b>		<b>R</b> 8	1.68	3 7	1.68	2.7	1.3	<b>8</b> 7	3	<b>3</b> 3	<b>8</b>	بر بر 12 کا	10 M	2	4 2 7 2 8 3 9 3	1.2	8 3	3 8	2	3 R a r	3 8	33	# 8 # 0	1.7	3 8	9
FLBSP H Acount	V	# 6 신	<b>7 9</b>	2	2 S	 	<b>第</b> :	# # 	= = =	# <b>3</b>	2.78	# # • •	8	2.3	3	2	8 9	2 E	# S	3 2	1 m	# # # #	2.5	20 0	8	8 <b>3</b> m m	3.6	4 M	3 5	<b>3</b>	<b>3</b> 70 00 00 00 00 00 00 00 00 00 00 00 00	4
FLDGP P. Acount		<b>8</b> 2			<b>*</b> 5	8 .	20:1	<b>3</b> 8	3	2	3 7		2 2	25 5	1 A	3 3		2 2	2 :		50.5	2 2 2 2 3 2	8 8	2 8	*	2 2	25	3 8	3 3	7 A	27.5	
Acount		8.3	7 S		2 1 2 1	80 · 50	8	R 2	# # # # # # # # # # # # # # # # # # #	85 58 85 58	3	27.53		9 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	3 5	2 S	3	8 % 8 %	2 2	3.5	= #    G   K	25 25 25 25 26 25	3.5	2.3	1 8	2	89.38	8. S	<b>3</b> 5 8	18 is	82.28 83.28	62 50
FIREN PLICEN UP, NICE ND, NICE LH, NICE WE BOTS OVERSON GLINTZ K the (a) the (a) the (a) the (a) the (a) the (a) the (b) the (				* <b>3</b>			-			• -	-	20 M	_	•	39.68		•			_						2. 15 25. 15 26. 15	2.8	8 8	<b>8</b> 8	1 2	2 8	1 5
This (m) (		<b>3</b>		-71.8			<b>#</b>	<b>8</b> 8	3			-72.10		-177.60 3		-7.4		-74.28	-							75 F			2 1	2 2	28 8	
MICC 194.		8	167- 1845 C		平 3 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		8	8 1	12	24.80 -112	전 - 약 :	7- 85	2 E0 -14	77- 81	7 m	7 25						4.98.4			3 8	13.48 12.48 13.48 14.48 15.48			4.8 -74.	21.88 -11	2 5	
MICC LIL. ht (a) t		_		19.61					-	-	8 8								2.5		2 F. E.			21		24.28		  	8 5		8 8	
(10C 10). ak (a) t				3 22			6.10 24			स्य म <b>ड</b> ्ड	5 A				; = ; =			33			8 8 8 8	8 4		2		2 2	2 2		9 2		23	
LOEN UP. I In (m) th		17.10	<b>成</b> 5	27.30	14.10	24.28		3 :	21.20	33.53		<b>3</b> 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	24.28	8	7 7	3 8	3	34	3.6	18	۳ ج	2 2 2	80.8		8	\$ 15.50 \$ 15.5	8	តិន	22.53	# # # # # # # # # # # # # # # # # # #	35.45	10.04
EIBN PLIC k (m) th			급 :	27.38	2 :	8 19	8	3 :	1 3	-									13.28		8 KI				11.10	10.10 10.10 23.10 23.10		3 8	<b>R</b> 5		3 8	•
		11.10	= : = :	# 22 # 24	= 1	ried R S	=	변 : <b>8</b> :								_	2 to 13 to 1			3 2	= = = =	2 2				2 2	_	<b>■</b> =	8:		3. S. S. S. S. S. S. S. S. S. S. S. S. S.	di R
7 CLAY		2	<b>a</b> :		2			= ;	= = 8 #	3 2	4 4							1.28 1.			- -					21		3 3 8 8			88	ייי
SILT A M 1		•	3	<b>i</b> a	. <b>.</b> .		-	<b>d</b>	ئە ق	<b>d</b>	- ~	<b>-</b> ;	٠ ـــ	mi e	4 4	<b>-4</b> -	4 41		4					, -, ,								
2500 x	: [		2	13	2	2 2	2	<b>8</b> :	2 3	3	8 8	8 :	- 2 2	8	 					2 8	2 1	= 8			::	88						_
#E	. 1	100.0		97.50	10.0			8 i		3.6	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	F 18		23.25				2.5	25	2 %				9							3 3	6
H GROVEL	-1	6 6.00 100.0	0.00 10.00	3 0.10 97.50	2 6.00 100.00		4 6.00 100.00			8	# # F	3	. 6.30 GB.72	2	0.00 St. 70 0.00 St. 20	93.65	5.55 St.1	0.66 97.80	25.55	F. 18 55.78		# 18 18 18 18 18 18 18 18 18 18 18 18 18		8.8		2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			99:38		28.45	10 M
EPTH (6)		-	-	6.0 30.1 6.00 100.00 6.0 12.3 6.10 97.50				0 36.2 6.00	45.6	41.2 6.00	4.5	13.8 0.00	B. B. 46.1 B. 30 GB. 78 B. 78 L	0 128.1 6.78	1 49.7 18.30 64.70 1 1 15.3 18.00 98.30	16.8 6.00 99.60	13.5 1.38 53.58	14.7 0.60 97.00	17.8 6.28 99.18	26.1 6.00 55.50	21.3 4.46 160.00	24.2 4.00 100.00	9 10	29.6 0.8 18.8	31.6 6.00 100.00	33.1 % 0.00 100.00	X. 1 . 2 . 3 . 3 . 3 . 3 . 3 . 3 . 3 . 3 . 3	37.6 9.8 35.36 33.1 p. 6 35.36	19.6 0.00 99.90	42.5 5.00 33.40 42.3 5.00 39.10	44.3 0.28 98.48	46.7 BC.98 No.CB
EAST DEPTH		0.216800.0	<b>221688.0</b>	47 35 M.	531200.0	238.00	545600.0	350406.0 36.2 6.00	35,000 44.5 p. 00	SCABOR. 0 41.2 0.00	55% AL 6 4.5 6.40	478448.0 13.8 0.00	59488.0	5 58688.0 126.1 6.76	553566.0 49.7 6.30 65.70 1 46226.0 15.3 6.60 96.90	442008.0 16.8 0.00 99.60	454446.0 13.2 1.30 93.90	47368.0 14.7 0.68 97.80	46296.0 17.0 0.20 99.10	8 492000.0 20.1 0.00 99.90	8 497686.0 21.3 8.00 100.00 8 September 22.7 8.00 100.00	597290.0 24.2 4.00 190.00	0.51200.0 25.6 0.00 100.00	221586.0 28.6 0.00 100.00	0.531206.0 31.6 0.00 100.00	0 535000.0 33.1 × 0.00 100.00	545500.0 36.1 0.00 100.00	SSEMEN ST. 6 0.00 35.30	8 497686.8 19.6 8.00 99.98	6 55,0000.0 44.6 0.00 55.40 8 55,400.0 42.3 0.00 55.10	56568.0 44.3 8.20 98.40	2/448.0 45.7 0.30 No.00
NORTH EAST DEPTH		410408.0 516808.0	416488.8 521588.8	410400.0 325400.0	410408.0 531208.0	A10400.0 538000.0	410408.0 545608.0	419498.8 359488.8 38.2 8.88	41948.1 3328.0 59.0 0.00	410408.0 SEASOR.0 41.2 8.00	AIDMALD 55558.0 42.1 0.20	424806.0 478406.0 13.8 6.00	410400.0 575200.0 410400.0 504000.0	418468.8 588888.8 128.1 6.78	410400.0 333500.0 45.7 8.30 63.70 1 424500.0 45230.0 15.3 0.00 90.90	424600.0 446000.0 15.8 0.00 95.50	42568.8 46488.8 %,4 8.38 83.78 42568.8 45888.0 13.2 1.30 93.98	45580.0 473580.0 14.7 0.60 97.00	46560.0 46200.0 17.8 0.20 99.10	455.00.0 455.00.0 13.2 0.10 33.70 455.00.0 452.00.0 20.1 0.00 59.90	46580.0 497600.0 21.3 0.40 100.00 445500.0 59240.0 22.7 0.50 100.00	46568.0 597286.0 24.2 4.00 190.00	4658.0 51288.0 25.6 8.00 108.00	445500.0 \$21500.0 \$0.6 0.00 100.00	465600.0 325400.0 30.1 0.00 100.00 465600.0 531200.0 31.6 0.00 100.00	465640 53688.0 33.1 × 0.00 100.00	455.00.0 5455.00.0 36.1 0.00 100.00	445560.0 355460.0 37.6 0.00 39.30	424680.8 497680.8 19.6 8.80 99.90	485680.8 564880.8 48.6 8.88 99.48 485580.8 554880.8 42.3 8.88 99.18	465600.0 569600.0 44.3 0.20 98.40	400690.0 3/4480.0 4b./ 0.30 30.00
NORTH EAST DEPTH		410408.0 516808.0	50.774 41648E.8 S2168E.8	81.276 42488.0 47358.0	86.674 419486.0 \$31288.0	M. 624 410400. 0 535000. 0	56. 523 41040E. 0 54550E. 0	86.473 419488.8 359486.8 36.2 8.88	50, 423 419449, 0 33229, 0 35, 0 1, 10 50, 373 41949, 0 35,000, 0 40, 6 0, 80	66.322 416480.0 354880.0 41.2 0.80	68,272 419480,0 359580,0 42,1 6,20	81,225 424600.0 478400.0 13.8 0.00	20. 172 410400.0 579200.0	80.072 419400.0 566000.0 124.1 0.70	DOL. RE2   410-400.0 593-500.0 49.7 8.30 6.30 63.70     A1. 176 424-500.0 482-500.0 15.3 0.00 90.90	81.126 424690.0 462600.0 16.8 0.00 99.60	81,376 455680,8 464880,0 514 81,38 83,78 81,38 45580,8 45480,0 13,2 11,38 93,98	A1.276 405604.0 473504.0 14.7 0.66 97.00	81.175 405640.0 402340.0 17.8 0.29 99.10	81.125 45546.0 45599.0 19.2 0.10 55.76 81.075 45560.0 45200.0 20.1 0.00 59.30	81.025 40550.0 497500.0 21.3 0.00 100.00 to 40.00 100.00 to 40.00 100.00 100.00 to 40.00 100.00 100.00	80.925 485680. 587280.0 24.2 0.00 100.00	80.873 465566 512984 6 25 6 9 9 9 9 9	80,774 46560.0 521600.0 20.6 0.00 100.00	50,724 40560.0 325400.0 30.1 0.00 100	80.624 40560.0 53600.0 33.1 × 0.00 100.00	20.523 405500.0 545500.0 36.1 0.00 100.00	88,473,46569.0,539468.0,37.6,0.00,39.39. An A23,445580.0,535290.0,33.1,0.00,99.70	81.025 424888.0 497689.0 19.6 0.00 99.90	88,373 46568.8 558889.8 44.6 8.98 55.48 Ap. 223 46588.8 55488.8 42.3 8.89 59.18	88,273 485680.0 569680.0 44.3 0.20 98.40	86.222 445686.0 5/4486.0 46.7 0.30 35.00
NORTH EAST DEPTH		30.628 50.624 419400.0 516800.0	30.628 50.774 416480.8 521680.0	26, 826 BB, 724 419440, 0 525440, 0 26, 958 B1, 775 42490, 0 47350, 0	38.828 88.674 419488.0 531288.0	30.828 50.624 410400.0 335000.0	30.626 56.523 410400.0 545600.0	30.627 66.473 419406.0 559466.0 30.2 0.00	36, 627 56, 423 419446, 8 333266, 8 45, 8 6, 8 36, 627 56, 373 419466, 8 55866, 9 46, 6 6, 8	30,627 86,322 410480,0 554880,0 41.2 0.40	34,625 84,272 419494,0 55%84,0 42.1 9,23 34,836 84,222 419484,0 574484,0 44,5 9,40	30.956 81.226 424800.0 476400.0 13.8 0.00	30, 625, 50, 172 419400.0 575200.0	30, 825 84, 872 418488, 8 586888, 8 128, 1 6,78	38,625 86,621 410486 353586 9.7 8,30 83.70 1 36,55 81,176 42486 64258 815,3 0.66 56,50	39.558 81.126 424888.0 448888.0 16.8 8.80 95.60	38,765 81,376 45548,6 45488,6 544 8,38 85,78 30,78 30,76 81,355 45548,6 45888,8 13,2	38,785 81,276 48560.0 473600.0 14,7 0.60 97.00	38,765 81,456 WESSEL 46288.0 17,8 6,29 59,10	38,765 81,123 465681,8 465881,8 13,2 8,19 75,78 38,785 81,675 465681,8 452881,8 28,1 6,10 59,59	38,785 81.025 46569.8 497588.8 21.3 8.00 100.00 3 2 3 2 3 2 3 2 3 3 3 3 3 3 3 3 3 3 3	34.765 84.925 45560.0 507200.0 24.2 4.00 100.00	38,785 Bitel 4,45560,8 51200,8 53,6 8,00 100,0	34.765 08.774 46560.0 \$21600.0 28.6 0.00 100.00	38,765 56,724,46560,0 325400,0 31,1 0.00 100,00 32,765 58,574,46560,0 531200,0 31,6 0.00 100,00	30, 785 80, 624 445600, 535000, 0 33.1 × 0.00 100.00	38,784 BB.523 46560.0 54500.0 34.1 0.00 100.00	36,784 86,473 46568,8 358488,8 37,6 8,89 39,39 36 36,34 An An An An Ansterna 18508,8 33,1 8,86 59,78	38,556 81,625 424886.8 497688.8 19.6 0.00 59.90	39,784 89,373 465690,8 558990,8 44.5 8.99 95,48 39,784 89,783 46,586,8 554890,8 42,3 8,89 99,18	30,783 60,273 465600,0 559600,0 44,3 0,20 98,40	26.763 BB. 222 45569.0 5/448.0 45./ 0.30 35.50
OGITLOE NORTH EAST DEPTH (deg) (m) (m) (m)		30.628 50.624 419400.0 516800.0	30.628 50.774 416480.8 521680.0	81.276 42488.0 47358.0	38.828 88.674 419488.0 531288.0	30.828 50.624 410400.0 335000.0	30.626 56.523 410400.0 545600.0	30.627 66.473 419406.0 559466.0 30.2 0.00	50, 423 419449, 0 33229, 0 35, 0 1, 10 50, 373 41949, 0 35,000, 0 40, 6 0, 80	30,627 86,322 410480,0 554880,0 41.2 0.40	68,272 419480,0 359580,0 42,1 6,20	30.956 81.226 424800.0 476400.0 13.8 0.00	20. 172 410400.0 579200.0	30, 825 84, 872 418488, 8 586888, 8 128, 1 6,78	DOL. RE2   410-400.0 593-500.0 49.7 8.30 6.30 63.70     A1. 176 424-500.0 482-500.0 15.3 0.00 90.90	39.558 81.126 424888.0 448888.0 16.8 8.80 95.60	38,765 81,376 45548,6 45488,6 544 8,38 85,78 30,78 30,76 81,355 45548,6 45888,8 13,2	A1.276 405604.0 473504.0 14.7 0.66 97.00	38,765 81,456 WESSEL 46288.0 17,8 6,29 59,10	81.125 45546.0 45599.0 19.2 0.10 55.76 81.075 45560.0 45200.0 20.1 0.00 59.30	38,785 81.025 46569.8 497588.8 21.3 8.00 100.00 3 2 3 2 3 2 3 2 3 3 3 3 3 3 3 3 3 3 3	34.765 84.925 45560.0 507200.0 24.2 4.00 100.00	28, 326, 326 B1.87, 545,081,8 512,081,8 53,5 6.00 104,08	34.765 08.774 46560.0 \$21600.0 28.6 0.00 100.00	50,724 40560.0 325400.0 30.1 0.00 100	30, 785 80, 624 445600, 535000, 0 33.1 × 0.00 100.00	MA 38,784 08.523 46560.0 54500.0 34.1 0.00 100.00	88,473,46569.0,539468.0,37.6,0.00,39.39. An A23,445580.0,535290.0,33.1,0.00,99.70	38,556 81,625 424886.8 497688.8 19.6 0.00 59.90	88,373 46568.8 558889.8 44.6 8.98 55.48 Ap. 223 46588.8 55488.8 42.3 8.89 59.18	30,783 60,273 465600,0 559600,0 44,3 0,20 98,40	88. 222 465688.0 5/4488.0 45.7 0.30 35.00

BEDREIR OFFSLORE MINERALS RESESSENT MODEL. page 15

NECON12	Krount	8.4	9.3		2 2	R 2	9.6	27		2 2	8 5	2 2	0.60	2 8	R 85	=	2 2 4 -		8 3		2 2		8 8	2	2 A		2 2	2	3;	2 2	8 .	8.3	8 1	3 3	3	38 7	2 8
IITON Z	Acount		35	R 21		2.60	4.8	# :		4	8 %	7 8 4 M	4.0	2 × ×	7 P	6.00	<b>8</b> 7 <b>8</b> 7 <b>9</b> 7		17.00	9.5	16.88	3 5	2 E	S	= g	8	3 8	2.3	<b>8</b>	<b>3</b> 8	P '9	6.28	ल ह ज र		2 2	20.00	# # # # # # # # # # # # # # # # # # #
STALRO T	Acount		1.28	8.	_ `	R 85	8.4			8	25	2 2	2; -	2.3		8	2 8	88	8 1	2 8 4 m	8 5		8 B	87	م ج ج	7	2 S	8	8	7 S	8	_		 8 8		33 1	2 8
AUTILE ST	Count	8.4	8 3		= :	3	33 4	2 2		2	25 8	_	_	2 2		8	= =		8 3		2 7	3	2 S	8:	8 8	8:		3	3 :		8	8	8 4	2 7		2 1	;
75	Scount Scount Scount Scount Scount	8.1	2 1		8 :		93	21		2	2 t		=	8 1		8	3 3		8 5			3	2 2	8:		8:	2 8	3	3 :		8	=:	= =	- 5	=	8 1	
K.F.LISP P.F.LISP HYMING PISSHRT NDARZ	count	81	= 3		3		=				31		8	3 2		8			8 2		3.5		 	8		8:		8	<b>3</b> :		3	= :	2 1 2 1		8	2 1	1 3
ALMS PR	Scount 1	82.	# E								a s		8	នុន		= 1	7 3	8	31	i A	2.5	8	8 2	8:	33	7:	2 7	3	3 :		3		 	3 3	<b>三</b>	# 4 # 1	
LIESP HAY	Ycount 8	3		3 37	3 5	2 周	8	서 6 목 8	B #	8	27 - 87 8		8	- - -		m :	 8		M = =	- W	તો તો જિલ્લ	_	 2 2	2	- 	8:	i ai	mi 2	m r 8 8	: d		તાં ત જીવા	ni -	- - - - -	<del>-</del>	mi - ≘ g	: :: : ::
169 P.F	Acount %	.2.		; .di	<b>3</b> 1	é é	8 8	*	# M		તાં ત શ ક	] ~i		 2			# M R B		3 T	1 2	તો તો જી. જી		તાં તાં જ જ	mi o	i	21		ui	ei .	;			2 Z		2		3 m 8 m
11	Scount Sc	3	4 • 8 8		2:		•	# •		-	22	: =		<b>8</b>		31	8 3				9 9	-		-		33	; <u>-</u>	3	3 ;		-	37			-		
	3	20 OB.	æ. 9	g	g :	3	<b>8</b>	5 8		8	81 8	<b>3</b>		# F	2 2		2 K	<b>5</b>	<b>3</b> 5	34	2i zi	3	2 2	223		91.6	i și	_		2	84	34 S	2 3	i gi	83.		. S.
	## (9)	4	≓ ₹		3		42.4	7 8	j #	4	3 2	8	37.2	d a	ä		= 0 5 ×		37.61	45.9	25 25 26 25	68.8	ਸ ਹ ਸ਼ੀ ਐ	77.7	ž xi		Ki	47.11	2 2	\$	47.0	47.9	# 4°	1 1	#	# a	39.4
20 ME 20		-	22-	-		1	F.87-	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		- FE	***	47.4	<b>—</b>	7 7	#	# F	4 55	M 18			4 121 - 121 -	F.151-	# # # # # # # # #   -	-7.6	-76.0	3	対グー	2.3	= 2 <b>\$ \$</b>		-66.58	# S	3				
MO. NIGO LAL NIGO		*	<b>≅</b> ₹	-			7.	# F	; <b>4</b>	6	87 S	5	11.98	R 전			다 년 당 왕		# F		<b>2</b>	17.38	e e	8.3		3 3		3.	7 7 5 6	3	5.5	20 5	R R			16.28 16.28	
		<b>M</b>			2 8	4	19.2	2	: :: :::::::::::::::::::::::::::::::::	3	2S	8	ສ :	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	24.68	2 8	3 3 3 3	24.60	# # % %		3 8 8 #	N I	d ~	8j k	1 2	33	# ස්	25.5	7 S	= 5	82°52	# # # #	2 F	8		<b>2</b>	24.8
GLATERN PLICOEN UP. NICC		=			3 3		3	2 A	3	8	<b>3 3</b>	3			3	3 3		3	2 2		=======================================	3		3 5		3 3	3 -	3			=	3 3		8	=	3 1	8
A. 1005		zi zi			# # # # #			3 3 3 3			2 E	75 75		គ <b>3</b>	21.28	83 ×			ත ද ස් ස්		8 R A ‡	# 5 24 2		16.38 16.38	# ±	3 3	\$ <b>3</b>	27.38	7 F	37.60	<b>8</b>		3 37 3 15	2		æ æ = æ	# # K
DENTERN AND AND AND AND AND AND AND AND AND AN			<b>3</b> 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	=	<b>4</b> 2	12.20	2:			 	2	19.68	=======================================	3 5		3 .	2 <b>8</b>	13.10	R 8	7.30	8 3 19 18	8 t	ಕ ನ	3 1		3 :	12,28	3.5	R 2	8	8	<b>3</b> 5	R 3	! <b>8</b>	8.5	7 E	8 8
	ŝ	7		39	# 5 4 e	8	<b>X</b>		8	8	3 3		8 1			2 1	3 8	8 2	<b>3 3</b>	=	2 =	3 8	3	3 1	2 2	<b>#</b> 8		82 :			3	<b>8</b> 1	1 3	8	2 2		3
_	×									_	-	_	_		_		•	-	9 4	_		•		• "	-	~ -	. –	_		•	•	•	_	_	_		
98 1	- 1	<b>3</b>		.g	# 5 * •	3	<b>7</b>		8			=	8 1		3	2 2		2		7	32	1.28	3 <del>3</del>	28		2 % % %		8.2	3 2	=	2				2 3		2
as '	2	77.30 9.90		66.98 6.00	<b>用される</b>	99.00	95.28 6.30	25.70 pt.10	99.38	8.8 .8		M. M. A. M.	81							99.44 P.38				2 2	_		_	99.38	2. 48 P. 28		8	8 8	29.28	9 9	90.00		0.00
	× × ×			1.30 86.90 6.40	元子 RSS R-	6.30 99.00 6.40	6.23 99.24 6.24	4.10 55.70 4.10 0.80 180.80 0.80	6.00 99.30 6.00	0.00 100.00 0.00		6.00 100.00 6.00	C. C. L. C. C. C. C. C. C. C. C. C. C. C. C. C.		C. C. C. C. C. C. C. C. C. C. C. C. C. C			0.00 10.00 0.00		0.16 99.46 p.38		6.70 97.60 1.20		2 2	_	2 3 3 3	_	6.30 99.30 0.20 5.30 0.30		29.58	8		C. 00 - 25: 20 - 4: 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	_	0.00 100.00 0.00		0.00 100.00
BROVEL	× ×	3 6.30 77.		1.38	25 25 25 25 25 25 25 25 25 25 25 25 25 2	2	<b>8</b>	23.9 4.40 195.70 45.10	8	21.2 6.00 106.00 6.00	24.1 0.00 39.30 0.00 24.1 0.00 39.30 0.00	25.5 6.00 100.00 6.00	28.9 0.00 198.00 0.00		31.0 6.00 100.00 6.00	No. 5 4.00 100.00 4.00		8 2		2			2.50 91.30	2 2		2 3 3 3	4.00 100.00	<b>8</b> 6		0.10 99.80	0.00	8 8	2	3	2 3	28.4 p. 10 100.00 p. 10	29.8 0.00 100.00 0.00
TEMEN BROWER	10 K 7 K	47.3 6.30 77.		10.4 1.30	2.7	0 15.7 6.30	0 17.1 0.20	23.9 0.00 1	19.8 0.00	•		•	-	-			34.2 0.80	12.0	37.4	9170 979	43.6 4.10	46.8 6.70 97.50	186.7 2.50 91.30	27.6 0.00 100.00	29.2 6.40 180.40	11.0 5.30 85.40	30.6 0.00 100.00	0.0 16.0 10.30	16.6 6.20	.0 19.4 0.10 99.00	.0 28.5 0.00 99.98	21.6 <b>2.8</b> 25.26	24.5 C.8	25.0 0.00	27.1 0.00	1500.0 28.4 p. 00 100.00 0.00 1.00 1.00 1.00 1.00 1	•
ENST DEPTH BROWEL		39360.0 47.3 0.50 77.	59728.8 22.1 6.80 186.	.0 464688.0 10.4 1.30	0 452000.0 11.7 1.90	.0 478400.0 15.7 0.30	0.462500.0 17.1 0.20	. 0 5120m. 0 23.9 4.00 1	.0 492888.0 19.8 8.00	0 497640.0	. 0 50728. 0	. 6 512000.0	. 0 516800.0	25486.0	6 531286.0	51698.0	0 540000.0 34.2 0.00 I	0.545500.0 35.0 0.00	0 555204.0 39.1 0.10	0.26000.0 40.0 0.10	0 369600 43.8 0.10	\$ 574486.8 46.8 6.70 97.68	0 554000.0 100.7 2.50 91.30	5 22 (540.0 27.6 0.00 100.00 1	525480.0 29.2 0.00 180.00	1 464000.0 11.0 5.30 89.40	S31298.0 38.6 8.00 100.00	1.0 473500.0 15.0 0.30	0 442900.0 16.5 0.20	8 48888.8 19.4 8.18 99.88	8 492888.8 28.5 8.88 99.98	8 497640.0 21.8 0.00 99.90 (	507200.0 24.5 0.00	0 512000.0 25.0 0.00	0.516800.0 27.1 0.00 1	320 Em.	0.526400.0
MORTH EAST DEPTH BROWEL		R22 405640.0 593640.0 47.3 0.50 77.		496588.8 454688.0 18.4 1.38	400000.0 468000.0 11.7 1.30 400000.0 473500.0 14.3 0.50	48688.8 478488.8 15.7 8.38	400000.0 462200.0 17.1 0.20	424894.0 512000.0 23.9 0.00 1	400500.0 492800.0 19.8 0.00	40000.0 497600.0		40000.0 512000.0	486588.0 516888.0	468688.8 \$25488.0	400000.0 531200.0	440000.0 336000.0 424900 0 516900 0	40000.0 S4000.0 34.2 0.00 1	40000.0 SASSOLO 35.0 0.00	40000.0 EEE00.0 39.1 0.10	40000.0 56000.0 40.0 0.10	48888.0 36958.0 43.8 0.10	486080.0 574480.0 46.8 0.70 97.50	40000.0 SHOOT.0 162.7 2.30 91.30	424006.0 121500.0 27.6 0.00 100.00	424800.0 525400.0 29.2 0.00 100.00	396000.0 464000.0 11.0 5.30 89.40 755000.0 11.7 3.30 00.40	424698.8 531299.8 38.6 8.00 100.00	335000.0 473500.0 15.0 0.30	355000.0 4/5400.0 1/.3 U.30	396800.0 468000.0 19.4 0.10 99.80	336666.6 492860.8 20.5 0.00 99.96	335,000.0 497,640.0 21.0 0.00 99.90 (	395808.0 587208.0 24.5 0.00	395000.0 512000.0 25.8 0.00 1	396888.8 516888.0 27.1 0.00 1	395000.0 521500.0	396000.0 526400.0
MORTH EAST DEPTH BROWEL		781 80.82 40568.0 59368.0 47.3 6.59 77.	XX 08.7/3 42408.0 36248.0 28.3 0.80 180. XX8 08.92 42408.0 58728.0 22.1 0.80 180.	81.376 400000.0 464000.0 10.4 1.30	81.276 400000.0 468000.0 11.7 1.90	81.226 48698.8 478488.8 15.7 8.30	81.176 400000.0 483200.0 17.1 0.20	81.123 ************************************	81.073 406500.0 492800.0 19.8 0.00	81.625 400000.0 497640.0	40000.0 50728.0	88.875 44688.4 512888.8	2 04. B24 40000. 0 51600. 0	58. 724 48568.8 \$25488.8	88.674 48888.8 531288.8	51698.0	26.574 40000.0 54000.0 34.2 0.00 II	1 80.524 488880.0 545580.0 35.8 0.00	8 86-423 40600-0 535200-0 33,1 0,10	0 00.373 40000.0 560000.0 40.0 0.10	48888.0 36958.0 43.8 0.10	00.223 40000.0 57440.0 46.8 0.70 97.60	00.123 40000.0 58400.0 100.7 2.50 91.30	20.774 424846.0 221580.0 27.6 0.00 100.00	86.724 424888.8 525488.8 29.2 6.88 188.88	1 81.376 396000.0 464000.0 11.0 5.30 69.40 11.1 34.395 34.00 40 40	A. 673 424884.8 531280.8 30.6 8.80 100.00	81.276.396000.0 473600.0 16.0 ° 0.30	61.175 395460.0 445260.0 16.6 0.20	81.125 396aan 8 468aan 8 19.4 8.18 99.88	81.073 396400.0 492800.0 20.5 0.00 99.90	AI. (C.) 356000.0 497600.0 21.8 0.00 99.50	26. 925 395000.0 587200.0 24.5 0.00	80.875 395000.0 512000.0 25.8 0.00 1	88.825 39686.0 516886.0 27.1 0.80 p	00. Ec.3 424000.0 335000.0	88.724 396888.8 526488.8
LATITUDE LOGITUDE MORTH EAST DEPTH GROWEL.		38,781 86,822 465686,8 593586,8 47,3 6,59 77.	34,556 04,975 42404.0 34724.0 24,5 0,00 100.	39.741 81.376 400000.0 464000.0 10.4 1.30	38.741 81.275 400000,0 465000,0 11.7 1.30	30.742 81.226 446698.0 478488.0 15.7 6.30	30.742 81.176 400800.0 462200.0 17.1 0.20	38.75 86.874 424886.8 512886.8 23.9 8.88 1	38.742 81.875 486580.0 492888.0 19.8 8.80	30.742 81.025 400000.0 497640.0	34.742 54.925 48688.0 59728.0	30.742 66.875 40600.0 512000.0	38.742 68.824 468888.8 516888.0	30.741 50.724 40000.0 226400.0	38.741 88.674 40000.0 531288.0	30,741 50,624 40500,0 53500,0 30,956 Ab 624 42400 0 51500 0	30.74 26.574 40000.0 54000.0 34.2 0.00	34.741 80.524 488880.0 545568.0 35.8 6.86	36.741 DO:473 40000.0 33040.0 37.4 0.00	35.746 50.373 40000.0 56000.0 40.0 0.10	36.746 db.273 40000.0 565500.0 43.8 0.10	38,739 68,223 46608,0 57448,0 46,8 6,76 57,60	34,739 Bil.123 40000.0 58400.0 104.7 2,30 91.30	38, 508 50,774 424696, 521690, 67.6 0.00 100.00 31, 730 A0 177 A0 40 40 50 50 50 50 50 50 50 50 50 50 50 50 50	30.956 80.724 424880.8 525480.8 29.2 6.00 180.00	30, 696 81, 376 396900, 0 464900, 0 11, 0 5, 30 89, 40 30, 698, M, 725, 39500, 0 46490, 0 11, 7 3, 30 90 40	30.958 00.673 424800.0 531200.0 30.6 0.00 100.00	39, 696 81, 276 396000, 0 473600, 0 15, 0 130	36.696 81.175 395489.8 47299.8 16.6 8.28	30.698 81.125 39600.0 48800.0 19.4 0.10 99.80	30.696 81.073 396000.6 492800.8 20.5 6.00 99.96	34.634 A. 14.23 356404.0 497640.0 21.8 0.00 99.39 (3.00 6	30.696 86.925 396860.0 507280.0 24.5 0.00	30.698 89.875 395000.0 512000.0 25.8 0.00 1	30.696 89.825 39690.0 516890.0 27.1 0.00 p	38, 55d 58, 56, 774 395880, 8 521580, 8	39, 696 89, 724, 395,000, 0, 526,400, 0
MORTH EAST DEPTH GROWEL		38,781 86,822 465686,8 593586,8 47,3 6,59 77.	23,040 34,550 56,923 42400,0 59720,0 22,1 0,00 100,	3.654 30.741 81.376 404000.0 464000.0 10.4 1.30	81.276 400000.0 468000.0 11.7 1.90	23,846 39,742 81,225 496980,8 478480,8 15,7 8,39	30.742 81.176 400800.0 462200.0 17.1 0.20	23.646 39.558 59.674 424586.0 512886.0 23.9 0.80 1	23.646 38.742 81.075 406580.0 492888.0 19.8 8.60	23.040 30.742 81.025 40000.0 497600.0	23.040 38.742 56.925 400001.0 DEVISE. 0 23.040 38.742 56.925 400001.0 507201.0	23.646 38.742 60.875 40686.0 512860.0	23.649 38.742 68.824 49696.8 516896.8	23.040 30.741 06.724 40000.0 \$2640.0	23.040 30.741 00.674 400600.0 531280.0	23, 848 38, 741 88, 624 488888, 8 336888, 8 23, 848 38, 958 AR A24 424888 8 515888 8	23.049 34.741 Bb.574 40000.0 54000.0 34.2 0.00	1 80.524 488880.0 545580.0 35.8 0.00	23.040 30.746 80.423 40000.0 535400.0 35.1 0.10	23.040 38.740 80.373 40080.0 568000.0 40.0	23.046 36.746 db.273 40000.0 36560.0 43.6 0.10	23.046 38,739 68,223 46608.0 574488.0 46.8 6.70 97.69 21 448 38 720 48 172 48848 6 55008 6 173 48848 6 55008 6 173 6 188 6 173	00.123 40000.0 58400.0 100.7 2.50 91.30	23.040 38.536 30.774 (24308.0 E21680.0 27.6 0.00 100.00 17.15 15.15 30.734 30.875 American Southern Asia and As	23.046 30.956 20.724 424800.8 525400.0 29.2 0.00 100.00	30, 696 81, 376 396900, 0 464900, 0 11, 0 5, 30 89, 40 30, 698, M, 725, 39500, 0 46490, 0 11, 7 3, 30 90 40	23.640 30.958 80.673 424890.8 331290.8 36.6 6.80 100.00	39, 696 81, 276 396000, 0 473600, 0 15, 0 130	36.696 81.175 395489.8 47299.8 16.6 8.28	30.698 81.125 39600.0 48800.0 19.4 0.10 99.80	23.040 30.659 81.073 396000.0 492000.0 20.5 0.00 99.90	AI. (C.) 356000.0 497600.0 21.8 0.00 99.50	30.696 86.925 396860.0 507280.0 24.5 0.00	30.698 89.875 395000.0 512000.0 25.8 0.00 1	30.698 80.825 396000.0 516000.0 27.1 0.00 1	38, 55d 58, 56, 774 395880, 8 521580, 8	39, 696 89, 724, 395,000, 0, 526,400, 0

FLDSP MANNING PASPHET HONG RUTILE STRUNG TITRN ZINCON Scount Scou	8	R 8		=	<b>8</b>	<b>8</b> 3		3.5	8		#.T	F. 8	8	= :	= :		7 7			3	8	8	= ;	R #		8	3	3 /		8	8	2 8	R 8		2	<b>8</b>	8		= :	<b>8</b>	<b>!</b> !		2
Scount Scount		<b>1</b> 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 4	16.00	16.98	17.00			8	3	=	8	<b>8</b>	16.8	8	3.5	4	1	2 4	16.68	16.38	16.28	16.2	# 8 # :	17.	2	14.20	2 : :		15 8	16, 18	8 :		16.9	=	=	3	3	2	2 :	# 5 # 5		16.28
Scount A		2 2 M 7	1 -	2 5 mi	M M	# :	<b>8</b>	1 2		3	8	3	2.1	<b>8</b>	<b>3</b>		2 8	R 8	R 8	8	1.68	2.38	종 라	= 1 ~ .	2 g	2	S ri	3 t	4 1	1 80 1 mi	3.10	<b>8</b> :	1 ~	8 6 M	2	3	2	2	3	<b>8</b> :	7. 2.	# # # # # # # # # # # # # # # # # # #	8
RUTILE STRUMD TITAN Scount Scount Sco		3 :			8	= :					2	=	2	8	2	2 ;	7 7				::	1.2	3	<b>3</b> 8		3	<b>1</b> 38	3 3			=	3 3		3	2	=	2	3	2 2	2 1	5 3		8
MAZ R		3 3			=	= :					2	=	6.78	2	=	3	7 / d (	2 1		R 8	=======================================	<b>8</b> .	8	<b>7</b> 8		3	F.28	3 3	Į	3	8	= 1		3	=	=	=	2	2 2	2 1	7 2		8
SPART AD Acount		3 :			8	= :					8	=	2	8 4	2		2 2				8	8.4	3	= :		3	8	3			=	3 3			2	=	2	= :	2 7	= :			
MINE R		<b>3</b> 3	7 T	2 2 1 mi	3.48	<b>8</b> :	<b>3</b> 5	2 Z	3	8	37	87	1.78	8	7 S	2	3 1	7 A	7 R	3 =	8	2 3	<b>8</b>	의 :		: :	2.10	8 2	8 3	2 1	35.55	93.7	2 g	1 2	2.4	2.4	<b>8</b> 2	1.8	8 :	₹ { ;	2 5 7.1	3	8
FLDGP HV Acount						3 :			7			1.78		J 10	<b>8</b>	8 i	2 2	2 2	8 8	R 19	8	2.6	7	3 :	2 2	. S.	3.10	33 ; ~ ,	2 g	1 2	4.10	37 E		8 8	2.68	2.68	2.78	2. 2.	<b>8</b> 3	<b>3</b> ;	# T	i M	3
FLBSP P.		3 2	2 8	1 2			<b>7</b> 8			: 3		6.20		2.	8	2 :	2 2				2	80	2	3 7		1 S	F. 8	80 :	<b>2</b> 5	3	1. W	3 3			27	9.6	9.60	2	<b>7</b>	<b>8</b> :	2 7 - 4		
1.3		2 8	R			8.8		_			_		_		33 %	2	2 2	R 1			A S	8	91.10	2 3	2 2	3 3		= :		3.6	88.58	2.5		1	8	8	3.15	2.3	8.5	2	ភេទ ល់ខ	RR	
RIEBA FLOOSH UP.NICC MP.NICC LILNICC ML DOTS GARBRON RUPRTZ N the (a) the (a) the (a) the (a) the (a) the (a) the (a) scowe						46.88 98								•	•	2 :							•		Ra		•			_	_	2	Ra		37.6	8	37	3	3 :	_	7 1	3 8	3
BOTS OVE NA (e) ti													_	3	<b>a</b>	8	-					-		-	2 2	2 2		8	2 2	R		2	3 4	7 2	1 2		8			ੇ ਨ	= 2	' ? <b>:</b>	3 8
410C HA.		3 to 5 to 5 to 5 to 5 to 5 to 5 to 5 to				19.99 -110.20				X. 45 - 131. 48	M -128.38	51.30 -151.50			1. 18 - 45. I	=	•	•		P	. 5		ė			2 #		3			3	= :		21. 10 -119.	1 18		8	3	8	<b>8</b> :	19.46 -186.	8 8	
10C LAL								_							-	2	_				18	25.28	_	27.50	_		8	8 2	•	_		_			24.78		=		8	2	2 1	8 8	
10C 100.1		ed s	d a	i d	zi	zi =	ed :	र्श र <b>इ</b> . र		j Xi BB		 : 8	<b>2</b>	38 27.	ai R	3	तं : ड	# :		6 8 8 8		8	# =	र्त : ड	i 8 8 1	3 3 3 8	2	<b>8</b>	e i	3 2	2	의 : 목 :	ស ន ខ រ		8	8	71	8	.12	<b>10</b>	# 1 = 1		
SH LP. H		3 1	e s	3 3	3	3	3 :	<b>4</b> 0	J =	) d			2	3	 20	4	4 ·	a .			1 3		3	= :			3	<b>3</b>	3 :	: 3	3	<del>2</del>	# ( 	8 8		W 50	8	8	•	30.10	e :		
(a) th		ર્સ :	ี่ ถึ				3 : 3 :			_		-	_	_	16.23			_		i s	3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		4:10	_			10 29.20		d x				B A S X					_		_	8 8	
		13.68	13.6	7 1	1510	15.56	12.5	16.2			3			12.80	15.8	3	10 m	4					1	<b>a</b>			12.	2			16.46	0 21.10			161	19.45	40 19.60		_			8j =	
A CLAV		3				3	3	33		3 4			6.3	3	3	1.4	-	3				3	3	3				3	3		3	3	3			3	4	<b>=</b>	<b>=</b>	_			
SIL		3				3	3	2 4		n c		1 2	1	3	3	23	6.7	*		u :			3	3		3 3	3	3	3		3	6.2	3			3	1.20	_	_	_			
98 % 9 %		5			85	8.	78°	86 S		1 3 1 3 1 3	i		RI K	100	100.0	7 78 -	97.8	<b>3</b>	st s	# 8	8 8	8	25.	F. 35	<b>8</b> , 8			=	2			F .95.74	8			9.3	25.3	93.46	97.28		33.5	# 5 # 8	a s
BROVEL at 5		7				=======================================	W -	M 8		4 J	1 1	4 14	<b>7</b>	20	-	35.6	1.0	あ   d	# 1 # 1	7			-		4			3	0		3	1 6.0	# :		7 K		ر ا	7	1.3	3 1.48		9 4	n 4
EFTH (a)		•	•		•	-	•	•	•	9 4		133		-	•	•	_	-	•				-	•	•	d x			_	એ ≈ -		_	_		7 17 91				-	•	-		0.0
E883	- 1	STIZE.	536.000			255.50	35,000	264000		26 % B	200		20000	545680	SSBABL.	8 4548BB.	8 45.08B.	0 47358B.	47848		V	497/64	1 STEP 1	8 SEPARE.	58728	316	2216	125.48B			54568		•							8 588888			10000
MDGM (a)	- 1	335.000.	396.00	78	30,702	395.0m	396888. (	396ag.	- T	38	30,00	20,50	8								70128					20128		391288.	39120	23 CMB.					70128								196 A 186
LATITUE LOGITUDE (deg) (deg)			<b>10 10 10</b>	8.574						<b>18</b> , 273					54.472	81.376	81.28		22.	2			2					DB. 724	88.674		1	372	474	42.	27		A. 223	12	86, 123	80.073	22. W	12.571	81.3/b
Tabe (deg)		36,698	36,698		(by m	34.697	38.697	30.697		96 96 96 97 96 98	00 m		38,625	100.00	100.00	38,655	M. 655	36.65	<b>1</b> 650				100	38,655	19 19 19 19			9	30,653		15	38, 957	30.654	# E			30,653	3 653	39.62	38,652	38.507	900	38.611
E 3			_	-			3	9	2 :	3 5	2 :	3 3	3	3	3	20	3	3	3	3	1	1	3	3	3	<b>3</b> 3	1	3	3	<b>1</b> 3	3	3	3	3	3	1	1	3 1 2	21.560	3.	3	3. E	*
BLOCKED AREA LATER (sq.ka)	!	23. E	<b>Ξ</b>	ਡ : ਹ :		<b>₹</b>	S S	3. S. S. S. S. S. S. S. S. S. S. S. S. S.	ا ا	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 2	ว่ ส	3	zi	ដ	oʻ	ដ	ដ	ଅ	ង ខ	3 8	3 %	រ	ឌ	2	ឱាក	3 %	រដ	ส	ឌ ខ	3 ສ	ีส	ત	ଅ :	3 8	3 %	1 2	1 ដ	1	-	ଅ	ದೆ :	# 1

5	۱.			•	=	,	<b>#</b>	•	9	•	•	,	,	7	9					, =		-	-		_		_				_	_	-		_	_			• •					_	_
at Acoust	3		=	-5	<u>-</u>	-5	-	3	9	3	3	3	3	3	3	3	4 ×			ł	3	3	=	1.8	=	=	3	3 .			=	3		3	3	=	9	<b>3</b> (	,	4	3	- R	3	9	4
	17.38	6.64	17.10	16.98	16.38	7 8	7.3	17.38	<b>1</b> 2	12.78	12.78	12 <b>8</b>	4	13.28	3	# E		1	14		3	3	5.10	3	8	<b>8</b>	<b>8</b> :	R :		2	7.4	8 : 1 :		3	2 1	<b>2</b>	2 2 3	2.	<b>8</b>			12.2	12.60	13.10	13,60
Į,	8	1	=	3	2	<b>2</b>	2	Ž,	<b>4</b> . W	<b>8</b> .	2	<b>8</b>	==	2	3 1	7 ?	4 ,	7 R	1		3	3	=	3	3	=======================================	3		R 8		<u></u>	23	3 5	=	37	=======================================	3	<b>4</b>	2 1	8 8	R 88	8	2 %	3.60	3.68
Seount Scount Scount	8.3	85	=	=	<b>8</b> 7	3:	8.	<b>3</b> :	=	9 4	<b>87 4</b>	<b>6</b> . io	8	3	2 :					8	=	84	=	3	8	=	<b>3</b> 3		R 8		=	= !		3	3.	=	83		# # # 4		2 8			2	2
誓	8.3	8	=	1.10	1.28	<b>3</b>	8.	7	1.10	9.60	20	5.5	=	3	2 :					8	8	=	=	3	8	8	8 3	9 8	R 8	8	8	= :	<b>3</b> 3	3	8	8	8		<b>3</b> 8	5 =	: 8	3	8	8	8
this (a) this (a) this (a) this (a) this (a) this (a) Acoust Acoust Acoust Acoust Acoust Acoust Acoust			8	=	=	8	8	3	8	3	8	3	8	2	8 :	3					3	8	=	8		=	8 3	ļ			=	<b>8</b> 8			=	8	<b>8</b> 8		B 1	1				8	=
Scount 1	2	8	=	=	8.	<b>3</b>	2.48	<b>:</b>	1.66	23	=	8	8	8	3	3 8	9 8	2 2	2	8	3.10	8	=	230	R	8:	e :			8	8	# 1	Ŗ	: 3	3	2	2 2		2 2 2	. 4	1 7	=		2	3
Scount X	8	7	**	m 8	2				_				_		M :			i a		_	m m	_	2	_	_	: 2 :	-i - -: :	i	i	mi S	من 13	એ : #: :	i Ra		_	시 유	એ <sup>,</sup> ≘ :	4 . R 1	તં~ જાકી	5 ~ R ¶	: M	: 중	· 서 : 28	70 3.	~
Acount Ac	•	M	10 3				20 m		_	서 교	ri E	ল •	_	ਲ : ਅੰ-					F	_		_	_	તો જ	2.7	e .	ল i			_	بر ا	A .	, ,	ai	K.2	7	ار ا		M ~	i	-	<del>-</del>	7	-	4
unt Mex	4		-		8	_	# T		2	53	-	=		7 T					2		W.1		E 9	=	3	3	= =			_	3	3		6	<b>-</b>	त्य <b>च</b>	-	3:			13	-	6.2	9.3	6.7
(m) Aco	24	81	<b>8</b>	9Ì	양						_	_		_					2		_		_	27.60			2 1			_	9i			ਤ ਕੁੱ	22	7 3	80 E					39.	8	<b>38</b> . Ed	89,68
(a) thk			49.60				4	7	e Pi	2.13	47.6	43.68	4	9 :	\$ 1	\$ 3		G	2	5	<b>8</b>	51.38	4	37.60	2	3	\$ 1		£	3	\$3°	₽ (		SI. 18	8j 3	<b>2</b> 9.	त्र : इतं :		2 3 2 3		4	47.38	SI. 8	57.78	£3,
a) thk	-19.60	12.9	-28.28	<b>F</b> 38	# 1	7 7	2	7.0	2 4 7	-160.28	-101-30	-18.3	-14.2	-				-116.38	-122.00	-127.78	-122.78	-123.88	-161.20	-136.28	-119.8	-176.10	29.EP	8 8	1 4	47.8	3.5	R S		4	-180.50	-165.8	- 18.8 2.8	R 8		10.4	10.4	-18.9	-106.50	-114.20	-119.50
that C			#. #	200	<b>8</b>				8	2.6	2	1.28	<b>ន</b> :	3				1 2	21.10	2	23.28	20 10	37 14	2	M.18	<b>3</b> 1	1 .								200	2	2 !							16.88	9
tht G	28,38	49.8	8.8	<b>3</b>	2 :		8	7	8	2	#	27.40	8 : 3 :	# 15 E		2 2	1 5	21.12	8,8	19.98	17.10	17.60	3.2	2	13.E	7 : ::	3 1		2 2 3 3	25	8		2 2 2 3	21.28	21.38	3	<b>स</b> १	3 2	e s	i z		R Ti	21.98	19.60	14.28
the Ca	8.4	=	3	2	3	2	<b>8</b> :	8	2	2	3	3	= :						8	2	3	3	3	3	=	3 3	3 3			3	3	3 3		3	3	2	8 2					=	=		8 4
this (a) this (a) this (a) this (a) this (a) this (a) Scount	1.3	8	41.38	3	8 :	2	8 3	1	2	41.68	<b>8</b>	3	9 2	<b>F</b> 5	B 1	8 8	RE	2	9	4.46	4.20	7.28	3	7.10	3	<b>8</b> 1			<b>8</b> 5	3	= :	3 5	# # # # # # # # # # # # # # # # # # #	<b>7</b>	<b>8</b> 6	2	2 2		# F	! g	e s i xi	37	31.90	2	
thk (a)	=	21.90	=		2 :		# : F	2 :	3	_	3	_	3 :		_									25.45		<b>m</b> (					_				9.3								19.10		
w #	<b>8</b> 7	1.50 2	138	91	8 :	8	2		8	=======================================	3	2	m :						8	20	_	F.38 PP	37 37	स्य : इ:		7 : 8 : 8 : 8 : 8 : 8 : 8 : 8 : 8 : 8 :	2 :			_	8			_	8:	¥ 8:			2 <b>4</b>	: =	: = : =	8	8	<b>8</b>	20
_	A.	1.10	m,	7	<b>3</b> (	2	2		8	2	=	2	83 18 70 18	8 2		8 8			= = =	1.23	_	_	1.38		_		# ·		_	_	_	3 7		_	2	2 3						=	2	•	8
* * *	*	7	=	3	8 :	3 ;	<b>8</b> :		2	8	2	2 :	<b>8</b> 8	R 1		R		1 2	3	8									_	_			_	_					4 d	i =4	; ===	=	*	_	87
* *	3	zí z	# #	<u>.</u>	8 i	si :				g E	<u> </u>	2 2 3	si s			8 8	8			-					3	_	33	-			_			99.38	33.55	gi m	<b>2</b> 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			•				S.	8
- 1	-	-	2	-	<b>.</b>	-		3	3	9	3	9						F. 28	_	3 0.80			_	824	-	_	3 %		_	_	87	3 3		3	3	-			; ]		_	6.10	2		B. 3
3	1.0 28.	1.0 45.	•	•	•		•		•	•	•	•	•	•	22	•			•	1.0 42.3	•	•	•	10 110.0	-	•	Le 114.6			_	-	7 7 7		•	•					- H	3.6	•	•	36.9	38
3	•	•	•	-	-	49/64				-	-	•	57226			3,7			55,000	155488E.			20100	-	-		75.00	7	47.5	478488.	44330	4000	49768		307288.	1364E	212								555.00
3	3668	424688.	WEAR.						The Age	385.488.	100 A 80.	105.480		200	205.488	305.488		305488.	385488.0	385488.	385488.0	205.48E.	42488	386.488.	206748			3016	381640.	3016an.	1916ae.	2010	M 1688.	381600.0	381686.0	15 COM	1816a.	2010	2016a.	381600.0	30168	381688.8	381600.0	381688.8	381686.0
(Tag)		<b>18.</b> 221			5								17.								-				_					227	2.13		2			-						-			88.424
(Page )	31.612		38.612	30,612	36.612	A. bic	AL 612	Se ble	A. 612	38,612	38.612	38.612			110 %	19 61	36.611	30.611	30,618	38,610	39.610	38, 689	100 mi	30,649				3	36.568	39, 568	26.56			36. SEB	9.568					26.0	26.56	B. 568	97.568		19.567
(mg. las)			## ## ## ## ## ## ## ## ## ## ## ## ##							1		# T				7	3	, ,-,	23.040 3		3	23.040	[7]	- 6	20.2			2.040	23.046	23.040	23.040			23.040	23.040	13.165	23.046			23 PM	23.040	23.040 3	23.040 3	3. BE	3.040 3
=									_																																				
	¥	53	H537		2/501	2/20	750		2	150	150			145.74	1000	15.28	H5384	H5385	H5386	H5387	H5388	3	2	H539	5			70	20	1243	100	245		HEA18	HDA19	¥		IN A	542	15424	<b>5</b>	H5426	15427	87 <b>4</b> 5	F5429

MINIS	**Count	3	2		3	37		8	<b>8</b> 3		8	g :		3			3	=	3:	8 5	=	2 2		88	: :	= 1		=	8 8 4 4	8 5	27			3	= 1		2 3	
ITRN 2	Scount Scount Scount	3	2			12.00	17.9	17.70	17,38	4 4	1.60	2 F	13.88	12.10	8:3	# # = =	1.2	11.30	8 F	12.10	2			R 1	2.73	7.5	2 4	14.70	8 S 	13.78	13.80	2	::	11.10	<b>8</b> :		= = = = = = = = = = = = = = = = = = = =	9.0
STALED TITM	*Count	3	2		3	8		==	37			3 5		7	8	2 2	3		<b>8</b> 8	1 8 1 m		3 3	3	8 I	: :	3 2	3 = 3 ~	4.10	3 5	3	3 /			2	<b>3</b> :		2 3	
BUTILE ST	Kount	3	2	3 5	3	8			2.5		2	2 :	3 M	2	75 T	= =	2 2	=	3 5		=	3 3	3	2 2		= 5		1.70	8 1	2	# F			8	2 1		8 2	
		=	8	8 9	3				9.7		2	<b>P</b> 3	3 M	2	7	3 5	3	=	3:		=	3 3		81	: :	= 1	3	2.	2 2	2	7 7	2 2		9	2 :		2 2	
OH THE	Acount Acount	=	- :	, :		_	8 8		8	3		8 3			8	8 8		3	3 2		3	3 2		<b>3</b> 1		8 5	3	=	2 1		8 3			8	<b>8</b> 8		8 3	
116 PE	Scount &	8	2	9 5 Min		3	8.8	8	8.8		18	8:		2	8	3 R			= :	18	٠ ج	P 1	2	3.8	1 8	R	8 8		ខ្លុខ	3 3	7	Ŗ		8	8 :	2 2	2 5	8 89 Ni mi
I €	Acount N			**			2		2 017	2 7 2			4 10 10 10 10 10 10 10 10 10 10 10 10 10		8	# <b>1</b>	1 M		m e 5		1.10 3	* *	: 8	3 1	8 8			3							用:	3 3		9 83 9 83
BP P.R	Scount to	<b>3</b>		M			M M M		_	: :	_	ನ : ನ :		: M : S	m 8	# # # #		1.20	**		3	2 c			; ;			1.28 2.							_	÷ ÷	-	
		-	 8			_			81	6 a		<b>d</b> (			-i	<b>a</b> a			# 4 R 5	id F3	200			31	i		6 d 8 8	3	= . = .		2 2			8	= ;		_	 
DA GLIPAT	(a) this (a) Scount	*	*	E N	i #	gi	3	i si			2	<b>#</b>		20	99	# 3		8	# 8	1 2	87.1	2.5		8	2 2 2	2.16	i d		ਡ 8 <b>ਨ</b> 5	i =	_	, i		25.			8	2 2 3 2
E DVRBR		N. I.	7	2 5 2 5 3 7			3 5	4	47.70	1 2	4	20.00	e e	4	_	3 2		10	25.50 25.50	_		2.3		- 6	3	-	. 4	4	; ;	<b>†</b> \$			1 3		\$	2 K		ર્યું <b>કું</b>
C 196, ED	(m) this (m) this (m) this		4	7 P			# 2 # #	4	•	r a		36	₹ 6 - 1 - 1 - 1 - 1	_		-182	1		-116.98	-121.4	-131.9	15.4							2 8 F				-162.3			-115.6		-141.6
CLL MIG	3	2. S	R H	3 ×	×	3	3 5	=	11.28		3	8 i	त्र ह कं ≪	7	7.50	# E	3		# S		-	स्र ह	R ∓ i zi	4	7 =	=		11.3		3 3	80 6	7 T			_		-	# # % % **
ID. AIC	12 (12)		# * * * * * * * * * * * * * * * * * * *		12:		8 8	2	86.58	1 2 2		21.8	<b>8</b> 8	i d	3	<b>8</b> 3	៖ <b>គ</b>	2	3 3	1 4	15.28	년 일 2 8	# # F	8 7	3 3 3	2	2 2	Z	2. 28 2. 28	3 3	2	R S	3 X	8	33 : 33 :	17.9	16.10	13.16
18	7	2	2	8 1	18	2	8 1	18	8	8 8	8 8	8	8 8	3 8	8	8 1	8 8	18	8 1	8 8	8	8 1	3	8	18	8	В	8	8 8	8 8	8	2 1	2 2	8	8	8 8	8	8 8
UP. MI	3	3	3	<b>d</b> •	4	=	4		<b>d</b> (	-	ة خ	<b>-</b>	<b>4</b>		<b>-</b>	<b>d</b> 4	4	<b>.</b>	<b>d</b>	ة خ	-	<b>d</b> (	نے ن	<b>d</b>	4				4 4	<b>.</b>	<b>-</b>	3 6		4	₫.			<b>-</b>
PL (OCSSN UP.N)	i) thk (s) thk	42.40 B.1	39.28	2 8 14 8	R				39.60		4.10	41.38	2 K	2	24.00	# # # # # # # # # # # # # # # # # # #	27.68	20.00	# 5 S		45.10				2 2 2 3 3 4	用が		# # # # # # # # # # # # # # # # # # #	2 : 2 :		N. 20	<b>3</b> 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		27.70		2 2		\$ 55.58 \$6.28
ALANTERN PLICEDN UP.NI	thk (m) thk (m) th	\$ 5	<b>2</b> 2	rd a	i si	=	K PA					<b>8</b>	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	: 8	3	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3 8 8 8		19.60 Jy.30	, at		<b>8</b> 1				P. W. W.			· · · · · · · · · · · · · · · · · · ·		N :	ed a	19.28 24.68	10 27.	න් : ක :		8	
CLATERN PLICE	(a) thk	\$ 5	15 88 35.	阿爾斯	i si		K PA			# =		<b>8</b>	2	: 2	3	3 1	3 8 8 8			, at		# 1 to 1	13	8:		_				3 33	N :	ed a	ಕನ ಕನ	10 27.	න් : ක :	이 3 이 3	19.80 45.	2 B
T CLAY	S at S thk (a) thk	CH 829 42	15 88 35.	阿爾斯	1 2		× × ×			# =		<b>8</b>	2	1.8	0.00 10.60	20.00		0.00 19.10	19.60	F. 28 12.38	6.38 38.38	おい	1	6.25 6.00		_		6.10 6.30		3 33	N :	ed a	ಕನ ಕನ	10 27.	න් : ක :	이 3 이 3	19.80 45.	33.48 45.48 45.48
T CLAY	at 5 at 5 thk (a) thk	CH 829 42	6.28 X5.88 39.	阿爾斯	1 2		× × ×			# =		30 0.60 0.00 9.30	2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10 Lts Lts 14.64	20.00	M LM LM 19.M 27.	28 6.00 6.00 19.10	25 C. 19. 19. 19. 19. 19. 19. 19. 19. 19. 19	F. 28 12.38	60 6.30 6.30 36.50	おか あり ある	1	10 1.50 6.25 6.00		20 0.60 1.00 0.30		00 C.10 L.30	28 6.78 6.18 6.88	3 33	B.18 8.00 12.40 35.		ಕನ ಕನ	6.00 0.00 19.10 27.	70 4.00 4.00 19.30 29.	이 3 이 3	0.10 0.10 19.80 45.	33.48 45.48 45.48
SOO SILT DAY	at 5 at 5 at 5 th (a) thk	CH 829 42	6.28 X5.88 39.	阿爾斯	1 2		× × ×			# =		30 0.60 0.00 9.30		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10 Lts Lts 14.64		M LM LM 19.M 27.	28 6.00 6.00 19.10	93.90 0.00 0.00 19.60		94.66 6.38 6.38 34.58	おか あり ある		10 1.50 6.25 6.00		97.50 0.60 1.00 0.30		00 C.10 L.30	28 6.78 6.18 6.88		B.18 8.00 12.40 35.			6.00 0.00 19.10 27.	C 00 13.30 29.		0.10 0.10 19.80 45.	98 0.28 0.26 0.24 45. 38 0.44 0.55 35.99 46.
SPRIE SOO SILT CLAY	MAN AND MAN AND MAN THAN (M) THAN	CH 829 42	6.28 X5.88 39.			7 2.70 94.90 1.80 0.60 0.00 0.	× × ×		6 6.10 90.60 6.30 6.40 8.10			4 G.00 59.30 G.60 G.00 5.30		1.0 10 10 10 10 10 10 10 10 10 10 10 10 10	3 4.00 104.00 4.00 6.00 14.66			6.10 99.30 6.00 6.00 19.10	A.10 99.98 A.80 A.80 19.68		6.78 95.68 6.38 6.38 35.58			2.29 %.10 1.50 6.23 6.00		6.26 97.30 6.60 1.00 6.30		L. 95.45 C. 10 L. 30			0.00 99.90 0.10 0.00 12.40 35.			99.56 6.66 6.00 19.10 27.	C 00 13.30 29.		0.10 0.10 19.80 45.	98 0.28 0.26 0.24 45. 38 0.44 0.55 35.99 46.
SOO SILT DAY	(m) and 3 and 55 and 55 and 55 thic (m) thick	2, 43, 4,60 99,10 6,28 6,10 22,99 42,	8.0 48.1 8.70 99.80 8.20 8.20 35.80 39.			8.0 11.7 2.70 94.90 1.00 0.60 0.00 0.			.0 14.6 0.10 90.60 0.30 0.40 0.10		. 0 21.0 0.00 59.10 0.30 0.00 0.00 0.00 0.00 0.00 0.00 0	1 254 C. C. C. C. C. C. C. C. C. C. C. C. C.		1.0 25.1 4.00 104.00 4.00 10.00 10.00	2.6 32.3 4.00 100.00 4.00 6.00 14.66	10 M.0 4.00 99.90 4.00 6.00 19.60		.0 34.9 6.10 99.98 6.08 6.00 19.10	10 Mail 210 99.99 0.00 0.00 19.69		8 41.2 6.78 95.68 6.38 6.38 35.58		2 4 4 6 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 11.0 2.35 %.10 1.50 0.25 0.00		0 17.3 0.20 97.50 0.60 1.00 0.30		0 21.2 6.00 99.00 6.00 6.10 6.30	10 22.8 0.00 99.28 0.70 0.16 0.20		0 27.4 0.00 99.30 0.10 0.00 12.40 35.			33.0 6.20 99.80 6.00 6.00 19.10 27.	3.0 34.3 6.38 99.78 6.00 6.00 19.38 29.		38.3 0.38 99.50 0.16 0.10 19.80 45.	.0 33.7 0.60 99.30 0.20 0.20 0.34 55.40 45. .0 42.4 0.60 99.30 0.40 0.30 33.90 46.
EAST DEPTH GRONEL SOND STLT CLAY	(m) (m) and 35 and 35 and 35 thic (m) thick	.0 554000.0 43.4 0.50 99.10 0.20 0.10 22.90 42.	8 355,00.0 40.1 0.70 50.00 0.26 0.20 35.00 33.		-0.0/2004.0 16/10 Pact X:30 1:00 0:10 0:10 0:10 0:10 0:10 0:10 0	A.0 464000.0 11.7 2.70 94.90 1.80 0.60 0.00 0.	18 454890.0 15.4 0.45 99.28 0.30 0.30 0.10 0.45 354 355 0.45 0.45 355 0.45 355 0.45 355 0.45 355 0.45 355 0.45 0.45 355 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.		LO 4220LO 14.6 C.10 98.60 C.30 C.40 A.10		. 0 497686.0 22.0 6.00 99.10 6.30 6.00 6.50	8.0 SEMBLE 25.4 C.00 29.38 C.60 0.00 5.38		1.0 51690.0 29.0 0.00 100.00 0.00 0.00 14.	1.0 E1680.6 30.3 0.00 100.00 0.00 0.00 10.64	L. S. S. S. S. S. S. S. S. S. S. S. S. S.	1.0 Million 20.3 11.10 25.20 11.00 4.00 13.20 CA.	. 0 54600.0 34.9 0.10 99.90 0.00 0.00 19.10	. B.5456a.0 3k.3 a.10 99.38 a.00 a.00 19.50	. B. STONER, B. S. D. B. S. S. S. D. B. B. B. B. B. B. B. B. B. B. B. B. B.	.0 550000.0 41.2 0.70 90.50 0.30 0.30 30.50	10 12/100 0.10 0.10 12/10 0.10 0.10 0.10 12/10 1	18 17/2010 11:4 1:38 3/100 11:4 11:4 3/100 11:4 11:4 11:4 11:4 11:4 11:4 11:4 1	R.O. 664000.0 11.0 2.29 96.10 1.50 0.29 0.00	0.0 452000.0 17.9 41.50 35.70 41.50	E. 6 47846E. 6 17.3 6.29 97.30 6.69 1.00 6.30	\$10 \$1200.0 15.0 0.10 \$1.00 15.0 0.70 15.0 0.1	6.0 49206.0 21.2 6.00 99.00 6.00 6.10 6.30	1.0 497604.0 22.8 0.00 99.28 0.70 0.10 0.10	THE SECTION OF STATE	0.0 51280.0 27.4 0.00 99.90 0.10 0.00 12.40 35.	1.0 516280.0 29.9 0.44 99.90 0.48 0.48 16.80 29.	1.0 12/15/00 0 34.3 0.00 100.00 0.00 0.00 0.00 10.00 24.	4.0 531206.0 33.0 6.20 99.80 6.00 6.00 19.10 27.	.0.536400.0 34.3 0.30 99.70 0.00 0.00 19.30 29.	19 546681	0.556466.0 38.3 0.38 99.50 0.10 0.10 19.80 45.	8 XXX200.0 33.7 0.60 98.90 0.20 0.20 0.20 02.40 45. 8 X50000.0 42.4 0.80 98.30 0.40 0.56 35.90 46.
NORTH EAST DEFTH GRONEL SIND SILT DJAY	(m) (m) (m) net % net % net % net % this (m) this	2, 43, 4,60 99,10 6,28 6,10 22,99 42,	331544.0 35550.0 44.1 6.70 95.80 6.25 6.20 35.00 39.	Wilden States 71.8 Mes Size 6.20 6.44 W. W. W. W. W. W. W. W. W. W. W. W. W.	AND CONTROL OF THE CO	376000.0 464000.0 11.7 2.70 94.90 1.80 0.60 0.00 0.	376588.8 46388.0 15.4 0.48 59.38 0.38 0.30 0.18 0.48 35.	275000.0 47500.0 15.0 15.0 25.20 0.40 0.40 0.20 35.	37600.0 45200.0 IL.6 0.10 99.60 0.30 0.40 0.10		376584.0 477684.0 22.0 4.00 29.10 4.30 4.00 4.60 3.50	376800.0 302400.0 25.4 0.00 59.30 0.60 0.00 9.30	376584,0 577284,0 56,9 6,00 99,60 6,30 6,00 6,00 9,70 4/2, 27.44 4	37500.0 51500.0 29.6 0.00 100.00 0.00 0.00 14.00	376000 221600 30.3 0.00 100.00 0.00 0.00 10.60	376884.6 55648.6 31.0 6.00 99.90 6.00 6.00 19.60	3/5000, 33/500, 23.3 (c.10 27.30 (c.00 4.00 13.50 5.50 77.50 (c.00 37.50 5.50 77.50 )	376500.0 SA6000.0 34.9 0.10 99.30 0.00 0.00 19.10	376806.0 545506.0 36.3 0.10 59.30 0.00 0.00 19.60		376500.0 56000.0 41.2 6.70 90.60 6.30 6.30 30.50	276984 0 15408 0 41.9 0.60 25.20 0.30 0.30 45.30 15.30	2 4 4 6 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	372888,0 464888,0 11.8 2.29 95,10 1.30 6.20 4.00	3/2000.0 45200.0 17.9 91.50 Me. 70 91.50 Me. 70 70 70 70 70 70 70 70 70 70 70 70 70	372001.0 478401.0 17.3 0.20 97.30 0.60 1.00 6.30	37200.0 (4220.0 16.8 0.10 95.0 0.70 0.70 0.70 0.70 1.72 1.72 1.72 1.72 1.72 1.72 1.72 1.72	37200.0 49200.0 21.2 0.00 99.00 0.00 0.10 0.30	372001.0 477501.0 22.8 0.00 99.28 0.70 0.10 4.00		37200.0 51200.0 27.4 0.00 99.90 0.18 0.00 12.40 35.	372000.0 316300.0 28.9 0.00 99.90 0.00 0.00 16.00 28.		372000, 531200, 33.0 0.28 99.50 0.00 0.00 19.10 27.	372000.0 535000.0 34.3 0.30 99.70 0.00 0.00 19.30 29.		372000.0 559400.0 38.3 0.30 99.50 0.10 0.10 19.80 45.	.425.372000.0.355200.0.35.7 0.60 90.30 0.20 0.20 25.40 45. 375.372000.0.56000.0.42.4 0.80 90.30 0.40 0.30 35.90 46.
NORTH EAST DEFTH GRONEL SIND SILT DJAY	(m) (m) (m) net % net % net % net % this (m) this	381680.0 554000.0 43.4 0.60 99.10 0.29 0.10 25.99 42	. 86. 274 331568.0 SESSER.0 44.1 6.70 SE.80 6.20 6.20 35.00 33.	Wilden States 71.8 Mes Size 6.20 6.44 W. W. W. W. W. W. W. W. W. W. W. W. W.	AND CONTROL OF THE CO	376000.0 464000.0 11.7 2.70 94.90 1.80 0.60 0.00 0.	376588.8 46388.0 15.4 0.48 59.38 0.38 0.30 0.18 0.48 35.		37600.0 45200.0 IL.6 0.10 99.60 0.30 0.40 0.10		376200.0 477600.0 22.0 0.00 29.10 0.30 0.00 0.50 3.76200.0 477600.0 22.0 0.00 29.10 0.30 0.00 0.00	376800.0 302400.0 25.4 0.00 59.30 0.60 0.00 9.30	376584,0 577284,0 56,9 6,00 99,60 6,30 6,00 6,00 9,70 4/2, 27.44 4	376200.0 516200.0 29.6 0.00 100.00 0.00 0.00 14.00	376000 221600 30.3 0.00 100.00 0.00 0.00 10.60	5 Mt. 723 376300.0 525400.0 31.0 0.00 99.90 0.00 0.00 19.60	3/5000, 33/500, 23.3 (c.10 27.30 (c.00 4.00 13.50 5.50 77.50 (c.00 37.50 5.50 77.50 )	1 80.575 37680.0 54600.0 34.9 0.10 99.90 0.00 0.00 19.10	0.00.523 376000.0 545500.0 34.3 0.10 99.90 0.00 0.00 19.60	3/2000.0 339900.0 3/2 0.03 22/7 0.01 0.10 12/30 12/30 3/20 0.30 12/30 20/30	1 04.375 376000.0 56000.0 41.2 6.70 98.60 6.30 6.30 36.50	80,223,376,880,0 154,900,0 14,90 0,60 39,800 0,1	3/5000.0 13/400.0 12.4 1.30 3/100 01.30 51.30 11.00 11	81.375.372884.0 464884.0 11.8 8.29 95.10 1.30 8.29 8.00	0.0 452000.0 17.9 41.50 35.70 41.50	372001.0 478401.0 17.3 0.20 97.30 0.60 1.00 6.30	\$10 \$1200.0 In. \$1.00 \$1	41.075 372000.0 492300.0 21.2 0.00 99.00 0.00 0.10 0.30	372000.0 457600.0 22.8 0.00 99.28 0.70 0.16 4.80	3/2000_0 3/2000_0 24,5 0.00 25,3 0.00 24,5 0.00 24,5 0.00 34,5 0.00 34,5 0.00 04,5 0.00 04,5 0.00 10,5 0.00 04,5 0.0	37200.0 51200.0 27.4 0.00 99.90 0.18 0.00 12.40 35.	Be. 825 372888.0 516880.0 28.9 0.46 99.90 0.48 0.48 16.00 28.	372000.012215.013.0 34.3 0.00 100.00 0.00 0.00 10.00 10.00 24.	86.675 372804.0 531204.0 33.0 6.29 99.80 6.00 6.00 19.10 27.	1 86.625 372860.0 535860.0 34.3 6.30 99.70 6.00 6.00 19.30 29.	372900.0 546600.0 35.6 0.30 99.70 0.00 0.00 19.70 22.	80.475 372000.0 550400.0 38.3 0.39 99.50 0.10 0.10 19.80 45.	08.425.372000.0 XX200.0 33.7 0.60 98.90 0.20 8.20 8.20 25.40 45. 0.80.375.372000.0 X60000.0 42.4 0.80 98.30 0.40 0.30 35.90 46.
NORTH EAST DEFTH GRONEL SIND SILT DJAY	(m) (m) (m) net % net % net % net % this (m) this	546 34.37 54.24 31560.0 35400.0 43.4 6.60 39.10 6.25 6.10 20.39 42.	THE SECTION SECTION SECTION OF SECTION 14.1 C. 70 SECTION 14.20 C. 20 SECTION 350.	120 SEG BB. 224 WISBER B 3744BL B 71.6 3.00 57.00 B. 75 B. 7	SECTION OF THE SECTION OF SECTION	337 38.525 81.375 376000.0 464008.0 11.7 2.70 94.90 1.80 0.60 0.00 0.	3 34,255 81,255 37686,8 45886,0 15,4 6,44 59,38 6,39 6,39 6,10 6,44 55, 55 5,	28, 25, 21, 25, 37,000, 97,500, 15, 10, 10, 10, 10, 10, 10, 10, 10, 10, 10	34.525 81.175 376806.0 442206.0 14.6 6.10 99.60 6.30 6.40 8.10		34.25 81.85 37684.8 42584. 21.8 6.80 59.10 6.30 6.00 6.50	HO 38,525 88,975 376888.0 32488.0 25.4 6.80 59.30 6.60 6.00 51.30	3 34,525 86,925 37686,0 37726,0 85,9 6,00 99,66 6,30 6,30 6,00 9,70 42,0 13,00 6,00 9,70 42,0 13,00 13	3 34,525 54,655 375444 0 515544 0 25,8 0 4,00 104,00 0,00 0,00 14,80	38.255 88.775 376888.0 521688.0 38.3 8.00 108.00 6.00 0.00 18.60	3 34 353 84 753 376396 8 555486 31.0 6.00 59.30 6.00 6.00 19.60	SECTION OF THE PROPERTY OF THE PARTY OF THE	34.20 46.373 37646.0 S4686.0 34.9 6.10 99.90 6.00 6.00 19.10	34.25. 44.555 376.04.0 54.564.0 36.3 4.10 59.59 4.00 4.00 19.60	34,250	34.24 84.375.376866.9 55886.0 41.2 6.79 94.69 6.39 6.39 36.59	W. 12. 20. 25. 376.000. 854.000. 14.9 0.66 12.00 0.20 0.20 0.20 0.20 0.20 0.20 0.2	3.41.22.3 BE.22.3 TIGARE BASHER STAME 47.4 B.70 SE.36 B.20 B.20 34.40	30,481 81,375 372000,0 464000,0 11.8 2.20 96,10 1,50 0,20 0,00	3 36 451 21.253 375900,0 462690,0 17.9 51.38 35.76 51.38 51.49 51.39 51.49 51.39 51.49 51.39 51.49 51.39 51.49	34.482 81.225 372000.0 478400.0 17.3 0.20 97.50 0.60 1.00 0.30	949 34,422 81,173 372990,0 442290,0 16,8 9,19 35,89 84,70 84	34.42 81.073 37200.0 49200.0 21.2 6.00 99.00 6.10 6.30	No 31,422 81,825 372001,0 497601,0 22,8 8.00 99.28 8.70 8.16 8.80	THE SHIPPY SHIPPY STORMED SHIPPY CALLS THE WAY SHIPPY SHIP	34.452 80.875 372884.0 512884.0 27.4 0.00 99.39 0.18 0.00 12.40 35.	34.422 84.423 372884.0 516880.0 28.9 6.46 99.99 6.48 6.40 16.40 28.	NAS JOSEPH POR TATA STORMAN MATERIAN MA	30,481 86,673 372006,8 331206,8 33.0 6,29 59.80 6,06 19.16 27.	30,481 80.625 372860.0 535860.0 34.3 0.30 99.70 0.00 0.00 19.30 29.	948 38,441 88,573 372880,0 546880,0 53,6 8,38 99,70 0,58 0,58 19,77 12,77 12,77 12,77 13,77 14,77 15,7	946 38.461 88.475 372888.0 55488.0 38.3 6.38 99.50 6.10 8.10 19.88 45.	848 38.481 88.425 372988.8 332288.8 33.7 8.68 98.38 8.28 8.28 25.48 45. 848 38.488 88.375 372888.8 558888.8 42.4 8.88 98.38 8.48 8.38 35.39 46.
EAST DEPTH GRONEL SOND STLT CLAY	(m) (m) (m) net % net % net % net % this (m) this	546 34.37 54.24 31560.0 35400.0 43.4 6.60 39.10 6.25 6.10 20.39 42.	23,646 34,556 86.274 331566.8 55566.8 44.1 6.76 59.68 6.28 6.20 35.89 33.	23.040 36.566 BR.224 MIGRAE 5744BL 71.0 3.00 55.00 B.70 B.40 34.30 MG	AND CONTROL OF THE CO	2.337 38.325 81.375 376000.0 464000.0 11.7 2.70 94.90 1.80 0.60 0.00 0.	23,040 34,525 41,225 376684,0 46484,0 15.4 (4.46 99.28 (4.36 4.16 4.46 35)	275000.0 47500.0 15.0 15.0 25.20 0.40 0.40 0.20 35.	23.040 30.525 81.175 37600.0 44200.0 IL.6 (L.10 90.60 0.30 0.40 0.10		376584.0 477684.0 22.0 4.00 29.10 4.30 4.00 4.60 3.50	23,040 38,525 88,975 376888.0 322488.0 25.4 6.00 59,30 6.64 6.00 5,30	23,046 36,525 66,525 376,686,0 567,286,0 66.9 6.00 99,60 6.30 6.00 9.70 42.	37500.0 51500.0 29.6 0.00 100.00 0.00 0.00 14.00	23.040 38.255 88.775 376806.0 221606.0 38.3 8.00 100.00 6.00 6.00 18.60	23.040 JALSES BALTES TREASON SECTION 11.0 4.00 92.90 A.00 4.00 19.60	O CONTROL OF STREET OF THE STATE OF THE STAT	23.040 38.29 88.375 376408.0 540008.0 34.9 8.10 99.30 8.00 R.00 19.10	23.040 38.224 88.255 376806.0 58.506.0 38.3 8.10 59.30 8.00 8.00 19.60	N BELLATO STANDOLLO STORMENO ST. D. CL. CO. 755.70 CL. D. CL. C. 155.30 L. C. C. C. C. C. C. C. C. C. C. C. C. C.	23.646 35.24 86.375 376200.0 55000.0 41.2 6.70 95.69 6.30 6.30 36.50	23,046 W1923 80,225 376800,0 154800,0 41.9 0,65 39.88 0,18 0,18 45.18	180.225 376800 574400 47.4 0.70 29.30 0.20 0.20 37.40	1.147 38.481 81.375 372888.0 464888.0 11.8 2.28 96.10 1.30 8.20 8.00	DESCRIPTION OF STREET OF S	23.046 38.482 81.225 372000.0 478400.0 17.3 6.20 97.30 6.66 1.00 6.30	372000 042200 16.8 0.10 95.00 0.70 0.70 0.70 0.70 0.20 0.20 0.70 0.7	23,040 38,442 81.073 37200,0 42200,0 21.2 6.00 93.00 6.00 6.10 6.30	23.040 38.442 81.023 372000.0 497500.0 22.8 0.00 99.28 0.70 0.16 0.00	3/2000_0 3/2000_0 24,5 0.00 25,3 0.00 24,5 0.00 24,5 0.00 34,5 0.00 34,5 0.00 04,5 0.00 04,5 0.00 10,5 0.00 04,5 0.0	23,040 38,482 80,875 372800,0 512800,0 27.4 0.00 99.90 0.10 0.00 12.40 35.	23,046 34,422 86,825 372866,8 516860,8 28.9 6,66 99.99 6,68 6,69 16,69 28.	26,773,372000,0121500,010,30,3 0,00 100,00 0,00 0,00 0,00 10,00 0,00	23,046 38,48 50,675 372000, 531200, 33.0 0,29 99.50 0,00 19.10 27.	23,046 30,481 80,625 372860.0 535600.0 34,3 0,30 99,70 0,00 0,00 19,30 29,	372900.0 546600.0 35.6 0.30 99.70 0.00 0.00 19.70 22.	23.040 38.461 88.473 372000.0 530400.0 38.3 6.30 59.50 6.10 8.10 19.80 45.	38,481 86,425 372666,8 332266,8 33.7 6,66 98,98 6,28 6,28 6,38 25,46 45, 1.38,486 86,375 372666,8 556666,8 42,4 6,88 98,38 6,48 6,58 35,98 45,

GEDNGIA OFFSHONE MINERALS ASSESSIDAT NEDEL page 19

ZIRCON	<b>Mount</b>	8.0		=	2						8	6.3	2 4	23	R :					E		8	8 .	= -	2	===	P.10	-	8 i	R	3	6.2	=======================================	9	2 :	2 8		20	8.4	= :	i. 8	=======================================	2 :	=	2	<b>2</b> 2	}
TITAN ZI		3	= 1	=		3 2			91 %	A		3.98	13.60	13. 80 13. 80	음 : 신 :	9 :						2	8	8 4	=	2	8	1.10	<b>3</b> 5		7 E		3	8	<b>7</b> :	B #		8	6.50	16.98	7.80	6.38	20.5	16.10	4.10	\$ = d c	2
STAURD TI	count		8	=	2	= 1	_				8	8.	8	3	# :	2 1	3 t	 					8	8	8	8	8	8	8 :	3 5	Ŗ <b>Ş</b>	8	=	=	= 1	3		7	2.00	1 867	8	=======================================	3	8	_	<b>8</b> 3	!
ALTILE STA	Scount Scount Scount		=	=	2	8 2	_	6 1	3		8	8	7 2	河 河	<b>7</b> :				3			8		8	=	=	8	=	= :			=		8	= :	3 8	1	8	8	2 8	m 8	=	m :	2 :	R :	ភ្	1
	Acount %		3	8	2	 8 :	_ `	 8 1	: -			-	38	-i :	e i	3 :						3	2	2	=	=	= =:	=	= :				=	ط 12:	2 :			8	=	=	=	=	<b>4</b>	= ;	= ·	 3 2	i
ACH THE	Acount to	3	-	=	ď							-		-						T		-	4	4	9	ā	-	ž	<b>.</b>				<u>.</u>	-	2 ;			3	3	=	-	<u>.</u>	-	<b>.</b>		23	
K. FLISP P. FLISP HYMING RESHRT NOWN	Acount Aco	3	3	3	3	3	3	3 3			3	3	3	3	3						3	3	4	3	3	3	3	3	33			3	3	3	3 :			3	3	3	3	3	3	3	3	33	
THANH O		_	34	3.9	2.0	7	2	7 2	2	l m	7	45	3.5	M .	M .	7	1	10		4		20	3.10	3.8	7	33	27	m M	2 .	7 6	4 m	3	7	2.0				2	2	3.1	3.1	70	2.6	ر ا	E.1	- 1.3	
P P.FLD	nt Acount	, A	4.2	4.	2	d .	-	4 4	1 2	3	*	85 m	서	# F	7 : M	4 .	4 ,	4 4	7		4	4	4.4	7	÷.	₽. 4.	7.5	4	M .	# X	4 4	~	i	3	75 S	4 -		4	4	3.18	Mi Mi	3.16	<b>元</b>	ਲ ਨਾਂ	RI I	M M	i
K.R.DS	A Scount		2	시	2 4				3	12	8	<b>8</b> 7	3	2	R :	<b>₹</b> 8	R S				3	77	<u>ئ</u>	M	<b>1</b>	3	=	3	= 8	3 4		=	2	3	# 1 -	8 8	R 8	1.2	3	1.7	8:	1.5	<b>8</b> 7	2	用	₹ ₹	
DIAPRT2	a) Scour		8.8	2	83.28 13.08		7	F 3		8	3	91.78	91.38	9. E	# :	<b>8</b> 8	R S	8 8 N a		3	69.68	27.38	27	F. 10	8. T	9	59. 10	<b>8</b>	20.5			2.7	2.2	9 9	ही ह	i a		8	91.38	20.00	87 87	<b>39</b> , 65		8j :	93.80	<b>=</b> ₹	
JAL BOTS OVERADM	(a) this (a) Scount		8.3	<b>89</b> . 18	8	d :	7	3 A 9 3	2	2	¥.2	45.38	\$ ·\$	<b>45</b> 28		7 3	R S			63.68	7.	2	83.28	97.00	<b>3.</b>	<b>8</b>	29.5	<b>8</b>	2 S	R 8		3	<b>8</b> 8	8	2. S	K		2.5	2	25.48 25.48	31.50	33. E	8 8	100 m	37.8	4.28 4.58	
	(a) the G	1 2	-161.98	-149.98	2	-78.18		2 is	3	47.10	20.73	31	S 15	26. 26.			R :			-117.3	-121.60	-12.3	-147.30	-154.28	-165.10	-156.38	-71.70	<b>63</b> .00	22.	2	2 th	-73.40	-72.88	-73.98				-73.16	# T	<b>47.48</b>	8i 8i	-14 -18 -18	3 :	-163.90	186.56	-117.60	
		27.10 -1	8	8	8	2 :		27	8	11.78	7	10.00	10.38	_	10 to	B #	R S	7 T	3	1 8	3	8	2	8	2 2 2	21.28	_	7.78	3 1	B 8	3	35	<b>8</b>	2.88	3 2	R	1	2	3	14.98	_	8	3	19.30	2	19.16	}
NO. NICE LIL NICE	the G		11.30	12.60		n a		= # 5 %	25.5	2	8.13	21.90	23. 42.	គ :	e :	B 8	RS	R S		1	3	17.98	1.8	11.10	16.2	# 1	8	13.65	9 : 5 :			8	# H	8	2		2 3	2	24.28	200	S Ki	27.00	<b>8</b> 1	27	3	<b>3</b> 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
. MIDC M	thk (a)	3	9.0	3	8						3	2 4	200	2			B			Ę		8		8	2	2	=	=	2 1			=	2	6.10	2 :			3	33	_	8.3	_	_	2	2	2 2	1
GLATERN ALTOCEN UP. NIOC	thi (a) this (a) this (a) this (b) this		15. W	8.4	8 :		R :		32.58	4.6	a	8 4	<b>8</b> d	2	# :	<b>3</b> 8	R :	2 A	2 17		8	91 %	£.10	8 9	8 4	2	8	2	3 1	2 2	8 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8	15.98	8.	200	3 5		9	===	16.30	=	16.98	9.50	\$ i	20 ×	80 F.	
TERN P.	(a)	3	19.60	M.68 4	8:	_		7 /	78		2	•	M 85.1	2	8 1	B 8	R :		1 2	8	1 37	3	=	7 867	3	7 87	8		<b>#</b> 8	8 =	2 44 5	8	8	3	8 :	3 1	3		8	8	2	<b>7</b>	_	3 :	2	2 8	
1	94	-	_	_	<b>8</b> :		7	7 2	3	8	=	8	=======================================	<b>3</b> ;	= : 8 :					7	8	18	3	25.	\$ \$	<b>1</b>	21 R	3 3	변 : 음 :			2	*	<b>8</b>	원 : 목 :	2		2	21	=======================================	=	8. E.	= :	ਕ ਵ	_	ਨ ਲ ਨ ਵ	
1	*	3	<b>8</b>	R	2	2 :	3 /	 e a	3 8			8		= :	2 :	8 2	8 1	81	3 2			8	8	8	3	<b>.</b>	<del>ວ</del>	8	31			8	:	3	<b>.</b>	8 8		8	8	:	8	=	= 1	<b>*</b>	两:	<b>*</b> * *	
1	14	±	=	8	2			4 2 p			3	2	2	<b>5</b>	# (	r a	R 1				_	2	3	4 8	3	ط ج				_			=	٠ 1	<b>=</b> 1				2	=	=	• 2		<b>3</b> :	_	# 10 m	
1	¥	27.	8	*	원 :	el :				gá	8	8	35.	8 :	ri s		_	Ŕ 8	i g			-			•	si E	si :	2 2 2 2	77 75 85 85 85 85 85 85 85 85 85 85 85 85 85		rigi Roman	<u> </u>	=	1					=	3 3	10 IS	_	gi :	23.62	<b>\$</b>	8	
1	* * *	-	7	2	7 1.1	n (		<b>d</b>		2	2 P	2 6.	7	2								9			5.48	9	-	-	3	1 1		9	7	-	3		2 -	9	-	4	3	-	<u>.</u>	3		9 4	
=	3	0.0	•		•			F 19.3			-	•		-	•			7 2					•	•	-	_	_	_	1.0 13.0				_	1.0 23.4	•	8			•	-		_	_	_	_	Ř ∓	
1	3	0 35A888	0.55%88.		•			4724				•		-	-									•	•	•	0 464000.	46888	0 478488.0	7,11,000	49288	49764		•	6 512886.	- Sibora	SKAR .	53128	0 536.00B.	8 S46668.	8 54568B.			9.250000.	6 36489B.	569680.	
1-	3	372888.	37288B.	372888.				10 C										10 / C			. K72							43					42000.					3		42000	12000 A			<b>42000</b>		Azessa.	
12	(Bap)	M 325	88.275	<b>207</b>	81.37		27.	2 Z	2		2	<b>20.97</b> 5	<b>8.</b> 925	80.87				100		1	47	45	37.37.3	<b>10</b> 123	<b>88.</b> 275	<b>1</b> 22	81.377	2	X :	2 2		81.625	86, 975								88.523		22 .42		22 28	<b>28</b> 272	i
TITLE	(F)	36.48	30,400	36.468	10. A.M.			19 7 7 19 19 19 19 19 19 19 19 19 19 19 19 19		M 439	M 439	38, 439	36.439	別で				10.450 17.450 17.450	17. V 18.	24.4	12.437	38, 437	38.437	38, 437	38, 437	30,436	38, 914	W 912	36.915 34.915	M. 313	36.915	30,915	30.915	30.915	36.915	46. 313 78. 913	20 M	30,915	30.914	30,914	30.914	38.914	30.914	30.913	30.913	30.913 30.913	-
	(sq. ke)	840 to	# n	15, 120	0.371	1	7	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7	# z	10 m	23.040	23. PE	23.06	7			1	7	1	7	1	23. PM	23.040	37 EE	9.510	23. PM	75 75 75 75	1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		1 2	23.040	23. 840	23.046	23.046			7	33.040	23.040	23.046	23. PM	23. 840	23.040		1	
BLOCKID AREA	3	6189						200															HSS62			_			1991																		
=		면	2	亞	2	9 !	₽!	99	2	4	4	4	42	열 !	오 9	2 9	9 9	2 9	ī <u>č</u>	9	. Q	2	Ø	Ā	Ţ	Ä	Ø	4	9	2 3	2 9	4	Q	Q	<b>9</b>		2 19	20	ğ	<b>1</b> 0	2	Q	2	9	2	158 158 158	!

ZIECON		<b>2</b> 1			2	2 2		8	8	1.28	F. 68	82.2	2 8	R 3	6.6	9.00	8	8 8 4 9	R 8	R 2	=======================================	<b>7</b>	3	의 : 시 :	; ;	3	3 5	R 8	3 3	8	2 8	2 2	80	2.7	82 °	8.	<b>8</b> 8	R 8			=	•	7
I 3		3:		8	8 c	8:3	2 2	3	9.3	7.38	7.20	8 2	<b>3</b>	16.78	15.40	14.10	13.10	12.48	12.8		7	=======================================	10.60		4 4	13.86	200	15. 2	: 8	11.60	3 :	7	3	16.28	84	12.40	12.51 5.52	10.4		1.3	11.50	11.20	8
STRUBO TITON	1	= 1			8:	8 3			3		3:	8	2 S		3	=	=	2 :				7	3			=	3			=			8	1.70	8	2	3 3				=	8	ž.
RUTILE STRUBO Xcount Xcount		<b>8</b> 1		: :	1:0	2		Į	F		8	8 :	3 5		2	2	=	2 3	3 3			=	2	2 : 3 :		=	3 3			=	2 1		3	8	=	3	3 3				8	= :	=
ᄩ		8 1		3	3	8:	B 1		I	3	=	= :	8 1			8	=	<b>3</b> :	<b>3</b> 1			=	3			=	3 3			=	3 5		3	8	=	2	3 1		3		8	2 :	2
MET TON		= :	3	8 8	8	8:	8 1	8 8		1 8	=	8:	8 2		3		8	8 :	<b>8</b> 1		1 8	8	8:	= :		8	8:		3 8	=	8 5	3	3	8	=	8	3 1				8	8 :	=
VALUE PERMIT ICHAZ I		<b>3</b> :	e		2	<b>a</b> :		: 4 : 3			3	2	<b>.</b> .			8	8	8	2 : 2 :			2.60	87.7	33.		2.30	88.6	R 2	8	3	e e	R	22	8	4.10	n n	a e	8 8	8	1 25		2.80	
FLDSP HATH Kounk You		93.1				ri ·						2.7				# P										8		R S	R S			2 2	t #1	8	3	4.78 3.	<b>.</b>		? =	: 8	<b>8</b> 5	2	_
P P.F.D	- 1	8 m					3 8			3 4									8 2				3.10			-		-	_ ~	_	99 7	4 -					÷ .		*	: <del>-</del>	m 9	mi i	ri ⊈
K.F.DGP P		3	•		1.9	_	_	7 7		-				7 3 N -		1 2			= ;				_	_			_									3.	37				-	9.1	-
a Scour		7		2	E. 28	8		\$ 5 5 5	-	i ភ	-	•	_	7 5 6 4	-	4		_	_ `		2 2	_		_				-		_	M 1		2.5	4	4.69		69.3	•		86.5	1 .79	_	96.19
OVENERAL C		47.8	2		-	11.38	# S	1 1		R 85	14.98	16.78	17.70			17	7.3	15.20	<b>M</b> :	4	1 1	15.10	15.78	16.4		_	12.68	_ `	4 4		_			195	4	10.00	7:	2 2	1 2 2	2 2	15.40	-	ź
HE BOTTS		-141.00		-213.10		10 T	100 to	# # # #			61.38	4	39			3	19.68	49.4	# I	다 다 다	1 5	14	3	2.3	8 F	7	# B	<b>3</b> :	7	200	52.7	2 2	9	4	3	-3.E	#			7 T	,	•	Ę,
The Co		8		R S		17.4	19.5		8 9	<b>3</b>	31.8	20 20	M.18	R 1	3	<b>8</b>	100	19.10	20 E	3 S	# 4 5 K	2	27.38	27.40	2 3	지	15.78	8 : ::		2.5	ន ដ		2 5	1	3	8	12.5	15.66		19.5	21.78	24.4	27.00
D. MICC 1 thk (m)		19.30	8 : 14 :		3	17.8	# :			1 4	17.58	17.38	19.8	<b>8</b> 8	2 2		17.20	17.98	7 :	8 S		1 25	23.15	2	7 T	12.18	15.28	17.16		19.00	19. 40	त्र : र्ह्म :	2 2	8	3	A. 10	<b>?</b>	15, 18		7.71	9	19.60	29. IB
the (m)		8	2 :		3	= 4	3	3 5				3	3	3 5				3	3	3 3		3	=	=	3 3			3		3	=	3 3		Į	3	3	=	2	3 3		3	=	8
M NECOTI		7.4	8	R A		7:	33	8 5		3 5	3	**	3	주 : 리 :			3	27	13	3 3		8 8	8	3 4	2 2		8	2.5	7 7	3	8	2	7 8	7	8	6.7	=	<b>3</b>	2 ;	7 2	3	8.	2.5
GARTERN PLICEN LP.NICC MD.NICC LLANICC INLINIES OFFENDIN GLIGHTZ N.FLUSP P.FLUSP WYNINS PREPART MONZ the (a) the (b) Scours Scours Scours Scours Scours Scours		7.69	_	Z P	_	9.6	8.1	<b>?</b> :	# # *! c	9 2	3	<b>8</b>	9.10	2 8	# <b>1</b>	M 2	8 2	14.88	13.10	8 : =	<b>3</b>	2 8	11.30	10.00	9 9		2.1	8	R 1	8.4	14.10	8 i	2 2		3	87.6	10.40	= =	2 ×	7 4 7 4	# # ±	13.60	12.50
TO WE		8	88	8 9		8	3	2 2					=	3 3				=	=	2 :	2 2		3	3	8 5			3			3	2				3	=	8	3 3		8	3	2
-			=	ត្ រ		3	28	= 1					3	<b>3</b> :	= 8	R 3	17	110	=	3	3 :		3	3	3 1	3 5	3	<b>8</b>	3 5		=	3	2 2			8	<b>1</b>	23	<b>用</b> :		2 8		2
J" _		8	87.68	# : <b>#</b> :		3	8	8; :	8 1	8 8		2 2	2	3	5 5		: 3	8	8.	= :	3 1			8	8 3		18	8	2 8	R 55	=	3	2 1		8 M	8	<b>8</b> 3.6	99.10	<b>3</b> ;	2 F 3 S		8.6	98.38
Gental Son	- 1	20	70 E	S F			8	<b>8</b>		<u>s</u> 8	: s	35	3	83 1	d a		8 86 8 79	=	8	3 3	# : # :			8	3 :	* *	13	8	2 1 2 1	8 8	3	8	2 : 2 :			6	2 3	6 9 1	83	= =			8
	- 1	55	<b>-</b>	<b>-</b>			•	<b>-</b>	eri (				-		ni •	11.5	7.4	16.3	14.0	17.9	18.6	2 6 6	4.22	24.0	7.7		1	17.2	14.6	19.2	19.4	21.0		7.5		16.	17.9	19.6	18.4	5.61	2 2	. a	3.6
-		45	-	•			•	•	•	•			•	•	•	•			•	•	•	•		=	2:	,	; ;	3	3 :		•	•	•	, .				•			•		
	9	0.57280	.0 554000.	. 0 308308.		34.56	. 8 SSB488.	. STR. 20	. S. Been	.0 254886.	2744	27.22	99795 0	. 0 5000m.	2,000	3436		25.000	. 0 56480	.0 359580	9446	20,72	. 0 55650	. 6 593688	9 536 80		250	9	- 55.800 - 55.800	16.95 B		•	•	2000				9	•	-	A 56.06.00		
		4288	42000		1 6		2448 <b>8</b>						3440							26.188	3											_			TANK B			5 354488			5 254466		
	9	171.00	121	20.07		Pb. 517	<b>28.</b> 466	86.415	26.36.5	20 314 20 314		PA. 161	100	8	<b>3</b> 1	<b>8</b> 1		-	-	-	<b>8</b> 3			\$	28	<b>S</b> 1	M. 465	8	# :	# 313	8	1 20.164	<b>z</b>		2000		8	88.456	\$	_		A 211	
ATTI DE	9	38,912	31,912	36.912		3	3	<b>3</b>	정	2 2 3 3	N K	N 12	집	2	12.21		בו מולים	22.213	212.52	32.21S	22.22	2 2	12	2.210			N K		20 169	2 5 E	3	22.168	2 2 3	1912		2 2							i 23
		11		_			_	_	_					_	-	•	2 2	3	3	7	3	7 3	7	3	ង	M S	2 2	3	3	3 3	3	3	3	2	2 %	3 3	3	3	3			2 3	3
DLOCKTO AREA LL	(sq. ks)	27.040	<b>₹</b>	23.08	₹ 3 :	4 2	23.6	₩.	₹ %	ਤ ਹੈ ਹਵਾਲੇ		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	<b>₹</b>	₹ 73	3	<b>3</b> 3	<b>1</b> %	3	ន	<b>₹</b>	ສ	ត់ ន	1 a	2	ë.	7	1	ส	<b>₹</b>	zi a	i ສ	ដ	ສ່	ត្ល	ส์ 🤻	9 2	zi	ส่	E E	<b>8</b> 8		3 %	1 8

- š	II.		• •		• (			_		_		_		-		_			_				_										
ZIRCON	- 1	1 7	8 8	3 8		: :	-		-		 	2.0	4 4	3	5 5 5 6	1	 - 2		-	# R	1.0	2.8	w 4	23			8.	1 4	2	- 5	8 :	3 8	1
TITAN F Kounk		16.28	9 9	1	# S	12.00	8 :	2 7		10.50		10.00		# # # # !	3.:	8:1	# # # # # # # # # # # # # # # # # # #	2:1:3		의 주 약	2 5	3	8 8 5 4	2 =	8	R 8	7. 1		3	2 2	2 2	8 5	1
STALIND 1		1.68	8.1		2 1		3 3	2 S	6.28	3 5	R 83	8.7	2 2 1 1	8 2		8			_	_	87.78	8	8 8 01 -	3 5			3:			<b>.</b>	8 1	ļ 8	1
AUTILE SI Scount		8 8	= 1	8 8	= 8 1	18	8 :	8 8	8	8 8	8 8	8 8	1 2	8 1	8 8	81	8 8	8 8	88	2 2		8	8 2	8:		22	21		2:		21		
F 4	- 1		21		e 1	, e	•	• •		<b>.</b>	# <b>#</b>			•		-		•		<b>-</b>	-	-	<u>ئ</u> م	4	<b>.</b>		3		4	3 3	3 3	13	4
T MD40	- 11	4 -3	3 3	3	3 -	:3	3			3 3	3 3	2:		3	3	3				3 3	3 3	3			H	3 -			3				
REPHET I			3 3		3 4		3		8	3 3		3 3	3	3 2		3				= =	33	3	1 N					3 3	3 3		3 3		
ILFLESP P.FLESP HYMING PASSHET MENGZ Kowank Kowank Kowank Kowank Kowank	1	2 2		8	4 r	4 4		# E			2 %	8 2	8 8	7 5	8 8 8 8	<b>3</b> 7	2 2	3 5 M		7 7 7	2.5 2.5 5.5	8 2	1 5 1 4	ر ا ا ا ا		R 25	8 8 mi vi			7 R			12.3
FLIED Acount	S. M	2	<b>8</b>	2.4	2 Z	8 1 13	8 %		86.5	2 ×	2 2 2	R 1	8	R = 4	3 4	<b>2</b> 8	1 3 1 1 1 1	2 A	3	3 R	~ m	<b>3</b> 3	3	2 3 4 4	21		6 H	R	28		<b>8</b> 9	6.28 6.28	3
FLDGP P	1	8	<b>≘ 3</b>	8	<b>3</b> 8	8	8 1	, A	8	<b>3</b> 3	: 8	8 5	8	M S	Ą	8 5	3	3 3	80 1		8 8	88	3	<b>3</b> 3			25.2				8 =		
172 [f.] :ount 1	1	8	- 8 8		 8 7	18	81	: 8	8	<b>-</b> -	18	<b>20 3</b>	3 8	 	_		1 M	<b>8</b> 8	8:	2.8	교리	a) e	2 =	지 # 로 =	ai .		= 2		<b>≈</b> 8				2
ON GLANTZ (a) Scount	1 12	2	<b>a</b> a	3		2	38	i s	91.			20 20	3	<b>a</b> -	4	29 1	<b>i</b> ≃	9.5			<b>S S</b>	25.3	-		67.6	4	24 4 24 4	8	# 12 m		81.8	2. 2.	
G the (a)	18.6		2.6 9.3	-		12.4	451	9 2	14.7	2 2	1	2.5	14.78	7.6	4	<b>1</b> = <b>1</b>	12.4	17.20	15.9	14 4	5 K	3 2 2	14.2	~ d	4 6	2 2			3 3		3 3	8	8
	56.22	\$	-19.68	-M		3	왕 2		<b>3</b>		19	# 5 F	-31.4	<b>3</b> 2 2 2 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	8	28	7	2 H	*		# # # #	35 7	2	년 2 2 3	3 2	2	3 3		3		3 3	3	8
10.N10C L4.N10C 1) the (a) the (a	25	8 · 5	5 th	8	12.6	15.98	3.5	12.0	3	# 4 % %	2 2	2 2	2		4	8 5	19	17.68	# 15 m	2 2 1 xi	នេះ សំគ	20 N	3.5	# # # #	20 a	3	3 3	3	2 2		2 2		8
THE COLUMN	87.65		3 R	200	# # 4 <u>4</u>		<b>8</b> 7 5	8 3	9.10		3 3	<b>8 3</b>	7.20	8 S	3	2 2		2	37.50	RR	想黑	2d 2	2	7 B	3 2	3	===		<b>2</b> 2		8 8	8	8
UP.NIGC M	3	8	B	81			2 7	3	= 1	8 8	8	a a		2 8	8	* *	8	= = = =	8:	88	2 2 2	81 S	88	3 2	8 8	8	::		<b>3</b> 1	: =	22	2	3
1 (E) (G)	8	2	 B 2	81	2 25		21		m:		. <del></del>	2 2	2	=	n:	4 4 • 4	8	ණ හී බි	3 2			d		<b>-</b>	<b>d</b>			-	3 3	1 3	33	-	-
CLATERN PLICES (P.NICC 10.NIC thk (a) thk (a) thk (a) thk	m	4		_	2 70		<b>-</b> -	. <del>.</del>			<b>H</b>	2 %		<b>4</b>	<b>d</b>	3 -	: -:	<b>-</b>	<b>-</b>		9 2	<b>∌</b> 6	3	3 3	m 2	-	-	-			33		9
	13	10.4	10 70 17 16			=	12. A		m ≥ = :	4 2		표 제 6 6		7 7			11.28	12.6	12.68	12		ਨੇ <b>=</b>	14.10	7 2	3 5	2	= =	=	3 3		3 3	3	8
¥ 6	3	3		3	1 3	8 3			8 1		3	2 2	3		8		3	= =	8 8			3 3			3 3			2	2 2 4 4		: :	8 :	=
SILT A M	3	8	2 2			3	3 2		8 1		8	2 2	m 8	n A	<b>8</b> 3	3 8	8	<b>*</b> =	8 1						3 2	2	= =	8	<b>8 8</b>	2	2 = 3 =	<b>8</b> 8	<b>3</b> 7
	1 -	4	3 2	3		€ (	- 4	_		_	-	-	•	<b>4</b>	•	4		4	-	3	33			3 3	3 4	4	-					_	_
	96.58			7.60 0.3	9.00 P.13	9.20		8	28	RR	85	R 8	37.0		2 ·		2			3	3 8 3	R 8	3:	3 R	8 8	<b>用</b> :	2 2	_	- 4 - 8	_	3 8	2 :	₹
2 ¥	1.00 99.90			28 97.88 6.3	_				3.2		8 :		_							•		# # # #	24	3 R	<b>3 3 3 3 3 3 3 3</b>	<b>8</b> 7	2 S.	97.40		2 3	23 25 25 25 26 28	99.80	4.25 4.25
A N N N N N N N N N N N N N N N N N N N	1 6.00 39.	8 8	8 . Z	8.3	3	2		3	21		3		29.16	2 7 2 7	* 5	2 =	9						14.20 65.40	2 % SI:		6.68	2.10 97.20	2.68 97.40	# # # # # # # # # # # # # # # # # # #	F. 35 95.78	2 E	98.0	 99.
(a) st % st %	. CL. 1.00 99.	25 B 25 B 25 B 25 B 25 B 25 B 25 B 25 B	3.7 2.50	16.9	24.5 A.40	12.6 1.29	24.5 4.00 24.5 4.10	0 21.2 6.00	22.7 6.8 1		27.1 0.00	33.6	9.5 29.16	16.7 2.80	17.8 1.40	19.3 6.10	20.4 0.10	2:5 C.10	1 25.9 A.W.	22.9	28.9		9.4 14.29 65.40	6 17.6 1.10 St. 20	18.6 1.78 99.88 18.6 1.28 99.88	0 19.3 6.66 99.30	8 21.9 2.10 97.30	.0 25.6 2.60 97.40	# 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	55.00 B. 00 95.00	8 .2.2 1.28 1 .3.3 1.88	6 34.1 1.89 99.	8 36.3 <b>6.88</b> 99.
CAST LEPTH CHRALL SAND (a) (a) at 15 at 15	SHARK 8 25.1 6.00 99.	2000m.0 25.6 p.m 99.	531284.0 3.7 2.50	8.3	24.5 A.40	12.6 1.29		0 21.2 6.00	21		LO 27.1 0.00	33.6	29.16	16.7 2.80	* 5	19.3 6.16	20.4 0.10	35000.0 22.2 6.10		574486.8 25.9 8.88	264000.0 28.9 0.10	253546,0 Mc. 0,18 95.95	S21680.0 9.4 14.20 65.40	53(206.0 17.6 1.10 98.70	536000 18.0 0.70 99.00 54000.0 18.6 0.20 99.00	0 19.3 6.66 99.30	64230,0 21.9 2.10 97.90	612300.0 26.6 2.60 97.40	622446.0 38.1 0.30	627200.0 30.9 0.30 59.70	63680.0 33.3 0.00	641688.8 34.1 8.88 99.	646488.8 36.3 8.88 99.
(a) (b) (c) of 5 of 5	SHARK 8 25.1 6.00 99.	2000m.0 25.6 p.m 99.	531286.0 3.7 2.50	0 535406.0 16.9 1.90	.0 54550L 0 2L 5 L 40	0 SSM40L 0 22.6 0.20	. 55000. 34.5 4.10	0 55480E.0 21.2 6.00	0 359586.0 22.7 0.00 1	0 57228.0 25.6 0.00	0.504006.0 27.1 0.00	1 3936.00 29.6 0.00 1	0 S21646.0 9.5 20.10	531200.0 16.7 2.00	0.53500.0 17.8 1.40	0 545500.0 19.3 0.10	.0 25040L.0 28.4 0.10	35,000.0 25.2 0.10	564864.0 22.9 0.00 1 569564.0 24.4 0.00 1	574464.0 25.9 0.00	2/200.0 2/.0 0.10 26/000.0 20.9 0.10	250 Sept. 10 25.7 10.00 25.20 10.00 25.20 10.00	9 S21600.0 9.4 14.20 65.40	531286.0 17.6 1.10 98.70	536000 18.0 0.70 99.00 54000.0 18.6 0.20 99.00	545500.0 19.3 0.00 99.30	642200.0 21.9 2.10 97.90	612800.0 25.6 2.60 97.40	61/646.0 28.4 1.38 622446.0 36.1 0.30	627200.0 30.9 0.30 99.70	63688.0 33.3 0.00	641686.8 34.1 8.89 99.	8 646488.8 36.3 8.88 99.
(a) (b) (c) of 5 of 5	354488.0 584888.0 25.1 8.80 99.	254480.0 544680.0 25.6 p.mp 99.	54%64.0 53124.0 3.7 2.50	54854.0 53544.0 16.9 1.90	34964.0 54564.0 24.5 0.40	12.6 1.29	549546.0 354046.0 26.5 6.10	549640.0 364880.0 21.2 6.00	22.7 6.8 1	54564.0 57924.0 25.6 6.00	549584.0 584884.0 27.1 0.00	345500.0 353500.0 23.6 0.00 1	9.5 29.16	SHAME 6 \$31200.0 16.7 2.30	17.8 1.40	54688.0 545686.0 19.3 6.10	SHABBL 0 359488.0 20.4 0.10	344884.0 SARRA, 0 22.2 4.10	1 25.9 A.W.	34458.0 57448.0 25.9 8.00	544506.0 254006.0 28.9 0.10	544886 9 593586 36 8 6 16 95 36	24000.0 S21600.0 9.4 14.20 65.40	Section 531206.0 17.6 1.10 98.70	546888.0 535888.0 18.0 0.70 99.00 546888.0 18.6 0.20 99.00	S46000, 8 34560.0 19.3 6.00 99.30	573600.0 642300.0 21.9 2.10 97.90	573500.0 612000.0 25.6 2.60 97.40	57.5540.0 617540.0 28.4 1.30 5735540.0 622440.0 30.1 0.50	573500,0 627200,0 30,9 0,30 99,70	573646.0 636846.0 32.2 0.20 573600.0 636840.0 33.3 0.00	573680.0 GAISSES 34.1 0.00 99.	573600.8 646400.8 36.3 0.00 99.
	B0.118 EXHAM. 8 SHAME 8 25.1 6.88 59.	60.659 354480.0 556880.0 25.6 8.80 99.	80.669 549680.8 531280.8 3.7 2.50	NA AN 528 549540 535400 16.9 1.90	B3 80.517 54560.0 54560.0 20.5 0.40	M3 M4.465 549540.0 55940.0 22.6 0.20	MGS 204.412 545504.0 355504.0 22.3 9.20 MGS 204.354 549504.0 355004.0 24.5 0.10	863 86.313 549586.0 554886.0 21.2 6.80	549548.8 55958.8 22.7 6.48 1	M2	MAI 80.110 549500.0 584000.0 27.1 0.00	000 04.005 373544.0 355594.0 25.6 6.00 1	M. 86.771 SAMBOLD S21580.0 9.5 29.10	M 06.670 54400.0 531200.0 16.7 2.80	H9 89,619 544880,0 535880,0 17.8 1.46	00.517 54400.0 54560.0 19.3 0.10	M9 D0.466 54400.0 33040.0 20.4 0.10	M. 355 54400.0 35000.0 25.2 0.10	00.314 544800.0 354800.0 22.9 0.00 1	00.212 544500.0 574400.0 25.9 0.00	00.110 SH200.0 SA400.0 23.9 0.10	00.050 344000.0 150000.0 25.7 0.00 55.20 0	26.771 54000.0 521500.0 9.4 14.20 65.40	60.670 S46000.0 S31200.0 17.6 1.10 98.70	84. 619 348884.0 335884.0 18.0 0.70 99.80 84.35 84.358 348884.0 34888.0 18.6 7 0.26 99.80	66.517 54800.8 54560.0 19.3 6.00 59.30	75, 204 573640, 0 25440, 0 20, 8 1, 25 50, 50 75, 50 75, 50 57360, 0 60, 250, 0 21, 9 2, 10 97, 90	79,082 573580,0 51280,0 26,6 2,60 97,40	73, 731 37,5580,0 617,580,0 28,4 1,38 79,780 573,580,0 622,480,0 39,1 0,50	79.649 573604.0 627204.0 34.9 8.30 99.70	79.5A7 573600.0 636000.0 32.2 0.20	79.496.573600.0 641600.0 34.1 0.00 99.	79.445 573600.0 646400.0 36.3 0.00 99.
	M4 32 12 04.110 354404.0 584804.0 25.1 6.00 99.	M4 32,124 60,639 354460,0 566600,0 25,6 0,60 99,	22.084 80.669 549680.0 531280.0 3.7 2.50	22 864 80.619 54560.0 53600.0 16.9 1.90	22,863 80.517 549680.0 545680.0 28.5 0.40	22,683 98,465 549569,0 52948,0 22,6 6,20	FF 22-663 DB.364 54564.0 55684.0 29.5 0.10	2.063 80.313 549500.0 354800.0 21.2 0.00	22-862 86-253 54958-8 55958-8 22.7 6-88 1	54564.0 57928.0 25.6 0.00	22.001 80.110 54550.0 58400.0 27.1 0.00	22.000 0A.000 54560.0 55560.0 29.6 0.00 1	22-M1 88-771 SHABBA 221586.0 9.5 29.16	2.041 06.670 54400.0 531200.0 16.7 2.40	22-040 80-619 544880,0 536880,0 17.8 1.46	32.040 00.517 54400.0 54560.0 19.3 0.10	22.040 80.466 54400.0 330400.0 20.4 0.10	2.639 M.35 SHORE 55000.0 2.2 6.10	22,639 66,314 544666,6 554666,8 22,9 6,00 1 22,639 66,253 54466,8 55566,8 24,4 6,6 1	32.639 50.212 544500.0 574460.0 25.9 6.00	22,038 88,110 544880,0 554880,0 20,9 6,10	32.037 80.000 544500.0 53330.0 10.0 55.30 32.037 80.000 544500.0 53330.0 10.0 10.0 59.30	31.998 db. 771 34000.0 321600.0 9.4 14.20 65.40	31.997 60.676 SARREL 0 SUIZREL 17.6 1.10 98.70	31.997 84.619 540004.0 536004.0 14.0 9.70 99.80 31.997 84.548 540004.0 14.6 × 8.28 99.80	31,997 86,517 54808,8 345,68,8 19,3 6,88 99,30	Z. 25/ 75, 25/ 27, 25, 26, 6, 25, 26, 6, 25, 26, 26, 26, 26, 27, 26, 27, 29, 27, 29, 27, 29, 27, 20, 2	32,255 79,842 573640,612364,0 26,6 2,60 97,40	22.294 79.700 573.00.0 623.00.0 23.14 11.30	22.294 79.649 573646.0 627286.0 34.9 4.30 99.70	22.231 79.347 57360.0 6.22000.0 22.2 0.20 22.231 79.547 573600.0 63600.0 33.3 0.00	22,292 79,496 573680,8 641680,8 34,1 8,89 99,	2.291 79.445 57360.0 646400.0 36.3 0.00 99.
(deg) (a) (a) (b) ut 1 et 1	23.040 22.125 80.118 SHARL 8 SHARL 8 25.1 8.00 99.	M4 32,124 60,639 354460,0 566600,0 25,6 0,60 99,	11.142 22.084 80.669 549600.0 531200.0 3.7 2.50	NA AN 528 549540 535400 16.9 1.90	23.040 22.083 80.517 549600.0 545600.0 20.5 0.40	M3 M4.465 549540.0 55940.0 22.6 0.20	23, 640 12, 663 16, 354 549540, 8, 55860, 8, 25, 6, 18	23,040 22,063 80,313 549600,0 554800,0 21.2 6,00	549548.8 55958.8 22.7 6.48 1	23.044 32.062 04.161 54560.0 57920.0 25.6 0.00	MAI 80.110 549500.0 584000.0 27.1 0.00	23.044 22.000 04.000 34500.0 33500.0 23.6 04.00 1	M. 86.771 SAMBOLD S21580.0 9.5 29.10	23. Mo 22.0H 08.670 SH400.0 S31200.0 16.7 2.40	H9 89,619 544880,0 535880,0 17.8 1.46	23.040 32.040 00.517 544800.0 545500.0 19.3 0.10	M9 D0.466 54400.0 33040.0 20.4 0.10	2.639 M.35 SHORE 55000.0 2.2 6.10	00.314 544800.0 354800.0 22.9 0.00 1	32.639 50.212 544500.0 574460.0 25.9 6.00	22,038 88,110 544880,0 554880,0 20,9 6,10	32.037 80.000 544500.0 53330.0 10.0 55.30 32.037 80.000 544500.0 53330.0 10.0 10.0 59.30	31.998 86.771 540006.0 521606.0 9.4 14.20 65.40	31.997 60.676 SARREL 0 SUIZREL 17.6 1.10 98.70	31.997 84.619 540004.0 536004.0 14.0 9.70 99.80 31.997 84.548 540004.0 14.6 × 8.28 99.80	31,997 86.517 SABBE 8 SASSBL® 19.3 6.86 99.30	PM 22.2% 75.30 3/4500.0 56230.0 21.9 2.10 97.90	32,255 79,842 573640,612364,0 26,6 2,60 97,40	73, 731 37,5580,0 617,580,0 28,4 1,38 79,780 573,580,0 622,480,0 39,1 0,50	22.294 79.649 573646.0 627286.0 34.9 4.30 99.70	22.231 79.347 57360.0 6.22000.0 22.2 0.20 22.231 79.547 573600.0 63600.0 33.3 0.00	MB 22,292 79,496 573680.8 641680.8 34,1 8,88 99,	573600.0 646400.0

ZIRCON	1			=	2 5	2 <b>8</b>	2.80	2.5	2 F	2	=	8	8 S	ŀ		3		2 %	8.2	2 Z	8	2	7 7 8	2		3	3 3		8	8 I	1 m	2 <b>2</b> 5 M	8.3	3 8 N -		<b>8</b>	2 2		3
<u>                                   </u>				25	27		2	2			=	8			3	3	2 S	R 2	8	3 3		3		=		3	2 3	8 3 4 4	=	2 3		3	3			2	3 3		4.80
STALIND TITON				3	<b>M</b> 3		3	2	3 3		3	=	3 :		3	3		2 2	3			3		=		3	3		=	3 3		3		3 3		=			6.3
RUTILE S Scount		3 3		3	7 2		=	3	2 2		3	2	3 :			=	2 5		3			3		=			3 3		8	2 1		3	3		3	8	3 3	2 5 6	6.3
1 3		3 3		8.3	7 .		3	2	2 2			2	3 3			3	2 5		3			3		3	3 5		3		=	3 3		3	8			2	3 3		8
Acount Acount		3 :		=	3 :		=	=	= =	ŀ	3	8	2 :			3	3 3	8 8	=	3 5		= :		=	3 3	3	3 3		3	3 3		3	=			3		3 3	8
M.F.LIGO P.FLIGO MYMING PASPART MONZ S. Acount Acount Acount Acount Aco		2 1 1	8 3 4 4	3	# :	1 <del>4</del>	3	4.28	8 3 mi r	3	8	<b>8</b> .4	3 :			8	2 X	1 M	30	2 2	8	8 i	8 A 4 4	3	2 E	8	8 1 10 1	3 4 4	#	2 8	R g	3 i ri	<b>8</b>	<b>2</b> :	3	4.7	의 ( 당 )	2 8 d id	55. 25.
FLDSP H		2 2	2 3	8.3	21	2 2	=======================================	10 N	4 4 2 1	8 8	8 5	2	<b>8</b> 5	R 3	8 37 4 4	6.2	3 8		F.7	2 S	# #	4 i	2 2 4 4	<b>6</b>	4 4 4 4	3	8 8	9 8 4 4	W.	<b>3</b> 1	R R	3	8	<b>8</b> 5	(T)	6.40	<b>3</b> 7 :	# # 6 6	80 90
Acount		3 2		9,6	# 1 - 0	1 ~i	2.5	2.8	2 3	3	2	2	ति ह	R #		8	3 3	8 8 1 2	35 21	23	3	ਨ ਪ	2 2 (i (i	8	2 2 2	7	= 3	3 3	हा ती	35 c	2 2		2	<b>5</b> 3	3 3	1.00	99.5		
M GLIPHTZ K. (m) Yeounk			1 2 S		87.59	, A	65.40	77.38	7 F	2	8.19	91.80	8 8	1 2	1 3	3.	2 F		76.48	= 1	3	8:10	2 2 2 2 3 2	2	3 2	8	3 3		=	2		2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	2	2 2 3 3	2	63.30	200	8 7 7 8 7 7 8	8.
WESTER D	1	8 1			8 5	2 S		2	2 1		3	=	3 3						17.80	3:		3	33	=	3 3		3		17.78	9 19 19	2 2		=	3 3		=	3 3	2 S	3
th (a)		3 3		=	3 3		3	3	3 5			=	2 2			=	3 5		67.00	3 3		= :		=	3 3		3		8	9 X			=	3 3		3	3		3
N LP. NICE NO. NICE LIK NICE HAL BUTS CARBING (a) the (a) the (a) the (a) the (b) the		3 3		=			3	=	3 3			3	= 3			3			8			8		=			3			23.52	•		=	3 :		8	3		8
The (e)		3 5		3	= ;		2	=	= :			2	3 3	2 2		3	3 5			8 5		3	3 3	=	2 2		3	2 2		8 to 10			3	3 :		2	3	2 2	2
the (e)		<b>8</b> 8			8 :			8	<b>8</b> 1			3	8 :				3 5		=				3 3							33		1 8	8	3 1		3	2	2 2	2
		_	_	_	•	-	•		•			•	_	_	_	_		-	_	-	_	_		_			_		_	_		_	_		_	_			
the (a)		3 3			22				22								2 2		7.8																	8	8	2 2	
# 100 mm				0.0	0.00				200														2 2	8		8	8		7.00	3 7			9.00 0.00			9.0	0.0		
CLIATERN F thk (c		0.30 0.00 0.00		0.60 0.00 0.00	<b>-</b>								0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0			L'30 C.00 C.00	2 1		8	2 2		9.8	2 2	0.00	3 3		0.00		9.90 7.80	3 7						0.26 0.80 0.80	0.40 0.00 0.00		0.30
T CLAY QUATERN	-	1.10 0.30 0.00		2.10 0.60 0.00 0.00	<b>-</b>								C. 10 C. 00			LB LB LB LB	2 1		8	22		9.8	2 2	0.00			0.00		9.90 7.80	3 7						4.4 0.24 0.46 0.48	1.00 0.40 0.00 0.00	2.19 1.00 0.00 0.00	6.76 6.36 6.86 6.80
SILT CLAY QUATERN		20 20 00 00 00 00 00 00 00 00 00 00 00 0		2.10	70 2.58 6.70 6.			1				20 0.00	00 C.10 C.			8	20 MI 25 MI		100 600 9.30			L. L. L. 5.6 L.		****			0.00 0.30 0.00 0.00		76 0.00 0.00 7.00	06 6.00 0.00 9.70 A.40				21		3	1.00	2.1. 2. 2.1. 2.	67.9
SONO SILT CLAY QUATERN		C. C. C. C. C. C. C. C. C. C. C. C. C. C		2.10	70 2.58 6.70 6.			1.10 %.30 6.00 6.00 6.00 6.00 6				20 0.00	. O. O. O. O.	2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		8	20 MI 25 MI		44 Lm Lm 9.98	22		L. L. L. 5.6 L.	2 2	***			0.00 0.30 0.00 0.00		76 0.00 0.00 7.00	99,06 6,00 0,00 9,70 6,40				2 1 d d		3	1.00	2.1. 2. 2.1. 2.	0.00 99.00 0.70 0.30 0.00 0.00
ESCREE SOOD SILT CLAY QUATERN		4 6.00 26.50 5.10 6.		6.30 97.80 2.10 G.	6.68 79.78 2.58 6.78 6.		2.	5 1.10				A. 80 99.90 A. 60 A.	A.00 99.00 A.10 A.			C. 10 94.00 C. 10			8.64 99.44 8.80 8.80 9.90		C.4 99.66 C.80 C.80 C.80 C.80	6.10 59.30 6.00 6.00 5.00 6.00		0.00 99.90 0.00 0.00 0.00			0.00 99.00 0.60 0.30 0.00 0.00		4.28 99.76 9.08 0.08 9.98 7.08	A.23 99.08 A.00 B.00 9.70 A.40			6.00 100.00 6.00 6.00	F. B. 100. B. C. B		3	0.00 98.50 1.00 0.	2.1. 2. 2.1. 2.	67.9
GROWEL SOAD SILT CLAY QUATERN		0 44.4 0.00 90.50 1.10 0.		47.8 4.39 97.00 2.10 G.	0 46.6 6.60 79.70 2.50 6.70 6.		27.1	0 27.5 1.10	29.3 6.78	25.5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 35.1 6.00 99.30 6.00 6.	0 37.3 0.00 99.00 0.10 0.			. 35.9 C. 00 34.00 C. 00			25.6 4.68 99.48 4.88 4.88 9.98			1 26 6.16 99.90 6.00 6.00 9.00 6.00		34.6 0.00 59.50 0.00 0.00 0.00 0.00	23.8 c. 18 93.74 c. 28 c. 18 c		36.4 6.00 59.00 6.60 6.30 6.00 6.00		1 25.2 4.28 59.76 4.48 4.48 9.59 7.88	25.8 5.4.5 99.06 0.00 0.00 9.70 0.40			1.35.1 6.48 180.00 6.00 6.00	37.5 0.80 196.80 0.80	33.3 F. W. 93.28 F. W. 9.	41.0 0.00 99.40 0.40 0.	45.1 0.00 30.50 1.00 0.	0 50.7 0.00 97.50 1.70 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 48.2 0.00 99.00 0.70 0.
EAST DEPTH SHOWEL SHOW SILT CLAY QUATERN		.0 656000.0 44.4 0.00 99.50 1.10 0.	0.650000.0 47.5 q.10 39.23 11.30 q.	67440.0 47.8 0.30 97.00 2.10 0.	LO 677200.0 40.6 0.60 79.70 2.50 0.70 0.		1.0 66664.0 25.7 1.70	LO 612800.0 27.5 1.10	1.0 617600.0 29.3 0.70	A 527240 A 72 C A 10	1.0 62200.0 3.0 0.10	.8 635888.0 35.1 4.00 99.90 0.00 0.	L. 6. 641600.0 37.3 0.00 99.80 0.10 0.			L. 6.6.000L. 3 S. 9 L. 00 34.00 C. 00	0.0 655500.0 US. 4 0.10 95.90 3.00 1.30 0.00	MALE STANDARD NAME OF AN OFFICE AND ALSO ALSO ALSO	A. 1 6422A. 1 25. 6 4.40 99.40 4.00 4.00 9.90	00.0 GARGOLO 25.9 0.66 99.44 4.00 0.00 0.00 0.00	04.0 01/200.0 (3.4 0.44 29.56 0.00 0.00 0.00 0.00 0.00	R. B 62240K. B 2.6 0.10 99.90 R. 00 R. 00 9.00 A. 00	1.0 627204.0 34.9 44.00 59.30 6.00 6.00 5.00 6.00 6.00 5.00 6.00 5.00 6.00 5.00 6.00 5.00 6.00 5.00 5	AL S 535000.0 34.8 0.00 99.90 0.00 0.00 0.00 0.00	00.0 GA1GOR, 0.35.0 G.00 99.70 G.20 G.10 G.00 G.00 G.00 G.00 G.00 G.00 G.0	1.0 551200.0 45.2 0.00 30.70 0.30 0.44 0.00 0.00	8.8 655888.8 50.8 8.00 99.00 8.64 8.38 8.06 6.00	1.0 550000.0 57.0 0.00 57.30 1.70 0.70 0.70 0.00 0.00	L.O. 556400. 0 26.2 0 29.70 0.00 0.00 9.50 7.00	.6.642394.0 25.8 % 6.24 99.06 6.00 0.00 9.70 8.40		617500.0 31.9 0.30 99.70 0.00 0.00	. B 522484. B 35.1 6.18 189.18 6.18 6.18	627286.0 37.5 8.00 106.00 8.00 8.	0.0000000 0.	641546.0 41.0 0.00 99.40 0.40 0.	0 64640.0 45.1 0.00 98.50 1.00 0.	651280.0 50.7 0.00 97.50 1.70 0.00 651280.0 6.01	568886.0 46.2 6.00 99.00 6.70 G.
NORTH EAST DEPTH GRAVEL SHAD SILT CLAY CHATERY (a) (a) (a) in at 5 at 5 at 5 at 8 thk (i		343 573600.0 656000.0 44.4 0.00 90.50 1.10 0.	573544 0 65604 0 47.6 44.10 24.20 1.30 40.	573.00.0 67400.0 47.8 0.30 97.00 2.10 0.	573580.0 673280.0 44.6 6.68 79.70 2.50 6.70 6.	25,50,60,0,539,40,0,62,5 1.00 35,30 0.00 0.00 10	55.00m. 0 6400m. 0 25.7 1.70	568600.0 612800.0 27.5 1.10	568889.0 617680.0 29.3 0.70	200000 0 527000 0 35.9 U.10	36888.0 62288.0 3.0 6.10	358888.8 635888.0 35.1 6.00 99.90 6.00 6.	TG8800.0 641600.0 37.3 0.00 99.80 0.10 0.	25,2500.0 646480.0 33.2 0.00 95.40 0.40 0.		562600.0 666800.0 50.9 0.00 90.00 0.00	556890.0 655580.0 55.4 0.10 95.50 3.50 1.30 0.00	25,000,00 67,040,00 45,0 6,78 91,10 1,50 4,50 5,50 5,50 5,50 5,50 5,50 5,50 5	SHOOL 68230.1 25.6 8.68 99.48 8.00 8.00 9.30	25.4000.0 600000.0 25.9 0.60 99.40 0.00 0.00 0.00 0.00	254000.0 617600.0 30.4 0.44 59.66 0.00 0.00 0.00 0.00	SHORE, 6 52400.0 22.6 0.10 99.99 0.00 0.00 9.00 0.00	554881.0 527281.0 34.9 54.00 99.90 64.00 54.00 54.00 54.00 54.00 55.00 54.00 55.00 54.00 55.00 54.00 55.00 54.00 55.00 55.00 54.00 55.00 5	SCHOOL 6.35000.0 38.8 0.00 99.90 0.00 0.00 0.00 0.00	SEASON, 0 641640, 0 33.8 0.100 99.70 0.20 0.10 0.00 0.00	254000, 0.531200, 0.45.2 0.00 25.10 0.00 0.44 0.00 0.00	354881.0 635888.0 58.8 8.80 99.80 8.60 8.30 8.80 8.00	554000.0 558000.0 57.8 0.00 57.30 1.70 0.17 0.00 0.00 0.00 0.00 0.00 0.0	25220.0 53440.0 26.2 0.20 93.70 0.00 0.00 9.30 7.00	375296.6 662396.0 25.8 % 6.28 99.06 6.00 6.00 9.70 8.40		22/2010 bicome Cr. 1 1.30 22/70 bree tree 27/2010 biological bree 27/2010 bree 1.00 27/2010 bree 1.00 1.00 27/2010 bree 1.00 1.00 27/2010 bree 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	ESSER. 8 522484.8 35.1 6.48 100.80 6.80 6.00	25200.0 (27200.0 37.5 0.00 100.00 0.00 0.00	TOXOGLE BACTORE S 33.3 F. CO 75.26 C. CO C.	272200 641500 41.0 0.00 99.40 0.40 0.	559280.0 646480.0 45.1 0.88 90.50 1.80 0.	555290.0 651280.0 50.7 0.00 97.50 1.70 0.00 except a 65520 1.70 0.00	255 1232200.0 668000.0 46.2 0.00 99.00 0.70 0.70
NORTH EAST DEPTH GRAVEL SHAD SILT CLAY CHATERY (a) (a) (a) in at 5 at 5 at 5 at 8 thk (i		299 79,343 573600,0 656000,0 44,4 0,00 90,50 1,10 0,	79,292 57,3684,0 666684,0 47,6 64,10 54,23 1,30 6, 70 34, 22 1,30 6, 70 34, 27,240 6, 62,40 6, 51 6, 70 6, 10 2,64 6, 10	79,199 573500.0 57400.0 47.8 0.38 97.00 2.10 0.	79.140 573600.0 675200.0 40.6 0.60 79.70 2.59 0.70 0.	253 75, 553 554646.0 559466.0 52.5 1.00 54.5 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	222 79. ESA 55.0000. 0 600000. 0 25.7 1.70	252 79, 863 568686.0 612886.0 27.5 1.10	79.752 568800.0 617600.0 29.3 0.70	75. 761 School B 122 485. 1 55. 5 10 10 10 10 10 10 10 10 10 10 10 10 10	79.599 566800.0 62300.0 35.0 0.10	79.546 556000.0 635000.0 36.1 0.00 99.90 0.00 0.	79.497 358800.0 641600.0 37.3 0.00 99.00 0.10 0.	75,446 556260.0 646480.0 35.2 0.80 95.40 0.40 0.	73,330 S68690,0 621290,0 41.8 0.90 36.36 0.90 0.70 74.37 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	79.293 SERVER, 0 666000.0 30.9 0.00 90.00 0.00	79.242 S6888.0 665588.0 35.4 8.10 94.30 3.50 1.30 8.00	75,151 SAGONE, BETWEEN NEW TICK 31.10 1.50 P. D. D. D. T. T. T. T. T. T. T. T. T. T. T. T. T.	79,995 School 64230.0 25.6 0.60 99.40 0.00 0.00 9.90	79,554 SCARRE GROOM, 25,9 0,69 99,44 0,00 0,00 0,00 0,00 0,00	72.003 Johann B. Com. Co. 3 1.30 72.70 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1	79.701 SAMMA 6224MA 22.6 0.10 99.90 0.00 0.00 9.00 0.00	79,559 55488.6 627284.6 34.9 64.89 99.59 64.80 64.80 5.80 64.80 77 59 59 59 50 54.80 64.80 64.80 64.80	75.549 554880.6 535880.0 34.8 0.00 59.50 0.00 0.00 0.00 0.00	79.439 554000,0 641600,0 33.8 0.00 99.70 0.20 0.10 0.00 0.00 0.00	75.35 55.400.0 55.200.0 45.2 6.00 25.70 6.30 6.40 6.00 6.00	79,345 554660.0 655860.0 56.0 0.00 99.00 0.64 0.30 0.00 0.00	79.254 554000.0 (55000.0 57.5 0.00 97.50 1.70 0.70 0.70 0.00 0.00	79, 555, 355,000, 556,000, 656,2 4, 28 59, 78 4, 60 6, 60 9, 90 7, 80	79,996 379296.0 643296.0 26.8 % 6.26 99.06 0.00 6.00 9.70 8.40		73, 384 325,584, 8 12,584, 8 13, 9 8, 38 59, 78 8, 88 8, 88 8, 88	79,782 352246.8 52446.8 35.1 6.48 100.88 6.88 6.88	79, 651 355200, 0 627200, 0 37.5 0,00 100,00 0,00	75, 540 303204, 0 52004, 0 55, 3 6, 00 57, 36 6, 00 6, 10 70 54 0 70 54 0 70 54 0 70 54	79,496 575294,0 641680,0 41.0 0.00 99.40 0.40 0.	79, 447 555280.0 646480.0 45.1 0.00 90.50 1.00 0.	79, 397 555200.0 651200.0 50.7 0.00 97,50 1,70 0.00 77,50 0.00 77 55 0.00 77	79.295 535296.8 56.8888.8 46.2 8.88 99.88 8.78 8.
NORTH EAST DEPTH GRAVEL SHAD SILT CLAY CHATERY (a) (a) (a) in at 5 at 5 at 5 at 8 thk (i		32.290 79.343 57360.0 65600.0 44.4 0.00 96.50 1.10 0.	22,299 75,292 57,568,8 656688,8 47,6 6,18 58,29 1,38 6,39 5,39 5,18 5,59 5,59 5,59 5,59 5,59 5,59 5,59 5,5	2.28 79.199 573.48.0 674.8 0.38 97.48 2.19 0.	22,287 79,146 573680.0 672880.0 44.6 6.60 79.70 2.50 6.70 6.	22,223 75,925 35,6466,6 359,466,8 22,5 1,50 34,36 8,50 8,50 14,0 14,0 14,0 14,0 14,0 14,0 14,0 14,	2 22 79.854 55.888.0 GARRA 0 25.7	32,252 79,863 568684,0 612884,0 27.5 1.10	2. Zi 79. 72. 56888. 8 61768. 8 29.3 8.78	Section 15, All beautiful beautiful des sur le la	22,256 79,359 56886.0 62886.0 55.0 6.10	Me 22.249 79.546 556800.0 635000.0 36.1 0.00 99.90 0.00 0.	32.249 79.497 368600.0 641600.0 37.3 0.00 99.00 0.10 0.	22.246 79.446 358300.0 546400.0 33.2 0.00 95.40 0.40 0.40 0.40	22.247 73.355 EXCHANGE CALCANGE 41.8 4.00 Mark 4.00 Mark 7.5 4.00 Mark 1.00	22.246 79.293 568000.0 660000.0 30.9 0.00 90.00 0.00	22.245 79.242 56886.0 665566.0 39.4 0.10 94.99 3.59 1.30 0.00	CALCAS 75, 191 156,000 a CAMBAN CANA CALCA 15, 10 1, 10 4, 1	22.210 75,955 SAMO. 6.61230. 25.6 4.69 95.40 4.00 4.00 9.90	22,285 73,554 55,486,0 66,680,0 25,9 0,55 29,40 4,80 4,80 4,80 4,80 4,80	No. 273   73, 283   204, 284, 285, 285   285, 385   285, 385   285, 385   285, 385   385, 385   385, 385   385, 385, 385, 385, 385, 385, 385, 385,	2.288 79.701 SAMMA 6224MA 2.6 0.10 99.90 0.00 0.00 9.00 0.00	12-20 79-559 55480-0-0-27200-0-34-9 0-00 99-99 0-00 0-00 0-00 0-00 0-00	22.26 73.549 554886 6 55686.0 34.8 0.00 95.90 0.00 0.00 0.00 0.00	1 22,225 73,450 55,400,0 54,500,0 33,8 0,100 93,70 0,20 0,10 0,10 0,00 0,10 0,10	Z_1CO   Z_1+1   Z_1CO   Z_1+1   Z_1CO   Z_1-1   Z_1CO   Z_1-1   Z_1-	22.283 79.345 554000.0 556000.0 56.8 0.00 99.00 0.50 0.30 0.00 0.00	1 22 203 793 294 ESAMORO ESAMORO 57-36 CAMO 597-36 LI-76 CAMO 54-39 CAMO 54-3	2.167 79.956 359200 8 39400 8 36.2 4.28 99.76 0.00 0.00 9.90 7.80	22, 156, 79, 905 375/200, 6 64/200, 6 75, 8 7, 8 7, 8 7, 95, 50 4, 60 5, 70 5,		22.153 79.753 359500.0 617600.0 31.9 0.30 59.70 0.00 0.00	32 164 79,782 35500.8 62240.8 35.1 6.00 100.00 6.00 6.00	32.164 79.651 35900.4 627200.0 37.5 0.00 100.00 0.00 0.00	2. Ibs. 75. bar 20.50m; a backware 35.3 m; a 75.30 m; a 6.00 ft.	2. 15. 79. 496 57890, 6 61600, 6 1.0 0.00 99.40 0.40 0.	22.161 79.447 559200.0 646400.0 45.1 0.00 98.50 1.00 0.	22, 161 79, 397 555296.0 651296.0 50.7 0.00 97,50 1,70 0.00 72,50 74.5 95.50 1,70 0.00 75.50 74.5 95.20 1,70 0.00 75.50	FM 2C. IDS 79, 295 535208.8 BADDRESS BELS BELS BELS BELS BELS BELS BELS B
DIGITUDE NORTH EAST DEPTH SHOWEL SHAD SILT CLAY CHATERY (deg) (a) (a) (a) as 5 as 5 as 5 as 5 thk (d		23,040 32,290 79,343 573500,0 655000,0 44,4 0,00 90,50 1,10 0.	23,040 72,259 73,299 57,380,0 65,600,0 47,6 4,10 74,20 1,30 4,4	19,765 22,286 79,199 57,364.0 67440.0 47.8 0.38 97.80 2.10 0.	1.955 22.287 79.144 573540.0 675240.0 48.6 6.68 79.78 2.58 6.70 6.	253 75, 553 554646.0 559466.0 52.5 1.00 54.5 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	23. No. 22. 222 79. ECA 55.00m. 0 6.00mm. 0 25. 7	23, 646 32, 252 79, 663 568664, 6 612664, 0 27, 5 1, 10	23.846 22.251 79.722 568866.0 617680.0 29.3 6.78	75. 761 School B 122 485. 1 55. 5 10 10 10 10 10 10 10 10 10 10 10 10 10	21.040 22.250 79.359 36800.0 67200.0 35.0 0.10	23.040 22.249 79.548 568000.0 55.000.0 36.1 0.00 99.90 0.00 0.	23.046 32.249 79.497 358800.0 641600.0 37.3 0.00 99.00 0.10 0.	23,044 22,246 79,446 358,000,0 646,400,0 39.2 0,000 99.40 04.40 04.	73,330 S68690,0 621290,0 41.8 0.90 36.36 0.90 0.70 74.37 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	23.040 22.246 79.233 SEGMAN GEORGE 38.9 R. 00 34.00 R. BM	23, 646, 22, 245, 79, 242, 56,686, 66,5568, 93, 4, 4, 16, 16, 94, 39, 3, 36, 1, 38, 4, 88	75,151 SAGONE, BETWEEN NEW TICK 31.10 1.50 P. D. D. D. T. T. T. T. T. T. T. T. T. T. T. T. T.	23.040 (2).210 73.995 SAMOR 1 642200.1 (25.6 0.60 99.40 0.00 0.90	23.040 22.203 73.654 Extent 640001. 25.9 0.60 95.40 0.00 0.00 0.00 0.00	72.003 Johann B. Com. Co. 3 1.30 72.70 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1	23.646 20.286 79.701 35466.0 622460.0 20.6 6.10 59.59 0.00 0.00 5.00 0.00	23,040 (2,207 79,629 554000,027200,0 34,9 (4,00 99,90 0.00 0.00 5.00 0.00 0.00	23.040 22.286 79.549 554000.6 555000.0 34.8 0.00 59.59 0.00 0.00 0.00 0.00	23.040 (20.205 72.490 EA400.0 641600.0 33.8 0.00 99.70 0.20 0.10 0.00 0.00	23.046 (2).244 73.355 (54.000.0 55.120.0 45.2 0.00 30.70 0.00 0.40 0.00 0.00	23,040 22,283 79,345 55400.0 655000.0 56.8 0.00 59.00 0.60 0.30 0.00 0.00	79.254 554000.0 (55000.0 57.5 0.00 97.50 1.70 0.70 0.70 0.00 0.00	23,048 22,167 79,956 559200,0 559400,0 56.2 0,030 99.70 0,00 0,00 93.90 7.80	23, 040 .22, 166 79, 965 3375200.0 642200.0 26.8 V 0.20 99.00 0.00 0.00 9.70 0.40	CALLON TO 166 70,653 UNIVERS GENERAL DATE OF CALLON STATES OF CALLON STATES	73, 384 325, 384 6 12, 384 6 13, 4 14, 38 73, 78 14, 38 14, 38 73 14, 38	23.040 22.164 79.702 33500.0 622400.0 35.1 6.00 100.00 6.00 6.00	32.164 79.651 35900.4 627200.0 37.5 0.00 100.00 0.00 0.00	CALMAN AND TAX TAX SAME TAX TAX TO BACK TO TAX TAX TAX TAX TAX TAX TAX TAX TAX TAX	23.046 22.112 79.496 579900 641600.0 41.0 0.00 99.40 0.40 0.	23.648 22.161 79.447 355280.0 646480.0 45.1 0.00 36.50 1.00 0.	NA 22,161 79,397 555200.0 651200.0 50.7 0.00 97,50 1.70 0.	C.1.040 C.1.100 73.295 Z35200.0 668000.0 46.2 0.00 99.00 0.770 0.12.695 Z2.159 79.295 Z35200.0 66.20 0.40.2 0.00

GEONGIA OFFSHORE MINERALS ASSESSMENT MODEL. page 23

MCDM1	# M	<b>8</b> M	20	<b>8</b>	2	# 1 ai a	3 8	i A	3	9 10	=	=	<b>8</b>	8	3 3	4 ~	8	2.00	2.4	33 7		9 19	<b>8</b>	<b>8</b> 8	8	8	<b>8</b>	8 .	R R	3	3	8	8	2	<b>8</b> 2	# 8 4 a	2 2	8.7
TIGH ZIRCON Scount Scount	3	8	=	=	2	2 2				8	=	4.78	2	2	3 3			8	=	2 3		4.6	2		2 3	3	8	2 2	3	3 5 6 7	23	3	2	=	2 2			5.2
TALRO T	1	8	8	=	3	2 2			8	8	=	<b>6</b> . 98	2	2	8 2				=	<b>8</b> 5		8	=	3 3		8	= 4	8 3		3	1:3	=	2	2	2 2			8.1
ALTILE STAURD TITON ZIRCON Scount Scount		2	=	8	2	2 2			3	8	===	6.38	=	=======================================	3 3			8	8	8 2		8	8	3 3		2	=	8 3		3 3	0.60	8	=	8	2 ! -		8	2 %
1 12		8.	8	=		3 :			8	8	8	6.38	=	8	2 2			8	=======================================	3 3		8	=	2 2		=	=	3 3		: 3	3	=	8	3	3 3		3	2 2
ACOUNT IN	1		=	8	2	2 2				8	=	2	8	=	= :			=	3	= :		3	=			=	=	8 3			8	=	8	3	8 !		3	3 1
MINS PH Younk	3.38	3.64	3.98	_	_	77 E		3	8,	128	2.3	201	228	33	<b>8</b> 5		3 2 4	88 %	87	81		4.98	3.28	<b>2</b> 3	2	4.2	3.00	8 3		8	8.3	328	88	3:	2 2	2	3	23
FLISS HV	1	4.80		_	_	2 2			_			6.48			2 2	8 5						6.38		2 5				<b>8</b> 1	B 8	8 8				3 (	2 2		R	92.30
Krount 1	82.2	2.48	_					2 20	_							3 5	_			<b>8</b> 1	_			3 2			2.00	8.5	ŖS	3				_			8	9 96.1
MTZ K.I					_	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		_		_	1 22	10 10		ন :		2 2 2	_			2 2				3 1	l M		_	8 2						3 :			7. E	= ;
NA (a) X	Ш.	_	19.28 BA	_		3 2 3 1			3	2	<b>3</b>	8		_	_		3	=	=	2 1 2 1					_	_	2	2 :	B 8	7.3	_	_	_			6 S	3	2 F
BOTS OVE	×							3	3	8	=	_	_	_		_	3 8	=	=	<b>3</b> 1		_	-		. –		8	<b>2</b> 1		18		=	2	_			: <del>-</del>	8 1
(10C 10C)	269	48 -69.70		F. 17- 00				8	2	3	8						2 2	8	3	3 1 3 1		8			20 -7.4	=	8	= :		7		•			# '/-		: <b>:</b>	21
10C 14.)	1		_	ស់ ' <b>ខ</b> ៈ		5		: 2	3	=	=		_	_	80 8 80 8 80 8	R 9	i	=	<b>3</b> :	2 1		2	177	- I	# 2	2	- 2	21	4 d	20.00				3 :			=	21
(a) th	ដ	M 22.68	E.23	2	6 . R :				2	2	2	3	त्र श	8 : Z	ਹ ਹ			2	2	2 1		2	12.0		7	=	2	2 3		10.68	3	16.38	8:3	2.6			3	23
			_	Ξ,	∹ '			. –	_	Ξ.	_	~	3	3	7.	, ,		_	_	<u>ب</u> -	; –	7	7	3 7	-	-	_				3	=	•	_				-
EN UP.H	1	=	•						-	•	•	•	•	•	• •			•	•	<b>.</b>		•	-	• •		-	-	e •			•	-	<b>-</b>	٠ -				-
(a) the (a) thi	4	3 57 E	10.10 A	16.20					9 8 9				16.28	82					9	2 2			935		2.5	10 10 10	-	3 3		1 1 2 1		128	8.0	83				
GLATERN P. IGCSH UP. HIGC NO. HIGC 14. HIGC NV. BOTS OVERRON GLARTZ N. FLDSP P. FLDSP HAVRING RESHAT HONG. It that (a) that (a) that (a) that (a) that (a) that (a) that (a) that (b) Scount Sc	9.66 6.98 6.	<u>~</u>	9 9.10 10.10 6	9.00 10.20 0			9.00		0.00 0.00			. 4.00 4.00	9.10 10.20	2.00				9.00 G.00 G	2.0				9.80 9.60		L 28 9.40 0	0.00 0.00	7 87 87 1	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		9.00 A.20		9.88 L'38 L	- 5. E. S. E				9.00	256
A A	4	<u>~</u>	0 0.00 9.10 10.10 0.	6.00 9.00 10.20 E			40 90 60		0.26 0.00 0.00 0.	1 4.70 L.00 L.00 0	1.50 0.00 0.00 0	. 4.60 4.00 4.00 0	6.00 9.10 16.20 0	0.00 9.40 10.00 0				0.00 9.00 0.00 0	L. 0. 9.00 C. 0.00			1.30 L.00 L.00 0	0.00 9.00 9.60		Les L9 9.00 0	L. C. C. C. C. C. C. C. C. C. C. C. C. C.	7 60 60 60 6			0.00 9.00 0.20 0	6.10 6.00 6.00 e	6.00 9.00 A.50 A.	5. S. S. S. S. S. S. S. S. S. S. S. S. S.				6.29 9.00 0.00	9.0 9.0
SILT CLAY	C.00 C.00 9.60 A.	6.00 6.00 9.20 9.	4.00 6.00 9.10 16.16 6.	0.00 0.00 9.00 10.20 0					6.50 6.20 6.00 6.00 6	1 1.35 4.70 6.60 6.60 6	3.10 1.30 0.00 0.00 0	1.40 6.60 6.00 6.00 0	0.00 0.00 9.10 10.20 0	C. C. C. C. C. C. C. C. C. C. C. C. C. C				A.10 A.80 S.80 A.80 A				1.10 6.30 6.40 6.00 0	0.00 0.00 9.00 9.60		C.00 C.00 A.90 9.40 0		T 01 01 01 01 01			A.10 A.00 9.00 A.20 B	6.30 6.10 6.60 6.60 6	C. S. C. S. S. S. C. S. S. S.					0.90 0.20 9.00 0.00	0.00 0.10 0.00 0.00 0.00 0.00 0.00
SAND SILT CLAY	90 G.00 G.00 9,60 B.	20 0.00 0.00 9.20 9.	30 4.00 4.00 9.10 IA	26 C. C. C. C. C. C. C. C. C. C. C. C. C.			99.00 C.10 C.00 9.00 C.00 C		99.20 0.50 0.20 0.00 0.00	97.70 1.30 6.70 6.00 6.00 6	%.29 3.10 1.50 6.00 6.00 6	57.88 1.40 0.60 0.00 0.00 0	95.50 0.00 0.00 9.10 10.20 0	99.30 0.00 0.00 9.00 10.20 0				99.20 0.10 0.00 9.00 0.00 0.	99.88 4.28 4.80 9.80 4.80 4.80			93.48 1.10 0.50 0.00 0.00 0	99.60 0.00 0.00 9.60 0		186.00 6.00 6.00 6.30 9.40 0	29.30 A.00 A.00 B.00 A.00 A.	99.00 L.20 L.00 L.00 L.00 L			95.80 ft.10 ft.80 9.80 ft.20 ft	99.30 6.30 6.10 6.00 6.00 0	50 C.00 C.00 9.00 A					98.48 6.98 6.28 9.80 6.88	99.56 0.36 0.16 9.86 0.86 0.74
GRAVEL SOND SILT CLAY	90 G.00 G.00 9,60 B.	6,10 99,90 6,60 6,00 9,20 9,	4.10 99.30 4.00 6.00 9.10 16.	G. 16 99.86 G. 80 G. 86 9.86 16.					A. 80 59.20 A.50 A.20 A.80 A.80 A.	4.00 97.70 1.30 4.70 6.00 6.00 6	4.00 55.29 3.10 1.50 4.00 6.00 6	6.00 57.00 1.40 6.60 6.00					4.00 55:30 C.00 C.00 C.00 C.00 C.00 C.00 C.00 C.	R.80 99.30 8.10 8.80 9.80 8.80 8.	1			0.00 93.00 1.10 0.30 0.00 0.00 0	A.10 99.60 A.00 A.00 9.60 B		6.00 100.00 6.00 6.00 6.30 9.40 0	L. 69 59:50 L. 60 C. 60 C. 60 C. 60 C.	4.00 99.00 4.20 4.00 4.00 4.00 4.			4.00 99.00 4.10 4.00 9.00 4.20 0	99.39 6.30 6.10 6.60 6.	C.20 99.00 C.00 9.00 L.			* *		C. 00 95. 50 C. 90 C. 20 9. 00 C. 00	0.30 0.10 0.10 0.00 0.10 0.10 0.10 0.10
SAND SILT CLAY	.8 27.8 ft.80 99.90 ft.80 ft.80 9.68 8.	.4 23.1 6.10 99.30 6.40 6.00 9.20 9.	4.10 99.30 4.00 6.00 9.10 16.	26 C. C. C. C. C. C. C. C. C. C. C. C. C.			0 41.0	•	0 45.1 6.00 59.20 6.50 6.20 6.00 6.00 6.00	0 53.6 0.00 57.70 1.30 0.70 0.00 0.00 0	0 63.2 0.00 55.20 3.10 1.50 0.00 0.00 0	G. 80 57.18 1.48 G. 50 G. 10		C. 10 95.80 C. 80 C. 80 C. 10			0 41.2 8.08 35.30 0.00 0.00 0.00 0.00 0.00	0 43.1 0.00 99.30 0.10 0.00 9.00 0.00 0.	0 45.0 4.00 99.00 4.20 4.00 9.00 4.00 6.00 6.00			=	9 5		3	0 41.5 0.00	0 46.4 0.00			8 46.3 4.00 99.80 4.10 6.00 9.00	9 47.3 4.00 99.50 6.30 6.10 6.00 6.	6 35.0 G.28 99.00 G.00 G.00 9.00 G.	9 37.3 0.10	30.0		46.5 0.00 29.45	0 54.5 6.00	0.30 0.10 0.10 0.00 0.10 0.10 0.10 0.10
(a) (a) nd 3 nd 3 nd 3 nd 3	6 6.00 99.30 6.00 6.00 9.60 B.	642200.0 20.1 6.10 99.90 6.00 6.00 9.20 9.	.0 29.3 6.10 99.30 6.00 6.00 9.10 16.	10 22 0 0.10 99.80 0.00 0.00 0.20 10.			9 41.0	•	-	•	3	10 44.2 6.00 57.00 1.40 6.60 6.00	. 0 29.6 p. 00 29.30 p. 00 0.00 9.10 1	A.C. 16.10 99.30 0.00 0.00 9.00 1			•	•	3			.0 46.0 0.00	0 6 7 0 10 0 10 0 10 0 10 0 10 0 10 0 10		33.6 6.00 1	0 41.5 0.00	0 46.4 0.00	627286.0 49.2 0.80 99.30 0.40 0.10 9.80 0.80 0.80 0.80		8 46.3 4.00 99.80 4.10 6.00 9.00	9 47.3 4.00 99.50 6.30 6.10 6.00 6.	6 35.0 G.28 99.00 G.00 G.00 9.00 G.	0 37.3 0.10	30.0		46.5 0.00 29.45	0 54.5 6.00	2 0.00 99.50 0.30 0.10 9.00 0.0
HORTH EAST DEPTH SHOWEL SOND SILT CLAY	5 5 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	642200.0 20.1 6.10 99.90 6.00 6.00 9.20 9.	8 680000.8 29.3 0.10 99.30 0.00 0.00 9.10 10.	0.512380.0 32.0 0.10 93.80 0.00 0.00 9.00 10.	a birbar a sa. 3 L. W.	A 627248. 8 48. 8 4. 8 4. 8 4. 8 4. 8 4. 8 4.	6.0 629mg.0 41.0 g.m	0.0 635000.0	0.0 641500.0	88.8 646488.8	8.8 651288.0	.0 655000.0 4L.2 0.00 57.00 1.40 0.60 0.00	0.558460.0 29.6 6.80 99.90 0.00 0.00 9.10 1	0.64230.0 30.2 0.10 59.30 0.00 0.00 9.40 1			62248.0	0 £27286.0	0 (EBBB. 0	CALCAR .	6 6 6 4 5 6 10 99 20 6 20 6 20 6 20 6 20 6 20 6 20 6	.0 651280.0 46.0 0.00	0.0 598400.0 20.9 0.10	L. 6. 6. 6. 6. 6. 7. 3. 6. 10	8.8 612888.8 38.8 8.88 1	.0 617600.0 41.6 0.00	.0 62248.0 46.4 6.00	62724	6.36.0m.	0.0 641600.0 46.3 4.00 99.00 4.10 4.00 9.00	100.8 646400.0 47.3 0.00 99.30 0.30 0.10 0.00 0.	MOC. 0 559460. 0 35. 0 0.20 95.00 0.00 0.00 0.00 9.00 0.0	100.0 502200.0 37.3 0.10	8.6 GROOM. 8 38.8 8.00	5.0 bicher, 44.0 c. 25.35 c. 5.0	10.0 622401.0 46.5 0.00 99.40 0.00	A. 0 627200.0 50.5 0.00	0.522000.0 48.2 0.00 99.60 0.30 0.10 9.00 0.0
HORTH EAST DEPTH SHOWEL SOND SILT CLAY	SST 3554460.8 5394460.8 27.8 0.00 99.90 0.00 0.00 9.60 8.	206 354400.0 642200.0 20.1 0.10 99.30 0.00 0.00 9.20 9.	.0 680000.0 29.3 0.10 99.30 0.00 0.00 9.10 10.	2004 324404.0 612304.0 32.0 04.10 93.80 04.00 04.00 93.00 104.	THE PARTY OF THE P	2 38.6 G. W. W. W. W. W. W. W. W. W. W. W. W. W.	THAM I STAND II. O II	354484.8 636888.0	35448.0 641688.0	25448B. 0 64648B. 0	35448E.0 65128E.0	354400.0 655000.0 46.2 0.00 57.00 1.40 0.60 0.00	0.558460.0 29.6 6.80 99.90 0.00 0.00 9.10 1	7.550.0 6.020.0 July 0.110 59.50 0.180 0.180 9.480 1.		SASSER SINGER N. 3 C. M. 196. M. C.	54968.0 622488.0	549684.8 627284.8	54964.0 62200.0	•	54568.0 64648.0 4.5 6.80 59.20 6.30 G.	34%64.0 651294.0 46.0 0.00	S44880.0 536480.0 22.9 0.10	1 50-4 p. 10 10 37.3 p. 10	544884.0 612888.0 38.8 0.00 1	SAABBL B 617686.8 41.5 0.88	544888.0 622488.0 46.4 8.88	-	5440m. 8 6360m. n	544580.0 641680.0 46.3 0.00 99.80 0.10 0.00 9.00	NSG 544888.8 646488.8 47.3 6.88 99.38 6.38 6.18 6.88 6.	256 540000,0 559400,0 25,0 0,28 95,00 0,00 0,00 0,00 5,00 0,00	SABBBL 0 68 22 98. 0 37. 3 0. 10	SAGGG. 6 GASGGG. 8 38.8 8.88		704 54888.8 62248.8 48.5 8.88 99.48 8.5	SABBBL & 627288.0 58.5 6.00	0 48.2 0.00 99.60 0.30 0.10 9.00 0.10 48.2 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.
HORTH EAST DEPTH SHOWEL SOND SILT CLAY	79.557 354486.8 599486.8 27.8 6.88 99.98 6.88 6.88 9.68 8.	75.965 SZHARA 6 64228A 6 20.1 6.10 99.90 0.00 0.00 9.20 9.	79.855 554486.8 688886.8 29.3 6.18 99.39 6.08 6.08 9.18 10.	2004 324404.0 612304.0 32.0 04.10 93.80 04.00 04.00 93.00 104.	CALCAS STATES OF THE STATES OF	25440 A 67790 A 40 A 50	79.601 SSA400.0 62900.0 41.0 0.00	79, 520 55440L 0 63620L 0	79, 499 554480, 8 641680, 8	79,448 554488.0 646488.0	79. 397 SSHARE, B 651288.0	79.346 SSH400.0 655000.0 46.2 0.00 57.00 1.40 0.60 0.00	75, 257 5495,00 5294,00, 0 29, 0 0, 00 29, 20 0, 00 0,	72.50 12.50		TAY TAY SANGE TO SECTION OF THE TAY OF THE T	79. 783 5495.06.0 522400.0	79.622 549646.8 627284.8	79,601 549600,0 62900,0	73.351 549500.0 635000.0 73 540 549500 0 641540 0	73.449 545500.0 646400.0 44.5 0.00 59.20 0.30 Q.	79.338 3A964.0 651284.0 46.0 8.00	79.956 SHEER. 0 STRABL 0 32.9 8.10	73.30/ 344894.8 646894.8 53.4 0.10	79.865 SAABBL & 612888.8 38.8 8.88 1	79,735 SAABBL 8 617688.8 41.6 8.68	79.784 544888.8 622488.8 46.4 8.88	79.653 544644.0 627244.0	79.551 SAABB. B & SABB. B	75.500 544500.0 641650.0 46.3 0.00 59.80 0.10 0.00 9.00	79,456 54406.8 64646.0 47.3 6.00 59.59 6.30 6.10 6.00 6.	79.556 546000.0 558400.0 35.0 0.28 59.00 0.00 0.00 5.00 4.00	79,986 SHARRE, 0.68298.0 37,3 % 0.10	79, ES7 SAMME GARMEN 30, 80 G. 80	754 75,000 346000, 0 bickett 94,0 8,00 75,30 4.0	79,704 SABBBO 6224BB 48,5 0.00 99,40 0.00	991 79.654 SABBBB. 0 627288. 0 58.5 0.80	990 79,683 540000,0 622000,0 46.2 0.00 99.60 0.30 0.10 9.00 00
LATITUDE LONGITUDE NOTITY EAST DEFITH SHOWEL SHOW SILT CLAY (a) (b) (deg	948 22.123 73.537 354486.0 594486.0 27.8 6.80 93.99 6.80 6.80 9.66 8.	948 22.123 75.966 354484.0 642284.0 25.1 0.10 99.90 0.40 0.00 9.20 9.	646 22.123 79.655 55446C 6 6886C 6 29.3 6.10 99.90 6.00 6.00 9.10 16.	20.122 70.884 304480, 612880, 12.0 81.0 99.86 6.86 6.86 9.80 18.	SCHOOL TO THE STATE OF THE STAT	20,100 75,760 SEMAN B 627500 B 46 B 660 1	2.128 79.681 SHAM. B 5289. 6 41.0	22.119 79.558 554406.8 636808.0	22.119 79.499 STAMBLE GAISBLE	22,118 79,448 554488.8 645488.0	22.118 79.397 354488.8 651288.8	22.117 73.346 SSHORLD 655000.0 44.2 6.00 57.00 1.40 6.60 6.00	22,888 72,927 54,958,0 579,488,0 25,6 6,88 55,59 6,80 6,80 5,10 1	V-000 75.977 V-000-0 642/0-0 36.2 0.10 99.50 0.10 0.10 0.10		22-175 72-75-51-55-0 51-75-0 34-3 p.m. 180-0 p.m. p.m. p.m.	22.078 79.763 549606.0 622406.0	2.07 79.62 54564.0 627204.0	22.077 79.601 54960t.0 632000.0	W. O. W. M. M. M. M. S.	Zi 073 72, 449 S4560.0 64640.0 44.5 0.00 59.30 0.30 0.30	32.674 79.338 3495.04.0 651204.0 46.0 0.00	22.637 79.958 S44860.0 S94460.0 22.9 0.10	22.036 79.036 544890, 6 646900, 8 37.3 0.00	32.835 79.865 544888.8 612888.8 38.8 6.88 1	22.633 79.735 SHABAL 8 617686.8 41.6 B.88	22.634 79.784 544888.0 622488.0 46.4 6.88	22.034 79.653 544000 0 627200.0	22, 673, 79, 551, 554,880, 8, 636,880, 8	22.022 79.500 544000.0 641600.0 46.3 0.00 99.00 0.10 0.00 9.00	300 22.022 73.450 54400.0 546400.0 47.3 6.00 59.50 6.30 6.10 6.00 6.	PAG 31.993 79.558 SAGGGG SSSAGGG 35.0 0.20 99.50 0.00 0.00 9.00 4.	P40 31,993 79,906 54600,0 66250,0 37,3 0,10	PAS 31,993 79,657 54606.6 68006.0 36.0 0.00	PAG 21: 322 73: 000 344000.0 01/200.0 44: 0 0.00 35: 36: 46: 46: 46: 46: 46: 46: 46: 46: 46: 4	We 31.991 73.744 SAMMER 622480.0 45.5 0.00 99.40 0.00	M8 31.991 79.654 540000.0 627200.0 50.5 0.00	590 31,990 79,643 540000,0 622000,0 48,2 0,00 99,60 0,30 0,10 9,00 0,0
HORTH EAST DEPTH SHOWEL SOND SILT CLAY	948 22.123 73.537 354486.0 594486.0 27.8 6.80 93.99 6.80 6.80 9.66 8.	23.048 22.123 79.96 354486.0 642286.0 28.1 6.10 99.90 6.00 6.00 9.20 9.	23.046 22.123 79.855 554486.6 68088.0 29.3 8.10 99.90 8.00 8.00 9.10 18.	20.122 70.884 304480, 612880, 12.0 81.0 99.86 6.86 6.86 9.80 18.	CALEND ACTIC TATAN SEMESTER BITMEN SALA BANK	23.040 32.121 73.743 32440.0 02240.0 33.2 0.00 1	23.646 22.120 79.601 SHAME 0 520ME 0 41.0 A.M.	23.040 22.119 73.250 554406.0 636000.0	23.040 22.119 79.499 SS4400.0 GAIGOO.0	22,118 79,448 554488.8 645488.0	23.040 22.116 79.397 354406.0 651206.0	14.995 32.117 79.346 ESHARLO 655686.0 44.2 6.60 97.80 1.40 6.60 6.00	23, PHB 12, RBD 73, ST7 54,55,00, B 73,400, B 29, G 10, BB 59, SB 10, BB	27.00 17.00 17.00 18.00 19.00		21 PA 22 TA 72 TA 75 TA 55 SER S TAKES 34.3 P. M. SER DE DE DE DE DE DE DE DE DE DES DE DE DES DE DE DE DE DES DE DE DES DE DE DES DE DE DES DE DE DES DE DE DES DE DE DES DE DE DES DE DE DES DE DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DES DE DE DES DE DE DES DE DE DES DE DE DES DE DE DE DE DE DE DE DE DE DE DE DE DE	23.046 32.078 79.783 549680.0 622480.0	23.040 32.077 79.632 54950t.0 62720t.0	23.040 22.077 79.601 549600.0 632000.0	73.351 549500.0 635000.0 73 540 549500 0 641540 0	22,339 22,673 79,449 54954,0 6464810 44,5 0.00 99,20 0.39 0.3	9.120 32.074 79.336 349600.0 651200.0 46.0 0.00	23.648 22.637 79.958 544880.0 554480.0 22.9 8.10	73.30/ 344894.8 646894.8 53.4 0.10	23.040 32.035 79.885 54488.0 612880.0 38.8 0.00 1	23.040 22.033 79.735 54400.0 617600.0 41.5 0.00	23.048 22.634 79.704 544806.0 622406.0 46.4 6.00	79.653 544644.0 627244.0	23.040 22.023 73.551 54400.0 63600.0	20.540 22.622 75.540 544800.0 641600.0 46.3 4.00 99.80 4.10 4.00 9.00	4,500 32,022 73,456 544804.8 646404.0 47.3 6.00 59,59 6.30 0.10 6.00 6.	23.040 31.993 79.556 540000.0 559400.0 35.0 0.20 99.00 0.00 0.00 9.00 A.	23.040 31.993 79.906 546000,0 60200,0 37.3 0.10	23.040 31.953 79.057 54000.0 64000.0 30.0 0.00	PAG 21: 322 73: 000 344000.0 01/200.0 44: 0 0.00 35: 36: 46: 46: 46: 46: 46: 46: 46: 46: 46: 4	23,040 31,991 73,744 SAMMER SZEMER, 44,5 0.00 99,40 0.00	23.046 31.991 79.654 540000.0 627200.0 50.5 0.00	590 31,990 79,643 540000,0 622000,0 48,2 0,00 99,60 0,30 0,10 9,00 0,0

## SECTION 9.2

PAGE 1							10	:49:65	15 JUL	1988
Key	SAMPLEID	LAT	LON	NORTH	EAST	DEPTH				
1610	4540	30.047	70 747	701115	607764	074 0			-	-
1649 16 <b>59</b>	1649 16 <b>58</b>	30. 017 30. 017	79.717 79.508	321146 321389	623761 643855		0	48 96	37	22
1733	1733	30. 238	79.658	345785	629901	861	8	64	21	14
2279	2279	31.132	81.414	444139	468547	8	9	91	0	0
2280	2280	31.097	81.282	448165	473137	6	0	95	5	0
2284	2284	30.478	81.385	371671	463046	8	3	95	5	0
2419	2419	30.333	86.795	355558	519786	33.0	0	100	0	9
2420	2420	39, 353	80.892	357762	518411	28.0	9	100	0	0
1498 1663	1498 1663	30.670 31.678	81.003 79.995	392848 585834	499681 595262	20.0	8	199 196	8	8
1681	1681	30.830	80.750	418685	523909	36. 0 24. 0	9	100	0	8
1696	1696	30, 155	80.488	335891	549274	36. 0	1	99		8
1796	1706	31.333	80.232	466614	573096	36. 0	8	100	0	8
1743	1743	30.850	79.400	413891	652997	882	0	92	8	8
1752	1752	31. 478	79. 483	483425	644873	449	0	97	5	0
2373	2373	30.263	78. 750	349927	716464		0	94	6	8
2472 27 <b>8</b> 2	2472 27 <b>02</b>	38. 142 31. 888	79.545 79.200	335197 519491	648142 678484		31	61	7	9
1668	1668	31.823	80.018	521886	592985	38.8	<b>0</b> 1	98 98	0	8
2277A	2277A	32, 329	81.384	464922	471059	50.0		100	8	8
1653	1653	30.375	79.442	361188	649741	_	9	34	30	35
1742	1742	39.745	79.317	482369	661141	752	8	180	0	8
2374	2374	30.517	79.822	377521	689832		4	90	6	0
2485	2485	32. 453	79.847	591 <b>98</b> 2	588484	29.0	0	100	0	0
2411	2411	32, 297	79.717	573855	620832	40.0	1	99	0	8
2421	2421	30.350	88.933	357390	586488	26.8	2	98	0	0
2476 27 <b>0</b> 6B	2476 27 <b>96B</b>	30.863 31.800	79.168 79.280	4157 <b>89</b> 519491	675129 67 <b>8484</b>		15 8	82 8	3	0
1488A	1488A	31.842	80.758	522726	523655	17.0	8	98	2	0
1658	1658	39. 839	80. 907	411001	595001		8	73	18	8
1695	1695	39. 000	80.493	318714	548980	38. 0	0	100	0	0
1705	1705	31.502	89.275	485244	568850	32.0	8	100	8	9
1711	1711	30. 497	80.228	373894	574855	43.0		100	6	0
1747	1747	31.147	79.775	446318	616773	254	0	95	5	9
1757 2269	1757 2269	32. 813 32. 145	79.507 80.827	5427 <b>00</b> 556333	541843 516346	54 9	0	100 100	8	8
2275	2275	31.517	81.199	486717	471594	3	8	89	9	7
1664	1664	31.673	80.243	584298	571726	28.8	9	100	0	ø
2270	2270	32.073		548376	502989	8	0	100	0	8
1654	1654	38.498	79.453	374841	648434	752.0	0	99	1	8
2278	2278	31.333	81.384	466386	463500	4	0	100	0	0
2377	2377	38.358	78. 983	361919	780355		8	96	4	0
2383 2424	2383	38, 948	78.572	425297	732996		0	100	9	8
2474A	2424 2474A	39. 367 39. 572	81.858 79.525	359236 382878	494395 641448		<b>0</b> 39	1 <b>99</b>	9 23	9 25
2482	2482	31.922	78.578	534126	728969		9		8	0
1497	1497	30. 833		418948	500000	18.0	0	188	0	0
1685	1685	<b>30.</b> 167	80.750	337100	524072	32.8	8	100		8
1701	1701	31.003	80.492	429898	548528	31.0	8	100	0	0
1737	1737	30.507	88. 848	375140	592128	284	34	57	8	0
2429 2265	2429 2265	39.385	81.250	361293	475981	23.0	0	100	0	9
2263 1753	2263 1753	32.435 31.653	8 <b>0.</b> 38 <b>0</b> 79. 497	588634 582886	559286 642540	9 166	8	100 30	0 56	13
1731	1733	30. 183	79.887	339443	607186		8	54	19	15
2379	2379	30. 475	78.067	374897	781622		Ö	199		9
2380	2380	30.830	78. 975	414241	779796		0	100	0	0
2426	2426	30. 375	81.142	360167	486388		5	95	0	. 9
2473	2473	30.252	79.243		669014		10	89	. 0	0
2477	2477	31.008	79.323	431548	660065	684. 0	8	0	0	0

<b>PAGE</b> 2 Key	SAMPLEID	LAT	LON	NORTH	east	DEPTH			15 JUL WTSILT	
0470	0470	74 177	70 106	AA5797	678768	CAQ 8	16	81	2	0
2478 1665	2478 1665	31.133 31.685	79.125 80.510	445707 505439	546442	20.0	10	100		9
1674	1674	32, 468	79. 980	591694	595865	16.8	0	186	0	0
1763	1763	31.830	79.242	522753	666485	259	8	20	56	23
2295	2295	32.885	80.625	549731	535389	8.8	•	100	0	0
1773	1773	32.347	78. 740	580919	712690	347	8	53	29	18
1767	1767	31.827	78. 492	523216	711690	455 7		93	7	0
2281 2285	2281 2285	30. 930 30. 362	81.315 81.380	4217 <b>0</b> 3 358742	4699 <b>0</b> 6 463483	8		100	é	9
2289	2289	31.325	81.197	465453	481288	7.8	i	97	3	9
2290	2290	31.520	81.065	487049	493828	9.0		100	0	0
2384	2384	<b>30.</b> 988	78.717	421493	718221		9	100		0
2388	2388	31.533	78, 967	490317	693948				0	8
2398	2398	32. 883 32. 380	78. 450 79. 788	552330 583014	74 <b>0683</b> 61398 <b>0</b>	36.8	1	99	8	9
2408 2474B	24 <b>88</b> 2474B	38. 572	79.525	382878	641448		å	10	8	9
2483	2483	32.147	78.593	559843	726994		8		0	0
1482	1482	32.327	80. 038	576863	590515	16	•	100	0	8
1660	1660	31.168	79.967	448532	598479	46.0	1	99	0	0
1669	1669	32 <b>. 88</b> 8	79. 980	541626	596340	27.0	0	100		0
1670	1670	32. 189	80. 980	560638	594274	19.0	0	100		9
1712	1712	30.337	80.250	356149	572993	49.8		180 180	8	0
1659	1659	31.002 31.995	79. 983 79. 753	438847 548373	597 <b>060</b> 617768	48. 8 32		100	8	0
1758 1746	1758 1746	31.999	79.742	438898	620135	347		96	4	0
1764	1764	31.675	79.243	505567	666525	594	0		18	13
2268	2268	32, 273	80.695	578585	528724	- 11	3		. 0	0
2389	2389	31.383	78.667	474254	721891		8		0	8
2398	2390	31,213	78. 483	455798	739761			_	0	8
2484	2484	32.467	79.875	592532	685726	27.8		99		- 0
2705	27 <b>05</b> 27 <b>06</b> A	31.800 31.800	79.280 79.280	519491 519491	67 <b>8484</b> 67 <b>8484</b>		0		9	8
27 <b>86A</b> 1492	1492	31.340	81.017	467098	498414	15.8	•			0
1679	1679	31.168	80.760		522874	19.8			0	0
2296	2296	32, 262	80. 450	569385	551884	11.0		90	5	0
1680	1680	31.000	80.747	429446	524185			100		0
2291	2291	31.678			497946					0
1799	1700	30. 833			548136					8
1582	1502	38.312			582243 572939					0
1483 1736	1483 1736	32. 333 38. 390			587436					14
1732	1732	38. 147								
1768	1768	31.897						99	1	0
2399	2399	32. 177								
2410	2410	32.323			618601					
2414	2414	39, 267			6 <b>84858</b> 67 <b>8484</b>					
2701 1503A	2701 1503A	31.800 30.330								
1675	1675	32, 225								
1684	1684	30. 338								
1774	1774	32.333	79.000							
2409	2409	32.350								
1487	1487	31.850								
2293	2293	31.868								
2417 2475	2417 2475	30. 313 30. 683				900.				
1485	1485	31.988								
1667	1667	31.840								0
1678	1678	31.340				22.6	9 (	100	0 0	0

PAGE 3							16	149:35	15 Ju	1900
Key	SAMPLEID	LAT	LON	NORTH	EAST	DEPTH				
								-		
16578 1 <b>585</b>	16579 1 <b>505</b>	<b>39.</b> 667 <b>39.</b> 165	8 <b>0.000</b> 81.213	392905 336907	5958 <b>0</b> 1 479458	244. 9 15. 0	8	189		
1739	1739	30.518	79.693	376767	625373	639	8	109		0
1740	1740	39. 597	79.332	385907	659950	882	•	100	•	•
2397	2397	31.995	78.257	542983	759186	_	0	100	0	0
2407	2487	32. 403	79.810	585577	611913		0	100	8	0
2784 1495	2784 1495	31.800 30.992	79.200 81.225	519491 428517	678484		0	100	9	
1683	1683	38, 497	80.733	373671	478518 525591	16. 9 32. 0	9	100 100	9	8
1714	1714	30.010	80.257	319946	571688	86.0	0	100	0	8
1756	1756	31.838	79.510	522373	641008	69	9	97	3	
1772	1772	32.175	78. 750	561864	722148	406	0	78	16	13
17 <b>03</b> 2273U	17 <b>03</b> 2273U	31.350	88. 492	468318	548351	28.9	8	160	0	0
2288	2288	31.7 <b>0</b> 3 31.242	81.173 81.187	507379 456216	483575 482224	11 16. 0		189		8
2372	2372	39. 817	79. 888	322137	692887		8	98	2	8
1652	1652	30. 152	79. 447	336430	649599			0	0	
1488C	1488C	31.842	80.750	522726	523655	17.8	8	9	0	9
2376	2376	39.513	78.500	378145	739911		0	188	0	9
2382 2387	2382 2387	31.027 31.253	78.313 78.983	435474 459247	756464 692035		8	100	0	8
14868	14868	31.970	80.500	537032	547244	18.8		9	8	
150AB	15088	30.000	81.250	318632	475888	19.0	8	0	8	8
1496	1496	39.835	81.223	411154	478642	15.8	8	100	8	
1506	1506	30. 167	81.829	337073	498074	21.8		99	1	0
1784	1784	31.513	80.500	486416	547477	24.0	8	199	8	0
1776 2428	1776 2428	32. 362 39. 367	79. 447 81. 213	581397 359254	646152 479 <b>580</b>	36 22.0	8	199	8	0
2471	2471	30.067	79.678	326729	627395		8	11	37	42
2418	2418	39. 339	80.703	355289	528519	33.0		166	0	8
2283	2283	30, 643	81.485	389962	461192	8	8	99	2	
17398	17309	30. 888	80.070	328757	589621			0	8	8
1766	1766	31.817	79.003	521665	688992	450	0	99	1	9
1741 1797	1741 1797	38.655 32.475	79.175 78.888	392686 596864	674868 781956	792 324	0	97	3	8
2423	2423	39.363	81.025	358865	497598	24.0	9	166	8	0
2700	2700	31.300	78.883	464599	701460		•	8	0	0
1677	1677	31.948	80.620	534584	535914	17.8	9	188	0	0
1698	1698	30.492	80. 478	373202	550065	35.0	0	100	0	0
17 <b>68</b> 1751	17 <b>08</b> 1751	31.000 31.498	80.250 79.770	429659 485301	5716 <b>8</b> 2 616815	36. 9 64	8	189 99	8	9
2273	2273	31.789	81.129	508021	487793	13	8	100	0	0
2294	2294	31.972	80.752	537135	523464	10.0	26	74	0	0
1662	1662	31.513	88.828	486724	593056	41.8	8	100	8	0
1761	1761	32.177	79.258	561160	664208	54	0	100	0	0
24 <b>8</b> 6 1651	24 <b>86</b> 1651	32. 43 <b>0</b> 30. 843	79.847 79.333	588496	688432	27.8		180	8	0
1744	1744	30.843	79.575	324577 412925	66 <b>0</b> 691 636271	787	8	81	9 18	0
1749	1749	31.342	79. 475	468288	645075	484	•	MA	10	U
1499	1499	30.550	81.228	391762	478125	19.8	0	100	0	9
1676	1676	32.127	80.473	554410	549680	14.0	0	100	8	8
17 <b>82</b> 2266	17 <b>8</b> 2 2266	31.187	80.533	450199	544465	31.0	0	100	0	0
2297	2297	32.495 32.467	80.495 80.222	595228 592242	547443 573145	12 11.0	1 0	99 108	0	8
1750	1750	31.303	79.763	463694	617691	144	0	76	16	7
1775	1775	32.330	79.275	578133	662363	44	0	99	1	
1738	1738	30.520	79.867	376772	608738	480	0	96	4	8
1765	1765	31.762	79.108	515389	679157	558	8	95	_ 5	0
2386	2386	31.003	79.000	431584	690948	782.0	0	99	1	0

									45 80	1000
PAGE 4				APP DE L	FOOT	NCDTI.			15 JUL	
Key	SAMPLEID	ы	LUNL	NUKTH	EH51	חוץשע	MICIGHA	MIGHW	MISTEL	WIGEN
2412	2412	30.517	80.117	376189	584754	43.0	5	95	0	0
1655	1655	30, 668			645300		0	22	38	39
22779	2277B	32.320			471059	6	8	100	0	0
2277C	2277C	32, 320		464922	471859	6		100	8	0
2422	2422	30. 357	88. 978		502083	24.8	0	100	0	9
2287	2287	31.003	81.438	429869	458155	6	0	73	18	16
2375	2375	38, 885	78.750		715265		•	9	8	0
2708	2798	31.800	79.250		665670		0	6	0	0
14888	1488B	31.842			523655	17.0	0	8	0	9
1508A	1508A	30.000	81.250			19.0	9	98	5	8
1697	1697	30.340	80.500		548868	36.8	0	100 100	8	0
1707	1707	31.157	80.210		575297 618198	36. 0 46	0	100	0	0
1754	1754 2272	31.657 31.993	79.753 81.175			70 7	1	98	1	8
2272 2276	2276	31. 484				8	ò	71	10	18
1739A	173 <b>8</b> A	30. 088	80.070		589621		ě		18	15
2282	2282	39, 812				8			5	0
2381	2381	31.070			772733	849.8	0		9	0
1734	1734	30, 340	79, 733		621756	664	8	34	36	29
2703	2703	31.800	79.200	519491	678484	556.0	0		8	8
1484	1484	32, 160	80.268	558217	568992	15	0		0	9
1486A	1486A	31.970	80.500	537032		18.0	8		1	9
1494	1494	30.992				19.8	0		0	0
1504	1504	30, 255					0		•	0
1661	1661	31.327				41.0	8		0	0
1666	1666	31.850			562286	29.9				0
1672	1672	32.298				25.0			9	8
1682	1582	30.667							1	0
1713	1713	39.177				77.8 48			9	0
1755 1759	1755 1759	31.832 32.982			628511				0	0
1759	1759	32. 167				36				0
1771	1771	32. 162							42	15
2271	2271	31.842							4	0
1769	1769	31.985			712588	386				
1770	1770	32. 983	79.000	542351	688138	486	0	70	16	13
2385	2385	38. 953	78.916	426119	699646	862.8	0			0
2479	2479	31.383								0
2488	2480	31.598								0
2391	2391	31.403								0
1489	1489	31.683								0
1490	1498		80.767							9
1656 1657A	1656 1657A	30.667	79.737 8 <b>0.00</b> 0							. 8
1671	1671	32. 167								. 0
2292	2292	31.765								9
2416	2416	30. 275								0
2427	2427	30. 367						89	8	8
2286	2286	39.722				7		38	21	48
1500	1500	38. 493		373298	475528	17.0		198		0
1748	1748	31.190								0
2378	2378	38. 446								6
2415	2415	30, 300								3
2797	2707	31.800						-		9
1481	1481	32.333								9
2392	2392	31.483								8
2413	2413	30. 247								0 13
1735	1735	30. 35								4
1762	1762	31.987	13,63	ישונטרע.	, 0071(0	. 10/	, ,	, 93		

PAGE	5							10	<b>9:50:</b> 21	15 JU	1988
Key		SAMPLEID	LAT	LON	NORTH	ERST	DEPTH	WTGRAV	WTSAND	WTSILT	WTCLAY
1503B		15039	30. 330	81.250	355198	475968	12.0	0	8	0	0
2425		2425	<b>30.</b> 373	81.182	359977	490231	22.0	9	100	0	0
1686		1686	30. 880	80.758	318630	523341	36.0	8	100	8	8
1699		1699	30.667	80.497	392587	548219	38. 0	0	100	0	0
1709		1709	39.833	80.255	411185	571248	37.0	9	100		0
1710		1710	38.675	80, 225	393658	574239	42.0	9	188	8	0
2274		2274	31.543	81.193	489649	481696	12	1	95	4	0
2481		2481	31.680	78.800	506884	708548	543.0	0	0	9	8
1480		1480	32.493	79.763	595684	616187	20.0	0	100	8	0
1491		1491	31.512	8 <b>0.</b> 988	486124	501108	13.0	8	100	. 0	8
1501		1501	30. 483	81.000	372162	500000	26.8	0	99	1	8
1745		1745	30.863	79.728	414964	621581	461	15	78	9	8
1493		1493	31. 155	81.012	446596	498888	14.8	8	199	0	0
1479		1479	32, 493	79.582	595919	640772	20.0	9	188		0

	2	 	
			18
		20	540
		#: -33	
			2
4			
			- 8

*		
10		
a .		
,		

PAGE 1				10:51:0		L 1988
Key	SAMPLEID	QUARTZ KFEL	DSPAR PFELD	SPAR HEA	VYS PHOS	PHORITE
1649	1649					
1650	1650					2
1733 2279	1733 2279					
2280	2280					
2284	2284					
2419	2419					
2420	2420					_
1498	1498	92	3	3	0	
1663	1663	92	4	2 0	1	0
1681 16 <b>96</b>	1681 1696	95 86	3 5	5	5	3
1786	1786	80	3	4	2	8
1743	1743	40	8			
1752	1752		10			
2373	2373					
2472	2472		3 S			
2782	2702	89	5	2	4	
1668 2277A	16 <b>68</b> 2277A	87	J.	2	0	
1653	1653		•	•	•	•
1742	1742	Ú.				
2374	2374					
2485	24 <b>65</b>					
2411	2411					
2421	2421 2476					
2476 27 <b>9</b> 6B	27 <b>96B</b>					
1488A	1488A	87	2	6	4	0
1658	1658	93	3	1	1	0
1695	1695	86	5	3	2	0
17 <b>85</b>	1795	89	5	3	5	0
1711	1711	89	4	4	2	8
1747	1747 1757	19 84	3 7	2 5	2	0
1757 2269	2269	87	6	3	3	0
2275	2275	88	7	3	0	0
1664	1664	89	4	5	1	9
2270	2278	67	9	2	5	6
1654	1654					
2278	2278					
2377 23 <b>83</b>	2377 23 <b>8</b> 3					
2424	2424					
2474A	2474A					
2482	2482		-	_		2
1497	1497	92	3	5	8	9
1685	1685	92	1 3	3 5	3	8
17 <b>0</b> 1 1737	17 <b>0</b> 1 1737	98 28	3	2	8	0
2429	2429	89	6	3	0	8
2265	2265	94	4	2	0	0
1753	1753	72	5	8	8	9
1731	1731					
2379	2379					
2380	23 <b>80</b> 2426					
2426 2473	2473					
2477	2477					

PAGE 2				10:5	1:16 15	JUL 1988
Кеу	SAMPLEID	QUARTZ	KFELDSPAR			
2478	2478					
1665	1665	89	4	5	1	•
1674	1674	87	8	4	4	0
1763	1763	74	5	13	0	0
2295	2295	88	6	5	0	8
1773	1773	45	3	1	0	0
1767	1767					
2281	2281					
2285	2285					
2289	2289					
2290 2384	229 <b>0</b> 2384					
2388	2388					
2398	2398					
2488	2408					
2474B	2474B					
2483	2483					
1482	1482	91	2	5	1	9
1660	1660	88	5	5	1	0
1669	1669	98	4	3	2	0
1670	1670	92	3	2	2	0
1712	1712	85	5	3	6	0
1659	1659	90	5	3	8	0
1758	1758	84	6	5	3	0
1746	1746					
1764	1764					
2268 2389	2268					
2390	2389 2390					
24 <b>84</b>	2484					
2785	2785					
27 <b>06</b> A	27 <b>06</b> A					
1492	1492	91	3	3	2	
1679	1679	92	3	2	2	å
2296	2296	82	10	5	ž	i
1680	1680	92	5	2	8	ě
2291	2291					
1700	1700	90	3	3	2	0
1502	1502	91	5	4	0	0
1483	1483	86	5	8	8	•
1736	1736					
1732 1768	1732					
2399	17 <b>68</b> 23 <b>99</b>					
2410	2410					
2414	2414					
2701	2701					
15 <b>0</b> 3A	1583A	92	5	2	0	8
1675	1675	91	2	4	2	0
1684	1684	94	3	2	1	0
1774	1774	78	5	3	0	0
2409	2409	87	8	4	0	0
1487	1487	88	5	5	1	0
2293	2293					
2417	2417					
2475 1485	2475	04			_	_
1667	148 <b>5</b> 1667	94	4	5	0	0
1678	1678	92 95	2	2	3	0
1010	7010	10	3	1	0	8

1657B	PAGE 3			sonon acci i	10:51:2		UL 1988
1585   1585   1739   1739   1739   1748   2397   2397   2397   2397   2407   2407   2404   24	Кеу	SAMPLEID	BURRIZ KFE	LUSPAK PEELI	AJIH NHYGA	VIO PILL	SPHUKT IE
1739 1739 1748 1748 1748 1748 1748 1748 1748 1748							
1740 1740 2397 2397 2397 2397 2407 2704 2704 2704 2704 2704 2704 270							
2397							
2487							
2704   2704   1495   1495   1495   1495   1495   1495   1495   1495   1495   1495   1495   1495   1495   1495   1756   1756   1756   1756   162   18   16   1772   1772   1772   1772   1773   1784   1785   1785							
1495							
1714		1495	89	6	4	0	
1756							
1772						-	
1783							
2273U 2273U 2288 2288 2372 2372 2372 2372 2375 2576 2376 2376 2376 2382 2382 2382 2382 2382 2387 1486B 1486B 85 8 5 1 0 1586B 1596B 1596B 91 4 4 0 0 1794 1776 1776 85 6 1 7 0 0 2471 2471 2471 2471 2471 2471 2471 2471					-		
2372				_			
1652 1652 1488C 1488C 2376 2376 2382 2382 2387 2387 2387 1496B 1588B 85 8 5 1 0 0 1586B 1588B 1588B 88 6 4 0 0 15866 1586 91 4 4 0 0 1794 1776 1776 85 6 1 7 0 0 1776 1776 85 6 1 7 0 0 1777 1777 1777 1777 1777 1777	2288	2288					
1488C							
2376							
2382							
2387							
1486B       1486B       85       8       5       1       0         1596B       1596B       88       6       4       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
1496			85	8	5	1	100
1586 1586 91 4 4 8 8 1776 1776 1776 1776 85 6 1 7 7 8 2428 2428 92 3 2 2 8 2471 2471 69 23 4 9 8 2283 2283 17388 17388 17388 17388 17388 17388 17388 17388 17388 1751 1751 1751 1751 1751 1751 1751 17					•	_	
1704 1704 1704 87 3 5 4 0 1776 1776 85 6 1 7 0 2428 2428 92 3 2 2 0 2471 2471 69 23 4 0 0 2418 2418 2283 2283 17308 17308 17308 17308 17308 17308 17308 17308 17308 17308 17308 17308 17308 17301 1741 1741 1797 1797 12423 2423 2423 2700 2700 1677 1677 90 3 2 4 0 0 1677 1677 90 3 2 4 0 0 1678 1698 91 5 3 0 0 0 1708 1708 91 4 3 1 0 0 1751 1751 1751 91 4 4 0 0 2273 2273 2873 288 6 5 5 0 0 2294 2294 88 4 5 2 0 0 1662 1662 06 4 5 1 0 1761 1761 185 6 6 1 0 1749 1749 1749 1749 1749 1749 1749 1749				_		-	0.00
1776				•		-	\$ <del>-</del> 55
2428							
2471					_		
2418							
17388 17388 1766 1766 1741 1741 1797 1797 2423 2423 2700 2700 1677 1677 90 3 2 4 6 1698 1698 91 5 3 0 6 1708 1708 91 4 3 1 0 1751 1751 91 4 4 0 0 2273 2273 88 6 5 5 0 0 2294 2294 88 4 5 2 0 1662 1662 86 4 5 1 8 1761 1761 85 6 5 1 8 1761 1761 85 6 5 1 8 1761 1764 1744 1749 1749 1499 1499 88 7 4 0 0 1676 1676 91 4 2 2 0 1676 1676 91 4 2 2 0 1782 1782 93 3 1 2 0 2266 2266 93 2 1 3 0 2297 2297 84 8 5 1 0 1738 1738 1738 1738 1738							
1766 1766 1741 1741 1797 1797 2423 2423 2700 2700 1677 1677 90 3 2 4 6 1698 1698 91 5 3 0 0 1706 1708 91 4 3 1 0 1751 1751 91 4 4 0 0 2273 2273 88 6 5 5 0 0 2294 2294 88 4 5 2 0 1662 1662 86 4 5 1 0 1761 1761 85 6 6 1 0 1761 1761 85 6 6 1 0 1744 1744 1749 1749 1499 1499 88 7 4 0 0 1676 1676 91 4 2 2 0 1762 1762 93 3 1 2 0 2266 2266 93 2 1 3 0 2297 2297 84 8 5 7 0 0 1750 1750 83 6 7 0 0 1750 1750 83 6 7 0 0 1758 1758 1758							
1741 1797 1797 1797 2423 2423 2700 2700 2700 1677 1677 90 3 2 4 6 1678 1698 91 5 3 0 0 1700 1700 1700 1700 1700 1701 4 4 0 0 0 1701 1701							
1797 1797 2423 2423 2700 2700 1677 1677 90 3 2 4 0 1698 1698 91 5 3 0 0 1708 1708 91 4 3 1 0 1751 1751 91 4 4 0 0 2273 2273 88 6 5 5 0 0 2294 2294 88 4 5 2 0 1662 1662 86 4 5 1 8 1761 1761 85 6 6 1 0 2406 2406 1651 1651 1744 1744 1749 1749 1499 1499 88 7 4 0 0 1676 1676 91 4 2 2 0 1702 1702 93 3 1 2 0 2266 2266 93 2 1 3 0 2297 2297 84 8 5 1 0 1750 1750 83 6 7 0 0 1775 1775 84 8 6 0 0							
2423       2423         2700       2700         1677       1677       90       3       2       4       8         1698       1698       91       5       3       8       0         1708       1708       91       4       3       1       8         1751       1751       91       4       4       0       8         2273       2273       88       6       5       0       0         2294       2294       88       4       5       2       0         1662       1662       86       4       5       1       8         1761       1761       85       6       6       1       0         2496       2496       1651       1       0       <							
2700       2700         1677       1677       90       3       2       4       0         1698       1698       91       5       3       0       0         1708       1708       91       4       3       1       0         1751       1751       91       4       4       0       0         2273       2273       88       6       5       0       0         2273       2273       88       6       5       0       0         2294       2294       88       4       5       2       0         1662       1662       86       4       5       1       0         1761       1761       85       6       6       1       0         2496       2496       1651       1744       1744       1744       1744       1749       1749       1499       1499       88       7       4       0       0       0         1676       1676       91       4       2       2       0       0       0       0       0       0       0       0       0       0       0       0							
1698       1698       91       5       3       0       0         1708       1708       91       4       3       1       0         1751       1751       91       4       4       0       0         2273       2273       88       6       5       0       0         2294       2294       88       4       5       2       0         1662       1662       86       4       5       1       0         1761       1761       85       6       6       1       0         2486       2486       1       1744       1744       1744       1744       1744       1749       1499       1499       88       7       4       0       0       0         1676       1676       91       4       2       2       0							
1708       1708       91       4       3       1       0         1751       1751       91       4       4       0       0         2273       2273       88       6       5       0       0         2294       2294       88       4       5       2       0         1662       1662       86       4       5       1       0         1761       1761       85       6       6       1       0         2406       2406       1651       1       0       <					2		
1751       1751       91       4       4       6       6         2273       2273       88       6       5       6       6         2294       2294       88       4       5       2       0         1662       1662       86       4       5       1       8         1761       1761       85       6       6       1       8         1761       1761       85       6       6       1       8         1466       2406       1       1651       1744       1744       1744       1744       1749       1749       1749       1499       1499       88       7       4       0 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td>						_	
2273							
2294       2294       88       4       5       2       0         1662       1662       86       4       5       1       8         1761       1761       85       6       6       1       0         2496       2496       1651       1       1       1       1       1       0							
1662       1662       86       4       5       1       8         1761       1761       85       6       6       1       8         2486       2486       1651       1 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>							
2486		1662					
1651       1651         1744       1744         1749       1749         1499       1499         1676       1676         1702       1702         2266       2266         2297       84         1750       1750         1775       1775         1738       1738         1765       1765			85	6	6	1	0
1744 1749 1749 1749 1499 88 7 4 6 6 1676 1676 91 4 2 2 6 1702 1702 93 3 1 2 6 6 2266 2266 93 2 1 3 6 2297 2297 84 8 5 1 6 1750 1750 83 6 7 8 6 1775 1775 84 8 6 6 6 6 1738 1738 1738 1738 1755 1765							
1749     1749       1499     1499       1676     1676       1702     1702       2266     2266       2297     84       1750     1750       1775     1775       1738     1738       1765     1765							
1499     1499     88     7     4     0     0       1676     1676     91     4     2     2     0       1702     1782     93     3     1     2     0       2266     2266     93     2     1     3     0       2297     2297     84     8     5     1     0       1750     1750     83     6     7     0     0       1775     1775     84     8     6     0     0       1738     1738     1738       1765     1765							
1676     1676     91     4     2     2     9       1702     1702     93     3     1     2     9       2266     2266     93     2     1     3     9       2297     2297     84     8     5     1     9       1750     1750     83     6     7     9     9       1775     1775     84     8     6     9     9       1738     1738       1765     1765			88	7		_	
2266     2266     93     2     1     3     0       2297     2297     84     8     5     1     0       1750     1750     83     6     7     0     0       1775     1775     84     8     6     0     0       1738     1738       1765     1765	1676	1676	91		2		
2297     2297     84     8     5     1     0       1750     1750     83     6     7     0     0       1775     1775     84     8     6     0     0       1738     1738       1765     1765							
1750 1750 83 6 7 8 0 1775 1775 84 8 6 0 0 1738 1738 1765							
1775 1775 84 8 6 9 9 1738 1738 1765 1765							
1738 1738 1765 1765							
1765 1765				J	-	141	
		1765					
	2386	2386					

PAGE 4				10:5	i1:41 15	JUL 19	188
Кеу	SAMPLEID	QUARTZ	KFELDSPAR				
2412	2412						
1655	1655						
22778	2277B						
2277C	2277C						
2422	2422						
2287	2287						
2375	2375						
2708	2708					8	
1488B	1488B	84	7	6	1		0
1508A	1508A	91	3	4	2		0
1697	1697	91	4	2	8	8	0
17 <b>07</b>	1797	93	3	1	2		0
1754	1754	88	5	5	0		8
2272	2272	98	5	4	0		0
2276	2276	80	9	8	1		0
1738A	1730A						
2282	2282						
2381	2381						
1734	1734						
2703	2703						
1484	1484	98	4	4	1		0
1486A	1486A	84	7	8	8		0
1494	1494	89	6	2	1		8
1584	1594	89	7	3	1		8
1661	1661	98	4	4	8		
1666	1666	91	4	4	8		0
1672	1672	87	6	3	3		
1682	1682	96	5	8	1		0
1713	1713	93	3	2	1		
1755	1755	98	4	3	2		0
1759	1759	90	6	2	1		0
1760	1760	82	6	5	2		
1771	1771	67	14	7	0		0
2271	2271						
1769	1769				9		
1778	1770						
2385	2385						
2479	2479						
2480	2480						
2391	2391	A.P	_		,		100
1489	1489	86	6	4	1		0
149 <b>0</b> 1656	1490	89	5	5	0		0
1657A	1656	34	5	2	8		8
1671	1657A 1671	12	1	8	0		0
2292	5535	87	5	4	3		0
2416	2416	87 80	7 5	5	1		8
2427	2427	93	2	3	1		0
2286		73	2	3	1		0
1500	2286 1588	94	7	3	•		
1748	1748	29	3	3	0		0
2378	2378						
	2415						
2707	2797						
1481	1481	83	6	7	9		
	2392	63	ь	7	2		•
	2413						
1735	1735	63	6	7	•		p.
1762	1762	77	7	6	0		8
- 7 000		"	,	0	ď		•

PAGE	5						15 JUL 1988
Кеу		SAMPLEID	QUARTZ	KFELDSPAR	PFELDSPAR	HEAVYS	PHOSPHORITE
1 <b>503</b> B		1503B					
2425		2425					
1686		1686	94	1	8	3	0
1699		1699	89	4	4	2	9
1789		1709	95	3	1	8	0
1719		1710	95	5	2	- 0	0
2274		2274	88	6	4	1	0
2481		2481					
1480		1480	85	6	5	1	0
1491		1491	92	3	3	9	0
1501		1501	94	2	3	0	9
1745		1745	11	1	1	0	9
1493		1493	93	3	1	1	9
1479		1479	8888	6	5	0	0

*)			
8			
" r			
n sr a			
		-	
W 77			
	51		
2			
4			

PAGE 1									1	0:52:31 15 JUL 198	38_
Key	SAMPLEID	MAGNETITE	APATITE	MONAZIT	E RUTIL	E ZIRC	ON SILLIMAN	IITE KYANI.	ie stauroli	ITE LEUCOXÈNE TITANI	ITE
1649	1649										
1650	1650										
1733	1733										
2279 2280	2279 2280										
2284	2284										
2419	2419										
2429	2420										
1498 1663	1498 1663										
1681	1681										
1696	1696										
1706	1706										
1743	1743										
17 <b>5</b> 2 2373	17 <b>52</b> 2373										
2472	2472										
2702	2792										
1668	1668					_	_				_
2277A	2277A		0		0	6	6	1	2	1	3
1653 1742	16 <b>5</b> 3 1742										
2374	2374										
2485	2485										
2411	2411										
2421	2421										
2476 27 <b>068</b>	2476 27 <b>86</b> B										
1488A	1488A										
1658	1658										
1695	1695										
1785	1705										
1711 1747	1711 1747										
1757	1757										
2269	2269										
2275	2275				•	,		020		•	1
166 <del>4</del> 2270	1664 227 <b>0</b>		(	-	8	3	2 18		1	8	0
1654	1654			•	•	-	••		•		
2278	2278										
2377	2377										
2383	2383 2424										
2424 2474A	2474A										
2482	2482										
1497	1497										
1685	1685										
17 <b>01</b> 1737	17 <b>91</b> 1737										
2429	2429										
2265	2265				0	8	5		0	1	9
1753	1753		1	9	8	1	2		1	0	0
1731 2379	1731 2379										
2380	2380										
2426	2426										
2473	2473							2			
2477	2477										

th:												
		PAGE 2	COMPLETD	MOCMETITE	ADATITE	MONOTET	. 01111111	71000N	CILL IMMITTE	WANTE COURSE	10:52:42 15 J	UL 1988
		Ney	SHARITETTI"	MHOMETTIE	HPHITIE	UCLEH ( )	: KUIILE	ZINCUN	PILLIMATIE	KYANITE STAUROL	THE FERMIXENE	ILIANITE
		2478	2478									
		1665	1665									
		1674 1763	1674 1763									
		2295	2295									
		1773	1773		0	(	4	6		2	•	1
		1767 2281	1767 2281									
		2285	2265									
		2289	2289									
		2290 2384	2290 2384									
		2388	2388		10)							
		2398	2398									
0:		2498 2474B	24 <b>88</b> 2474B									
		2483	2483									
	14	1482	1482									
3		1669	166 <b>9</b> 1669									
		1670	1678									
2		1712	1712									
		1659	1659		0	1	4			2 1		1
		1758 1746	1758 1746		•	•	•	13		1	1	3
		1764	1764									
		2268	2268									
		2389 2390	2389 2390									
18		2484	2484									
		2765	2705									
		27 <b>8</b> 6A 1492	27 <b>06A</b> 1492									
		1679	1679									
	5	2296	2296									
		168 <b>0</b> 2291	168 <b>0</b> 2291		9	1				0	1	0
		1796	1700		0					0 2	1	0 1
		1582	1502		8	3	2	8		2 2	0	i
		1483 1736	1483 1736		0	0	8	7		0	•	1
		1732	1732									
		1768	1768									
		2399 241 <b>0</b>	2399 241 <b>0</b>									
		2414	2414									
50		2701	2701									
		1583A 1675	1503A 1675									
25		1684	1684									
		1774	1774									
a 11		2409	2489			_	_	_				1441
N 192 W		1487 2293	1487 2293		0	8	5	5		0	1	1
		2417	2417									
		2475	2475									
		1485 1667	1485 1667									
-		1678	1678							·,		

PAGE 3											3 15 JUL 198	
(ey	SAMPLEID	MAGNETITE	APATITE	HONAZITE	RUTILE	ZIRCON	SILLIMANITE	KYANITE	STAUROL:	ITE LEU	COXENE TITANI	ITE
16578	1657B											
1595	1505											
1739	1739											
1740	1740											
2397	2397											
2 <b>487</b> 27 <b>84</b>	24 <b>07</b> 27 <b>0</b> 4											
1495	1495											
1683	1683											
1714	1714											
1756	1756											
1772	1772		0	1	3	4		0		8		1
17 <b>03</b> 2273U	17 <b>03</b> 2273U		•		3		,	•		•		•
2288	2288											
2372	2372											
1652	1652											
1488C	1488C											
2376	2376											
23 <b>82</b> 2387	2382 2387											
1486B	1486B											
15068	15069											
1496	1496											
1506	1596											
1784	1784											
1776 2 <b>428</b>	1776 2428											
2471	2471											
2418	2418			4	7	, ;	5			1		9
22B3	2283		9	•		5 4	•	1		0		9
173 <b>0B</b>	17300											
1766	1766											
1741	1741											
1797 2423	1797 2423											
2799	2798											
1677	1677											(4)
1698	1698											
1708	1708											
1751	1751											
2273 2294	2273 2294											
1662	1662		•	1	1 4	•	8	7		3		7 0
1761	1761		8			5	8 6	7 2		3 6		0
2486	2406											
1651	1651											
1744	1744											
1749 1499	1749 1499											
1676	1676											
1702	1702											
2266	2266											
2297	2297		T.			-	4	_				
1750	1750		6	5	1 :	5 4	4	1	1	8		0
1775 1738	1775 1738			,	<b>U</b> '	•	•	1		•		v
1765	1765											
2386	2386							<b>*</b>				

PAGE 4										10:53:64	15 JUL 1988
Key	SAMPLEID	MAGNETITE	APATITE	MONAZITE	RUTILE	ZIRCON	SILLIMANITE	KYANITE	STAUROL	.ITE LEUCOXE	NE TITANITE
2412	2412										
1655	1655										
22778	2277B							15			
2277C	2277C										
2422	2422										
2287	2287										
2375 2708	2375 g 27 <b>88</b>										
1488B	14888		e 22								
1508A	1588A										
1697	1697										
1707	1707	25									
1754	1754										
2272	2272										
2276	2276										
173 <b>9A</b>	1738A	4 8									
2282 2381	2282 2381										
1734	1734										
2703	2703										
1484	1484	89									
1486A	1486A		a.								
1494	1494		9								
1504	1584	- 3								5	
1661	1661										
1666	1666										
1672	1672										
1682	1682										
1713 1755	1713										
1759	1755 1759										
1760	1760										
1771	1771		8	0	4	0		0		9	8
2271	2271		-	_		•		•		•	•
1769	1769										
1770	1770										
2385	2385										
2479	2479										
2480	2488										
2391 1 <b>489</b>	2391 1489										
1490	1490										
1656	1656										
1657A	16579										
1671	1671										
<b>229</b> 2	2192										
2415	2416										
	2427										
2236	2286		8	4	5 3	11		9		<b>0</b> 1	0
15 <b>00</b> 1748	1500 1748		0	1	3	10		0		1	0
	2378										
2415	2415							00			
	2707										
1481	1481										
2392	5335										
2413	2413										
1735	1735						19	e			
1762	1762										

PAGE	5											15 JUL 198	
Кеу		SAMPLEID	MAGNETITE	APATITE	MONAZITE	RUTILE	ZIRCON	SILLIMINITE	KYANITE	STAUROL:	ITE LEUCOX	ene titani	ΤE
•													
15 <b>0</b> 3B		1503B											
2425		2425					-						
1686		1686											
1699		1699											
1709		1709											
1718		1710											
2274		2274											
2481		2481											
1480		1480											
1491		1491				9							
1501		1501											
1745		1745									_		
1493		1493		0	2				1		0		1
1479		1479		8	= 3	5	7		8		0		1

				*		
<u>(i)</u>						
•						
				5.	18	:1
3 3						
			6			
		TZ.				
8						
	9					
2.4						17.

## SECTION 9.3

25 MITE								•								•	9 69							•	•			
15 JL 1								•								•	•							•	•			
18157129 PHDNE HDRAG								•							w.	•	•							-	•			
HTE BLAUCO	361					8		•								•	• -							•	•			
. DUNCATIES																	7							- 40	•			
SITE SPINE								<b>=</b>																æ				
ĐE MORLI								•								-								•				
TE MYEJSTI								•	ě.							•	• •			7 <b>2</b>				•	•			
DISITE ALGI								•																•	•			
15 JL 1966 Species sleibes prospire authore lindate author adalende aborliste spire, dunchterite blachprae hobbleage aberite																												
ANTHIBLE																8	G ≅							g*	H			
PESPANE																												
E SLF10ES										6													v		41			
SHACELD NICH GRAGET EPIDOTE TOLIGHELINE BLALCONITE								*								25		÷						M	-			
ADOTE TOJA								8								i	7 <b>3</b>							₩	ন			
A BOOKET EP								•								•	• •		Çe.					•	•			
LEID MICH								£	<b></b>			95		o						. S	01 <b>-</b>	5		e in				m 4-
3855	8631 87.23 87.23	1822 1822 1822 1822 1822 1822 1822 1822	641	891	2 2		32.53	F231	2 6	1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 2 2	36.2	3 3	12.1		8 23			3 2 3	2 2	245	168	127	200	2	23.2	87 77 77 77	247
Mey	1656 1713 2279 2289	2284 2458 2458	86.4	1681 3631	17.3	25.5	2782	22.77A 1653	2471 2474	# T T T	2421	276CB 1488A	<b>3</b> 23 93 9		Z [2]	18 E	25 S	50 E	200	24749 24749	2485	287	1737	2429 2265	22 5	82.8	92 V.	2473
				×											ě													

PASE 3
MAY....... SHALEID., NICH BANET EPIDOTE TILBHALINE BLAICINITE SPIPE SILFIDES PACKANTE NOWINGLE LINCHITE ZOISITE AUSITE AUSITE MPENSTRENE GROULISITE GRUND. BLAICHDHAE HANBLEDGE REERITE

•	•	• •	യും ത	• •
•	•	• •	• •	• •
,	•	• •	••	••
	•	• •	••	eno 🚭
	out	№ 👁	• «	• •
	ond .	<b>=</b> :	<del>(10</del> )	
	and	••	N	N
	en en	• •	••	• •
	•	••	n •	₹ 6
			961	
	m)	2 8	= &	ನ ೫
			*	•
*	•	M 5	<b>= 17</b>	m -
	_	10 a	**	ន
	å	2.5	• •	••
	-			
			ം വേ കൊമി കോ എം അത് ത്രിമ വി ശ്രീ	e du as un co
1585 1739 1739 1746 2397 2407 2714 1756 1756	2234 2272 2372 1562 2372 2372 2372 1566 1566 1566 1766 1766 1766 1766 1766			REES &
288382483145	22733 22733 22733 2273 2372 2372 2372 2		* CH	2 K 2 2 3 3
25111111111	: = 2 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3822223883	8 2 2 2 2 2 2 2 2 2 3 8	

•	•-
•	••
•	• •
	• •
•	
	••
•	••
•	<b>60 PT</b>
	ž (w
; <b>S</b>	= ~
*	
rw.	25
=	~ ~ ~
a	3 12
ş •	••
	<b></b>
2412 1655 2772 2422 2422 2422 2735 2736 1156 1157 1157 1158 1156 1156 1156 1156 1156 1156 1156	17.17 (19
2412 22175 22175 22175 22175 22175 22175 22175 22177 20177 20177 20177 20177 20177 20177 20177 20177 20177 20177 2	170 170 170 170 170 170 170 170 170 170
	· · ·

PRE 5
Key....... SORLEIB., MICH BONNET EPIDOTE TULBBELINE BLAUCDRITE SANDE SILFINES PRISHATE RAPHIBOLE LINCWITE 2015ITE RABITE HAPEISTADE GADALIBITE SPINEL BUIOTTIERITE BLAUCORPAE HAPBIELDRIE GEBRITE

												•	•
												•	•
												•	•
												•	-
												-	•
													es)
												•	•
												Q	•
												•	-
												15	61
												•	-
												*	7
											2	•	•
15030	<b>10</b>	9991	1699	1789	1710	\$7.2Z	2481	148	1491	1201	1745	1493	1479
1563	25.25	1686	6691	1789	1710	K214	2481	1486	1491	1501	1745	1493	1479

			8	8	
					× =
					3
					\$2 \$5

For convenience in selecting our reports from your bookshelves, they are color-keyed across the spine by subject as follows:

Red Valley and Ridge mapping and structural geology Dk. Purple

Piedmont and Blue Ridge mapping and structural

Maroon Coastal Plain mapping and stratigraphy Lt. Green

Paleontology Lt. Blue

Coastal Zone studies Dk. Green

Geochemical and geophysical studies Dk. Blue

Hydrology Olive

Economic geology Mining directory

Yellow Environmental studies

Engineering studies

Dk. Orange Bibliographies and lists of publications Brown Petroleum and natural gas

Black Field trip guidebooks Dk. Brown Collections of papers

Colors have been selected at random, and will be augmented as new subjects are published.

Publications Editor:Patricia Aligood

The Department of Natural Resources is an equal opportunity employer and offers all persons the opportunity to compete and participate in each area of DNR employment regardless of race, color, religion, sex, national origin, age, handicap, or other non-merit factors.